



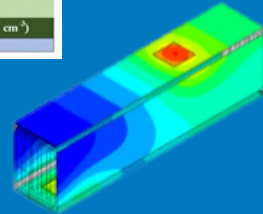
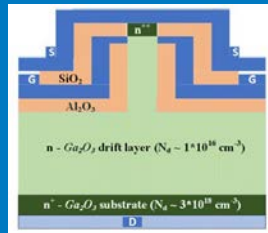
Automotive Power Electronics Cooling Technology Research at NREL

2022 Electronics Packaging Symposium
Sept 7-8, 2022

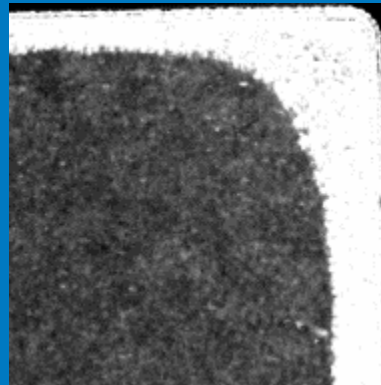
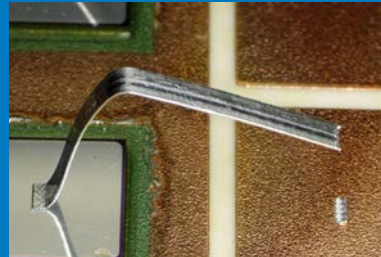
Gilbert Moreno

NREL APEEM Group Research Focus Areas

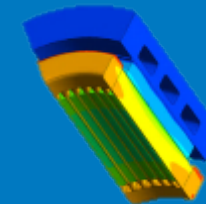
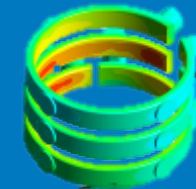
Power Electronics Thermal and Electro- Thermal



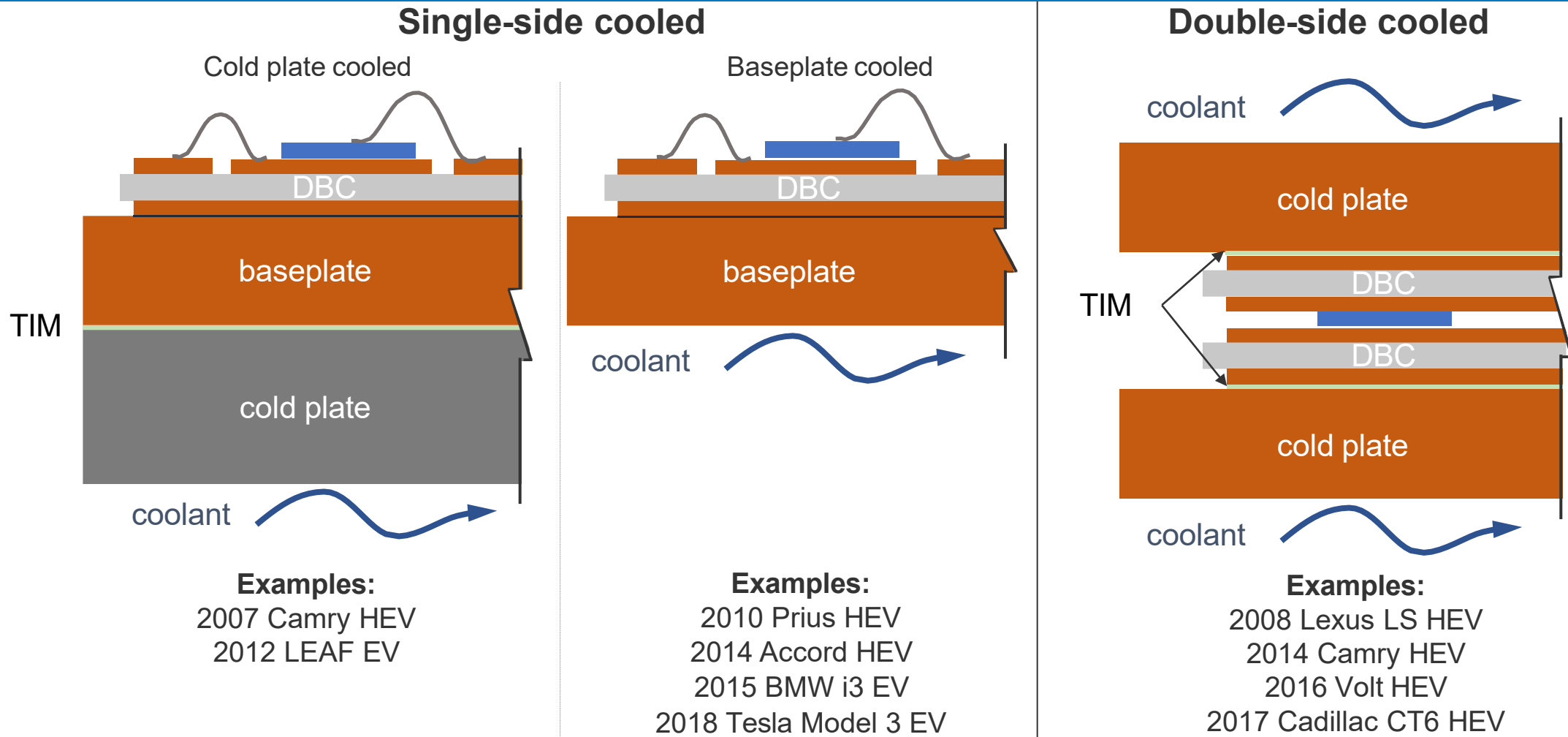
Advanced Packaging Designs and Reliability



Electric Motor Thermal Management



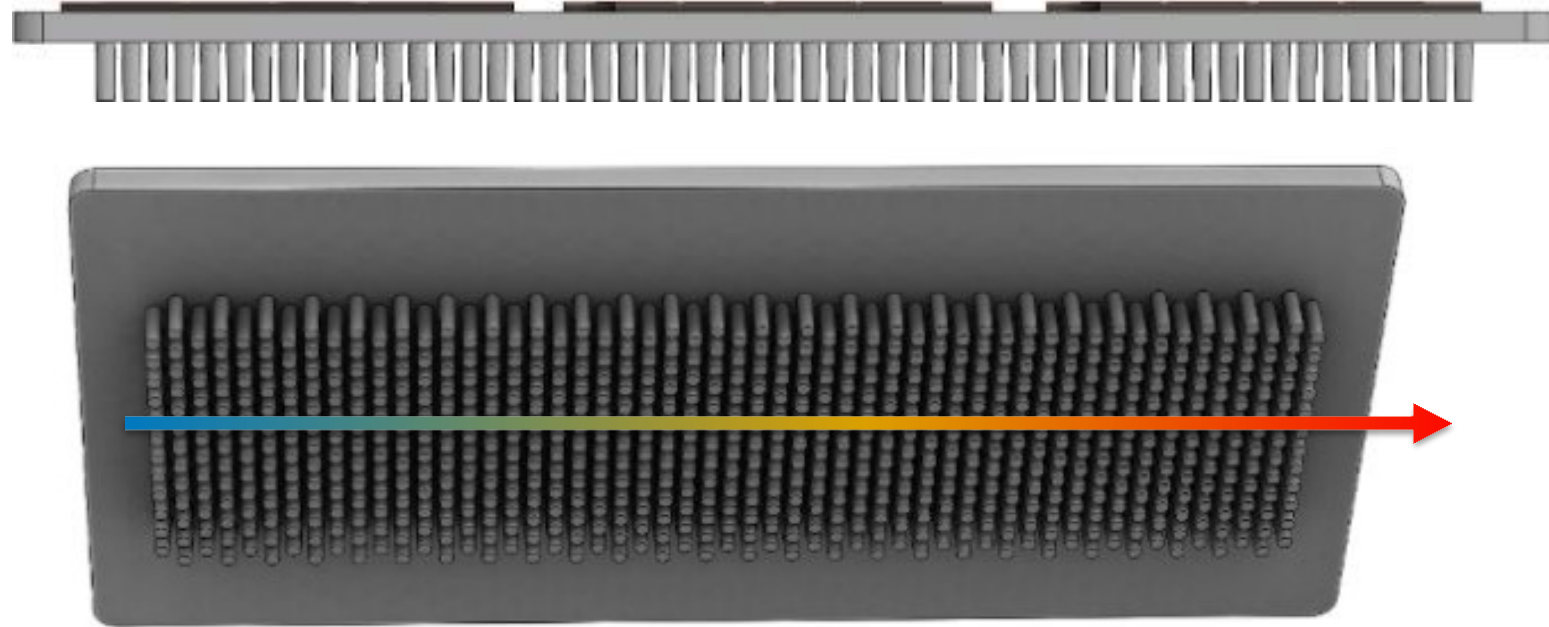
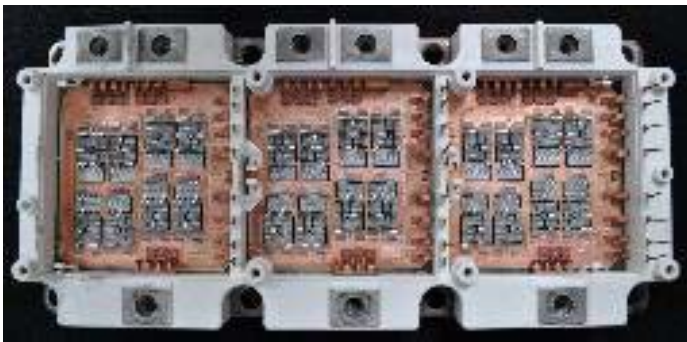
Typical Power Module Packaging Configurations



Automotive power electronics cooling trend

variations for each cooling configuration exist

2015 BMW i3 EV (Baseplate Cooled)

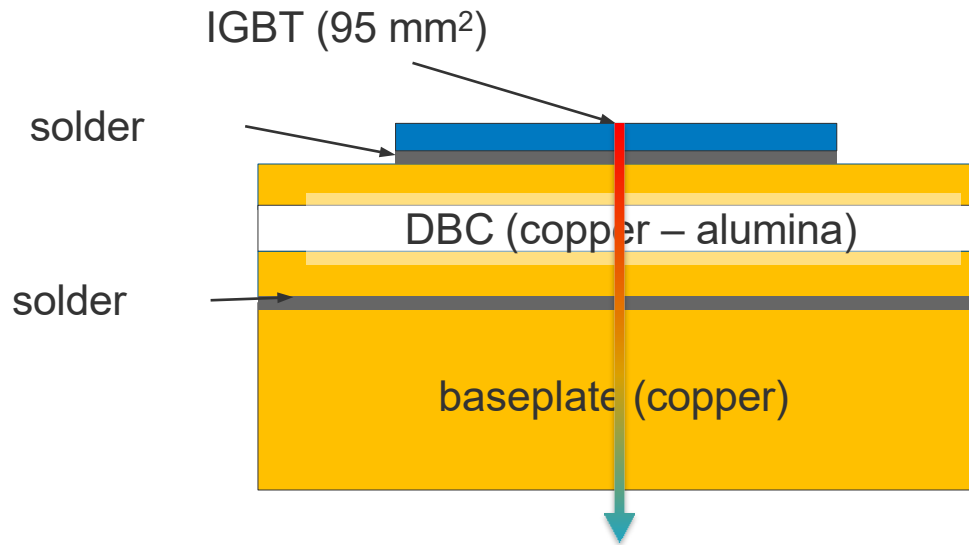


Copper heat exchanger; pin fins: diameter \approx 2.5 mm, height \approx 8 mm, gap between fins \approx 1.8 mm

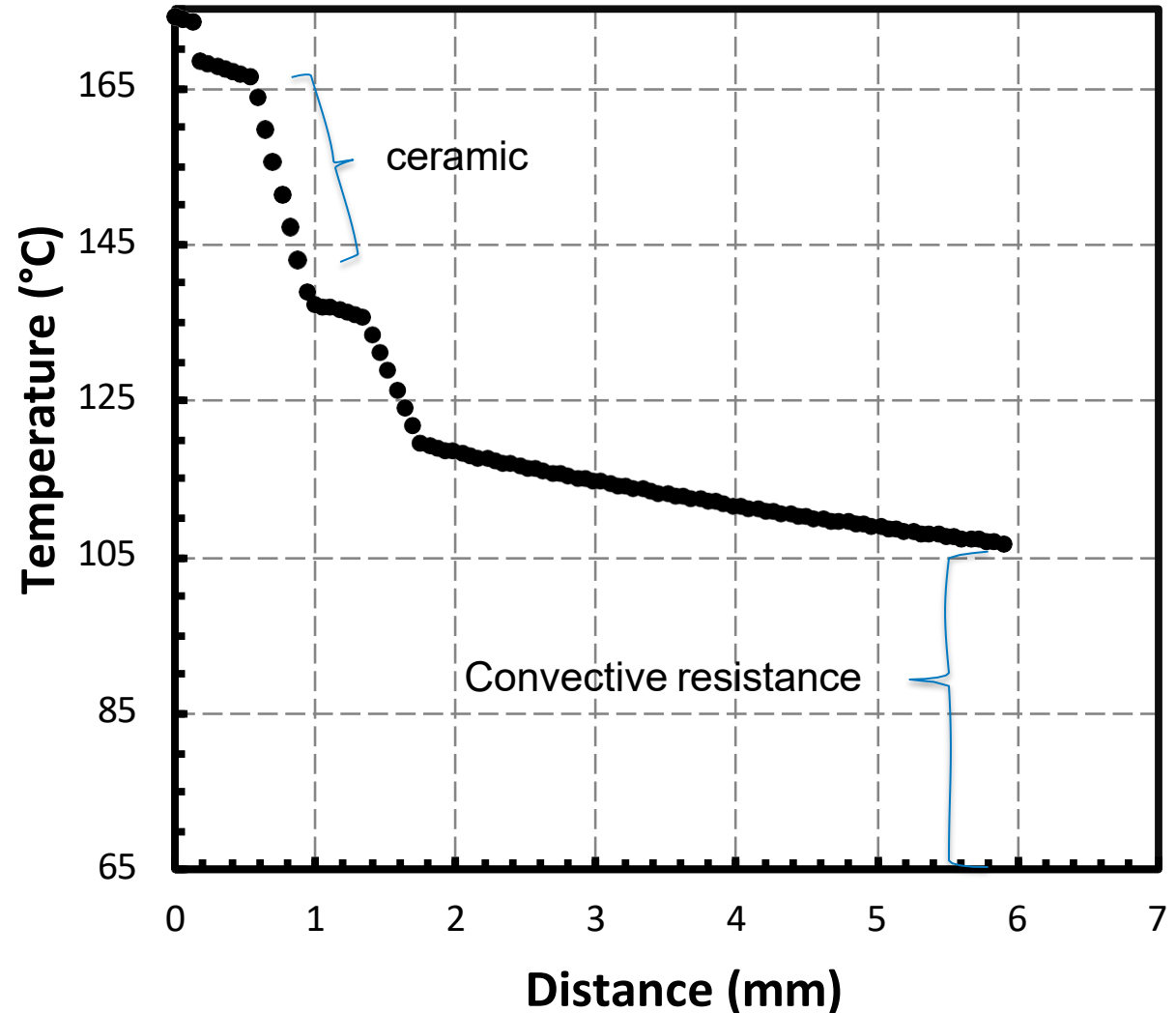
Power density: 18.5 kW/L *

*U.S. DRIVE. 2017. *Electrical and Electronics Technical Team Roadmap*.
<https://www.energy.gov/sites/prod/files/2017/11/f39/EETT%20Roadmap%2010-27-17.pdf>.

2015 BMW i3 EV (Baseplate Cooled)



- Package conduction resistance is about 64% of the total thermal resistance
- Ceramic makes up the largest thermal resistance within the package.
- Predicted to provide a 49 mm² ·K/W thermal resistance performance

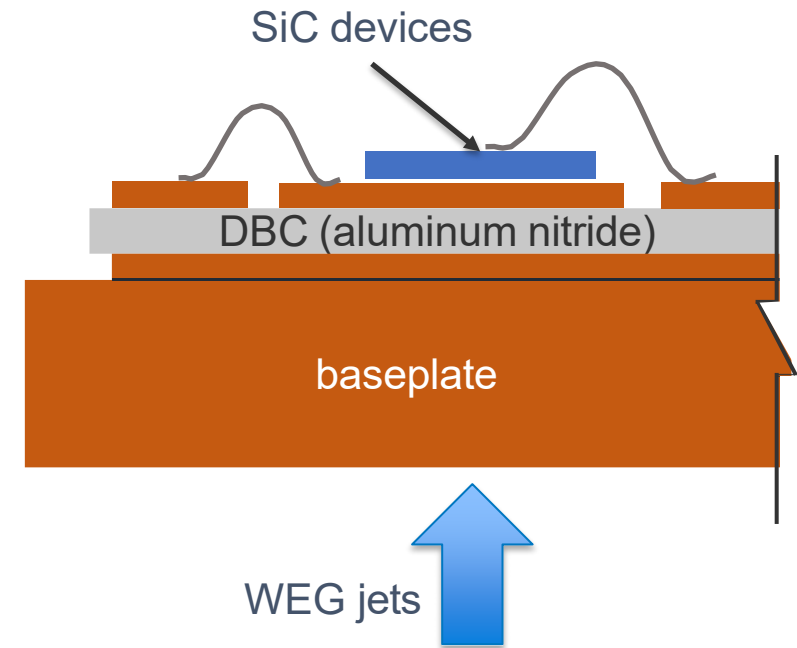


Advanced Cooling Technologies

Objective: Develop thermal management strategies to reach the U.S. Department of Energy power density target of 100 kW/L

Jet Impingement with Water-Ethylene Glycol (WEG)

- Created a silicon carbide (SiC)-based, half-bridge module
- Used a jet-impingement-on-module-baseplate cooling approach
- Complied with automotive guidelines (≥ 1 mm channels), minimized erosion-corrosion effects, and fabricated using in-house fabrication methods (CNC milling, SLA 3D printing, and wire bonding)



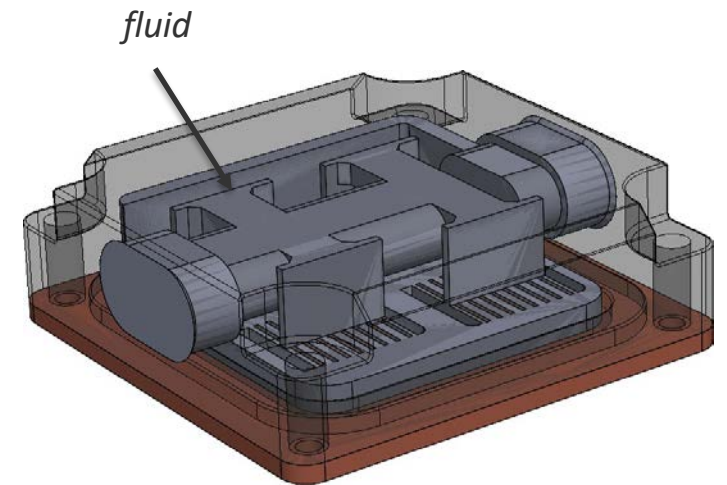
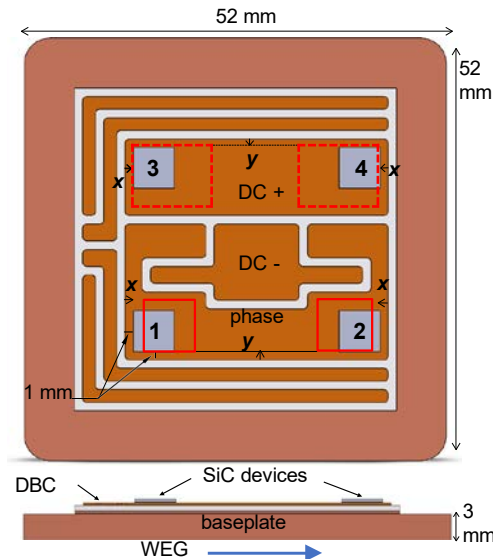
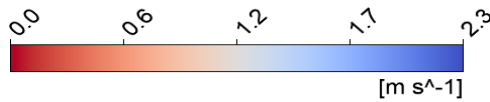
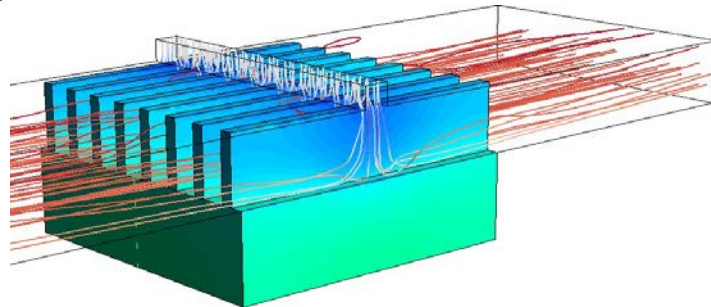
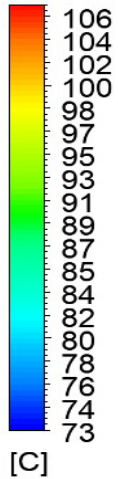
Jet Impingement with Water-Ethylene Glycol

Computed effective
HTCs using device-
scale CFD model

Optimized package
dimensions to
maximize thermal
performance using
FEA

Optimized fluid
manifold dimensions
to minimize thermal
resistance and
pumping power

Temperature



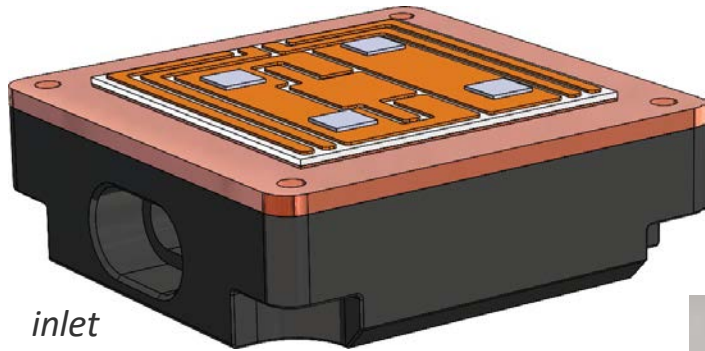
HTC boundary condition

package dimensions

Jet Impingement with Water-Ethylene Glycol

Predict a junction-to-fluid thermal resistance of $17 \text{ mm}^2\cdot\text{K}/\text{W}$ and 1.4°C device temperature variation at 0.8 psi pressure drop

CAD of module on manifold



inlet

SLA printed manifold

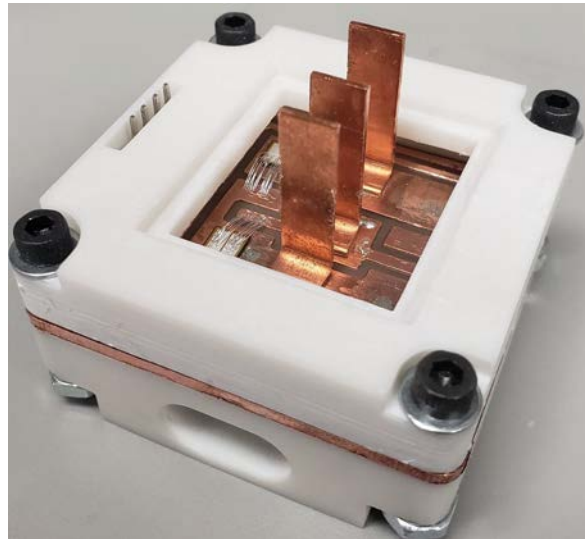
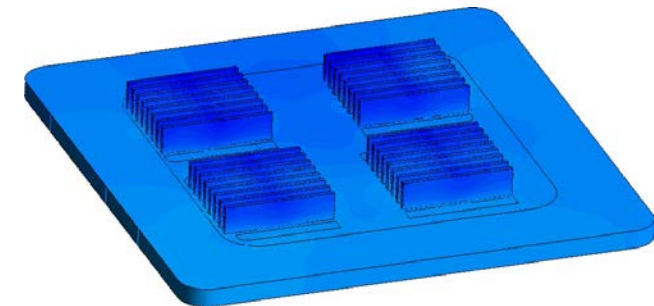
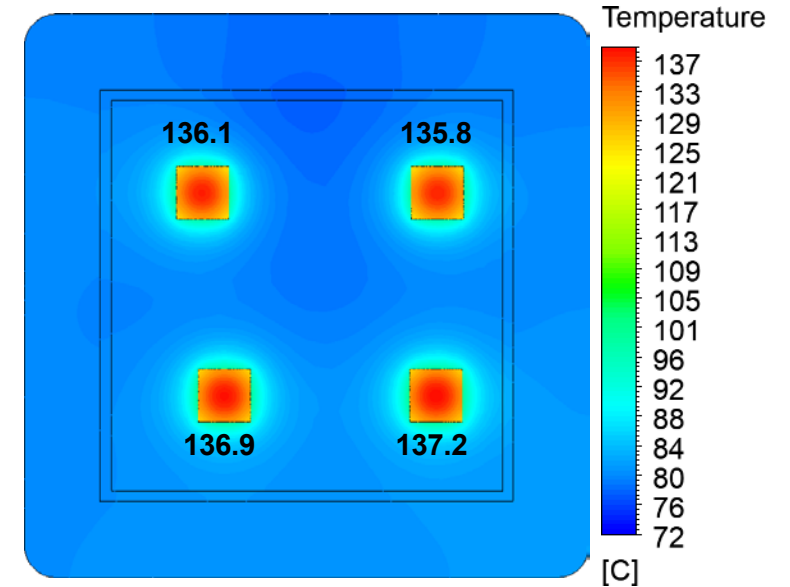


Image credit: Josh Major (NREL)

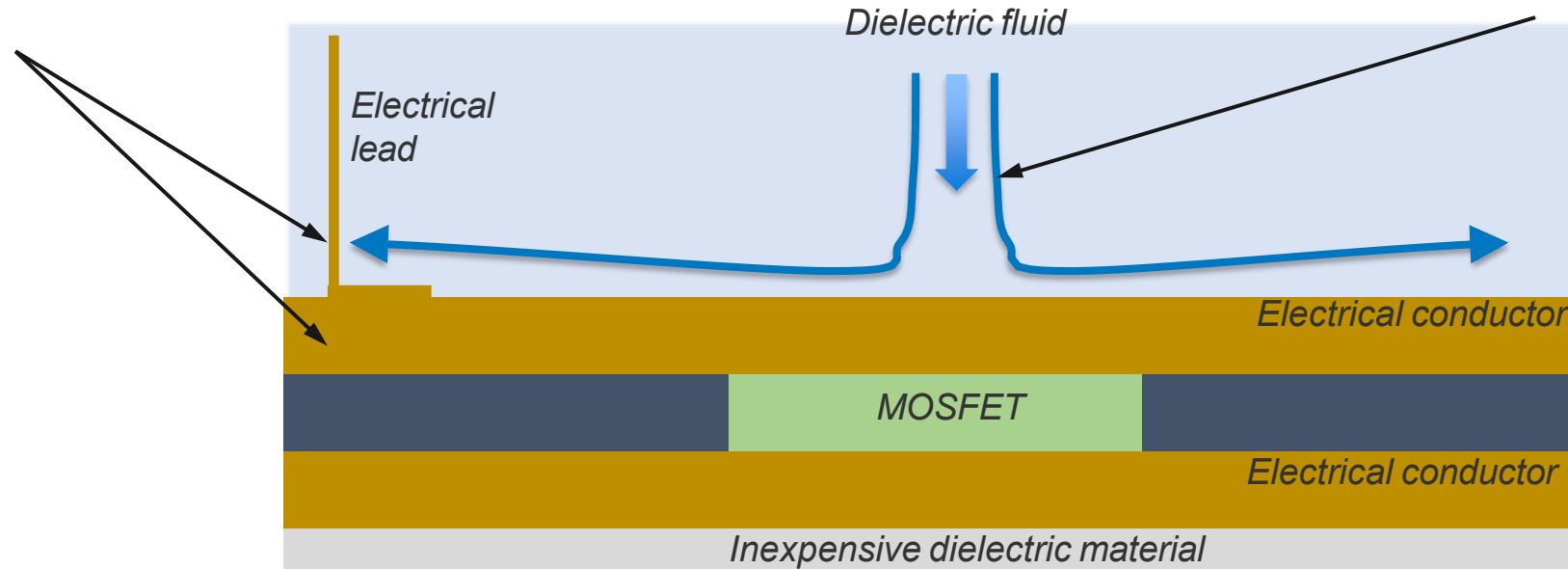


CFD-computed temperatures for 65°C fluid inlet temperature and a $433 \text{ W}/\text{cm}^2$ device heat flux

Dielectric Fluid Cooling Concept (Single Phase)

Allows for cooling of the bus bars/electrical interconnects to lower capacitor and gate driver temperatures

Improved cooling (single-phase heat transfer) via jet impingement and finned surfaces



Eliminates expensive ceramic materials

Improves thermal performance over conventional DBC-based designs

- Reduced package/conduction resistance to 33% of total thermal resistance using a relatively high convection coefficient ($17,300 \text{ W}/[\text{m}^2 \cdot \text{K}]$)
- Designed single-side and double-side dielectric fluid cooling concepts.

Dielectric Fluids (Single Phase)

- Selected synthetic hydrocarbons that are used in electronics cooling (single-phase) applications:
 - Alpha 6: DSI Ventures
 - AmpCool (AC)-100: Engineered Fluids
- Potential to use automatic transmission fluid (ATF) to decrease cost, use fluid already qualified for automotive use, enable motor–inverter integration.
- Challenge is to create a cooling system with high thermal performance using fluids with relatively inferior heat transfer properties as compared to water-ethylene glycol (WEG).

Fluid <i>(properties at 70°C)</i>	Thermal Conductivity [W/m·K]	Specific Heat [J/kg·K]	Density [kg/m ³]	Viscosity [Pa·s]	Flash Point [°C]	Pour Point [°C]
Alpha 6 ¹	0.14	2,308	792	0.0091	246	–57
AC-100 ¹	0.13	2,326	761	0.0025	180	–55
ATF ²	0.16	2,131	836	0.012	199	–45
WEG (50/50) ³	0.42	3,513	1,034	0.0013	>121 ⁴	–36 ⁵ (freeze point)

¹ Communications with vendor (DSI Ventures or Engineered Fluids)

² Kemp, Steven P. and James L. Linden. 1990. "Physical and Chemical Properties of a Typical Automatic Transmission Fluid." SAE Technical Paper.

³ Alshamani, Kaisar. 2003. "Equations for Physical Properties of Automotive Coolants." SAE Technical Paper.

⁴ Valvoline. 2019. "Safety Data Sheet ZEREX HD Nitrile Free Extended Life 50/50 Antifreeze Coolant." Accessed April 1, 2019. <https://sds.valvoline.com/valvoline-sds/sds/materialDocumentResults.faces>.

⁵ Valvoline. 2021. "Product Information: Valvoline ZEREX G05 Antifreeze Coolant." <https://sharena21.springcm.com/Public/Document/18452/f93a8057-fe75-e711-9c10-ac162d889bd3/c264d227-0dbd-e711-9c12-ac162d889bd1>.

Dielectric Fluids (Single Phase)

Single-side cooled

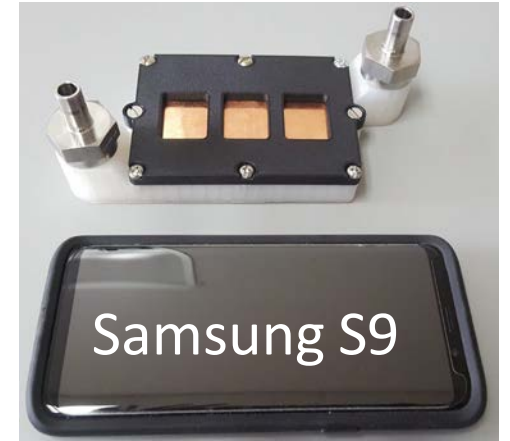
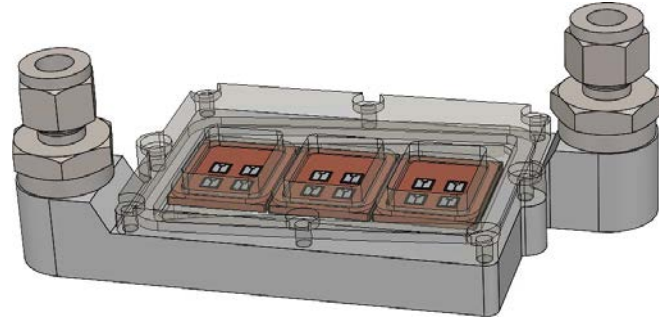
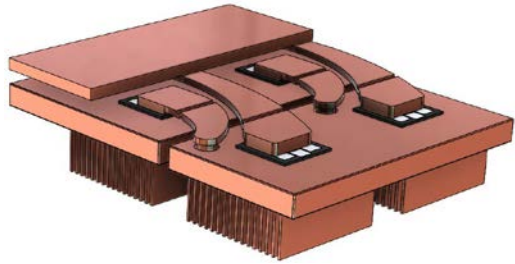
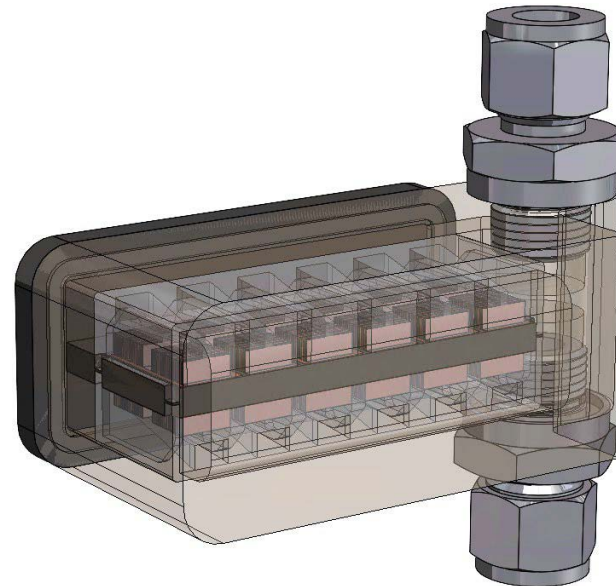
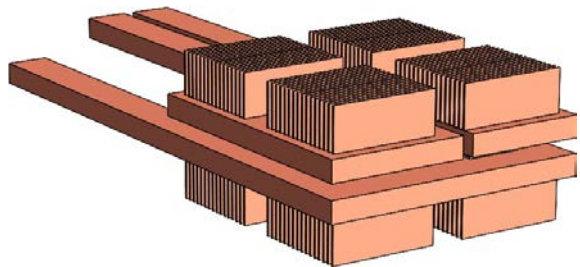
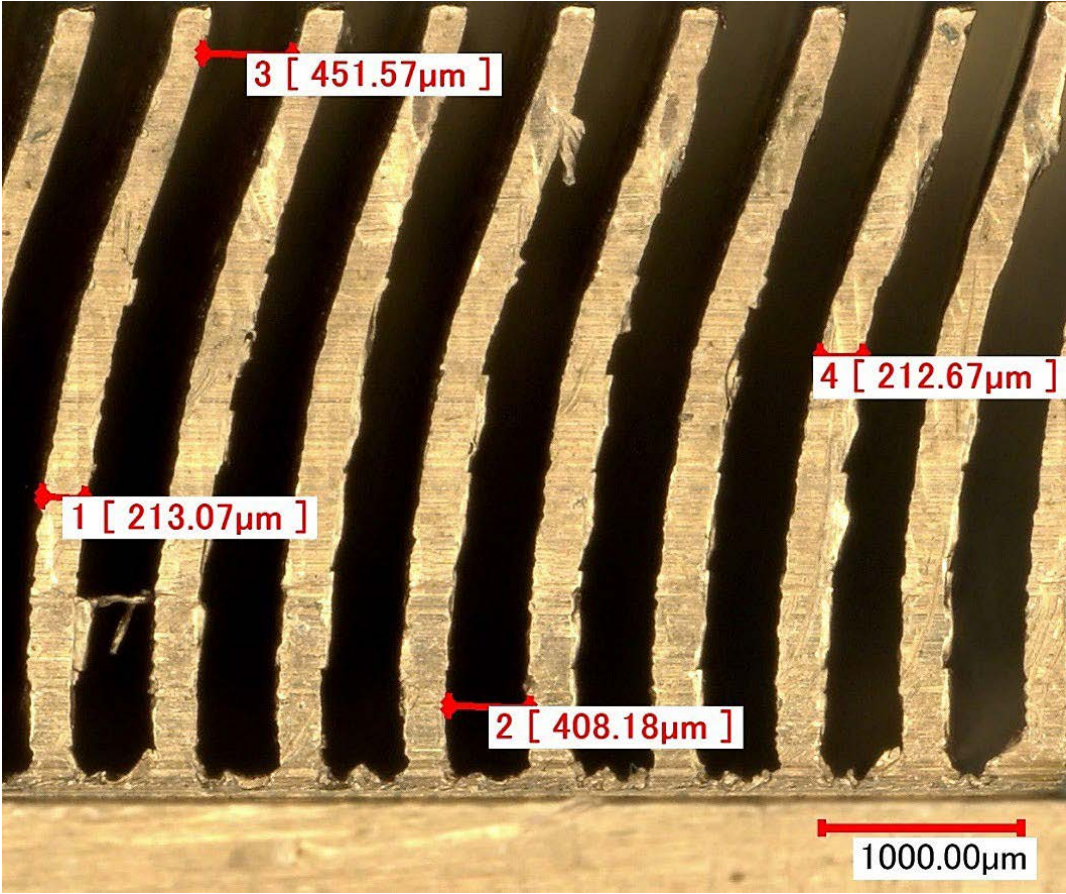
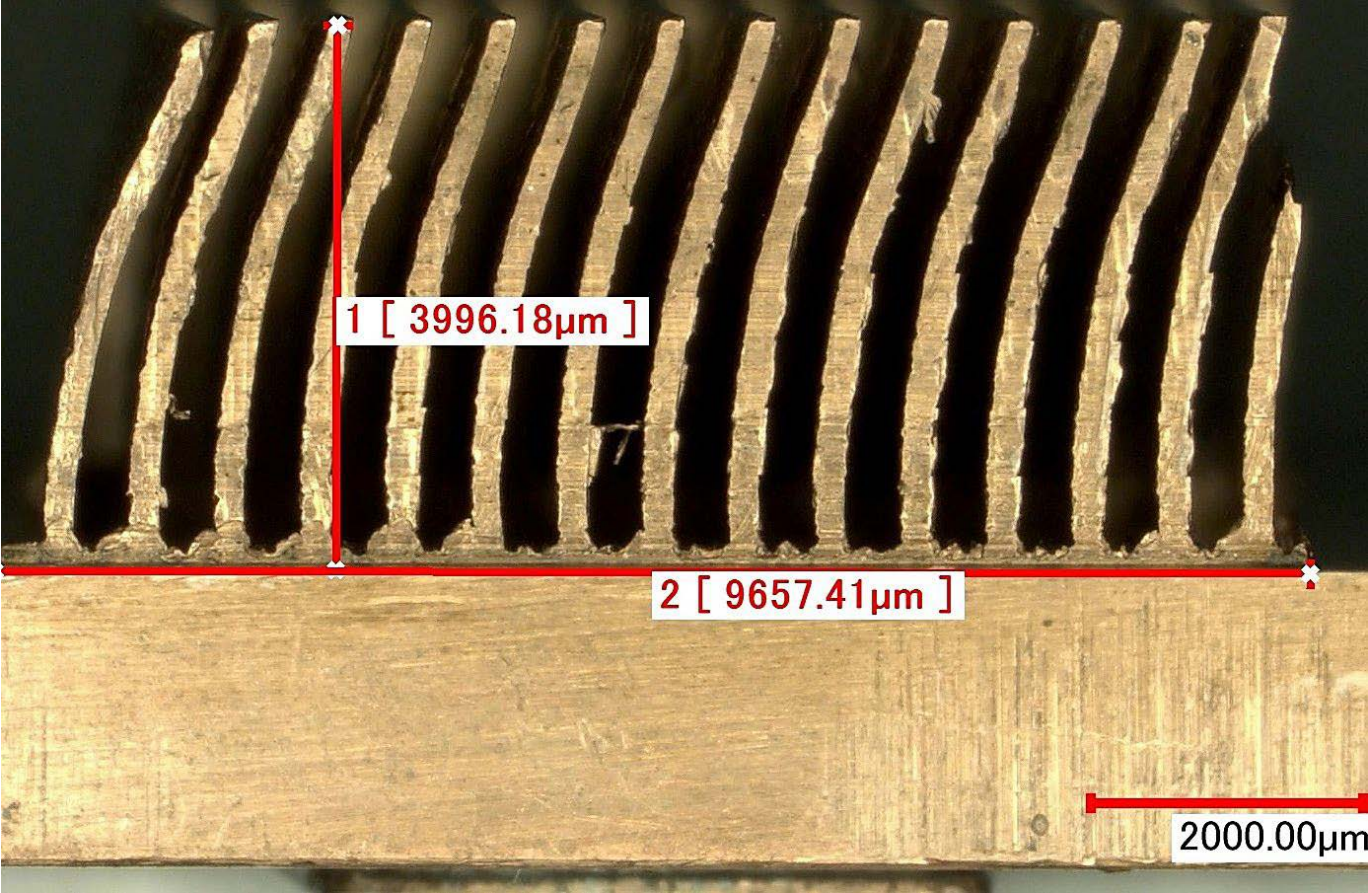
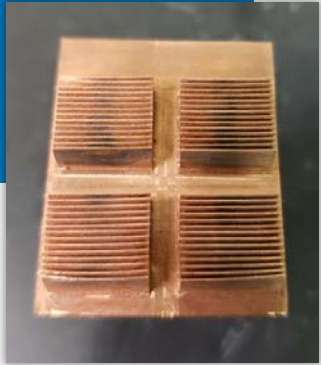


Image credit: Gilbert Moreno, NREL

Double-side cooled



Dielectric Fluids (Single Phase)



Dielectric Fluids (Single Phase)

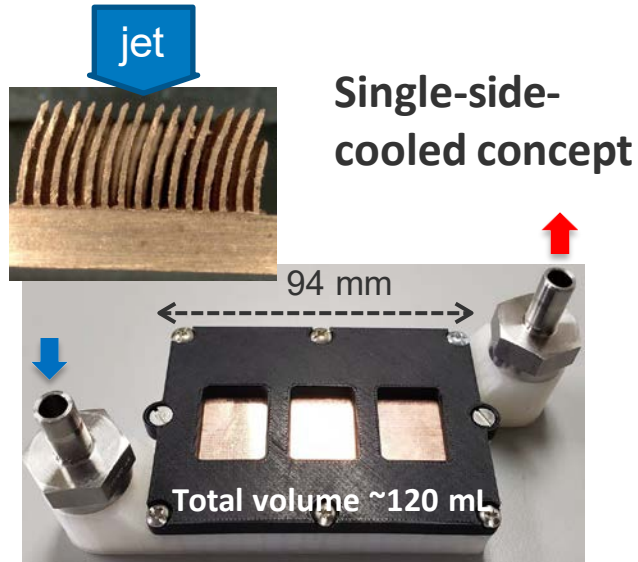
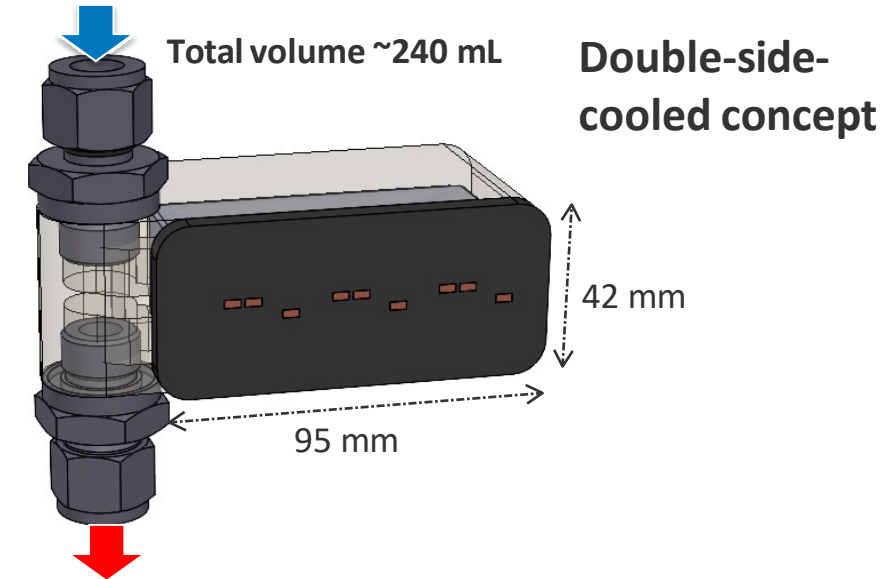


Image credit: Gilbert Moreno, NREL

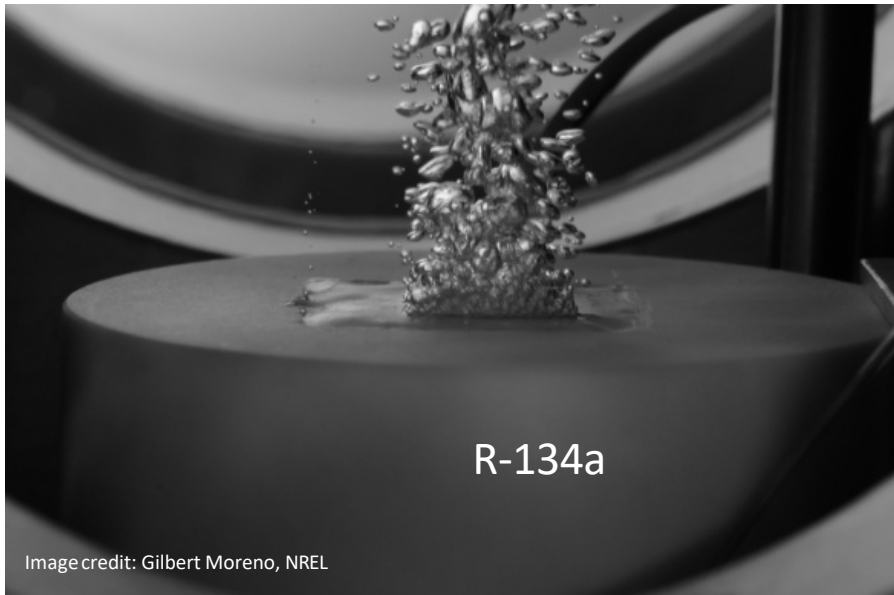


* Estimates assuming $T_{\text{fluid}} = 70^\circ\text{C}$

System	Thermal Resistance (junction-to-fluid)	Flow Rate	Pressure Drop	T_j Maximum	Device Heat Flux*	Total Volume (power modules and cold plate)
	$\text{mm}^2 \cdot \text{K}/\text{W}$	L/min	psi [kPa]	$^\circ\text{C}$	W/cm^2	mL
2015 BMW i3, (WEG cooled)	49	10	1.4 [9.6]	175	214	900
Single-side-cooled dielectric fluid	20	4.1	0.2 [1.4]	175	525	120
Double-side-cooled dielectric fluid	11	4.1	0.6 [4.1]	175	875	240

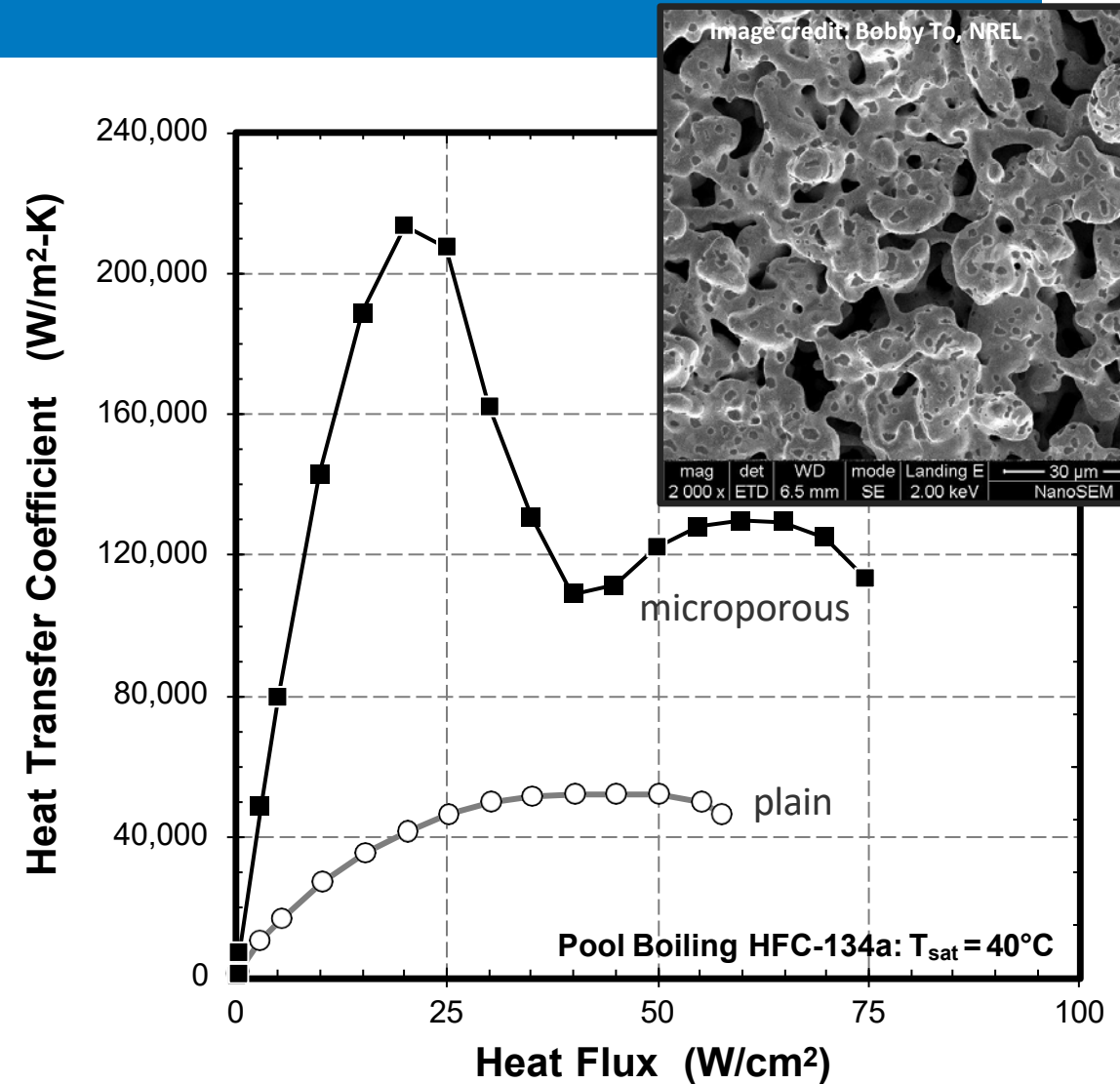
Two-Phase Cooling

- Measured boiling heat transfer performance on 10 × 10-mm heated surfaces and evaluated the following:
 - Refrigerants: R-245fa, R-134a, HFO-1234yf, HFE-7100
 - Enhanced surface: microporous coating, nanostructures
- Achieved HTC's ~50,000 W/m²·K on smooth (and no fins) surfaces
- Measured HTC's >200,000 W/m²·K within small heat flux range
- CHF is one of the major limitations of boiling heat transfer—requires enhanced surfaces to increase CHF and/or limit the heat flux on the boiling surfaces.



R-134a

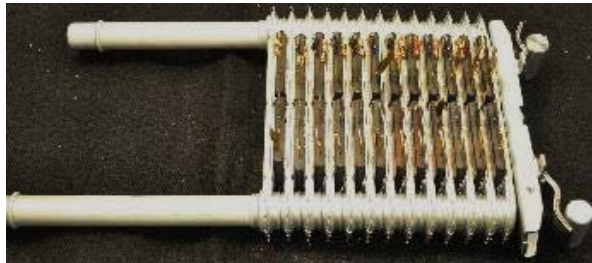
Image credit: Gilbert Moreno, NREL



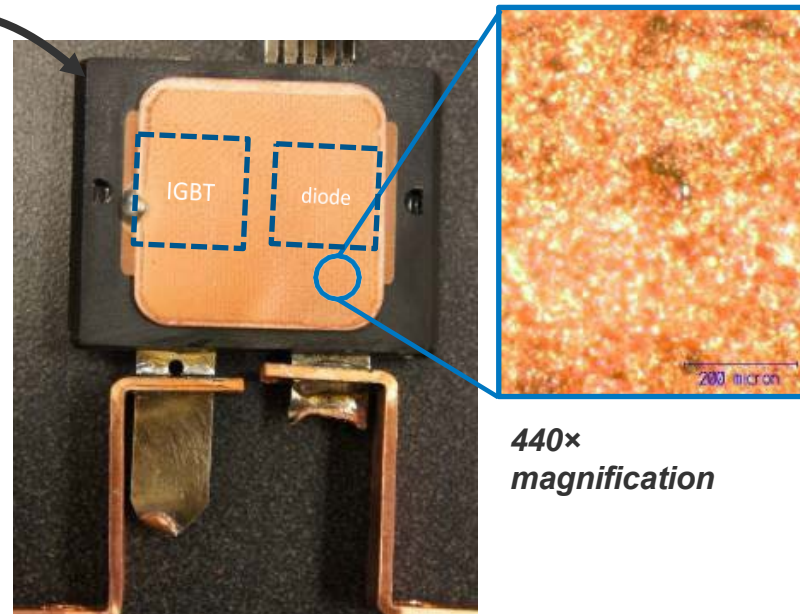
CHF: critical heat flux, HTC: heat transfer coefficient

Two-Phase Cooling: Immersion Cooling of a Module

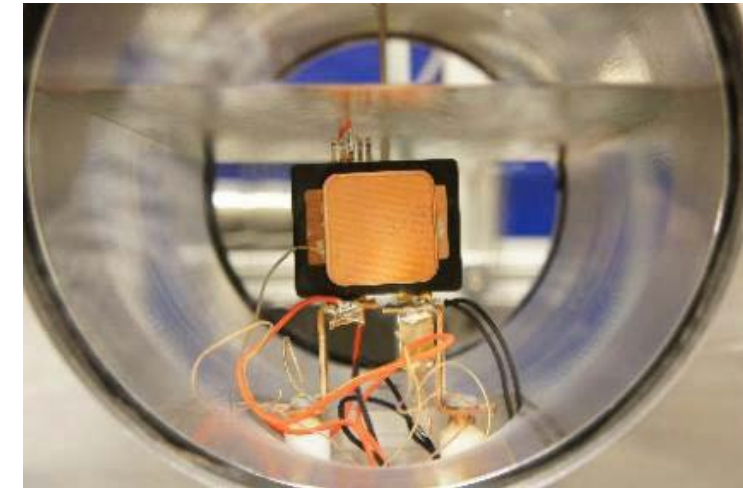
Immersion cooling two-phase (boiling) cooling of an automotive power module (2008 Lexus HEV)



Used a module from the 2008 Lexus



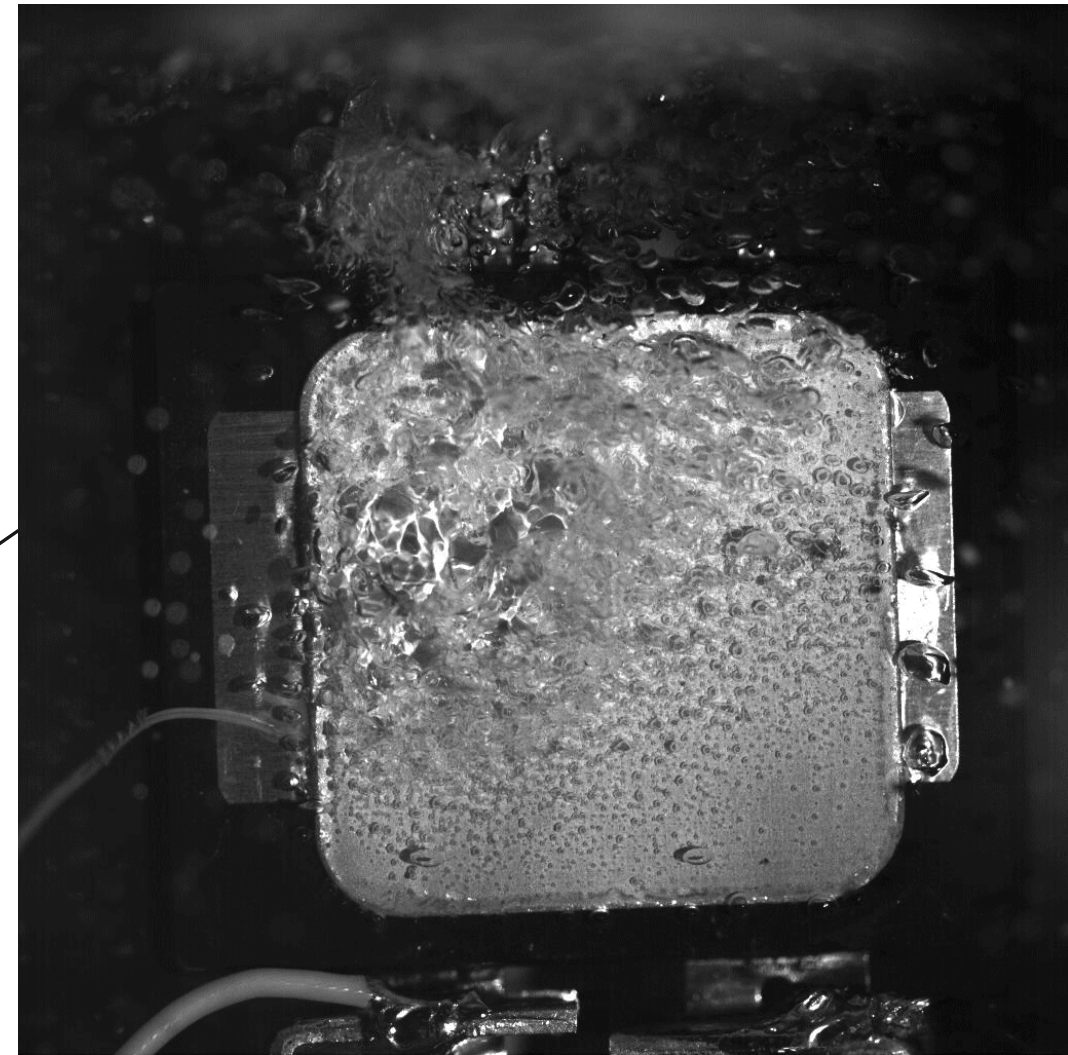
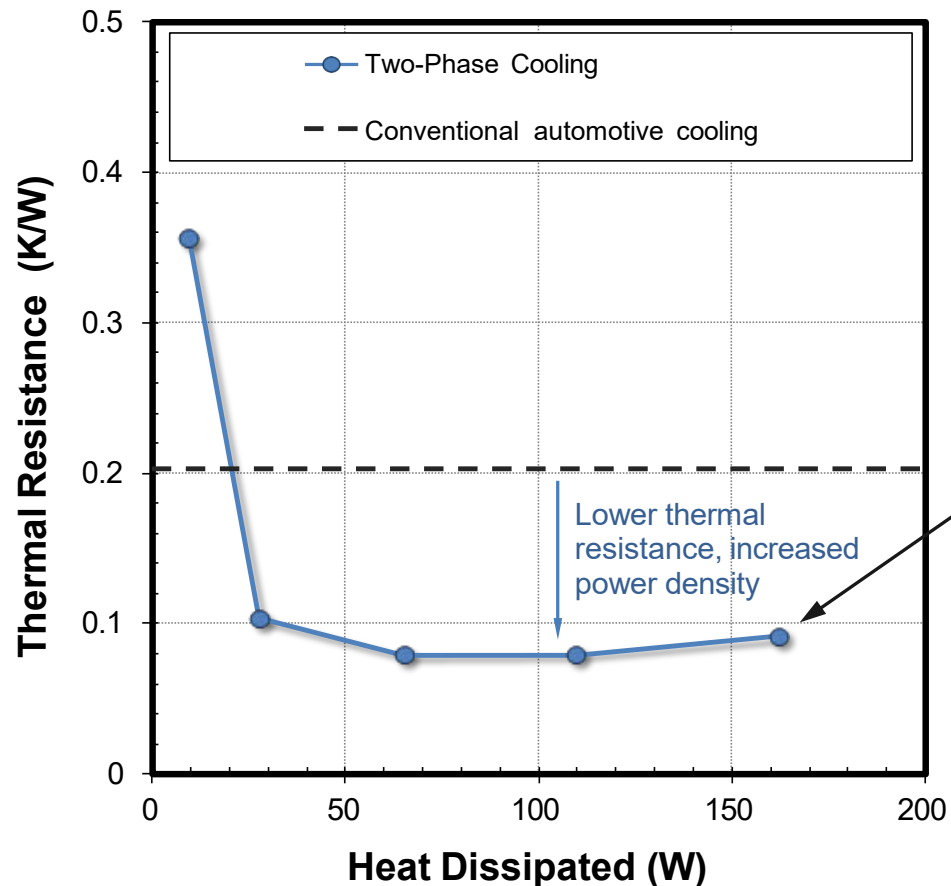
Applied microporous coating to the module



Immersed the module in HFE-7100 fluid

Two-Phase Cooling: Immersion Cooling of a Module

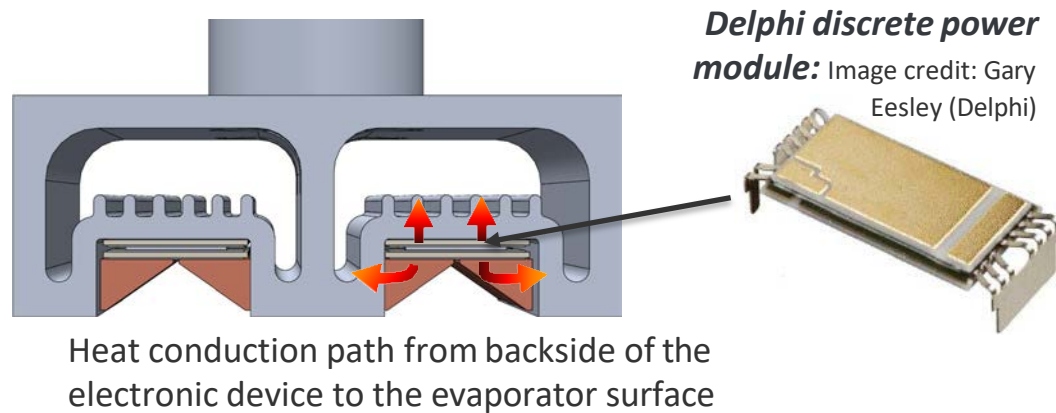
Two-phase cooling with microporous coating reduced thermal resistance by over 60% as compared with the 2008 Lexus system—better performance with no pump required.



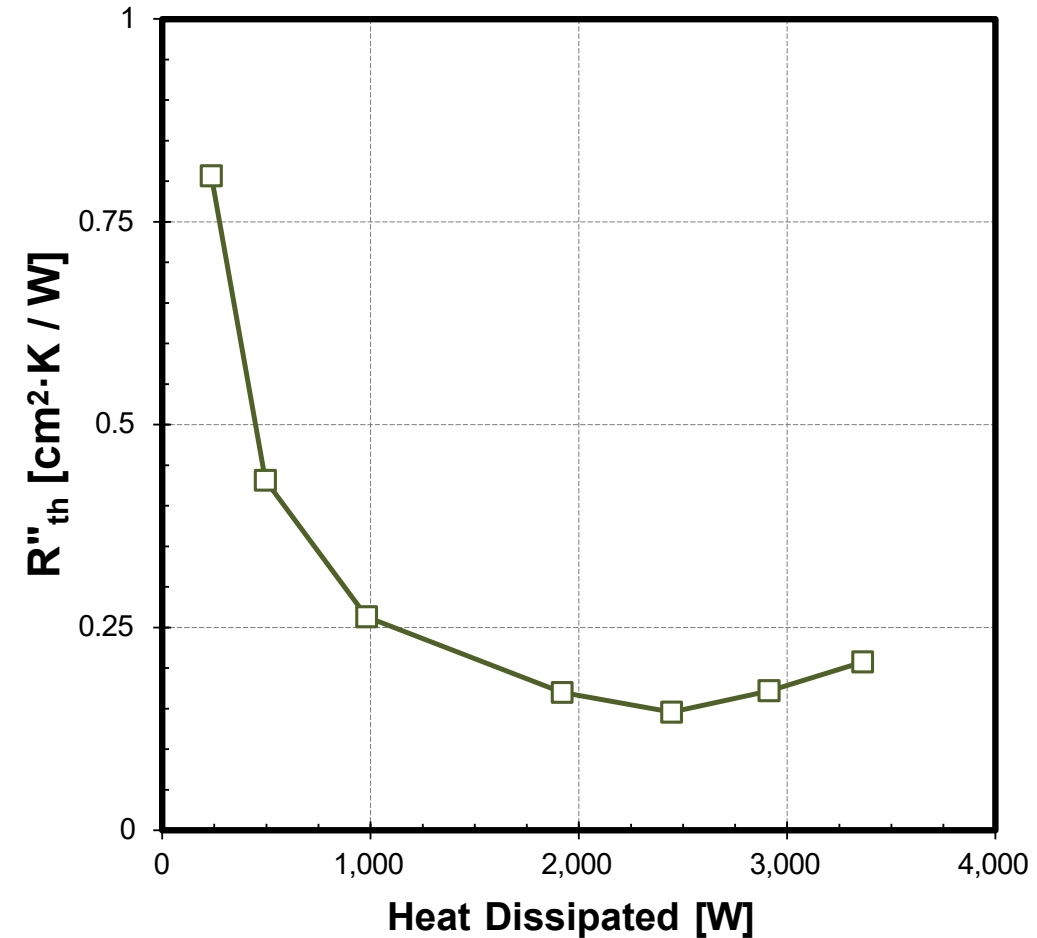
Immersion cooling: HFE-7100 refrigerant

Two-phase Cooling: Indirect Cooling Concept

Designed a passive, indirect two-phase cooling system to cool six Delphi power modules



- Fabricated from low-cost materials (aluminum) using low-cost manufacturing techniques
- Reduced refrigerant requirements to 180 mL, (HFO-1234yf = 200 g, R-245fa = 240 g)
 - Comparison: 2010 Toyota Camry air-conditioning system uses 510 g of R-134a
- Dissipated 3.5 kW of heat with only 180 mL of R-245fa

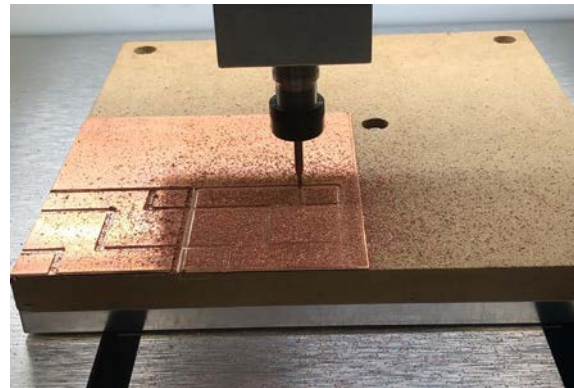
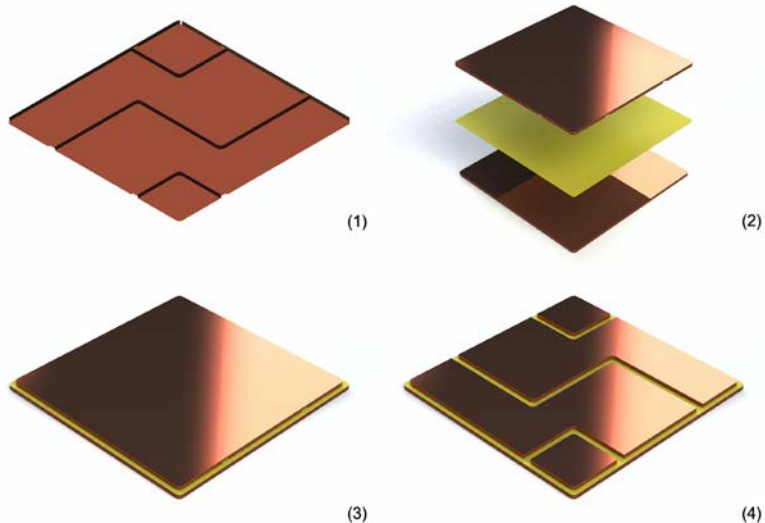


Alternate Substrates: ODBC Substrates

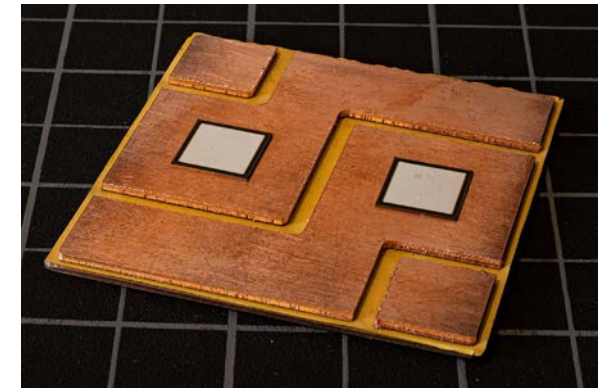
- Organic direct bond copper (ODBC) substrates
 - A polyimide dielectric is bonded with metal through elevated temperature and pressure
 - No limitations in metal material or metallization thickness
- The ability to bond thick copper metallization layers (1–1.5 mm) improves heat spreading directly below devices and lowers their junction temperatures
- Mechanical etching allows for fine width spacing (<1 mm) between conductor traces through thick metallization layers.

Substrate assembly process

- 1. Mechanically etch bottom face of top metallization layer.*
- 2. Assemble Temprion and metallization layers.*
- 3. Apply temperature and pressure to substrate stack.*
- 4. Mechanically etch top face of top metallization layer.*



Machining process



NREL prototype substrate

Acknowledgments

Susan Rogers, U.S. Department of Energy

NREL EDT Task Leader

Sreekant Narumanchi

Sreekant.Narumanchi@nrel.gov

Phone: 303-275-4062

Team Members

Doug DeVoto, NREL

Xuhui Feng, NREL

Faisal Khan, NREL

Josh Major, NREL

Paul Paret, NREL

Jeff Tomerlin, NREL

For more information, contact:

Principal Investigator

Gilbert Moreno

Gilbert.Moreno@nrel.gov

Phone: 303-275-4450

Thank You

www.nrel.gov

NREL/PR-5400-83645

This work was authored by the National Renewable Energy Laboratory, operated by Alliance for Sustainable Energy, LLC, for the U.S. Department of Energy (DOE) under Contract No. DE-AC36-08GO28308. Funding provided by U.S. Department of Energy Office of Energy Efficiency and Renewable Energy Vehicle Technologies Office. The views expressed in the article do not necessarily represent the views of the DOE or the U.S. Government. The U.S. Government retains and the publisher, by accepting the article for publication, acknowledges that the U.S. Government retains a nonexclusive, paid-up, irrevocable, worldwide license to publish or reproduce the published form of this work, or allow others to do so, for U.S. Government purposes.

