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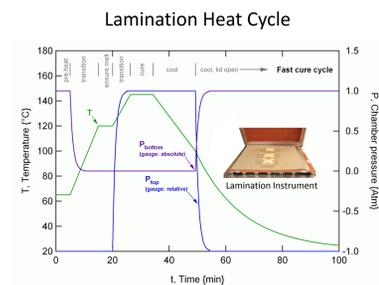
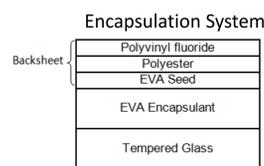
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## Objectives

- Develop a quantitative technique to measure adhesion and debond kinetics in EVA Encapsulants and TPE backsheets.
- Characterize the effect of ageing treatment duration, as well as the effects of environmental temperature and relative humidity on backsheet and encapsulant debond energy.
- Investigate the effect of mechanical stress, moisture and temperature on debond growth rate.
- Develop a predictive model of the effect of mechanical stress, moisture and temperature on debond growth rate.

## Encapsulation Specimen Preparation

A Polyvinyl fluoride-polyester backsheet with EVA seed was laminated to a layer of EVA encapsulation and a glass substrate.



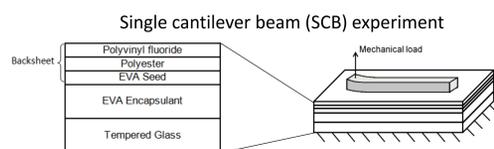
Lamination was performed at 145°C for 8 minutes at 1 atmosphere pressure.

The glass was cleaned prior to lamination, including: buffing with pumice powder; washing and rinsing.

The specimen components were fixed during lamination to improve their thickness uniformity.

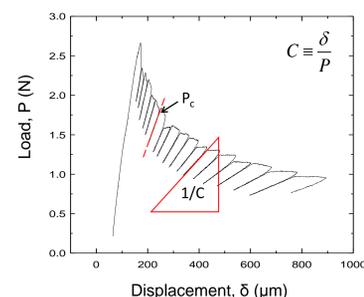
## Debond Energy and Debond Growth Experiment

A single cantilever beam (SCB) testing metrology, based on the well-known double cantilever beam method, was developed.



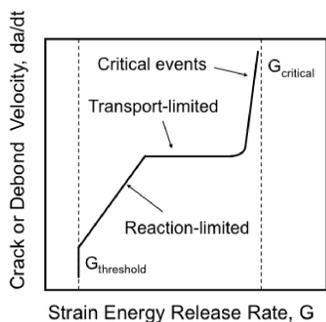
• A PMMA (or Ti) beam was bonded to the backsheet and a loading tab was bonded to one end of the beam. An incision was made through the backsheet and underlying encapsulant

• The glass substrate was rigidly fixed to a testing table and the loading tab was connected to a linear actuator in series with a load cell.



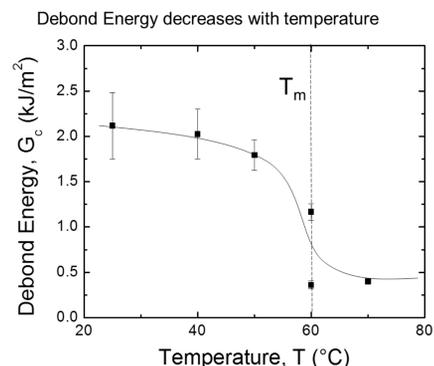
• Load and displacement were measured during the experiment. The debond energy,  $G_c$  was calculated using crack length ( $a$ ), critical load ( $P_c$ ), thickness of the beam  $h$ , width  $B$  and plane strain elastic modulus  $E'$ :

$$C = \frac{4a^3}{E' Bh^3} \quad G_c = \frac{P_c^2}{2B} \frac{\partial C}{\partial a} \bigg|_{a_c}$$

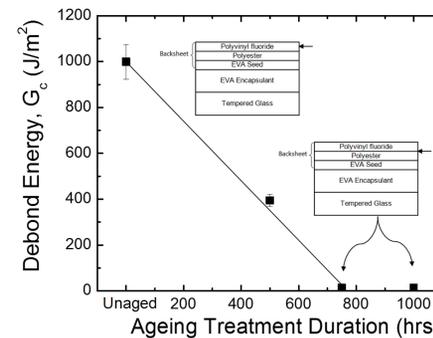


- To measure debond growth, the SCB specimens were loaded below  $G_c$ . The displacement was fixed and the load relaxation inherent to debond growth was recorded.
- Analysis of the load relaxation and increasing compliance determined the debond growth rates.
- The experiments were performed at selected values of temperature and relative humidity.

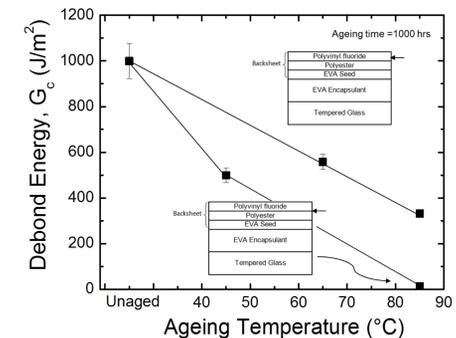
## Debond Energy of EVA Encapsulants and TPE Backsheets



- The debond energy of the EVA-glass structure decreased with testing temperature.
- The debond energy decreased precipitously at  $T \sim 60^\circ\text{C}$ , which corresponds to one of the transition temperatures of the polymer.



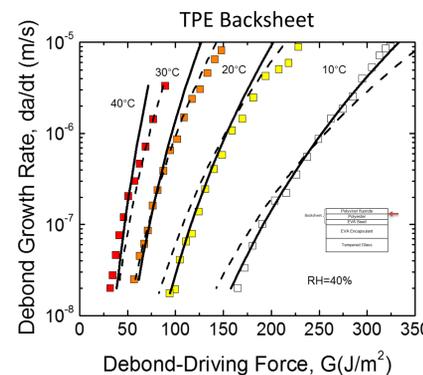
- The debond energy of the backsheets decreased linearly with ageing duration for 800hrs to very low values ( $\sim 28 \text{ J/m}^2$ ).
- Failure occurred at the PVF-PET interface



- Higher ageing temperature and relative humidity corresponded to lower debond energies.
- High values of debond energy corresponded to partially cohesive failure in the PVF.

## Debonding Kinetics of EVA Encapsulants and TPE Backsheets in Controlled Environments

### Temperature Effect on Debond Growth Rate

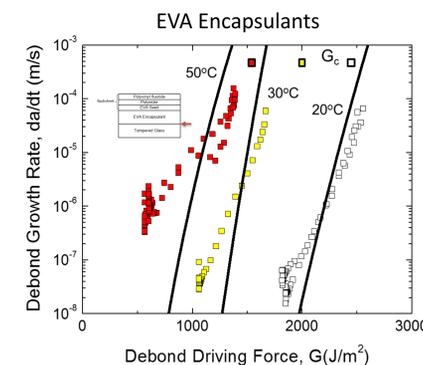
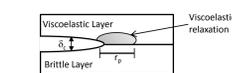


$$\frac{da}{dt} = \frac{\pi}{8} \frac{\delta_c}{\epsilon_y (\delta_c \epsilon_y)^{1/2}} \left( \frac{G}{E_0(RH)} \right)^{1/2} c^{-1} \frac{e^{-\frac{E_a}{R(T-T_0)}}}{1 - e^{-\frac{E_a}{R(T-T_0)}}}$$

Arrhenius

$$\frac{da}{dt} = \frac{\pi}{8} \frac{\delta_c}{\epsilon_y (\delta_c \epsilon_y)^{1/2}} \left( \frac{G}{E_0(RH)} \right)^{1/2} \frac{c_0 (T - T_0)}{10^{c_0 (T - T_0)}}$$

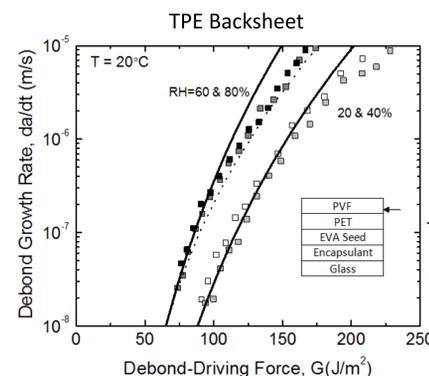
Williams-Landel-Ferry (1955)



The debond growth curves were shifted to lower values of  $G$  at higher temperatures.

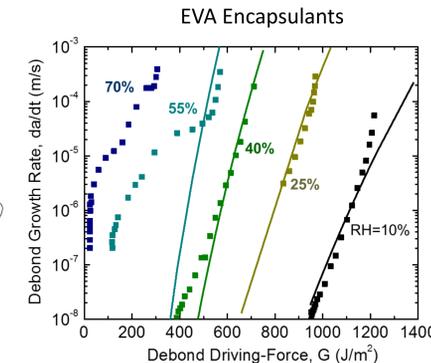
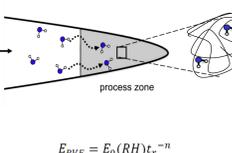
Lines are model predictions using the Arrhenius and the Williams-Landel-Ferry equation.

### Moisture Effect on Debond Growth Rate



Moisture-controlled viscoelastic debonding

$$\frac{da}{dt} = \frac{\pi}{8} \frac{\delta_c}{\epsilon_y (\delta_c \epsilon_y)^{1/2}} \left( \frac{G}{E_0(RH)} \right)^{1/2} c^{-1} \frac{e^{-\frac{E_a}{R(T-T_0)}}}{1 - e^{-\frac{E_a}{R(T-T_0)}}}$$



The debond curves were shifted to lower values of  $G$  with increasing RH.

Lines are model predictions using the humidity dependence of the PVF modulus (backsheet), and the plasticizing effect of water (EVA encapsulants.)

## Conclusions

- The debond energy of a PV encapsulant and backsheet were measured after several ageing treatments. The debond energy decreased with ageing treatment duration, relative humidity and temperature.
- The effect of mechanical stress, temperature and relative humidity on encapsulant and backsheet debond growth was reported. The debond growth rate increased up to 500-fold with small changes of temperature ( $10^\circ\text{C}$ ) and relative humidity (20%).
- The effect of temperature on debond growth was modeled with the Arrhenius and the Williams-Landel-Ferry equation. The effect of moisture on the debond growth rate was modeled with the humidity dependence of the PVF modulus and the plasticizing effect of water on EVA.

## Acknowledgments

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