

# Thermal Management of Power Semiconductor Packages – Matching Cooling Technologies with Packaging Technologies



**IMAPS 2<sup>nd</sup> Advanced  
Technology Workshop on  
Automotive Microelectronics  
and Packaging**

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# Acknowledgements

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- Jason Lustbader, National Renewable Energy laboratory (NREL)
- Advanced Power Electronics and Electric Machines Benchmarking, Oak Ridge National Laboratory (ORNL)

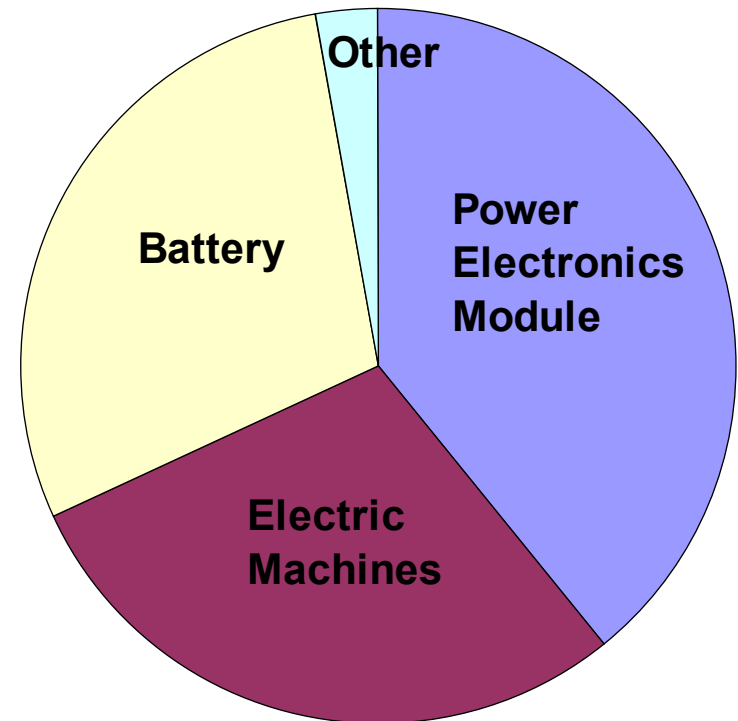
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Department of Energy

# Objective

1. Efficient heat transfer technologies can enable increased power density and specific power.
2. Thermal management is a path to reduce cost and maintain robust operation.
3. Thermal management should not be an afterthought but should involve an integrated systems approach.
4. Cost-effective solutions require **integration** of capabilities for **cooling**, **packaging** (materials/geometry), and **reliability** prediction.

## Toyota Camry - 2007



*Source: Technology and Cost Report of the MY2007 Toyota Camry - ORNL*

# Relevance of Thermal Management

Thermal management directly relates to improvements in cost, power density, and specific power.

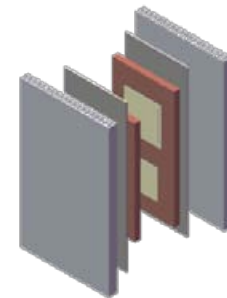
Prius PE MY 2004



Camry PE MY 2007



LS 600h PE MY 2008



Double-sided  
Cooling

## ***Impacts: Lower cost, volume, and weight***

“Easy ways to increase output power are paralleling more silicon chips and/or step-up the die size to increase current capacity. But this strategy is **unaffordable** in terms of both increased chip cost and packaging space.”

## ***Concern: Heat***

“The most significant concern for increasing current is intensified **heat dissipation.**”

Source: Yasui, H., et al, “Power Control Unit of High Power Hybrid System” – EVS23

# Outline

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## Background

- Department of Energy's Advanced Power Electronics and Electric Machines (APEEM) activity.
- Thermal management for power electronics cooling.

## Problem

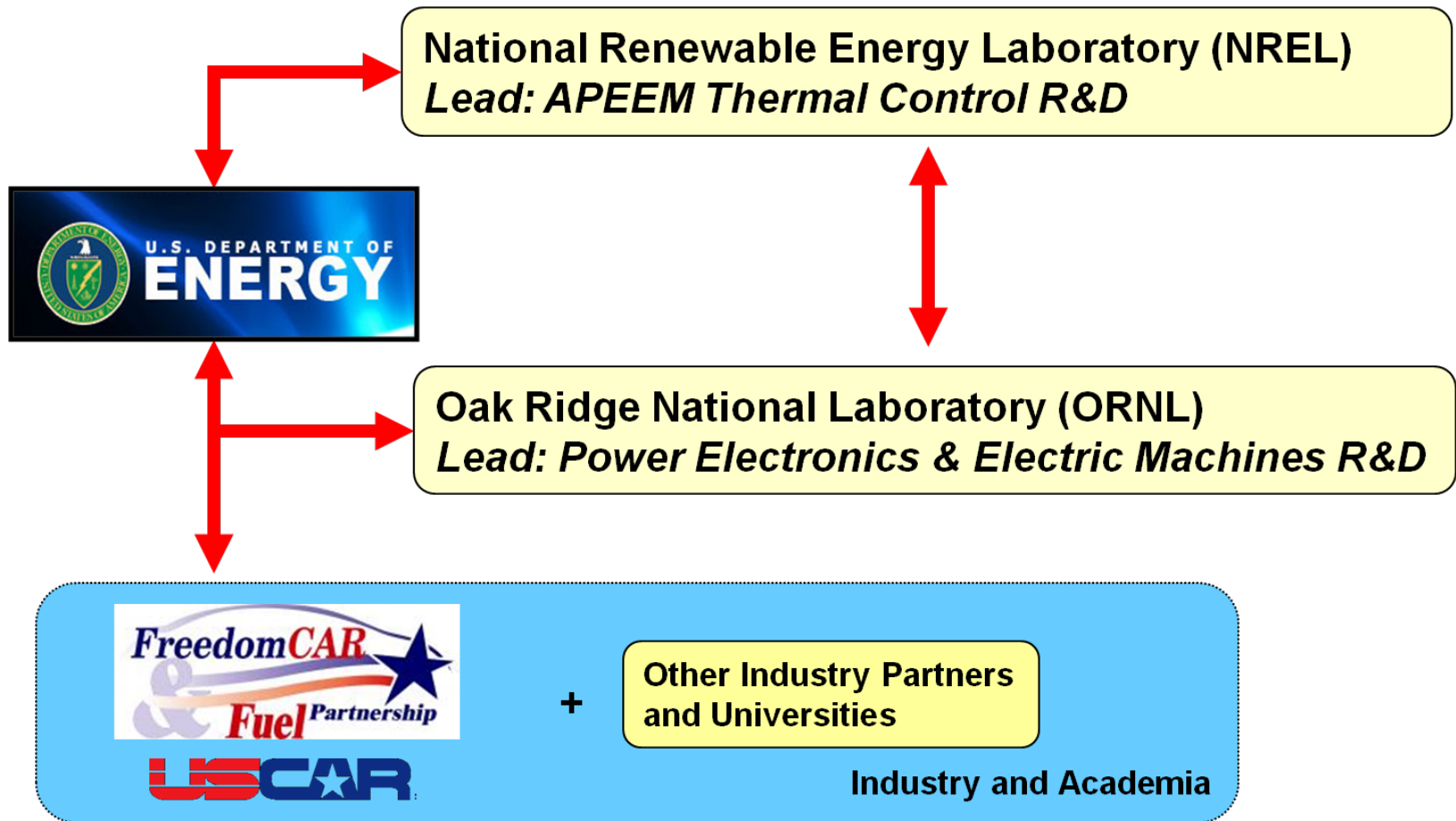
- Quantify trade-off interaction between packaging configuration and cooling technology.
- Identify effective packaging and cooling combinations.

## Approach

## Results

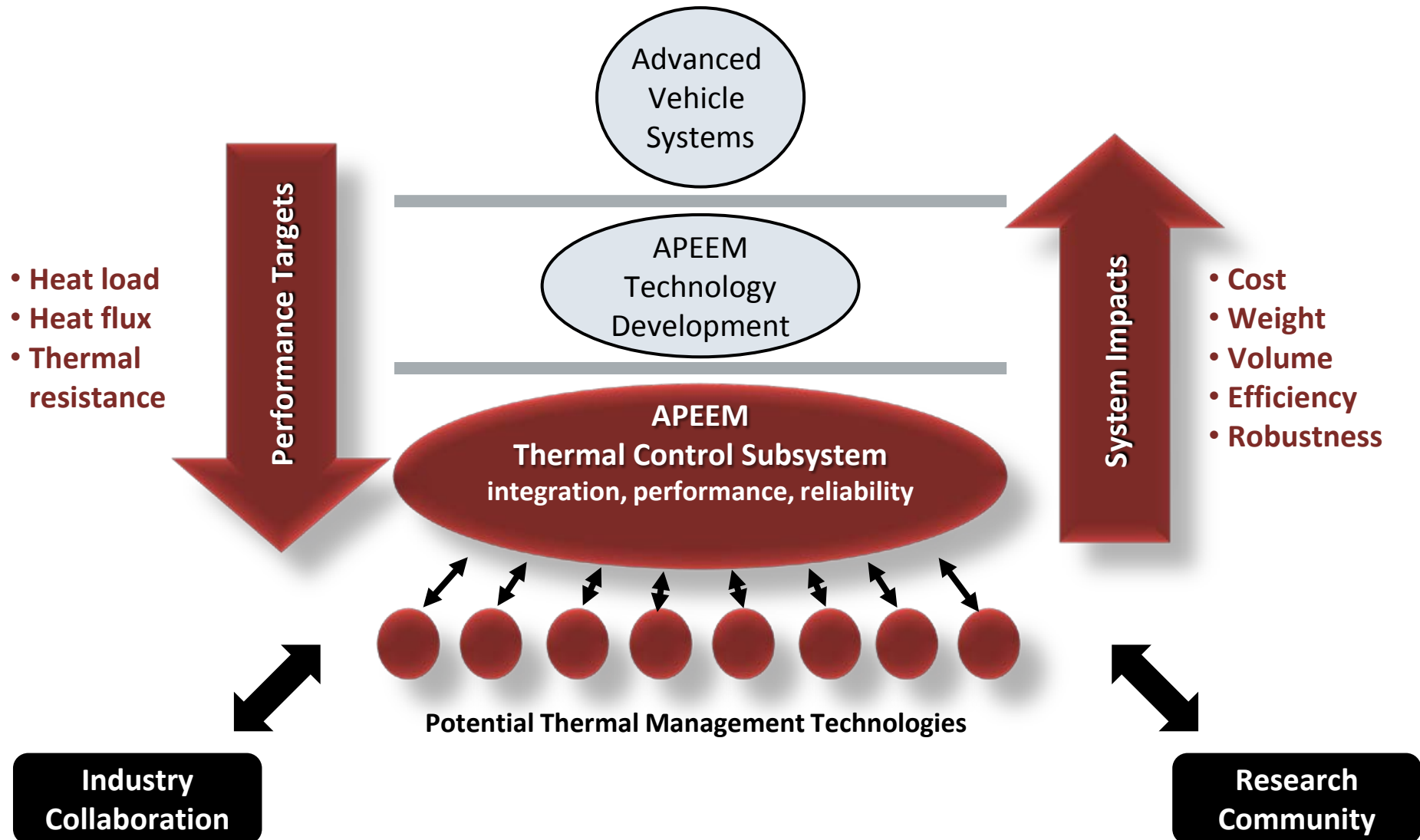
# Background

## DOE's Advanced Power Electronics and Electric Machines (APEEM)



# Background

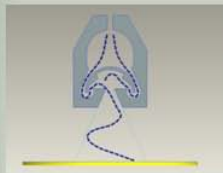
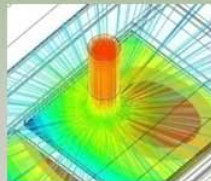
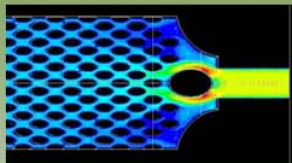
- NREL Advanced Power Electronics Thermal Overview



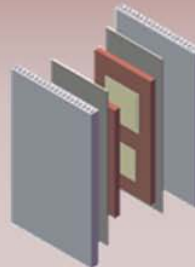
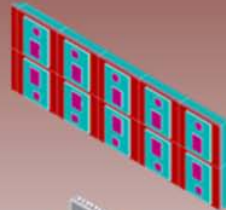
# Background

- NREL Advanced Power Electronics Thermal Focus Areas

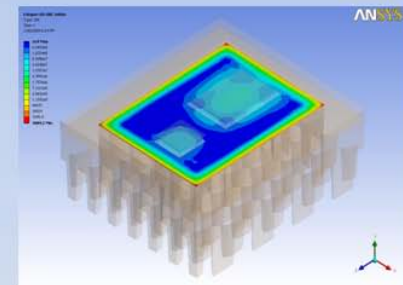
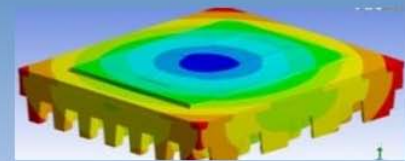
## Advanced Heat Transfer



## Thermal Systems Integration

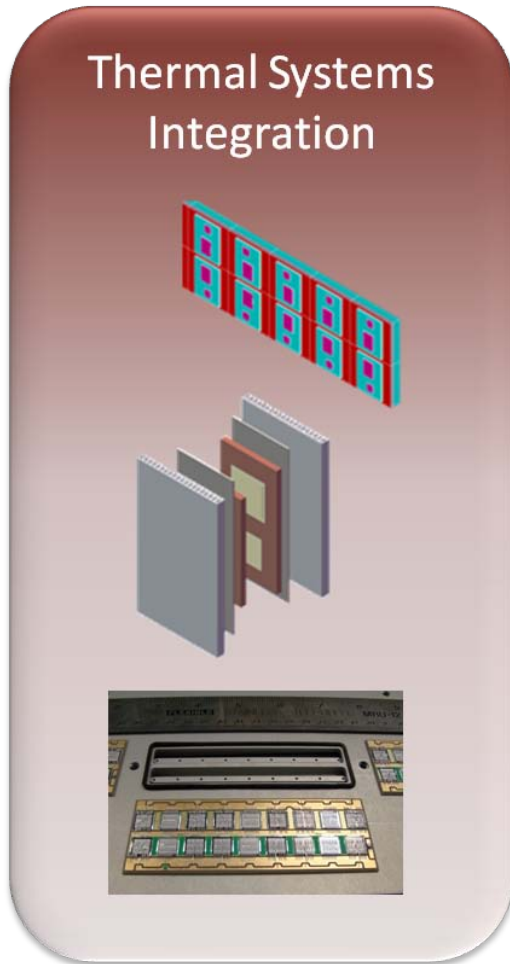


## Thermal Stress and Reliability

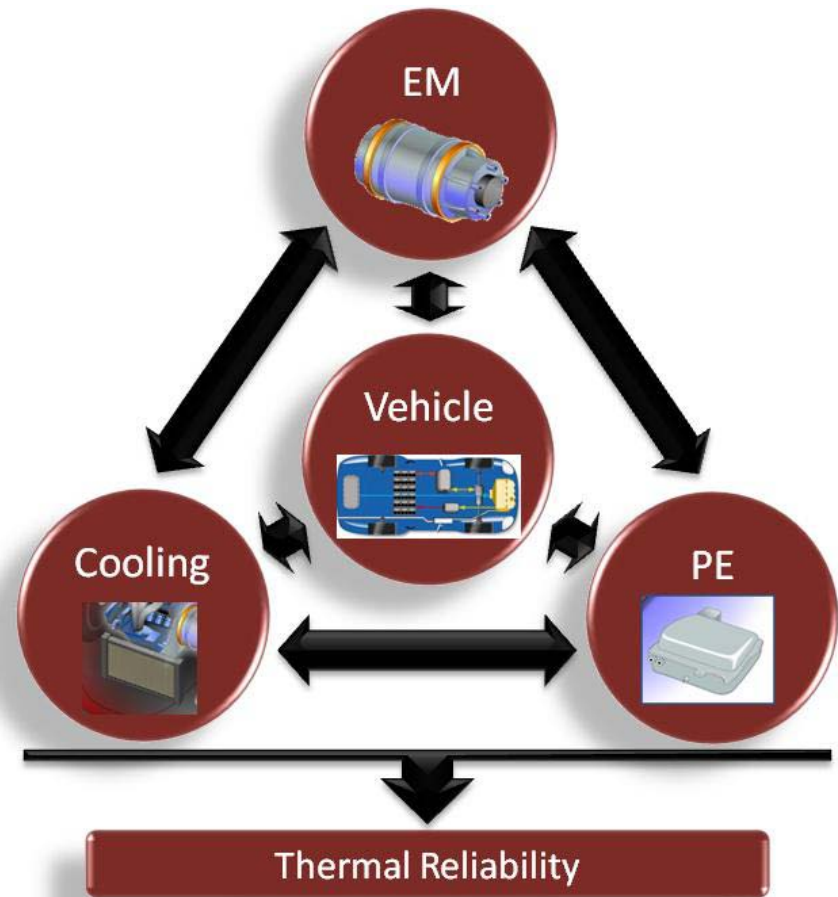




# Background



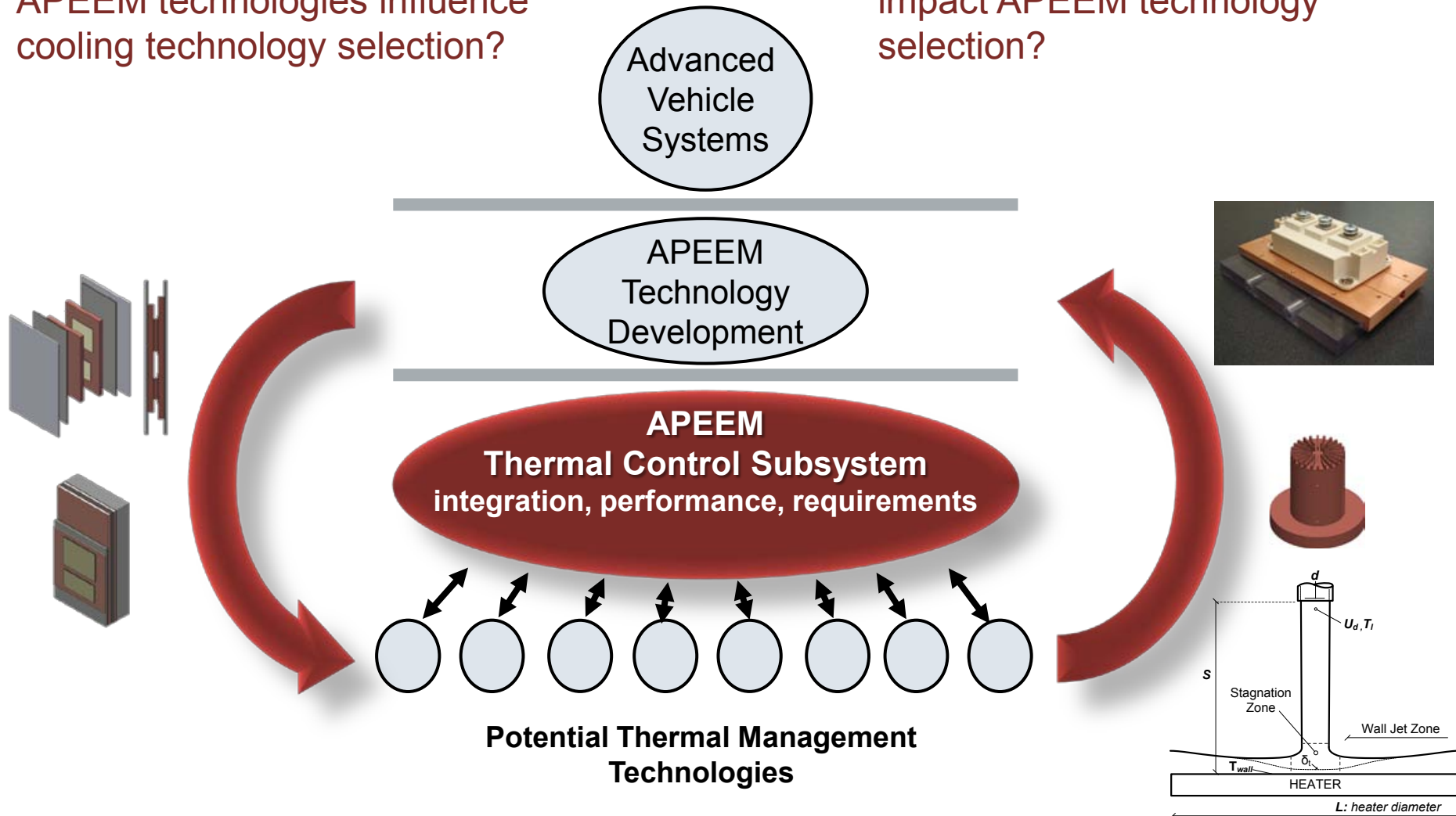
- Defines thermal requirements
- Links thermal technologies to electric traction drive systems



# Problem

How do developments in APEEM technologies influence cooling technology selection?

How do developments in cooling impact APEEM technology selection?



# Approach

Quantify interaction between package configuration and cooling technology on total thermal performance.

Heat Transfer & Fluid Flow Characterization

Cooling Technologies

Fins & Jets

1

Cooling Performance

Experimental Correlations, CFD Results, & Analytical

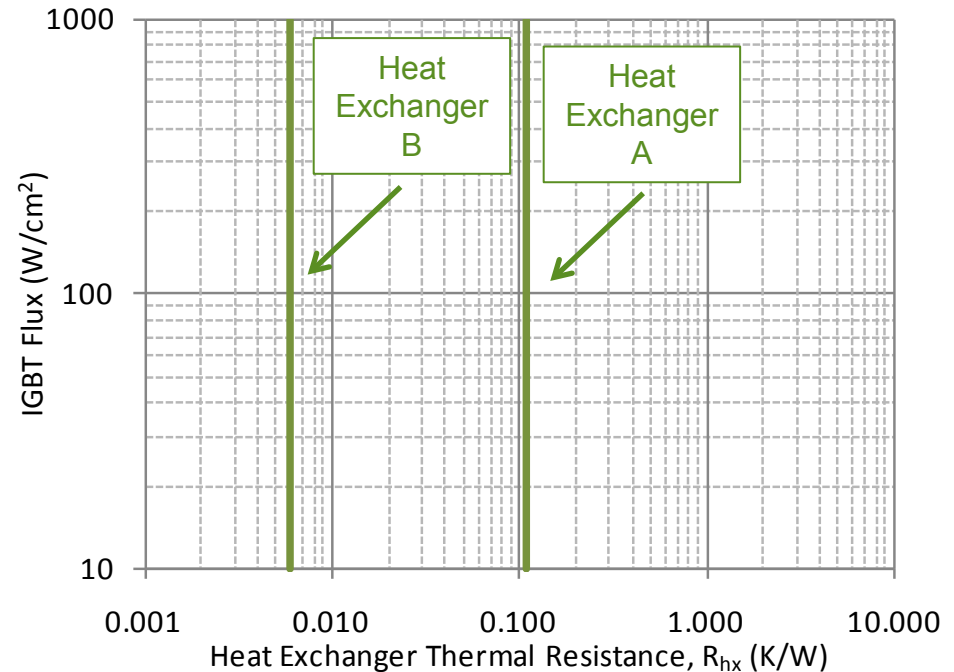
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Heat Exchanger Characterization

Effectiveness – NTU Method  
$$R_{NTU} = \frac{1}{\epsilon \dot{m} c_p}$$

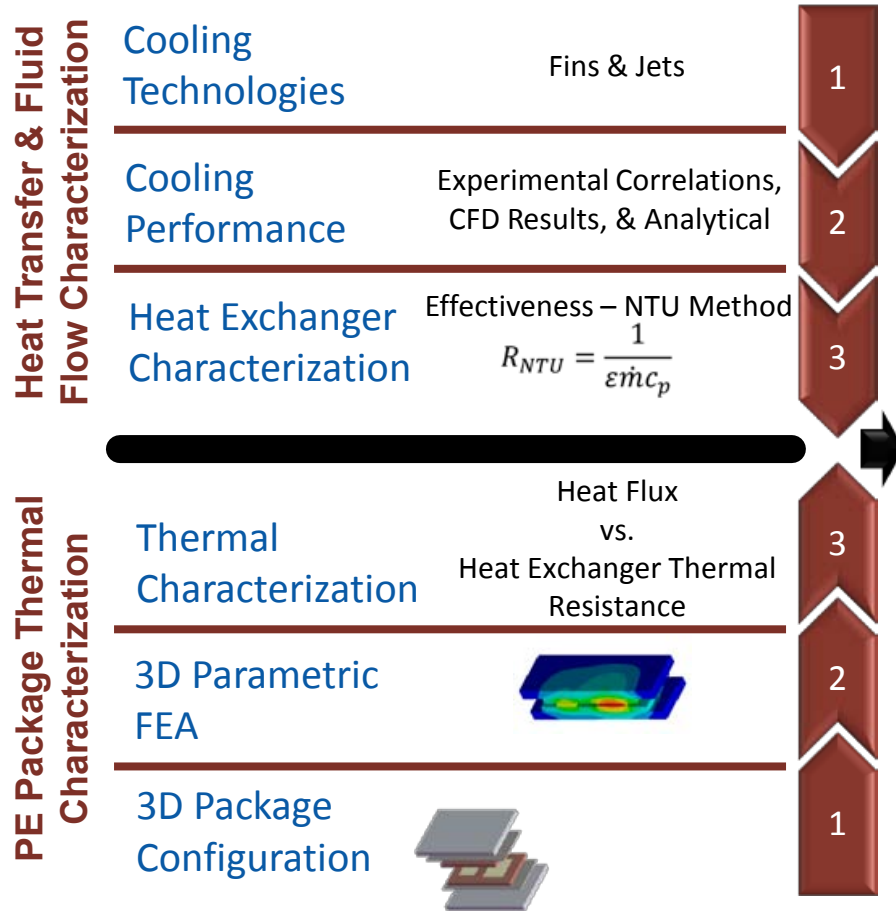
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## System Performance Trade-offs

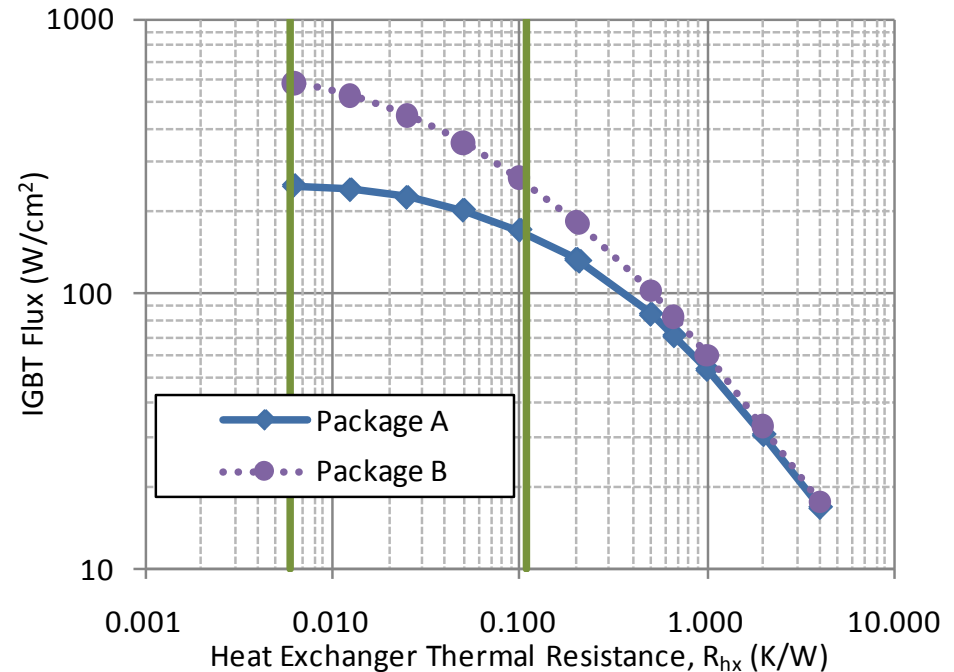


# Approach

Quantify interaction between package configuration and cooling technology on total thermal performance.

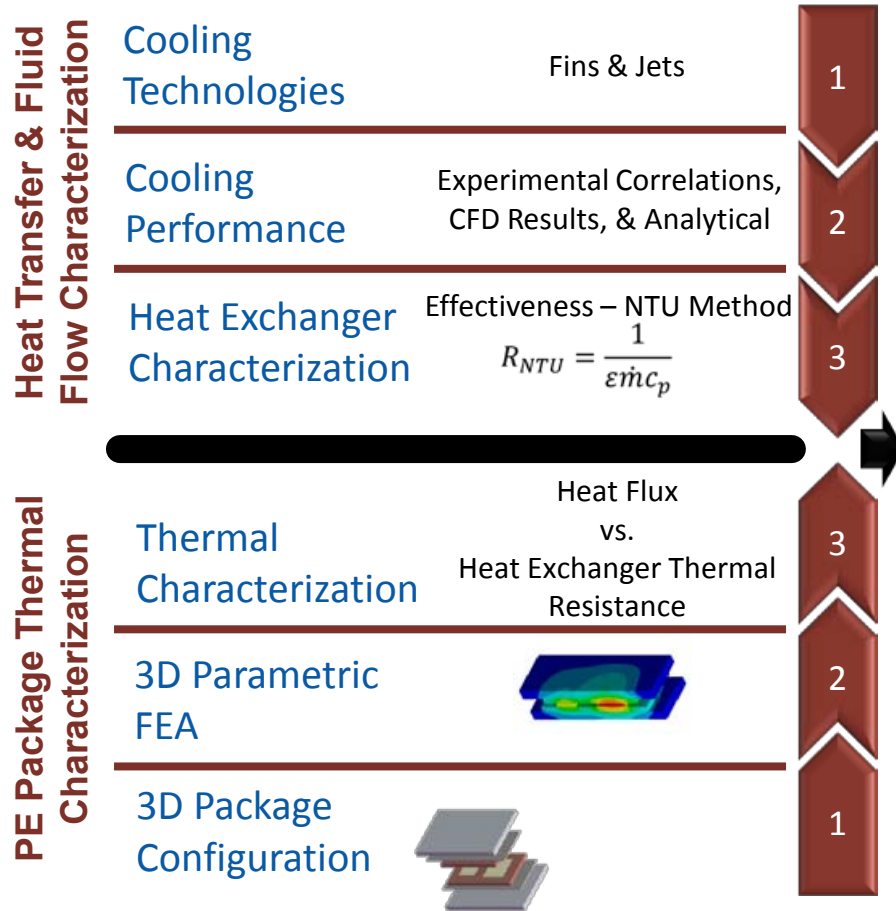


**System Performance Trade-offs**



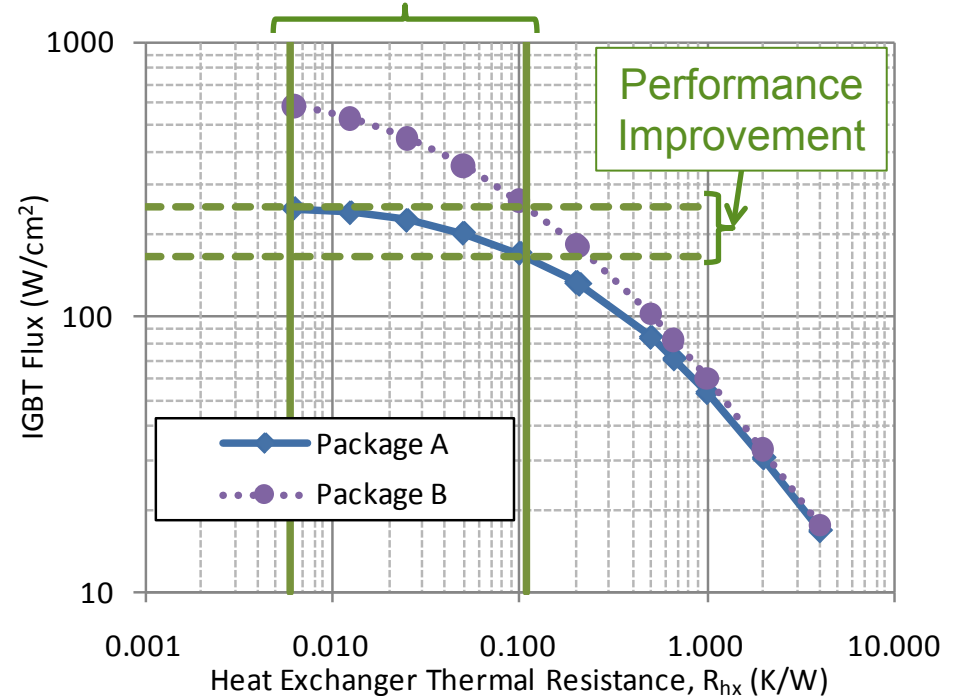
# Approach

Quantify interaction between package configuration and cooling technology on total thermal performance.



## System Performance Trade-offs

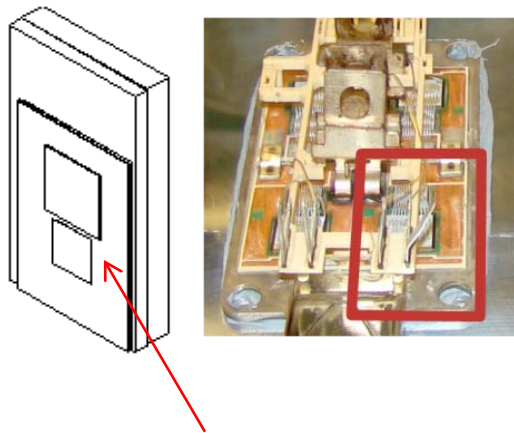
Required heat exchanger improvement for equivalent performance gain.



# Approach

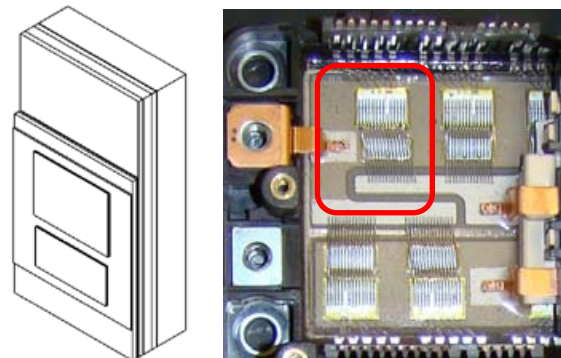
Applied process to range of package configuration examples approximated from in-use commercial packages with different geometries.

### Semikron SKM

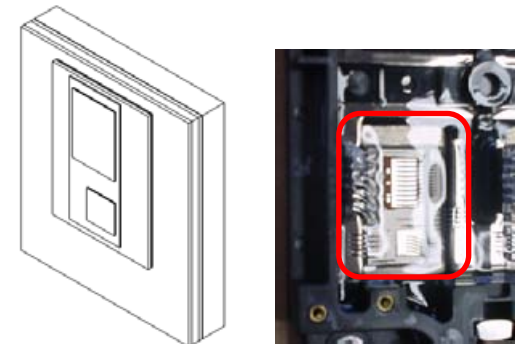


IGBT and diode pair

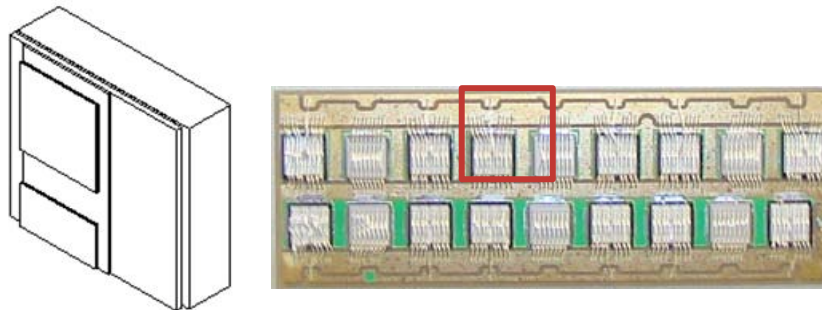
### Toyota Camry



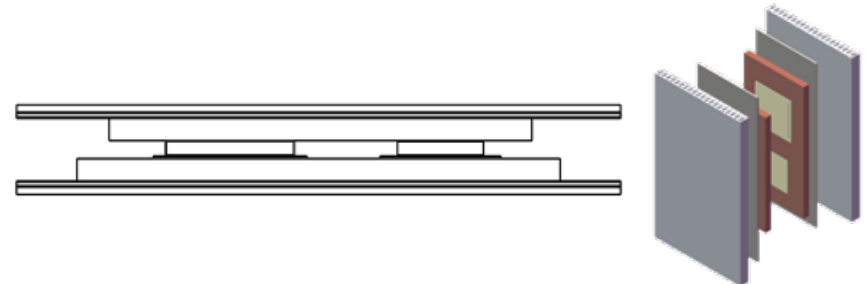
### Toyota Prius 2004



### Semikron SKAI



### Lexus LS 600h



# Approach

Layer		Baseline Package Configurations				Ls 600H
		SKM	SKAI	Prius	Camry	
IGBT/Diode (Si)		x	x	x	x	See referenced paper below
Solder		x	x	x	x	
Cu		x	x	x**	x**	
Substrate	AlN	NA*	x	x	x	
	Al <sub>2</sub> O <sub>3</sub>	x	NA	NA	NA	
Cu		x	x	x	x	
Solder		x	NA	x	x	
Heat Spreader	Cu	x	NA	NA	NA	
	Cu-Mo-Cu	NA	NA	x	x	
TIM		x	x <sup>+</sup>	x	x	
Heat Sink		x	x	x	x	
Cooled Surface Footprint Area: [cm <sup>2</sup> ]		15.34	3.90	16.86	7.68	15.00 <sup>++</sup>

\* Included additional model variation with AlN.

+ Modeled with reduced thermal interface material thickness of 0.05 mm.

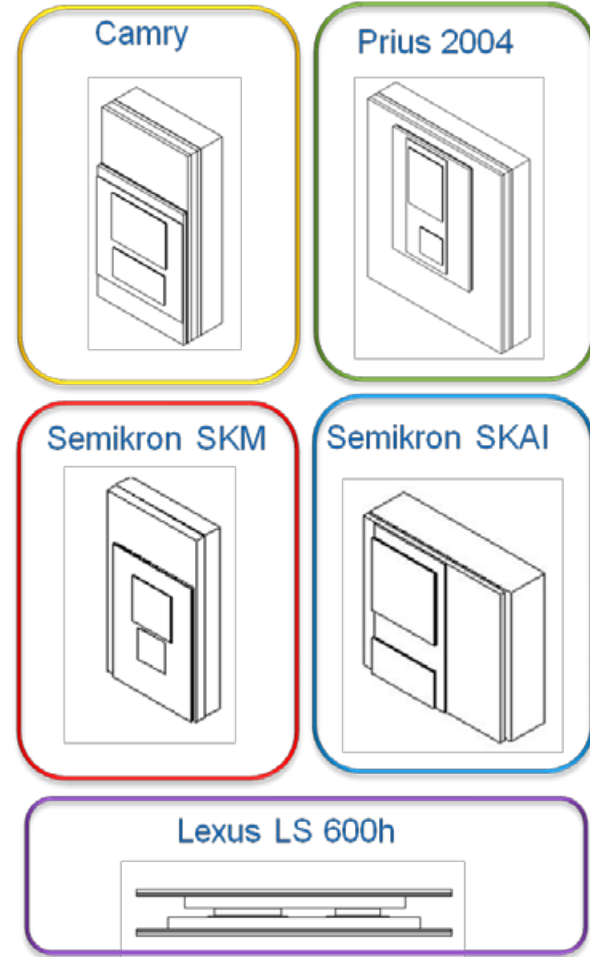
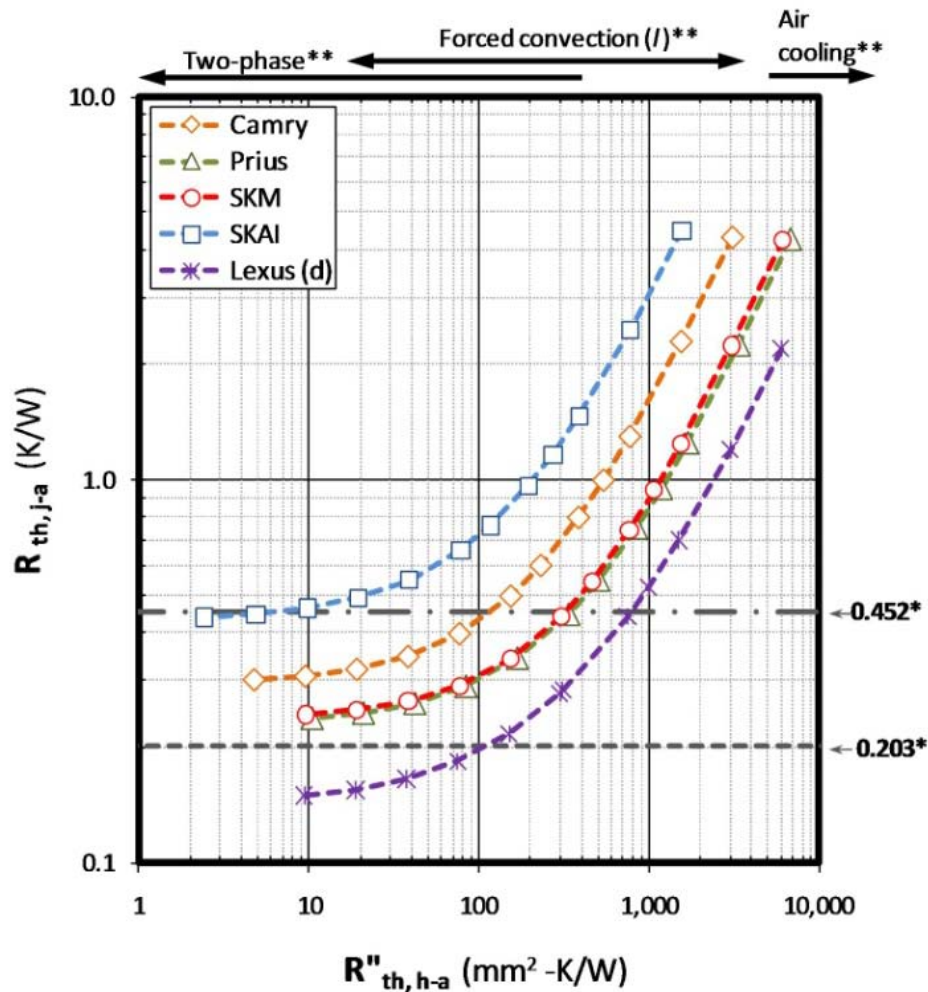
\*\* Assumed copper metallization layer.

++ Listed area is for one side of the package, and it is the same on each side of the package.

Reference:

K. Bennion and K. Kelly, "Rapid Modeling of Power Electronics Thermal Management Technologies," IEEE Vehicle Power and Propulsion Conference, Sept. 7-11, 2009.

# Results

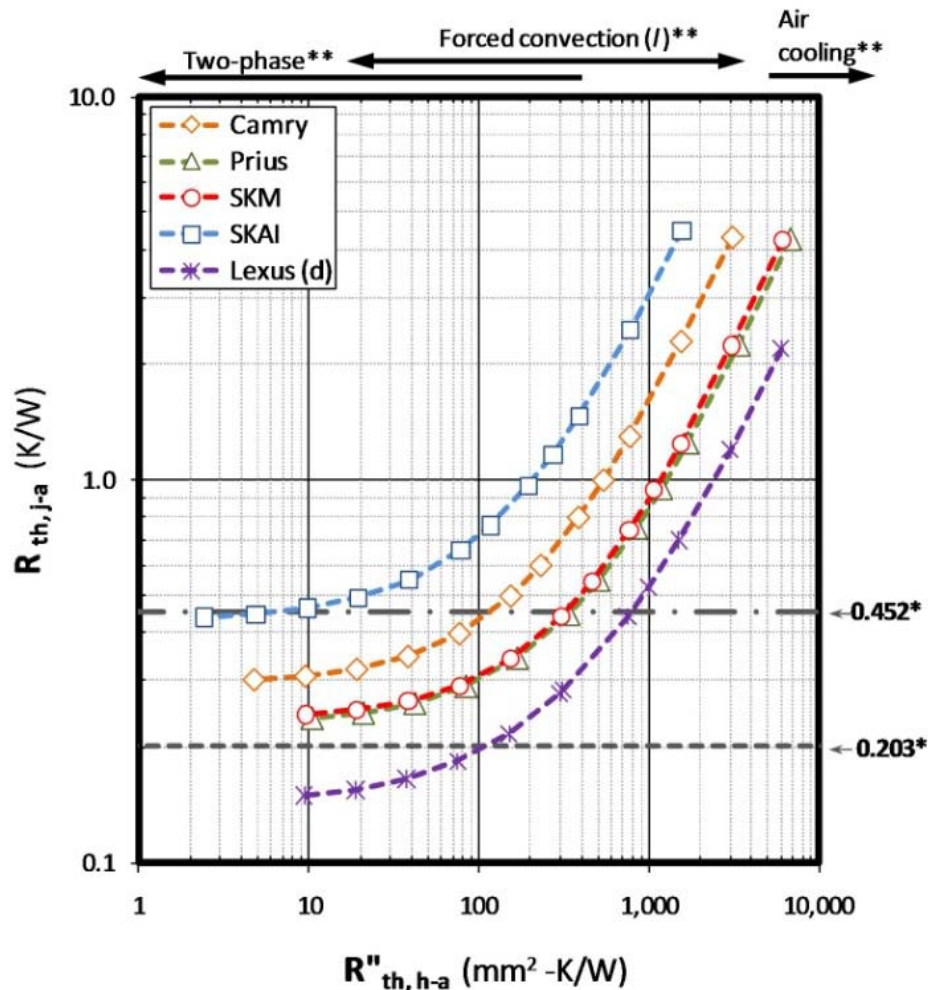


\* Sample single-sided and double-sided total thermal resistance. (Source: Y. Sakai, H. Ishiyama, and T. Kikuchi, "Power control unit for high power hybrid system," SAE 2007 World Congress, Detroit, MI, April 16-19, 2007, SAE Paper 2007-01-0271.)

\*\* Sample cooling performance. (Source: I. Mudawar, "Assessment of high-heat-flux thermal management schemes," IEEE Transactions on Components and Packaging Technologies, vol. 24, no. 2, pp. 122-141, June 2001.)



# Results

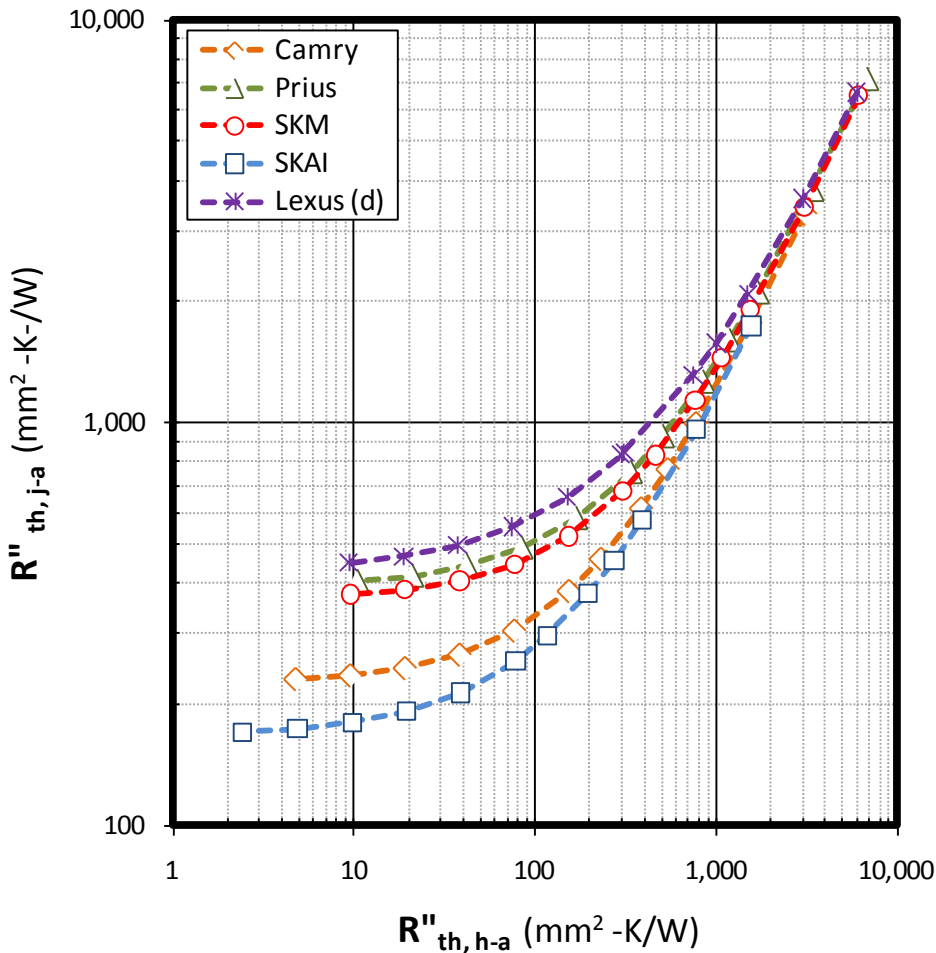


- All curves flatten as the heat exchanger performance improves ( $R''_{h,h-a}$  decreases).
- Package becomes thermal limitation.
- Difference in total thermal performance ( $R''_{th,j-a}$ ) is affected by the footprint area available for cooling.
- Method for comparing alternative heat exchanger technologies and package configurations.

\* Sample single-sided and double-sided total thermal resistance. (Source: Y. Sakai, H. Ishiyama, and T. Kikuchi, "Power control unit for high power hybrid system," SAE 2007 World Congress, Detroit, MI, April 16-19, 2007, SAE Paper 2007-01-0271.)

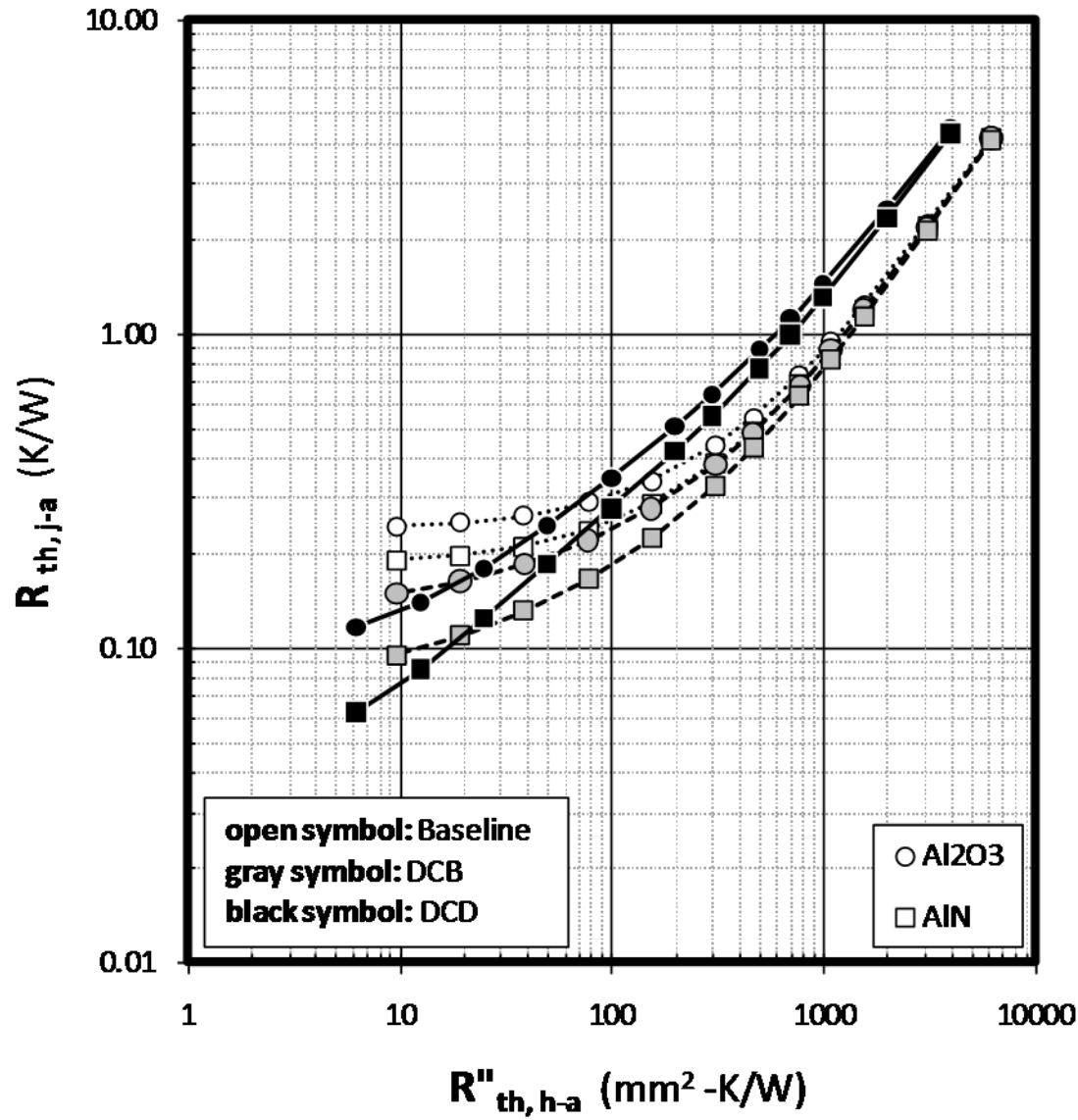
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# Results

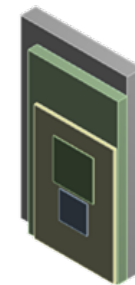
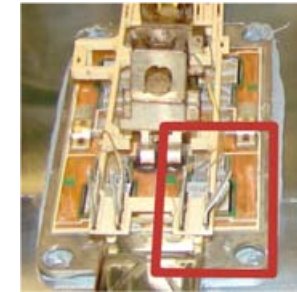


- Weight the total thermal performance ( $R''_{th,j-a}$ ) by the total footprint area available for cooling.
- Curves collapse onto a single curve as the heat exchanger resistance increases.
- Removes effect of different package footprint areas.

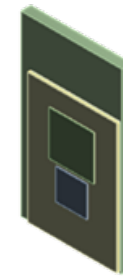
# Results



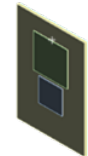
Package geometry, material, and cooling trade-offs



Baseline

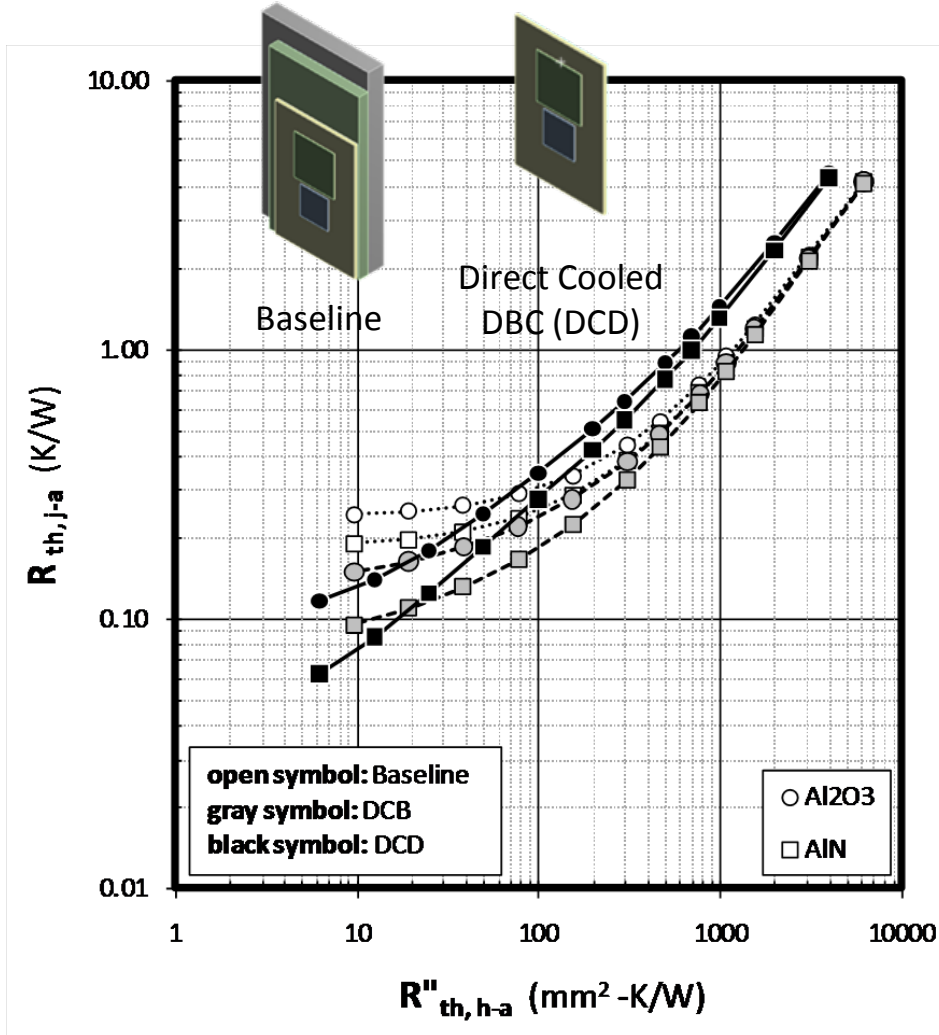


Direct Cooled Baseplate (DCB)



Direct Cooled DBC (DCD)

# Results



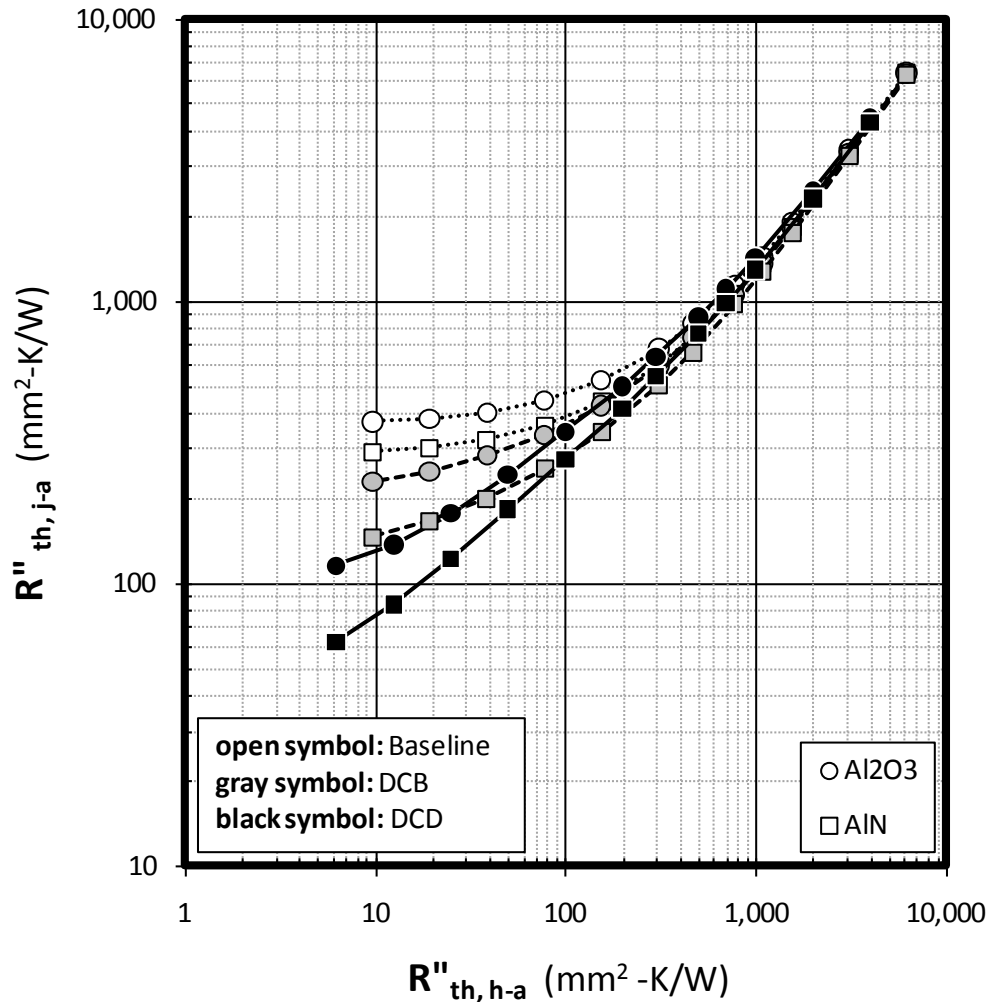
## Baseline

- At low  $R_{th,h-a}$ , the separation between Al<sub>2</sub>O<sub>3</sub> and AlN package resistance is more significant.
- Trade-off between material cost and heat exchanger performance cost.
- At about 100  $mm^2-K/W$ , switching to AlN would have a similar benefit to a 10X heat exchanger improvement.

## Direct Cooled DBC (DCD)

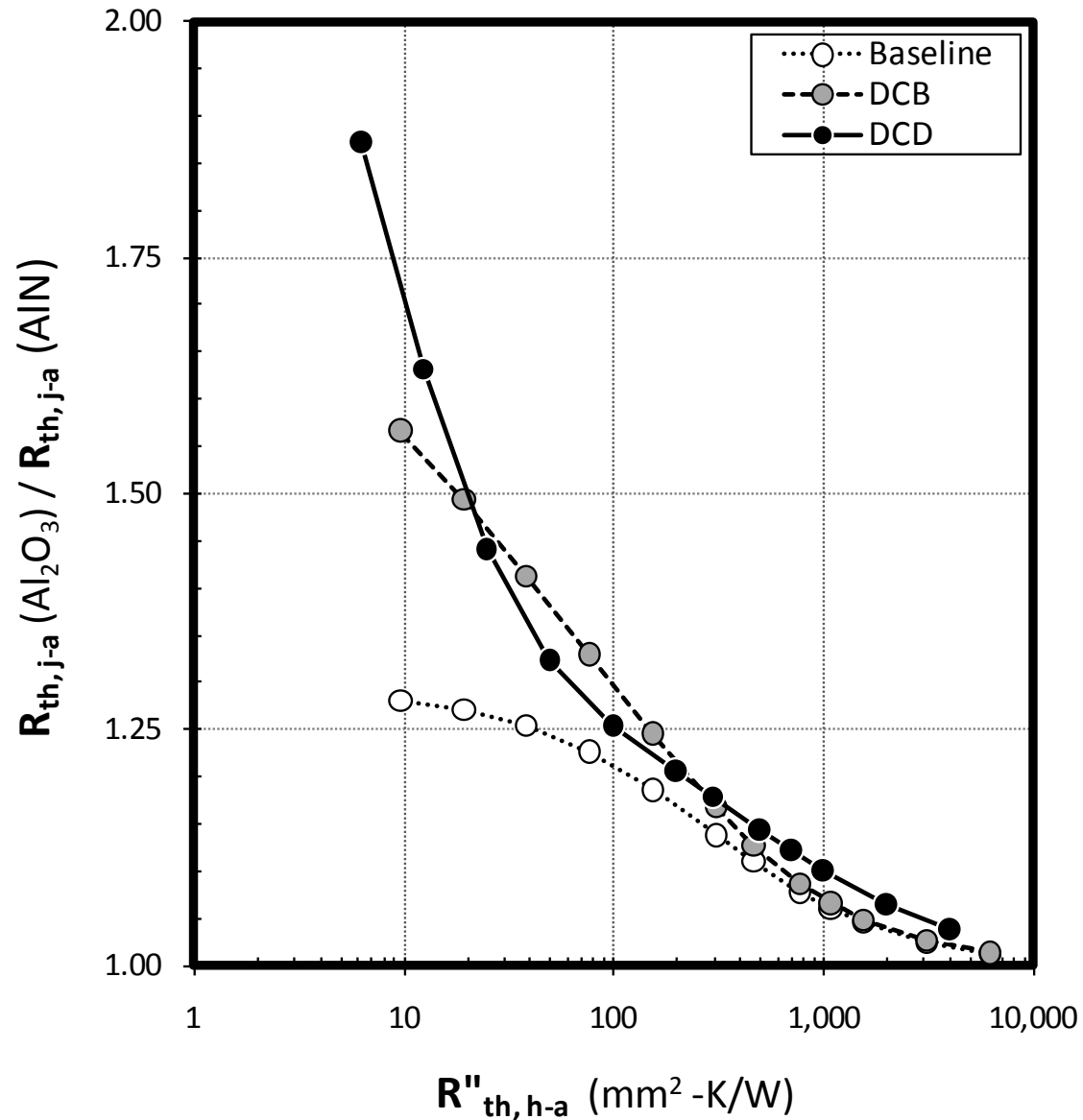
- At high  $R_{th,h-a}$ , the cooling area footprint and heat exchanger resistance dominate thermal performance.
- As the cooling technology improves, the thermal characteristics of the package become more important.

# Results

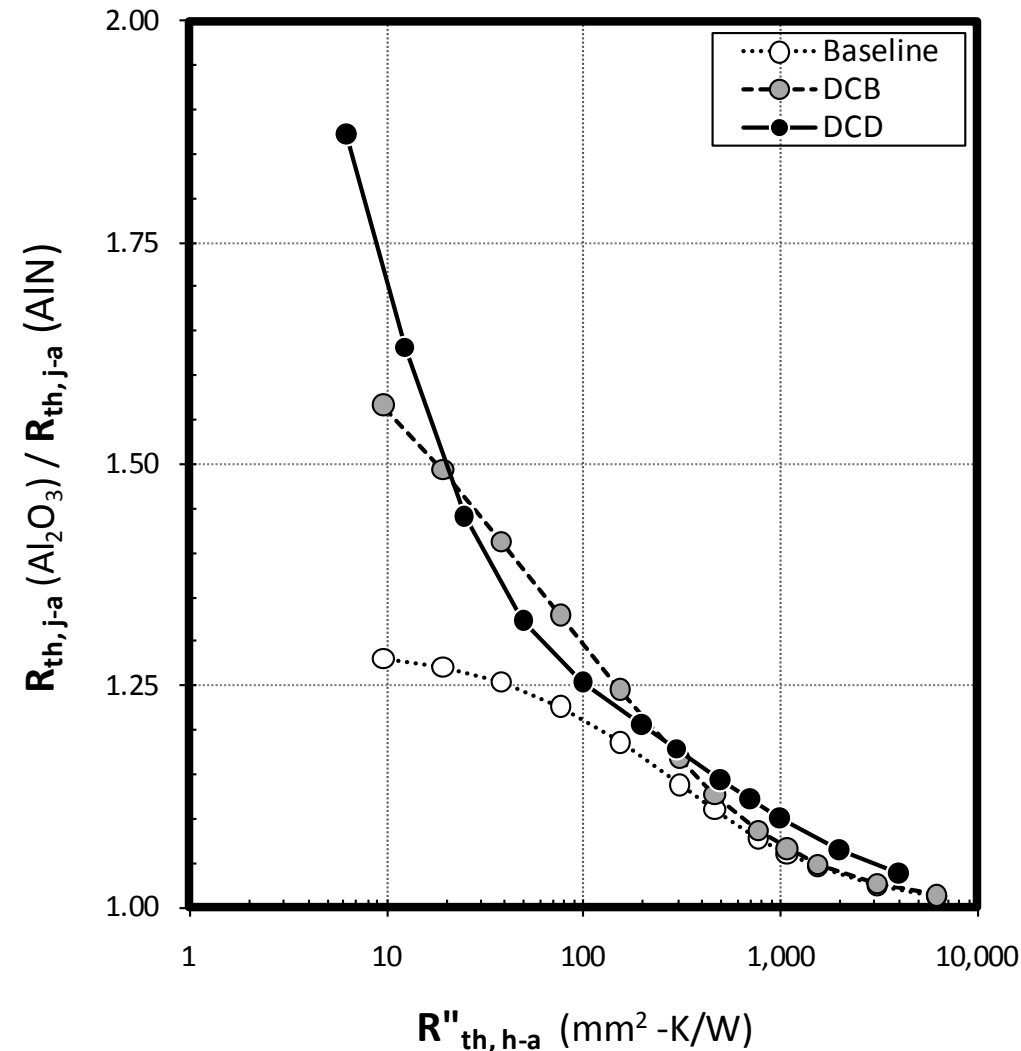


- Weight the total thermal performance ( $R''_{th,j-a}$ ) by the total footprint area available for cooling.
- Curves collapse onto a single curve as the heat exchanger resistance increases.
- Removes effect of different package footprint areas.
- Highlights impact of package.

# Results

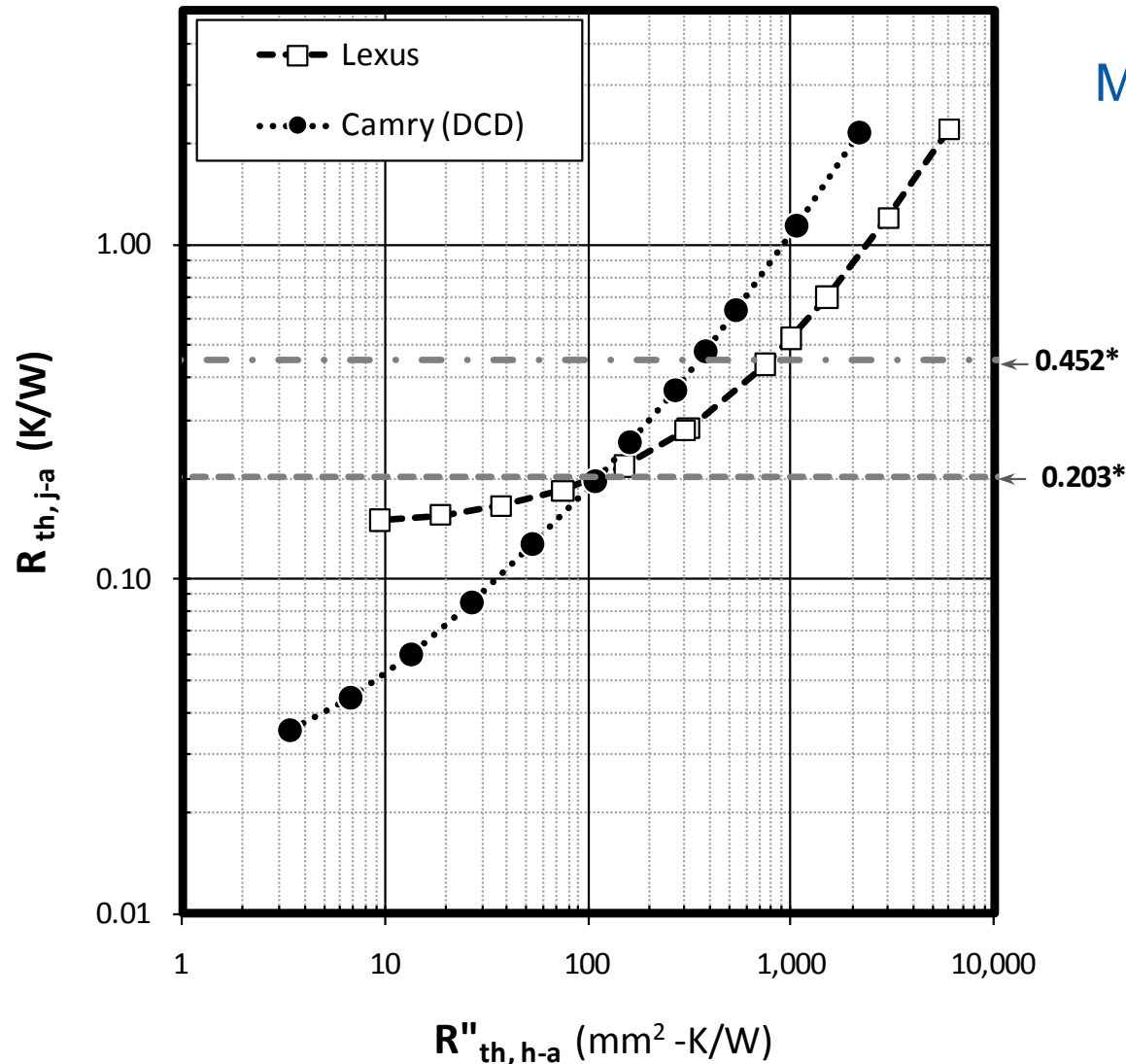


# Results



- The impact of a material with improved thermal conductivity depends on the package configuration and heat exchanger performance.
- The cost/benefit trade-off improves for more aggressive cooling and packages with fewer thermal bottlenecks.
- Relationship between package thermal performance and cooling technology can lead to a more expensive system than necessary if the relationship is not used properly.

# Results

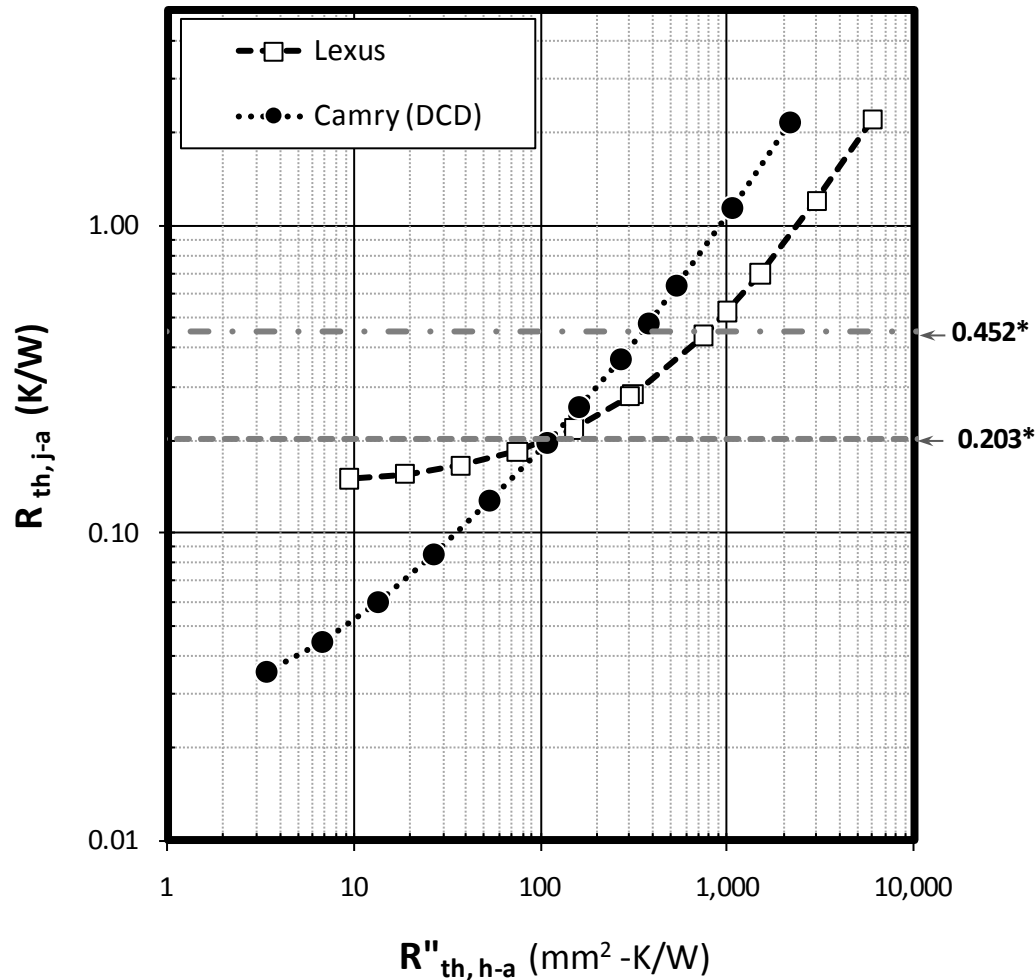


Matching package geometry  
and cooling technology

\* Sample single-sided and double-sided total thermal resistance. (Source: Y. Sakai, H. Ishiyama, and T. Kikuchi, "Power control unit for high power hybrid system," SAE 2007 World Congress, Detroit, MI, April 16-19, 2007, SAE Paper 2007-01-0271.)



# Results



## Matching package geometry and cooling technology

- To maximize the thermal performance, the package and heat exchanger technology should be investigated together.
- Identify appropriate cooling methods for a given package technology.
- Identify appropriate packaging options for a given cooling approach.

\* Sample single-sided and double-sided total thermal resistance. (Source: Y. Sakai, H. Ishiyama, and T. Kikuchi, "Power control unit for high power hybrid system," SAE 2007 World Congress, Detroit, MI, April 16-19, 2007, SAE Paper 2007-01-0271.)

# Conclusion

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- Thermal management plays an important part in the cost of electric drives in terms of power electronics packaging.
- Cost-effective solutions require an appropriate balance between package and thermal management design.
- Appropriate cooling technology depends on
  - Package application
  - Reliability
- **Integration** of capabilities for **cooling, packaging** (materials/geometry), and **reliability** prediction provide a system view of technology developments.