

Thermal Management and Reliability of Power Electronics and Electric Machines



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Importance of Thermal Management and Reliability

- Excessive temperature degrades the performance, life, and reliability of power electronics and electric machines.
- Advanced thermal management technologies enable
 - Keeping temperature within limits
 - Higher power densities
 - Lower-cost materials, configurations, and system
 - Improve lifetime/reliability
- Predictive lifetime models help in time-and cost-effective design.

DOE Vehicle Technologies Office Electric Drive Technologies (EDT) Program Targets



4X Cost Reduction

35% Size Reduction

40% Weight Reduction

40% Loss Reduction

2022 Electric Drive System

2012 Electric Drive System

\$30/kW, 1.1 kW/kg, 2.6 kW/L 90% system efficiency

(on-road status)

- Discrete components
- Silicon semiconductors
- Rare-earth motor magnets

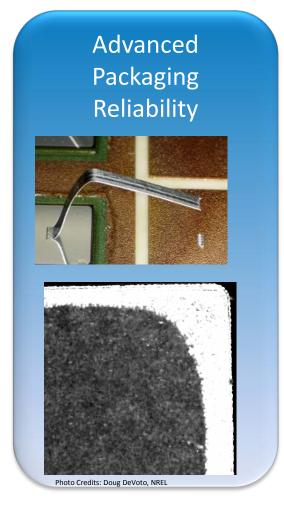
\$8/kW, 1.4 kW/kg, 4.0 kW/L 94% system efficiency

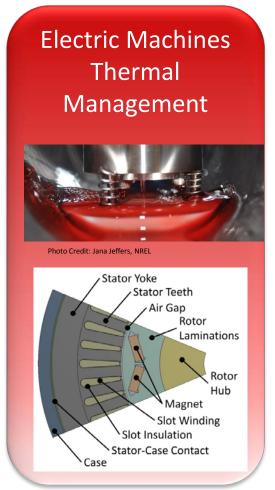
- Fully integrated components
- Wide-bandgap (WBG) semiconductors
- Non rare-earth motors

From DOE EV Everywhere Grand Challenge Blueprint, http://energy.gov/sites/prod/files/2016/05/f31/eveverywhere blueprint.pdf

NREL EDT Research Focus Areas







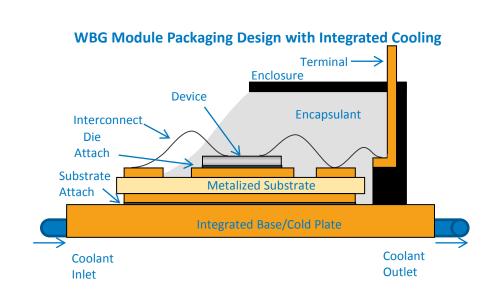
Enabling Materials

Research Focus Areas Will Reduce Cost and Improve Performance and Reliability

Power Electronics Thermal Management

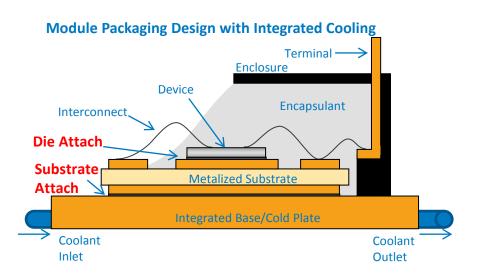
Power Electronics Thermal Management Strategy

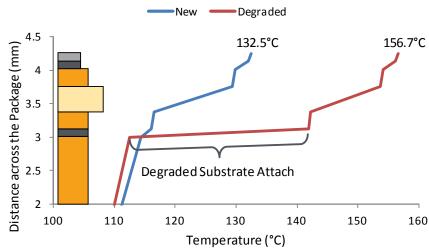
- Packages based on WBG devices require advanced materials, interfaces, and interconnects
 - Higher temperature capability
 - Higher effective thermal conductivity
- Low-cost techniques to increase heat transfer rates
 - Coolants water-ethylene glycol (WEG), air, transmission coolant, refrigerants
 - Enhanced surfaces
 - Flow configurations
- System-level thermal management (capacitor and other passives)



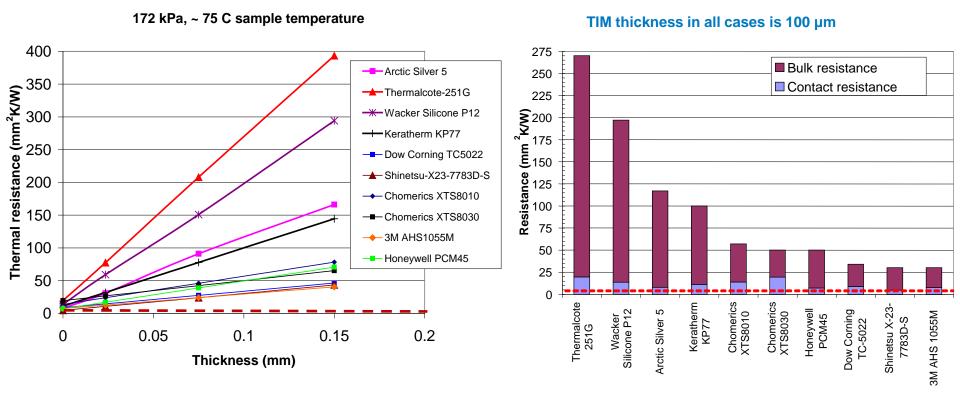
The Challenge with Interfaces/Interface Materials

- Interfaces can pose a major bottleneck to heat removal.
- Bond materials, such as solder, degrade at higher temperatures and are prone to thermomechanical failure.
- Problem can become more challenging for configurations employing WBG devices.





Thermal Resistance of Various Non-Bonded Thermal Interface Materials (TIMs)

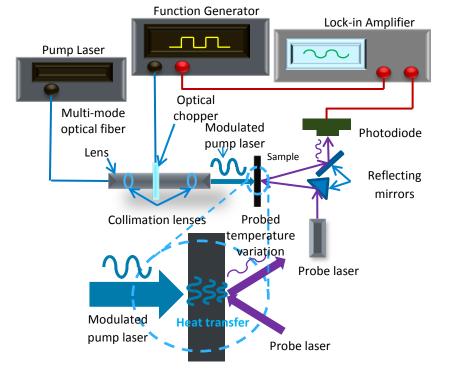


- Red dashed line in the two figures above is the target thermal resistance (3 to 5 mm²K/W).
- Most non-bonded TIMs do not come close to meeting thermal specification of 3 to 5 mm²K/W at approximately 100-μm bond line thickness.

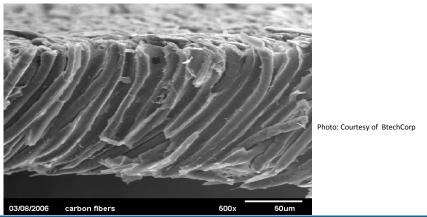
Thermal Resistance of Thermoplastics with Embedded Carbon Fibers

	Thermoplastic film HM-2
Bondline thickness (μm)	60
Bulk thermal conductivity (W/m·K)	37.5 ± 6.8
Contact resistance (mm²·K/W)	3.1 ± 1.1
Total thermal resistance (mm²·K/W)	7.5 ± 1.9

Frequency-domain transient thermoreflectance experiment configuration



 Thermoplastics with embedded carbon fibers show very good thermal performance

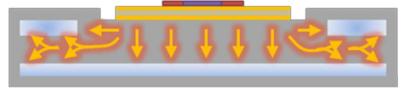


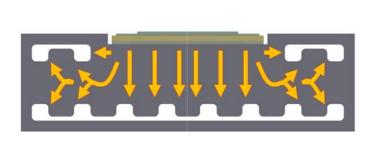
Other Bonded Interface Materials

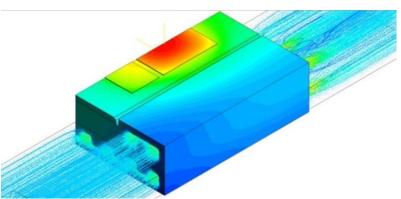
- Bonded interface resistance in the range of 0.4 to 2 mm²K/W is possible.
 - Materials developed in the DARPA programs are in this range
 - o Copper nanowires
 - O Boron-nitride nanosheets (0.4 mm²K/W for 30- to 50-μm bondline thickness)
 - Copper nanosprings (1 mm²K/W for 50-μm bondline thickness with very good reliability)
 - o Graphite solder
 - Nanotube-based

Integrated Module Heat Exchanger

NREL integrated module heat exchanger Patent No.: US 8,541,875 B2







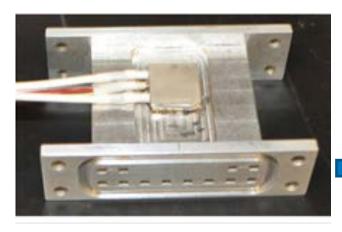
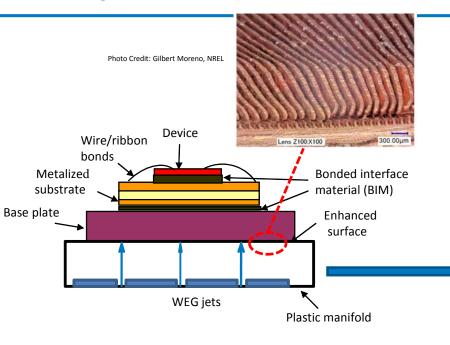
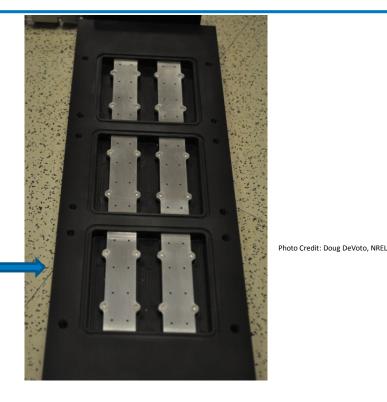


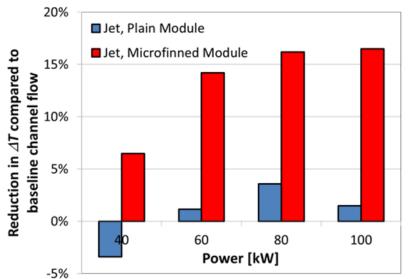
Photo Credit: Kevin Bennion, NREL

- Up to 100% increase in power per die area
- Up to 34% increase in coefficient of performance (efficiency)

Liquid Jet-Based Plastic Heat Exchanger







- Up to 12% increase in power density
- Up to 36% increase in specific power

Two-Phase Cooling for Power Electronics

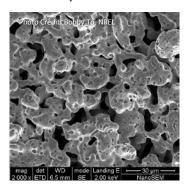
Fundamental Research

Module-Level Research

Inverter-Scale Demonstration



Photo Credit: Gilbert Moreno, NREL
Characterized performance of
HFO-1234yf and HFC-245fa



Achieved heat transfer rates of up to ~200,000 W/m²-K

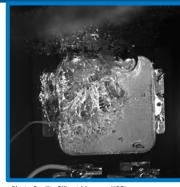
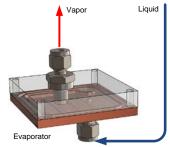
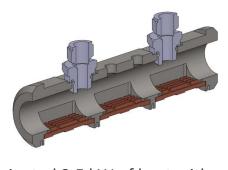


Photo Credit: Gilbert Moreno, NRE

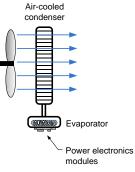
Reduced thermal resistance by over 60% using immersion twophase cooling of a power module



Quantified refrigerant volume requirements



Dissipated 3.5 kW of heat with only 250 mL of refrigerant



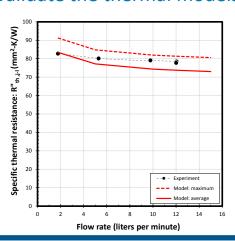
Predicted 58%–65% reduction in thermal resistance via indirect and passive two-phase cooling

WBG Power Electronics Thermal Management

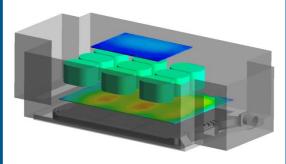
Create thermal models of an automotive inverter



Validate the thermal models



Simulate WBG operation using the inverter model



Quantify the inverter component temperatures under elevated device temperatures

Identify the primary thermal paths through which heat is conducted from the devices to the other components

Explore advanced cooling strategies





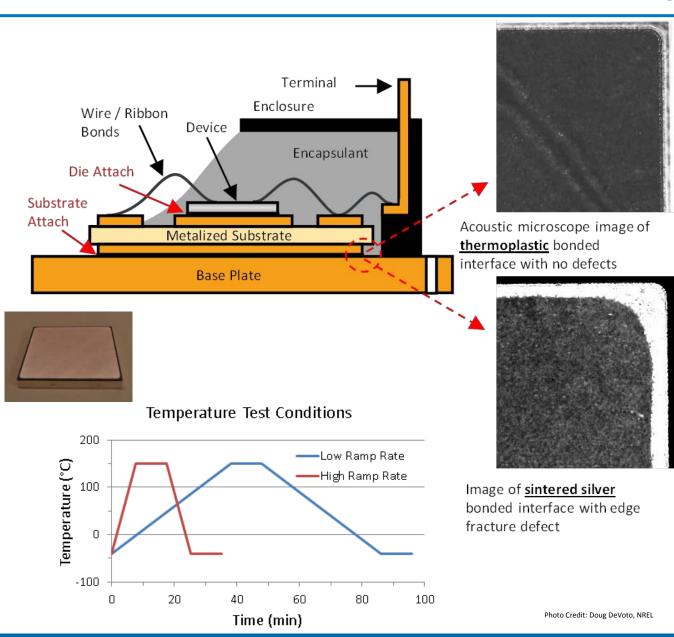
Evaluate different module topologies

Develop thermal management concepts to enable WBG power electronics

Experimentally validate some key thermal management concepts

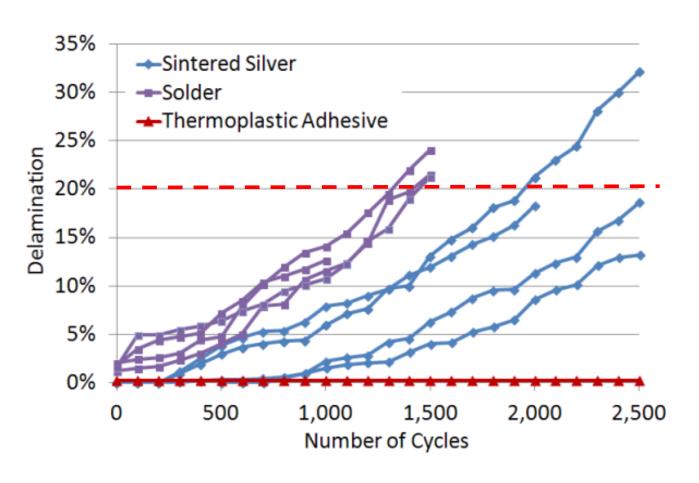
Advanced Packaging Reliability

Bonded Interface Material Reliability



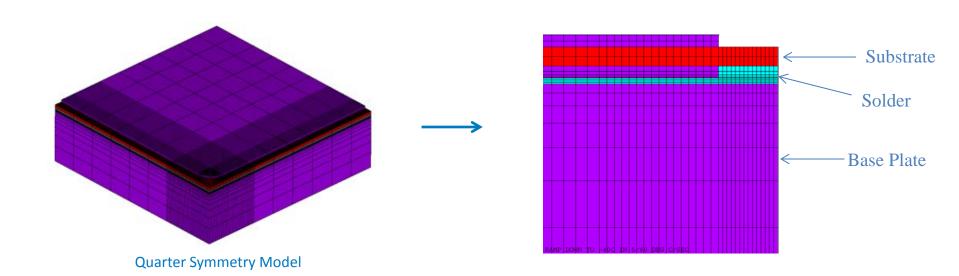
- Thermoplastics yield very good reliability
- Reliability of sintered silver is better than solder

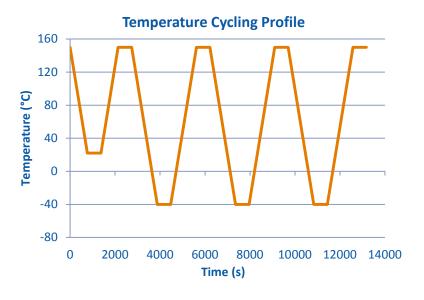
Bonded Interface Material Reliability



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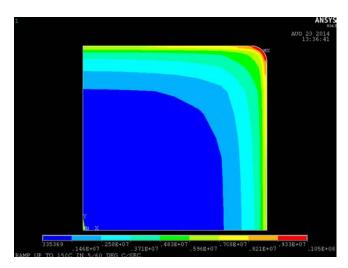
Bonded Interface Material Finite Element Modeling



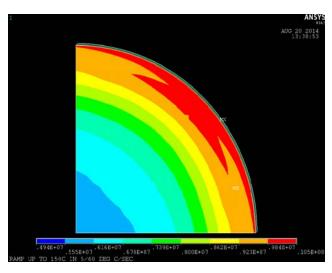


- Temperature cycling parameters:
 - -40°C to 150°C
 - 5°C/minute ramp rate
 - 10 minute dwell/soak time
- Anand viscoplastic material model applied to solder layer
- Temperature-dependent elastic material properties incorporated for base plate and substrate

Strain Energy Density



Top view of strain energy density contour plot in the solder layer



Corner fillet region

• Volume-averaged strain energy density/cycle (ΔW) in the corner fillet region is the final output

Impact of Geometric Variations on Reliability

Joint Thickness

Predictive Lifetime Model, $N_f = 2312.5 (\Delta W)^{-1.645}$

Profile	Joint Thickness (μm)	ΔW (MPa)	Predicted experimental cycles to failure – N _f
	50	2.65	465
Thermal cycle	100	1.36	1,400
	150	0.93	2,600

• Substrate Variation

Profile	Substrate	CTE (x 10 ⁻⁶ /°C)	ΔW (MPa)	Predicted experimental cycles to failure – N _f
Thermal cycle	Si ₃ N ₄	2.8	1.36	1,400
	AIN	4.5	1.08	2,000
	Al_2O_3	8.1	0.44	9,000

CTE: coefficient of thermal expansion

Si₃N₄: silicon nitride AlN: aluminum nitride Al₂O₃: aluminum oxide

Electric Machines Thermal Management

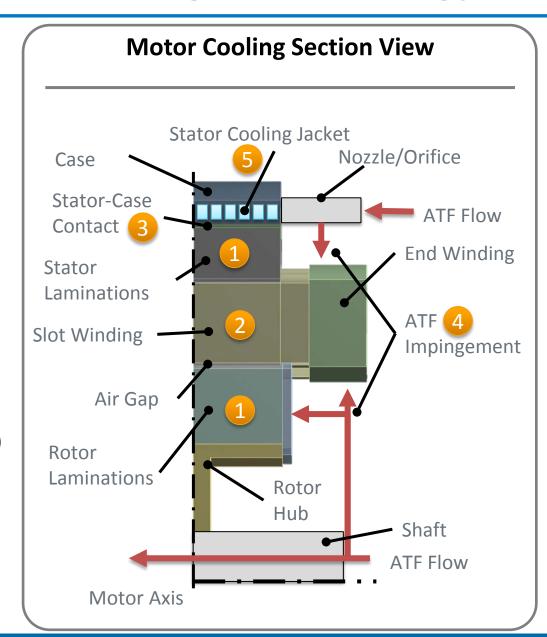
Electric Machines Thermal Management Strategy

Problem

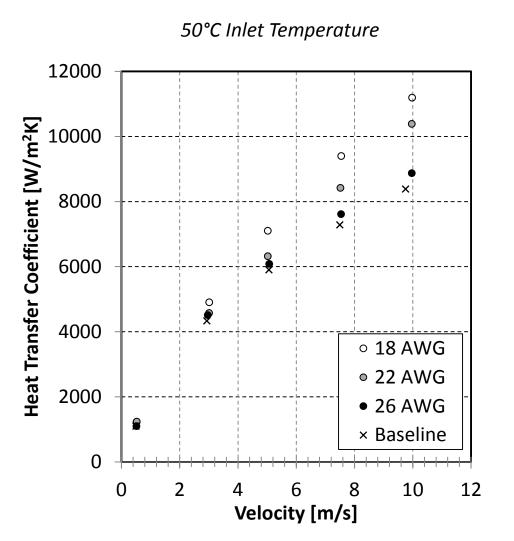
 Multiple factors impacting heat transfer are not well quantified or understood.

Contributing Factors

- Direction-dependent thermal conductivity of lamination stacks
- Direction-dependent thermal conductivity of slot windings and end windings
- Thermal contact resistances (statorcase contact, slot-winding interfaces)
- Convective heat transfer coefficients for ATF cooling
- 5. Cooling jacket performance

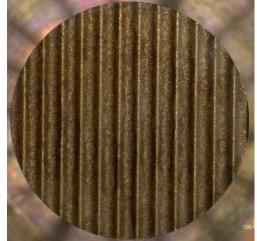


Transmission Oil Jet Heat Transfer Characterization





Side View



Top View

18 AWG surface target

Heat transfer coefficients of all target surfaces at 50°C inlet temperature

Surface features increase heat transfer

Note: Heat transfer coefficient calculated from the base projected area (not wetted area)

Photo Credits: Gilbert Moreno, NREL

Stator Thermal Management with Transmission Oil

 Enclosure allows direct impingement on motor for heat transfer measurements and flow visualization

Enclosure with stator and ATF cooling



Jet impingement on target surface

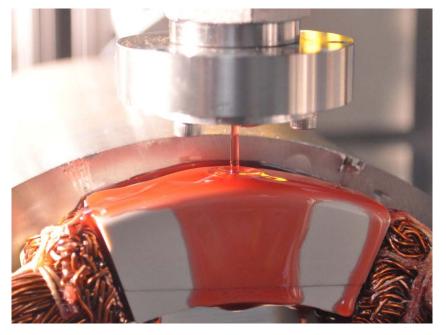


Photo Credits: Kevin Bennion, NREL

Motor Passive Thermal Materials Characterization

Stator laminations

Performing thermal analysis on passive thermal materials

Measure liner-to-stator thermal contact resistance

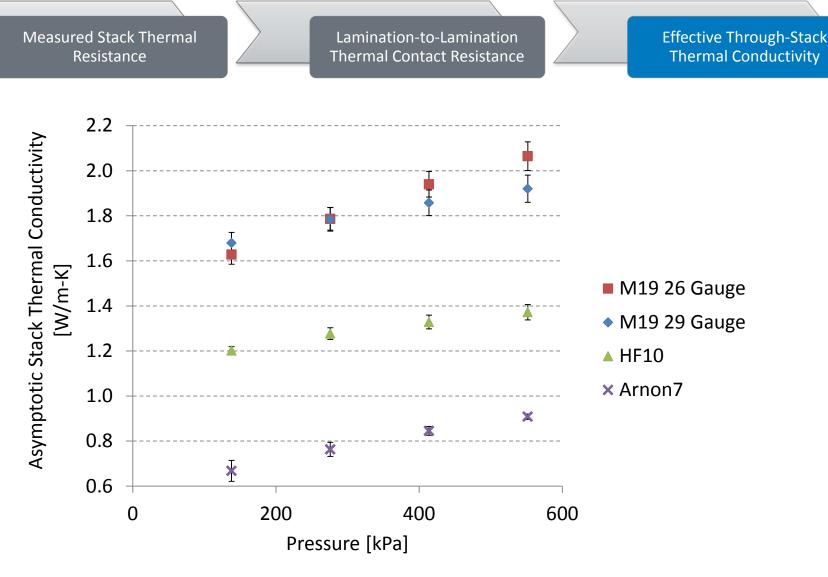
Measure winding-to-liner thermal contact resistance

Measure cross-slot winding thermal conductivity

Slot windings

Slot liner or ground insulation

Lamination Stack Effective Thermal Conductivity

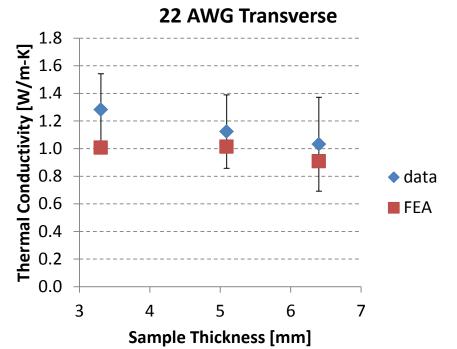


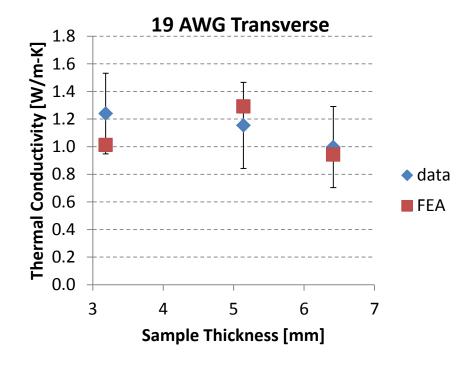
Error bars represent 95% confidence level

Transverse Winding Thermal Conductivity



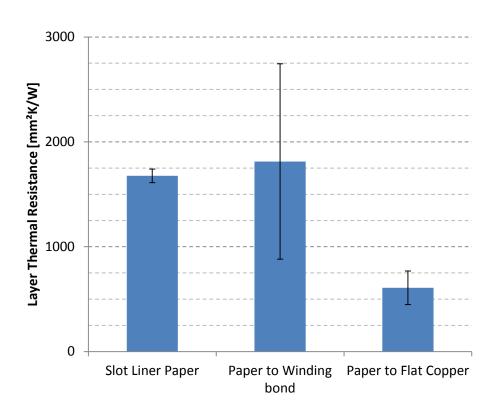
Photo Credit: Emily Cousineau, NREL





- Error bars represent 95% measurement uncertainty (U95)
- Finite element analysis (FEA) model results based on measured sample copper fill factor
- FEA assumes hexagonal or closed-pack wire pattern

Slot Liner Paper and Thermal Interface Resistances



- Limited sample size for measurements
- Slot liner paper thermal conductivity of 0.18 W/m-K (thickness 0.29 mm)
- Winding thermal conductivity measured to be 0.88 ± 0.11 W/m-K (U₉₅)
- FEA estimate of thermal conductivity is 0.99 W/m-K for measured copper fill factor

Participation in Industry-Led Projects

- Industry-led inverter development with VTO and AMO funding
 - Delphi inverter (VTO)
 - GM inverter (VTO)
 - Wolfspeed WBG inverter (VTO)
 - John Deere WBG inverter (AMO)
- UQM Technologies motor development (VTO funding)

AMO: Advanced Manufacturing Office VTO: Vehicle Technologies Office

Summary

- Low-cost, high-performance thermal management technologies are helping meet aggressive power density, specific power, cost, and reliability targets for power electronics and electric machines.
- NREL is working closely with numerous industry and research partners to help influence development of components that meet aggressive performance and cost targets through:
 - Development and characterization of cooling technologies
 - Thermal characterization and improvements of passive stack materials and interfaces.
- Thermomechanical reliability and lifetime estimation models are important enablers for industry in cost- and time-effective design.



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Industry and Research Partners

Industry OEMs	Ford, GM, FCA, John Deere, Tesla, Toyota
Suppliers/Others	3M, NBETech, Curamik, DuPont, GE Global Research, Semikron, Kyocera, Sapa, Delphi, Btechcorp, ADA Technologies, Remy/BorgWarner, Heraeus, Henkel, Wolverine Tube Inc., Wolfspeed, Kulicke & Soffa, UQM Technologies, nGimat LLC
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