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PHIL Validation of Ultracapacitor Storage for Black Start Application*

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Idaho Falls Power is municipal utility with five ROR hydropower plants on upper Snake River

- Idaho Falls ld Falls New Sweden GoogleMyMaps
 - Plants all connected to city's distribution and sub-transmission system.
 - Under normal conditions, plants are operated for maximum efficiency. Balancing is performed by Rocky Mountain Power. 8.9 MVA Upper Plant (ROR, Horizontal Kaplan Bulb)

8.9 MVA City Plant (ROR, Horizontal Kaplan Bulb)

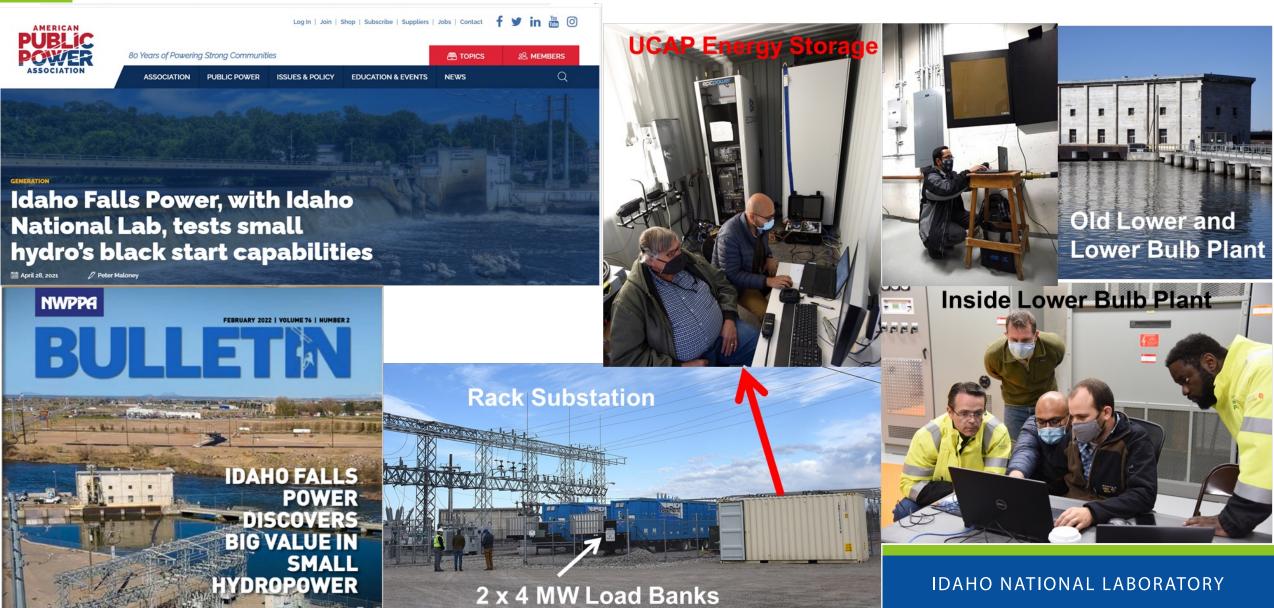
Blackstart Field Demonstration

8.9 MVA Lower Plant (ROR, Horizontal Kaplan Bulb) 2 x 1.8 MVA Old Lower Plant (ROR, Vertical Francis)

22.6 MVA Gem State Plant, (Vertical Kaplan)

Additional Info: https://www.ifpower.org/

Islanded Distribution Grid Black start: Successful Field Demonstration with Idaho Falls Power

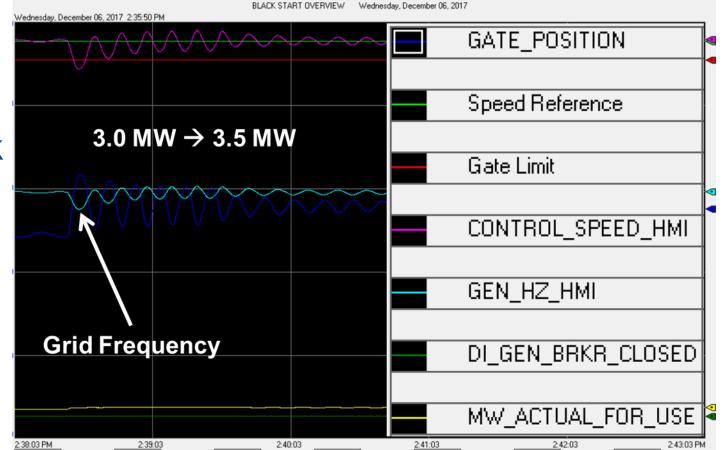


Islanded black start with ROR hydropower

From the December 2017 Field

Test

- Load stepping causes frequency stability issues
 - Potential trip off during black start
 - -Critical load carrying capability is limited
- Hydrogovernor and frequency protection settings need adjustment

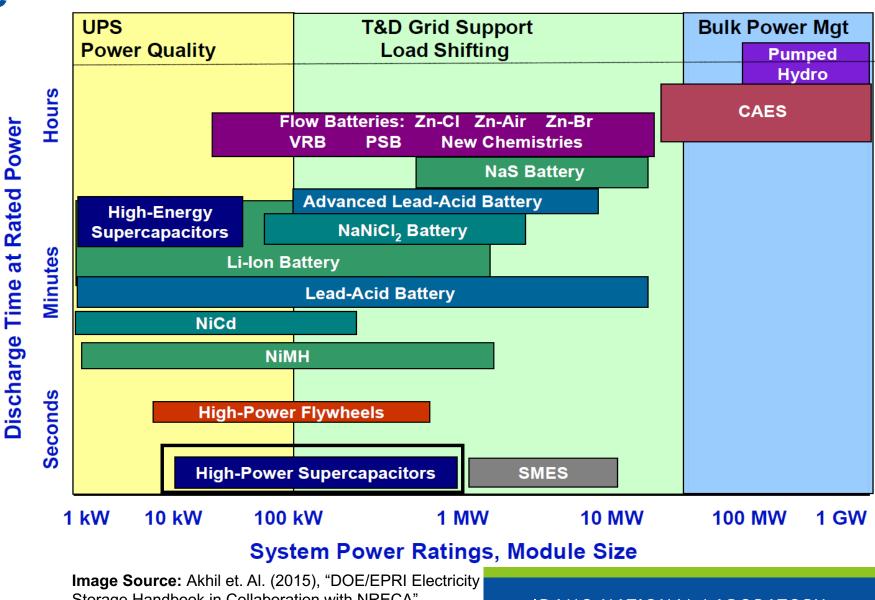


Can energy storage integration demonstrate improvement?

Energy Storage

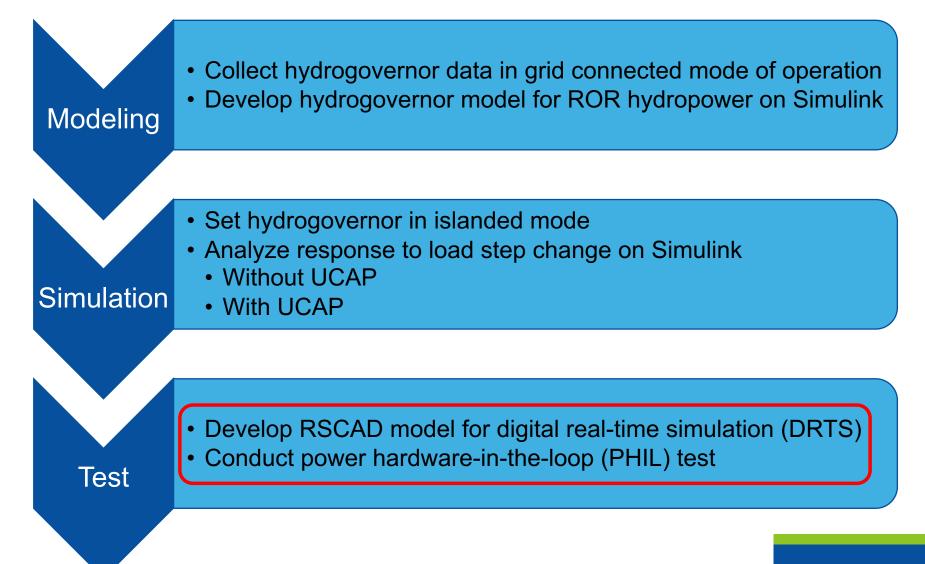
Ultracapacitor

 High power density
 Small form factor
 Enables mobility

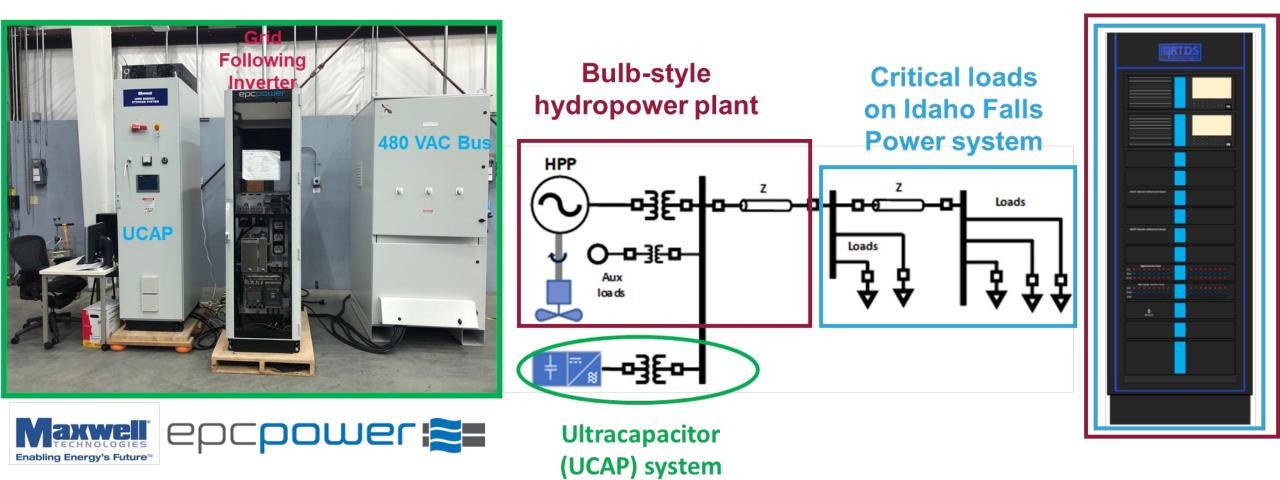


Storage Handbook in Collaboration with NRECA".

Steps to de-risk the field demonstration



RSCAD modeling for digital real-time simulation



AMETEK 540 kVA Grid Emulator

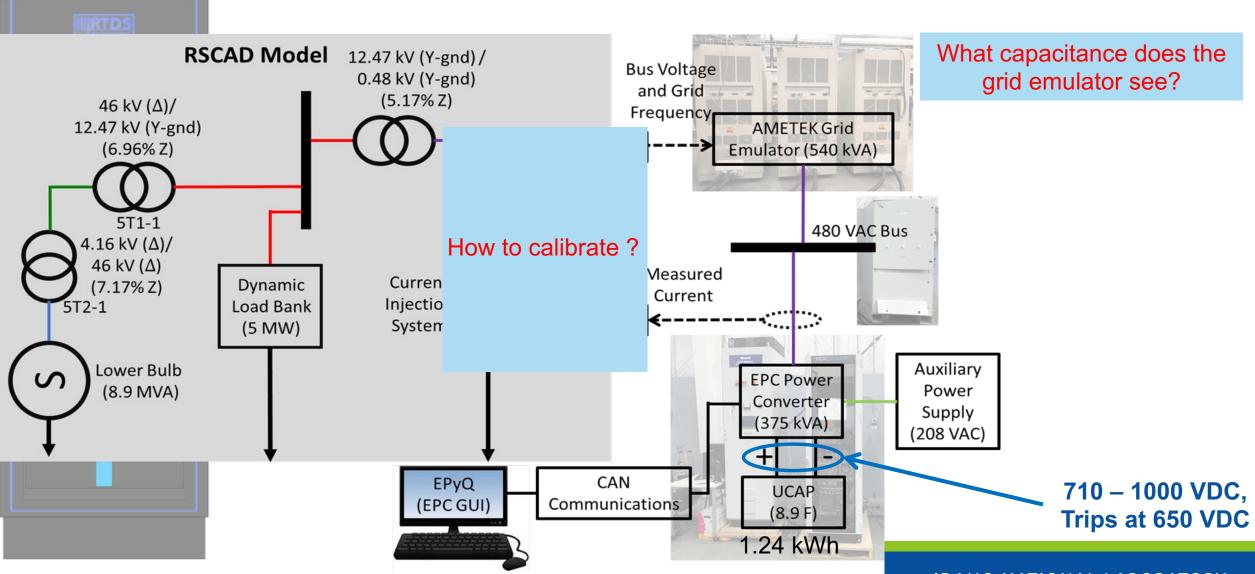




Tektronix Current Probing Assembly



"Closed-loop" Power Hardware In-the-Loop Testing

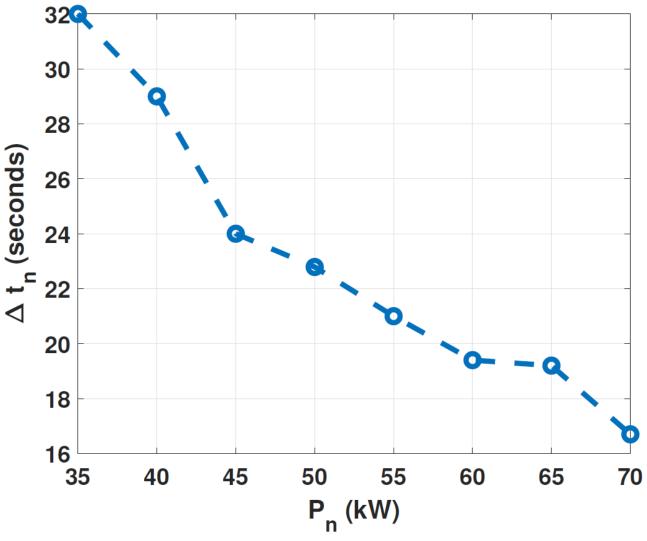


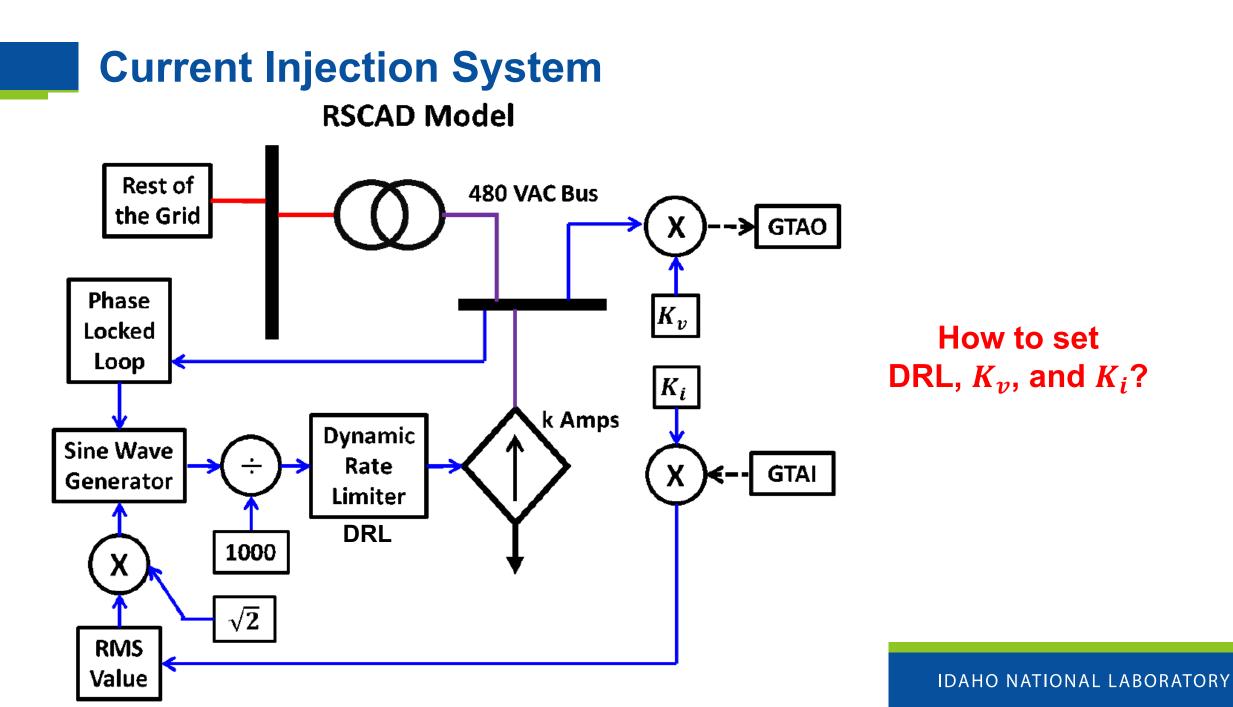
IDAHO NATIONAL LABORATORY

Ultracapacitor Characterization

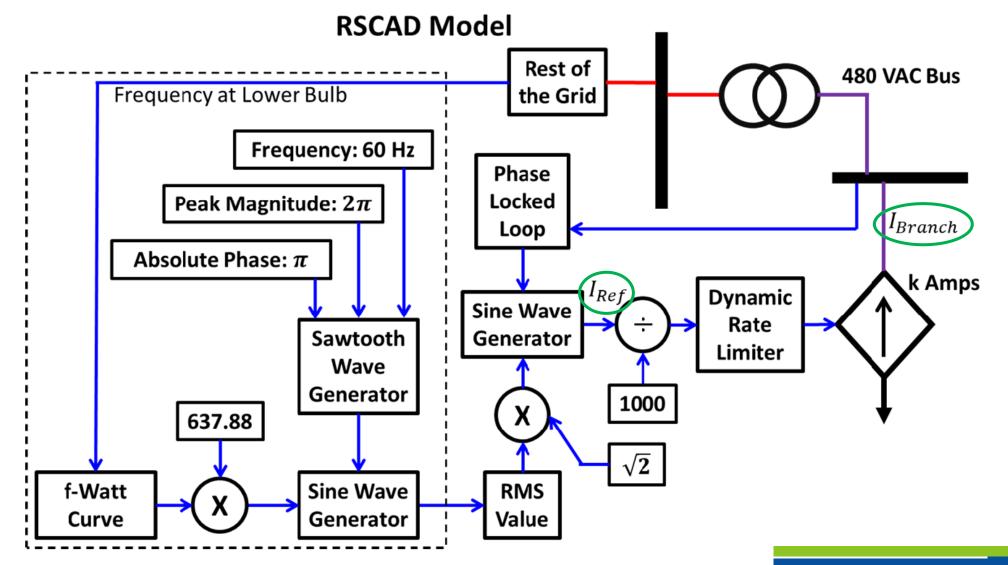
$$C_{480\text{VAC}} = \frac{2 \times 1000}{N_{\text{c}}(950^2 - 750^2)} \sum_{n=1}^{N_{\text{c}}} P_n[\text{kW}] \times \Delta t_n$$

• $C_{480VAC} = 6.7 F$

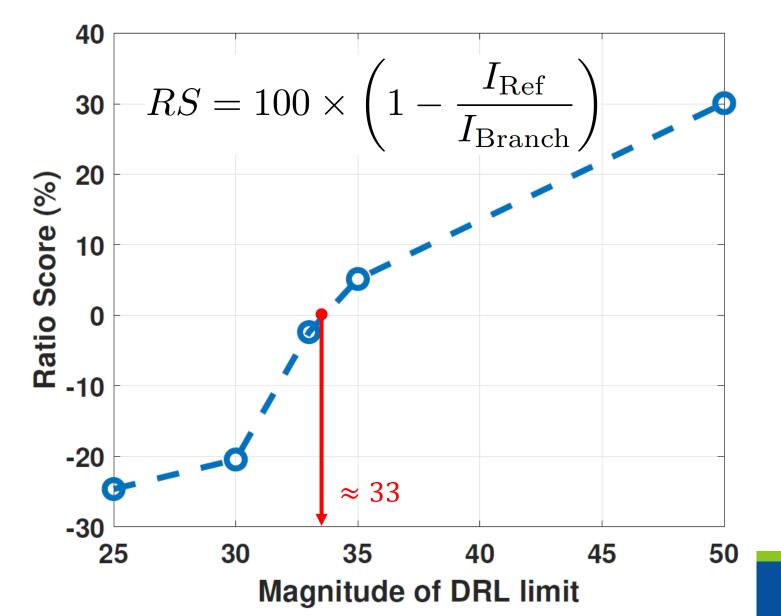




Analyze DRL Sensitivity through f-Watt Responsive Current Synthesis





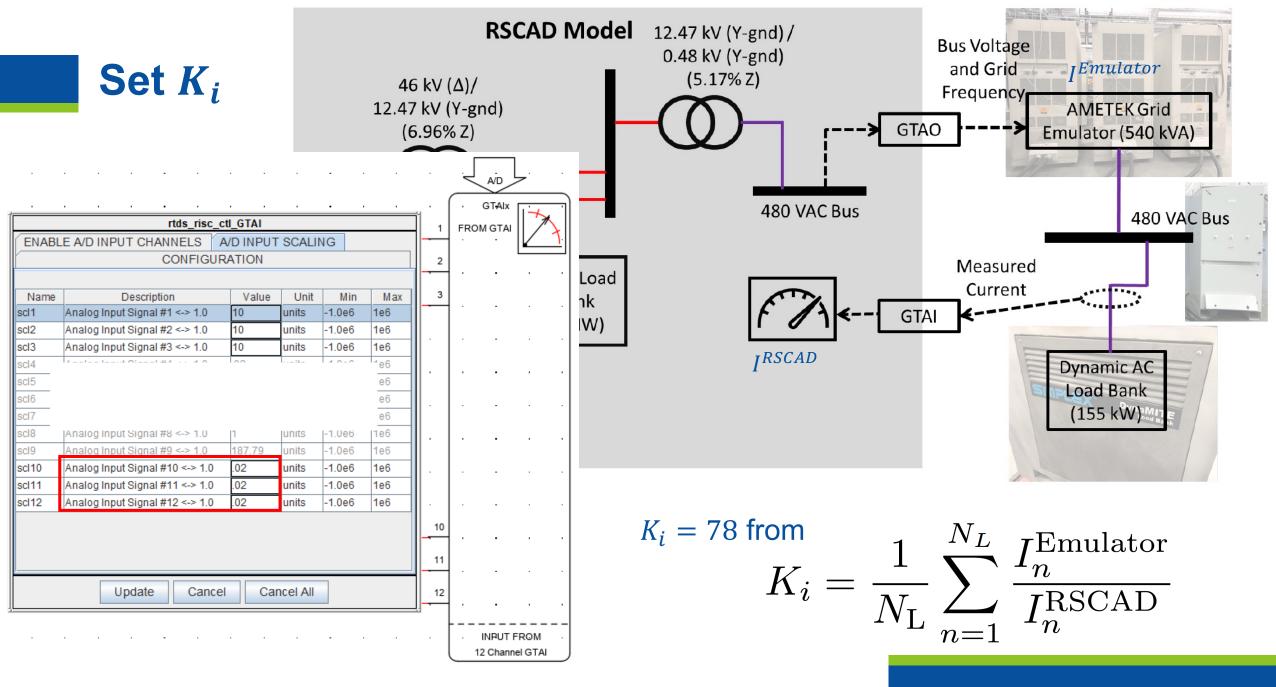


Set K_v

- Peak analog input to AMETEK grid emulator: 10 V
- Grid emulator's line-to-neutral amplification factor: 40
- Line-to-neutral peak value at 480 VAC bus $\approx 0.4 \ \text{kV}$
- $0.4 \times K_v = 10$
- $K_v = 25$

	•		
	· () ∍
		FOR GTAO	
	·	· · · ·	
VrefA O	10		
VrefB ⊖			
VrefC O	12		
	. (OUTPUT TO 12 Channel GTAO	

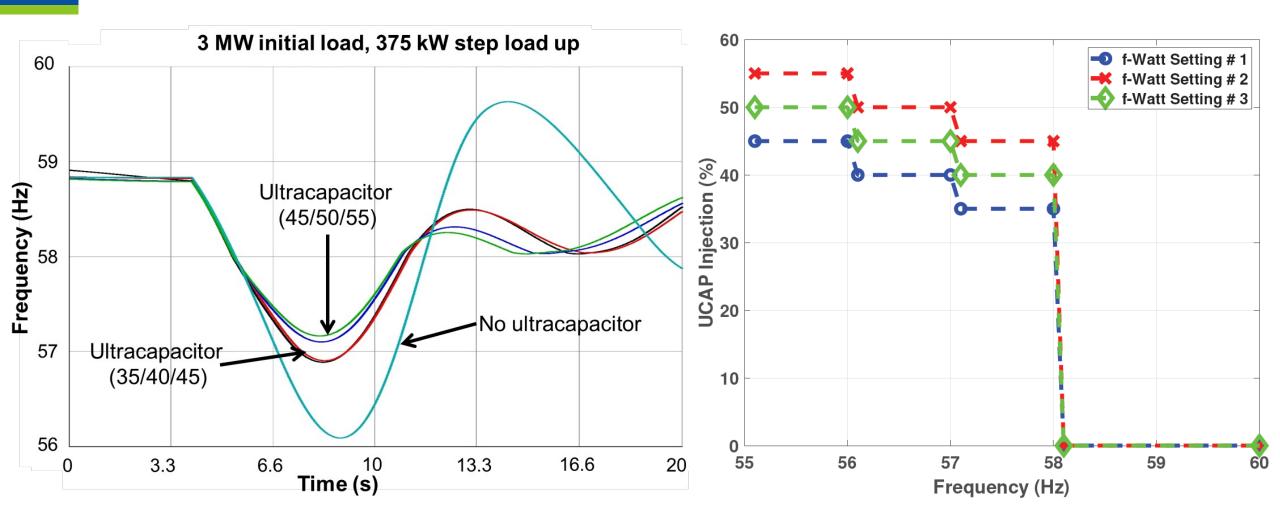
			I_GTAOOUT	OPTION	1	
			MENT DELAY			
D/A OUTPUT SCALING			PROJECTION ADVANCE FACTORS			
С	ONFIGURATION		ENABLE D/A	DUTPUTC	HANNELS	
Name	Description		Value	Unit	Min	Max
scl1	Chnl 1 Peak value for 5 Volts D/A out:		5	units	-1.0e6	1e6
scl2	Chnl 2 Peak value for 5 Volts D/A out:		5	units	-1.0e6	1e6
scl3	Chnl 3 Peak value for 5 Volts D/A out:		5	units	-1.0e6	1e6
scl4	Chnl 4 Peak value for 5 Volts D/A out:		1	units	-1.0e6	1e6
scl5	Chnl 5 Peak value for 5 Volts D/A out:		187.79	units	-1.0e6	1e6
scl6	Chnl 6 Peak value for 5 Volts D/A out:		187.79	units	-1.0e6	1e6
scl7	Chnl 7 Peak value for 5 Volts D/A out:		187.79	units	-1.0e6	1e6
scl8	Chnl 8 Peak value for 5 Volts D/A out:		187.79	units	-1.0e6	1e6
scl9	Chnl 9 Peak value for 5 Volts D/A out:		187.79	units	-1.0e6	1e6
scl10	Chnl 10 Peak value for 5 Volts D/A out:		5	units	-1.0e6	1e6
scl11	Chnl 11 Peak value for 5 Vol	ts D/A out:	5	units	-1.0e6	1e6
scl12	Chnl 12 Peak value for 5 Vol	ts D/A out:	5	units	-1.0e6	1e6
scl13	Chnl 13 Peak value for 5 Volts D/A out:		187.79	units	-1.0e6	1e6
scl14	Chnl 14 Peak value for 5 Volts D/A out:		187.79	units	-1.0e6	1e6
scl15	Chnl 15 Peak value for 5 Volts D/A out:		187.79	units	-1.0e6	1e6
scl16	Chnl 16 Peak value for 5 Vol	187.79	units	-1.0e6	1e6	



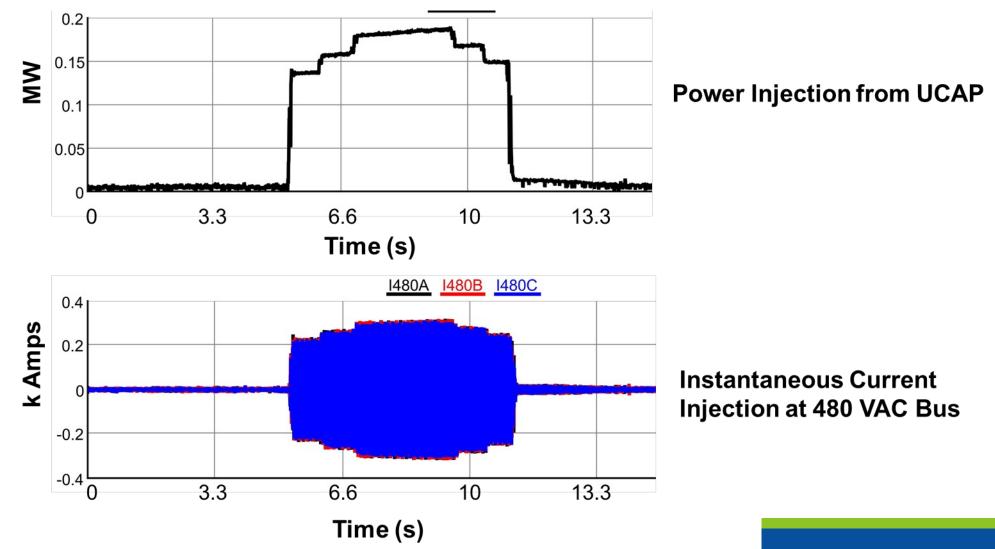
Test Sequence

Event Number	Event Description
E1	UCAP ESS: Disable inverter operation. Current injection model: 'Disable'
E2	"Lower Bulb" Unit: Set "Initial Mode of Lock/FreeSwitch" to "Lock" under "Mechanical Data and Con-figuration".
E3	Dynamic Load Bank": Set the desired value for steady-state load.
E4	Run load flow and initialize hydrgovernor turbine settings according to [6], [7]. This step must be repeated for each steady-state electric loading and prior to stepload change.
E5	Compile the draft file and load to RUNTIME.
E6	Start simulation and "unlock" the "Lower Bulb Unit" from E2.
E7	Apply a desired step load change on the "Dynamic Load Bank" and observe frequency and other variables of interest.
E8	Stop the simulation.
E9	EPC converter: Load the desired f-Watt setting via the EPyQ GUI. Enable inverter operation and current injection system from E1. Repeat E2 - E8.

Test UCAP system injection rates

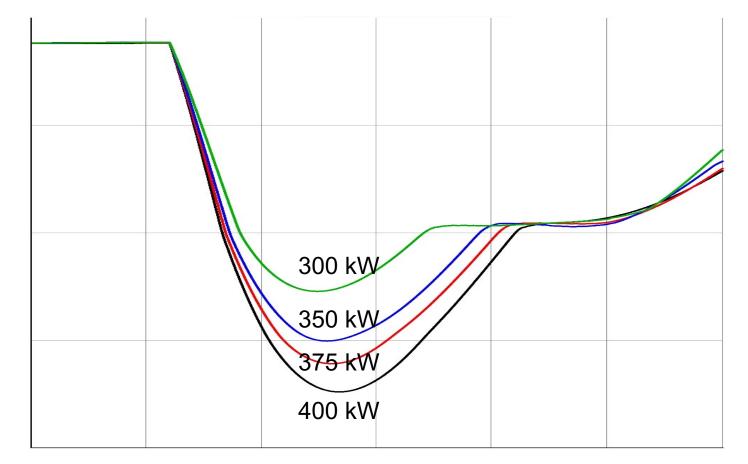


Observe UCAP response



Test maximum step load size

2 MW initial load, testing response to varying step load ups



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Time (s)

Conclusions

RSCAD Model is Publicly Available on GitHub

- https://github.com/IdahoLabResearch/Hydropower_Unit_Models
- Key findings
 - Pre-characterization of energy storage response drives the inverter control design.
 - A systematic approach to real-time simulation model calibration with hardware response can reduce effort and cost for PHIL preparation.
- Next steps
 - Develop operational-mode-aware-coordination scheme between hydrogovernor and inverter control for transient stability.
 - Explore inverter integration beyond grid following mode operation and frequency droop-based control to further improve islanded operation stability (e.g., lower the ROCOF, dampen oscillation).

Questions & Feedback S M Shafiul Alam

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Reference: Alam et al. 2022 "Enhancing Local Grid Resilience with Small Hydropower Hybrids: Proving the concept through demonstration, simulation, and analysis with Idaho Falls Power", INL/RPT-22-69038. DOI: <u>https://doi.org/10.2172/1891110</u>

Reference: Alam et al. 2022 "Power Hardware-Inthe-Loop Hydropower and Ultracapacitor Hybrid Testbed", IEEE PES GM 2022. DOI:

https://doi.org/10.1109/PESGM48719.2022.9917167

Reference: Panwar et al. 2019 "Experiences from Field Testing for Black Start of a Run-ofthe-river Hydropower Plant in Idaho Falls Power Distribution Grid", INL/CON-19-54888. Link



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