

Virtual Energy Storage (VES)

Prior work

Capacity characterization for short-term planning

VES capacity characteri zation for long-term planning

Capacity characterization of on/off and variable flexible loads providing virtual energy storage

Prabir Barooah

With Austin Coffman, Zhong Guo, Sean Meyn, Neil Camardella





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Workshop on Autonomous Energy Systems, NREL August 19-20, 2020



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Austin Coffman



Zhong Guo



Neil Camardella



Sean Meyn



Prabir Barooah



Energy storage needs for a renewable-rich grid



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Demand flexility can be used to provide virtual energy storage

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VES capacity characterization for long-term planning $\ensuremath{\textbf{Virtual}}$ Energy Storage: altering the power consumption of loads from the baseline demand.



Demand deviation Y_k = altered consumption P_k - baseline P_k^b Loads cannot compromise their quality of service (QoS) in providing VES

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Terminology

- *R^{BA}* : grid's requirement, remaining imbalance,...
- R : VES reference (for an ensemble of loads)
- feasible/within capacity: if Y can track R without violating any load's QoS, then R is within the capacity of the loads.

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Q1: Capacity characterization

- How to characterize VES capacity of a collection of flexible loads?
- Capacity characterization should be useful for planning

Planning horizons

- 1. Short term: can 10,000 water heaters deliver what is needed in the next hour?
- Long term: Should the BA contract 50,000 HVAC systems or 1,000,000 for the next year?

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Q1: Capacity characterization

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- Long term: Should the BA contract 50,000 HVAC systems or 1,000,000 for the next year?

Q2: Robust Distributed Coordination

How to coordinate an ensemble of loads to track a VES reference signal $\underline{\text{that maybe}}$ (slightly) outside the capacity of the ensemble?

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Answers in today's talk

(TCL: thermostatically controlled load)

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Ans to Q1.1: Capacity characterization of on/off loads for short-term planning (hour)

Given a prediction of the BA's requirement $\{R_k^{BA}\}_{k=1}^H$, determine the best reference $\{R_k\}_{k=1}^H$ for a collection of TCLs that is within their capacity:

- Within capacity: no single TCL need to violate its local quality of service.
- Best reference: R is closest to R^{BA} within some set Ω .





Answers in today's talk (briefly)

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Ans to Q1.2: Capacity characterization for long-term planning (year)

Given a statistical characterization of BA's requirement, determine how many loads are needed to meet the BA's requirement.



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NOT in today's talk (advertisement)

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Ans to Q2: How to design coordination algorithms that are robust to inaccurate capacity estimates?

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- Coordination algorithm should fail gradually if R_k is beyond capacity.
- Not true for most prior works, esp. those using dual ascent.



NOT in today's talk (advertisement)

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Ans to Q2: How to design coordination algorithms that are robust to inaccurate capacity estimates?

- Coordination algorithm should fail gradually if R_k is beyond capacity.
- Not true for most prior works, esp. those using dual ascent.

A proposed solution

 Coffman, Hale and Barooah, "Resource allocation with local QoS: Flexible loads in the power grid", CCTA, August 2020.

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Next week! Wed, August 26, 16:40-17:00, Paper WeC3.3.



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Q1.1: Capacity characterization of on/off TCLs, for short term planning

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Prior work: Capacity characterization of Hao et al., IEEE TPS'15

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VES capacity characterization for long-term planning "Aggregate Flexibility of Thermostatically Controlled Loads", Hao, Sanandaji, Poolla, Vincent, *IEEE Trans. on Power Systems*, 2015.

- ► The only QoS considered is the indoor temperature deviation (air conditioner): $\tilde{\theta}_k \stackrel{\Delta}{=} \theta_k - \theta_{\text{set}}$, constraint: $|\tilde{\theta}_k| \leq \Delta$.
- ▶ Ignore on/off nature; assume power is <u>continuously variable</u>: $Y_k^j = P_k P_k^{baseline}$.
- Model of indoor temperature deviation $\tilde{\theta}_k^j$ of the *j*-th TCL:

$$\tilde{\theta}_{k+1}^{j} = \mathbf{a}^{j}\tilde{\theta}_{k}^{j} + \mathbf{b}^{j}\mathbf{Y}_{k}^{j}.$$

▶ Define "total" quantities over *N* TCLs:

 $Y_k = \sum_{j=1}^N Y_k^j$ (power deviation) $Z_k := \sum_{j=1}^N ilde{ heta}_k^j$ (temperature deviation)

Ensemble model:
$$Z_{k+1} = aZ_k + bY_k$$
.



Prior work: Capacity characterization of Hao et al., IEEE TPS'15

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Capacity as a constraint on power deviation Y_k

A total power deviation signal Y_k is within capacity if

1.
$$0 \leq (Y_k + P_k^b) \leq \text{total rated power}$$

2.
$$Z_0 = 0$$
, $Z_{k+1} = aZ_k + bY_k$, $|Z_k| \le N\Delta$.



Prior work: Capacity characterization of Hao et al., IEEE TPS'15

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Can be used for short term reference planning:





Today: the other QoS metrics that affect VES capacity

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Individual load's quality of service (QoS)

- 1. Temperature
- 2. Cycling/lock-out
- 3. Total energy use over a billing period

Cycling constraint of a load

A load can flip on/off only once in any time interval of length τ :





Prior work on capacity with temperature+cycling constraints

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Related literature

- 1. Sanandaji, Vincent, Poolla, "Ramping rate flexibility of residential hvac loads", IEEE TSE'16.
- 2. Zhao, Zhang, Hao, Kalsi, "A geometric approach to aggregate flexibility modeling of thermostatically controlled loads". IEEE TPS'17.
- 3. Ziras, You, Bindner, Vrettos, "A new method for handling lockout constraints on controlled TCL aggregations", PSCC'18.

So far, no tractable method to relate cycling constraints to power deviation

$$m_k^j = egin{cases} 1 & ext{TCL j is on at } k \ 0 & ext{TCL j is off at } k \end{cases}$$

Challenge: nonlinear integer constraint at the individual:

• Minimum lock-out time for *j*-th TCL is τ^j :

$$\sum_{k=1}^{\tau^j} |m_{k-\ell}^j - m_{k-\ell-1}^j| \le 1, \qquad \forall k.$$



Proposed solution (Coffman, Camardella, Meyn, Barooah, ACC 2020)

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Main idea

Translate constraints to "fraction of loads that are" (no integers!)

$$n_k^{\text{on}} \stackrel{\Delta}{=} \text{fraction of loads that are on at } k$$

 $r_k^{\text{on}} \stackrel{\Delta}{=} \text{fraction of loads that flipped on (from off to on) at } k$
 $r_k^{\text{on}} \stackrel{\Delta}{=} \text{fraction of loads that are stuck on at } k$
And, similarly, $r_k^{\text{off}} := \dots, s_k^{\text{off}} := \dots$

(i) Quasi-homogeneous assumption:

Power consumption of the ensemble is equivalent to n_k^{on} : $n_k^{\text{on}} = \frac{1}{\sum_i P_{\text{rated}}^j} (Y_k + P_k^b)$

(ii) Evolution of various fractions

Example: $s_k^{\text{on}} = s_{k-1}^{\text{on}} + f_k^{\text{on}} - f_{k-\tau}^{\text{on}}$





Capacity characterization: a set of constraints on...

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 $\psi_k :=$

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$$\begin{split} & [Y_k, Z_k, n_k^{\text{on}}, s_k^{\text{on}}, s_k^{\text{off}}, f_k^{\text{on}}, f_k^{\text{off}}] \\ & Z_k = a Z_{k-1} + b Y_{k-1}, -C \leq Z_k \leq C, \\ & n_k^{\text{on}} = \frac{1}{\sum_j P_{\text{rated}}^j} (Y_k + P_k^b), \\ & n_k^{\text{on}} = n_{k-1}^{\text{on}} + f_{k-1}^{\text{on}} - f_{k-1}^{\text{off}} \\ & s_{k-1}^{\text{on}} \leq n_k^{\text{on}} \leq 1 - s_{k-1}^{\text{off}}, \\ & s_k^{\text{on}} = s_{k-1}^{\text{on}} + f_{k-1}^{\text{on}} - f_{k-\tau-1}^{\text{off}} \\ & s_k^{\text{off}} = s_{k-1}^{\text{off}} + f_{k-1}^{\text{off}} - f_{k-\tau-1}^{\text{off}} \\ & s_k^{\text{off}} = s_{k-1}^{\text{off}} + f_{k-1}^{\text{off}} - f_{k-\tau-1}^{\text{on}} \\ & s_k^{\text{on}}, s_k^{\text{off}}, f_k^{\text{on}}, f_k^{\text{off}}, n_k^{\text{on}} \in [0, 1] \end{split}$$



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Reference computation as convex optimization

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$$\begin{split} \psi &\triangleq [Y_k, Z_k, n_k^{\text{on}}, s_k^{\text{on}}, s_k^{\text{off}}, f_k^{\text{on}}, f_k^{\text{off}}], k = 1, \dots, H \\ \psi^{\text{BA}} &\triangleq [R_k^{BA}, 0, 0, 0, 0, 0], k = 1, \dots, H, \end{split}$$





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Optimal VES reference R is the first component, Y^* of ψ^*

Unique VES reference for the ensemble, R, for a given remaining imbalance $\{R_{k}^{BA}\}$.



Numerical example of VES reference planning

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 R^{BA} : from Bonneville Power Administration.

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Proposed method: BA Accounts for loads' cycling constraints Alternate method: BA **does not** account for loads' cycling constraints



Proof by closed loop simulation: Goldilocks and the three BAs

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- 1. BA plans reference ignoring loads' cycling constraints, and it forces ACs to disregard cycling constraints. (dictatorial BA)
- 2. BA plans reference ignoring loads' cycling constraints, but loads enforce cycling constraints. (oblivious BA)
- 3. Both the BA and the loads account for load's cycling constraints. (considerate BA)

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Reference tracking by ensemble and individuals' QoS:

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What we expect:

- 1. The ACs to cycle frequently.
- 2. **Good** reference tracking.

The dictatorial BA destroyed everyones AC's in obtaining VES!



Tracking in scenario 2: Oblivious BA

Reference tracking by ensemble and individuals' QoS:

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What we expect:

- 1. The ACs to satisfy their cycling constraints.
- 2. **Poor** reference tracking.

The oblivious BA paid the price in reference tracking error!

Tracking in scenario 3: Considerate BA (Proposed Method)

Reference tracking by ensemble and individuals' QoS:

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What we expect:

- 1. The ACs to satisfy cycling QoS.
- 2. **Good** reference tracking.

The considerate BA asked for just the right amount, so both parties were happy!



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Contribution

- 1. A computation friendly characterization of capacity of TCL ensembles to provide VES.
- 2. A balancing authority can use this method to compute the "largest feasible" reference signal for a load ensemble under its jurisdiction (convex optimization).
- 3. The method accounts for all three QoS metrics for the consumer: (i) indoor temperature, (ii) cycling, and (ii) energy use.

References

- (i) Coffman, Camardella, Meyn, and Barooah, "Flexibility capacity of TCLs with cycling constraints", *Amer. Control Conf.*, July 2020, ArXiV:1909.11497, 2019.
- (ii) Coffman, Bušić, and Barooah, "Aggregate Capacity for TCLs providing Virtual Energy Storage with cycling constraints", *IEEE Conf. on Decision and Control, Dec. 2019.*

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Q 1.2: Capacity characterization of <u>continuously</u> variable loads, for long term planning

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Capacity characterization based on statistics of grid's needs

- ▶ Problem: instead of the signal $\{R_k^{BA}\}$, only statistics of the stochastic process \mathbf{R}_k^{BA} is given. How do you determine if *N* loads are enough to deliver?
- Approach: use spectral density.

Reference

(i) Coffman, Guo, and Barooah, "A spectral characterization of aggregate capacity of flexible loads for grid support", *Amer. Control Conference, July 2020.*

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Spectral density

The spectral density $\Phi_{XX}(\omega)$ of a zero-mean W.S.S. stochastic process X(t) is the Fourier transform of its autocorrelation function.



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VES capacity characterization for long-term planning For simplicity, consider one HVAC load

QoS Constraints

- 1. Actuator constraint: $\max_t |Y(t)| < C_1$
- 2. Actuator (rate) constraint: $\max_t |Y(t+\delta) Y(t)| < C_2$ (fixed δ)

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- 3. Temperature constraint: $\max_t |\tilde{\theta}(t)| < C_3$
- 4. Energy or utility bill constraint: $\max_t |\tilde{E}(t)| < C_4$

Recall, for a load, $\tilde{E}(t) = \int_0^t Y(\eta) d\eta$.



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1. Replace by probabilistic constraints

1. Actuator constraint:
$$Prob(|Y(t)| < C_1) > 1 - \epsilon_1$$

2. ...

2. Obtain sufficient condition from Chebycheff inequality

If X is zero mean and var(X) < a then $P(|X| < C) > 1 - \frac{a}{C^2}$.

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3. Convert to constraints on the PSD of Y

Variance of X(t) is related to integral of $\Phi_{XX}(\omega)$.

4. Planning through projection onto a constraint set

$$\Phi^* = \arg\min_{\Phi} \int_0^\infty \left(\Phi(\omega) - \Phi^{(BA)}(\omega)\right)^2 d\omega$$





Numerical example

BA: Bonneville Power Administration.

BA's requirement: the part of net demand limited to [2,8] hours time scale.

Loads: HVAC systems in large commercial buildings. For each building, $|Y| \leq$ 40 kW, $\leq \pm 2^\circ$ F,.. Result:

 $\begin{array}{c}
10^{8} \\
 & \swarrow \\
 & \swarrow \\
 & \square \\$

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