

# Evaluating the performance and reliability of screen-printable fire-through copper paste on PERC solar cells

Suchismita Mitra<sup>1</sup>, Bill Nemeth<sup>1</sup>, Steve Johnston<sup>1</sup>, Harvey Guthrey<sup>1</sup>, Peter Hacke<sup>1</sup>, Ruvini Dharmadasa<sup>2</sup>, Thad Druffel<sup>2</sup>, Kevin Elmer<sup>2</sup>, Apolo Nambo<sup>2</sup>, Dustin Williams<sup>2</sup>, Ajay Upadhyaya<sup>3</sup>, Vijaykumar D Upadhyaya<sup>3</sup>, Ajeet Rohatgi<sup>3</sup>, Paul Stradins<sup>1</sup>

<sup>1</sup>National Renewable Energy Laboratory, Golden, USA

<sup>2</sup>Bert Thin Films, Louisville, USA

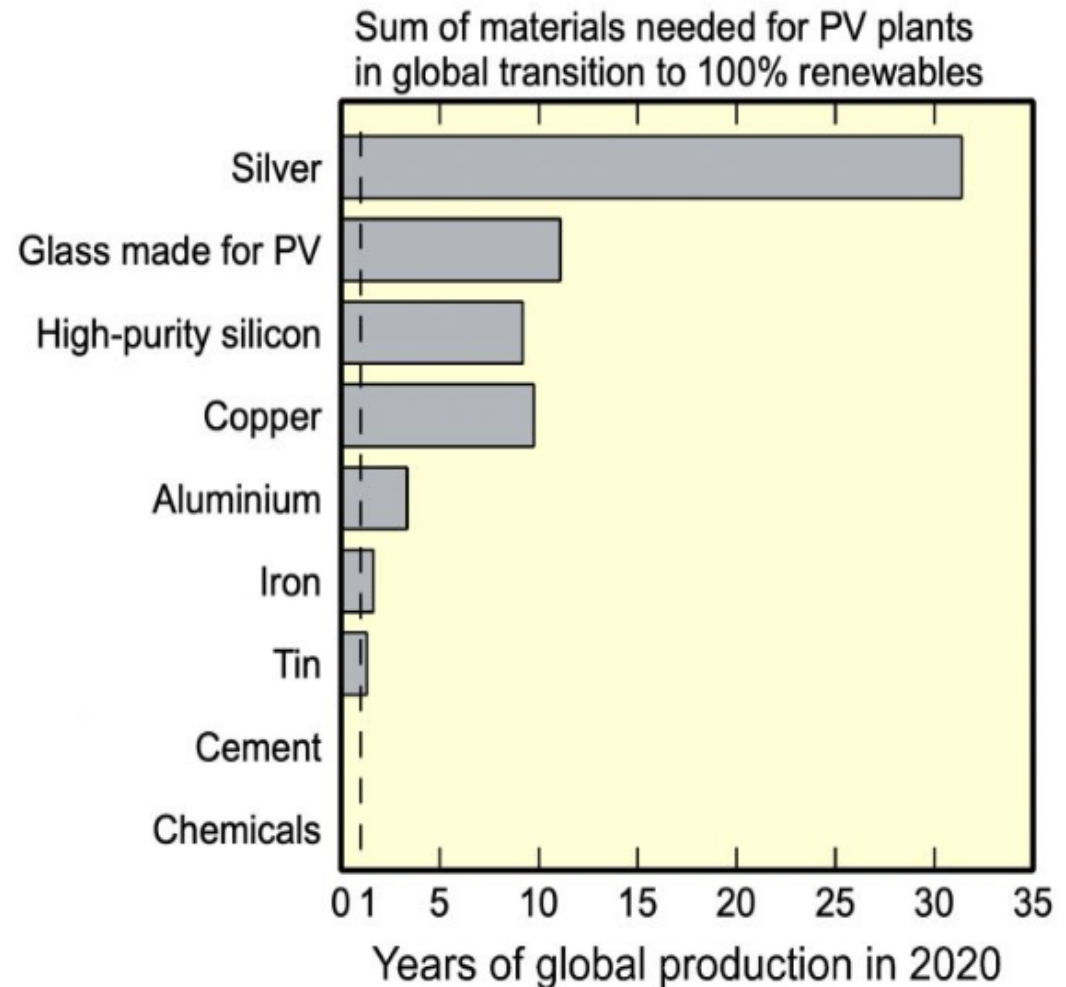
<sup>3</sup>Georgia Institute of Technology, Atlanta, USA



# Motivation

- Silicon PV is responsible for >170 GW of renewable energy
- 40 TW of energy needed for transition of our planet to 100% renewables
- Global production for Ag needs to continue for the next 30 years for global transition to 100% renewables.

*Silver is the most-expensive non-silicon material used in current c-Si technologies*



<https://www.changeanyway.com/is-solar-electricity-sustainable/>

# Why do we need an alternative material?

*A bifacial Silicon Heterojunction solar cell demands ~210 mg usage of silver paste  
(9 busbars, 24.5%, bifacial, M6 size wafer)*

Copper (Cu) is an excellent alternative to Ag

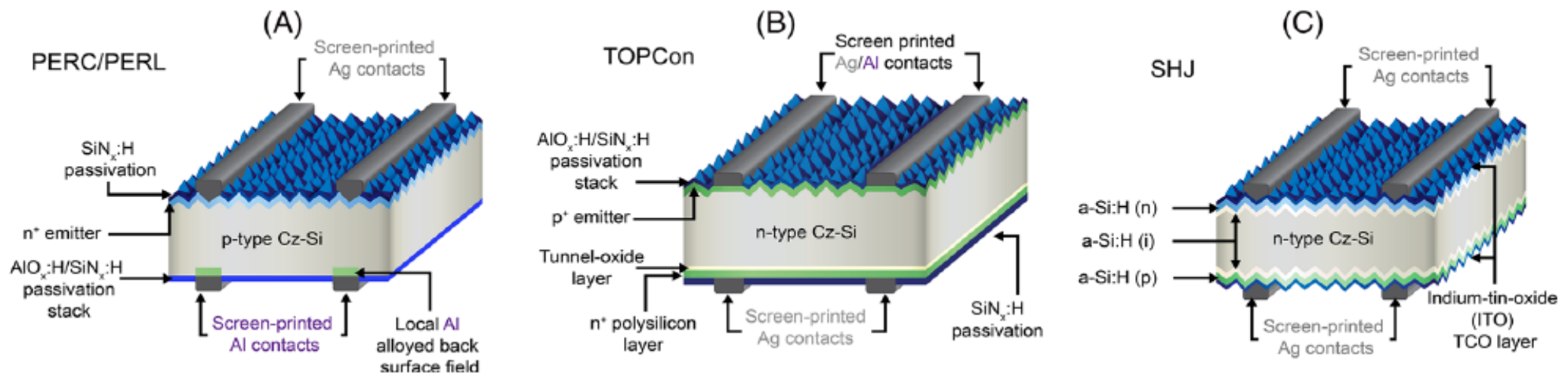
- ✓ 100 times cheaper than Ag
- ✓ Exhibiting similar electrical resistivities
  - ( $\rho_{\text{Ag}}=1.6 \mu\Omega\cdot\text{cm}$ ;  $\rho_{\text{Cu}}=1.7 \mu\Omega\cdot\text{cm}$ )
- ✓ 1000x more abundant

# Silver consumption in solar cells and modules

| Parameter (unit)                                       | PERC                    | TOPCon                    | SHJ                     |
|--|-------------------------|---------------------------|-------------------------|
| Silver consumption per cell (mg/cell)                  | 90.1–96.1 <sup>2</sup>  | 130–162.6 <sup>2,38</sup> | 198–242 <sup>2,39</sup> |
| Typical module power, 144 × half-M6 cells (W)          | 440–450 <sup>2,40</sup> | 450–460 <sup>2,40</sup>   | 465–470 <sup>2,40</sup> |
| Silver consumption at module level (mg/W) <sup>a</sup> | 14.4–15.7               | 20.4–26.0                 | 30.3–37.4               |

Note: Cell format is assumed as M6 (166 × 166 mm).

<sup>a</sup>Silver consumption is based on silver consumption per cell × 72 cells over the typical module power.



Ref: Hallam et al., *Progress in Photovoltaics: Research and Applications* 31, no. 6 (2023): 598-606.

# Electroplating or Screen Printing?

*Electroplating is the most common technique for copper metallization on silicon solar cells!*

-Highest efficiency achieved for copper plated bifacial SHJ cell C. Yu et al., Nature Energy 8, 1375 (2023)

- 26.41% (certificated by ISFH)
- M6 size wafer (274.5 cm<sup>2</sup>)

-Challenges in electroplating:

- Plating process, waste
- Copper-induced degradation
- Reliability

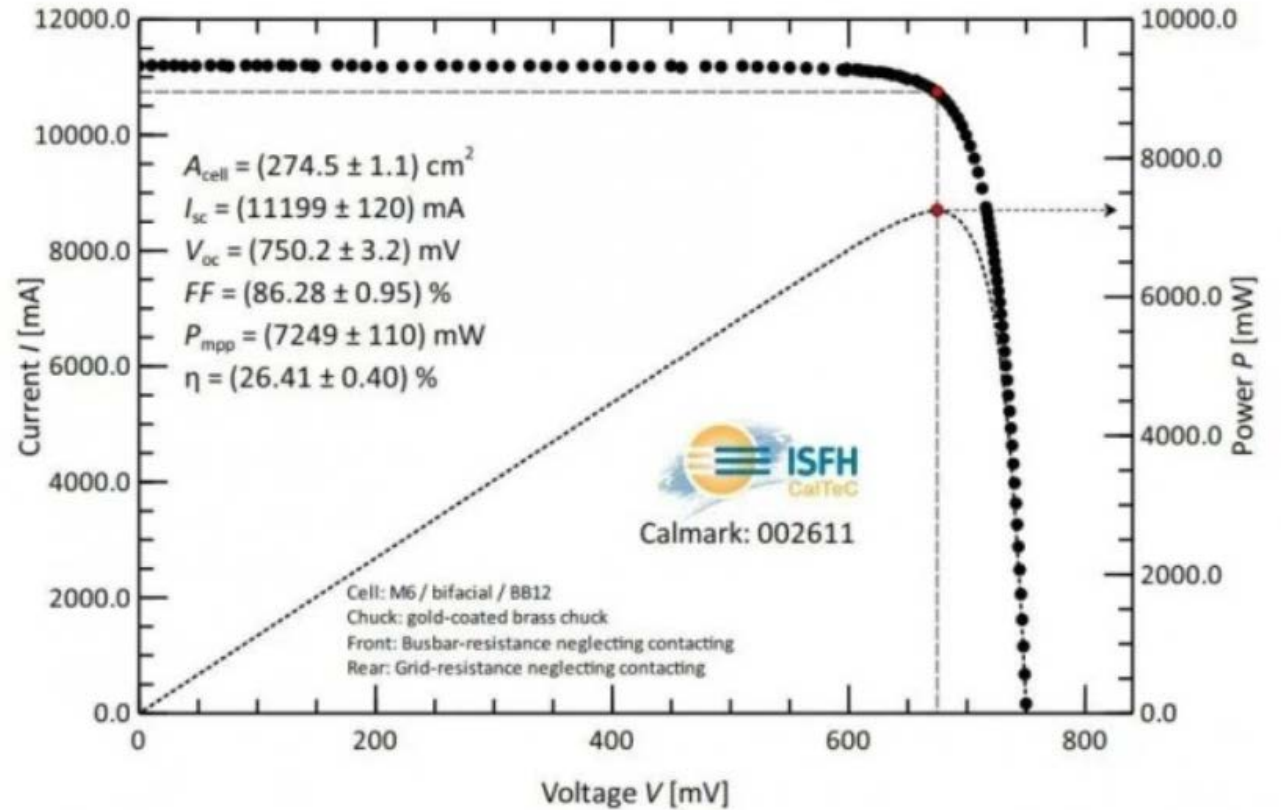


Fig. Measured IV characteristics under standard test conditions

*Screen printing is the most dominant metallization technology (>95%) for c-Si solar cell mass production and will continue to be the mainstream metallization technology*

# Challenges in preparing Cu paste

Pastes include

- Metal powders: For metallization
- Glass frits: To etch through the ARC
- Organic binders and solvents : For processability of the pastes.

Firing of pastes need high temperatures ( $>600$  °C)

- To remove the organics,
- To etch the ARC
- To sinter the metals.

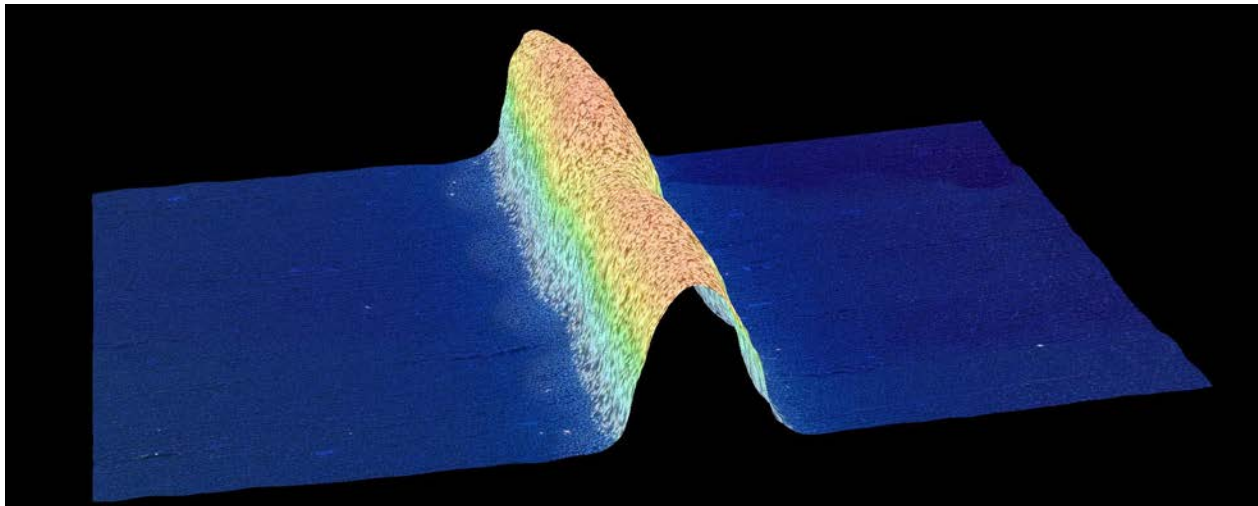
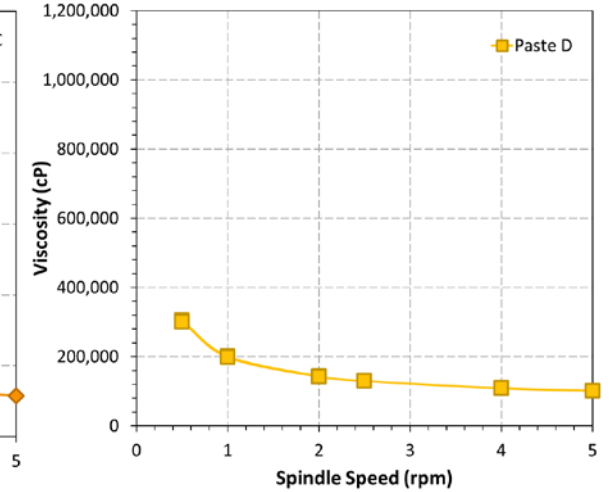
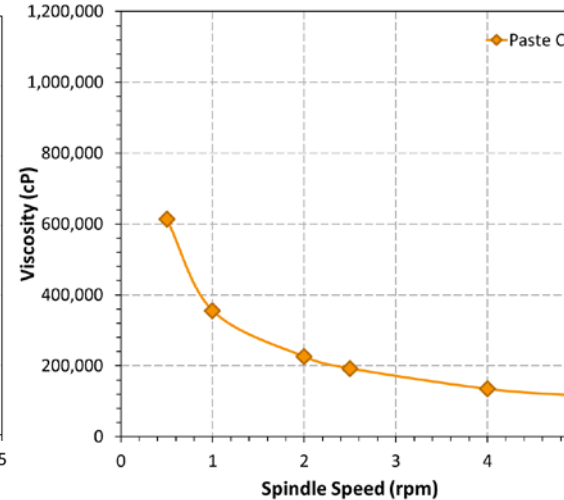
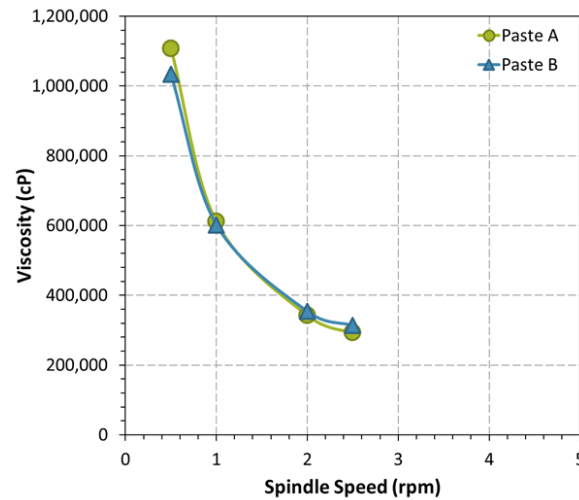
At high temperatures

- Copper can oxidize leading to high resistivity
- Copper can diffuse into Si and cause deep level impurities
- **Need of Cu diffusion barrier: laser ablation, deposition, silicide barrier formation, etc. ?**



# Rheology of Copper Paste

Rheology is controllable and is being optimized for fine line printing ( $< 30 \mu\text{m}$ ).



| Screen Parameter   | Value                               |
|--------------------|-------------------------------------|
| Mesh               | 400-500 mesh, 18 $\mu\text{m}$ wire |
| Screen tension     | 16-19 N/cm                          |
| Emulsion thickness | 12-20 $\mu\text{m}$                 |
| Print gap          | 1.2-2.0 mm                          |
| Print speed        | 75-150 mm/s                         |
| Squeegee pressure  | 6-10 kg                             |
| Squeegee durometer | 70-80                               |

# PERC Cells with fire-through Cu paste by Bert Thin Films

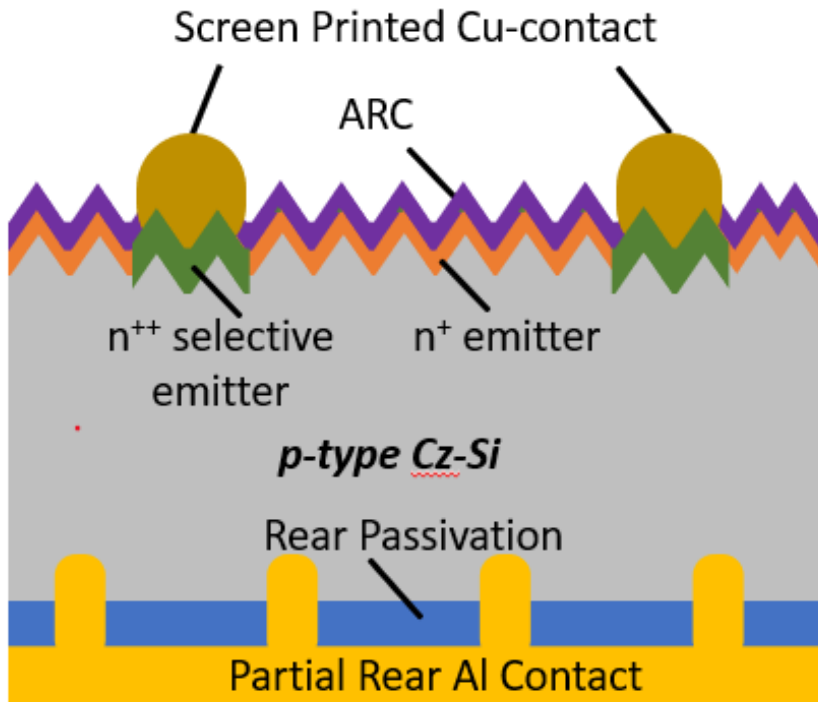


Fig. Schematic Structure of selective emitter PERC Cell

**Table: Details of cell structure**

| Parameter                | Selective Emitter                          | Homogeneous Emitter                        |
|--------------------------|--|--|
| Cell Size                | 166x166 mm <sup>2</sup> (M6)               | 166x166 mm <sup>2</sup> (M6)               |
| SiNx thickness           | 70-80 nm                                   | 70-80 nm                                   |
| Emitter Sheet Resistance | 150-160 Ω/□                                | 70-80 Ω/□                                  |
| Selective Emitter        | SE 110-120 Ω/□                             | none                                       |
| Backside Condition       | Polish + laser opening Al print/AgAl print | Polish + laser opening Al print/AgAl print |
| Busbar Number            | 9  | 9  |
| Width of Finger Pattern  | 65 μm                                      | 55 μm                                      |
| Width of Bus Bar Pattern | 0.45 mm                                    | 0.45 mm                                    |

## **Firing process**

- *Al contact at rear side is printed, dried and fired*
- *Cu paste is printed and dried*
- *Front Cu contact fired (peak temperature varied between 550°C to 630°C)*



# Early Studies on Contact Formation (16 cm<sup>2</sup> devices)

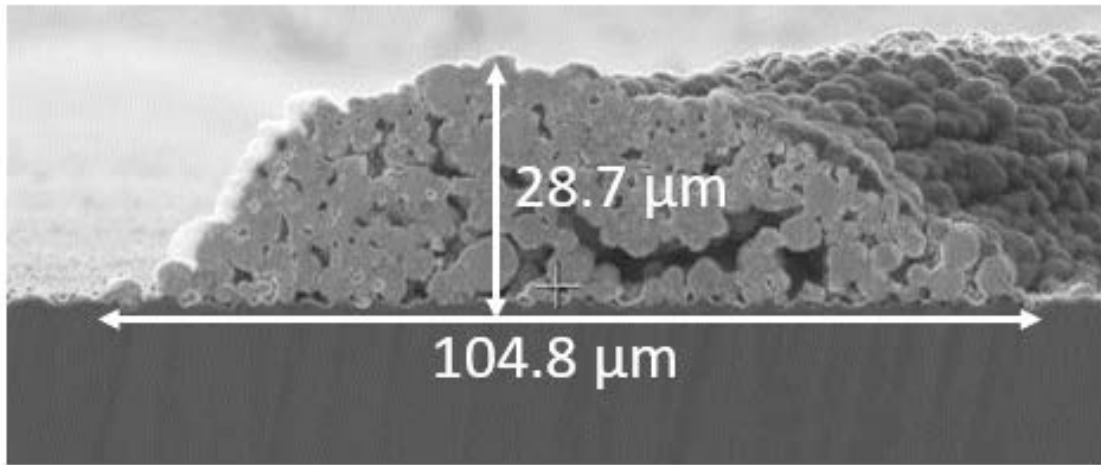


Fig. Cross-sectional SEM-Image of Cu finger

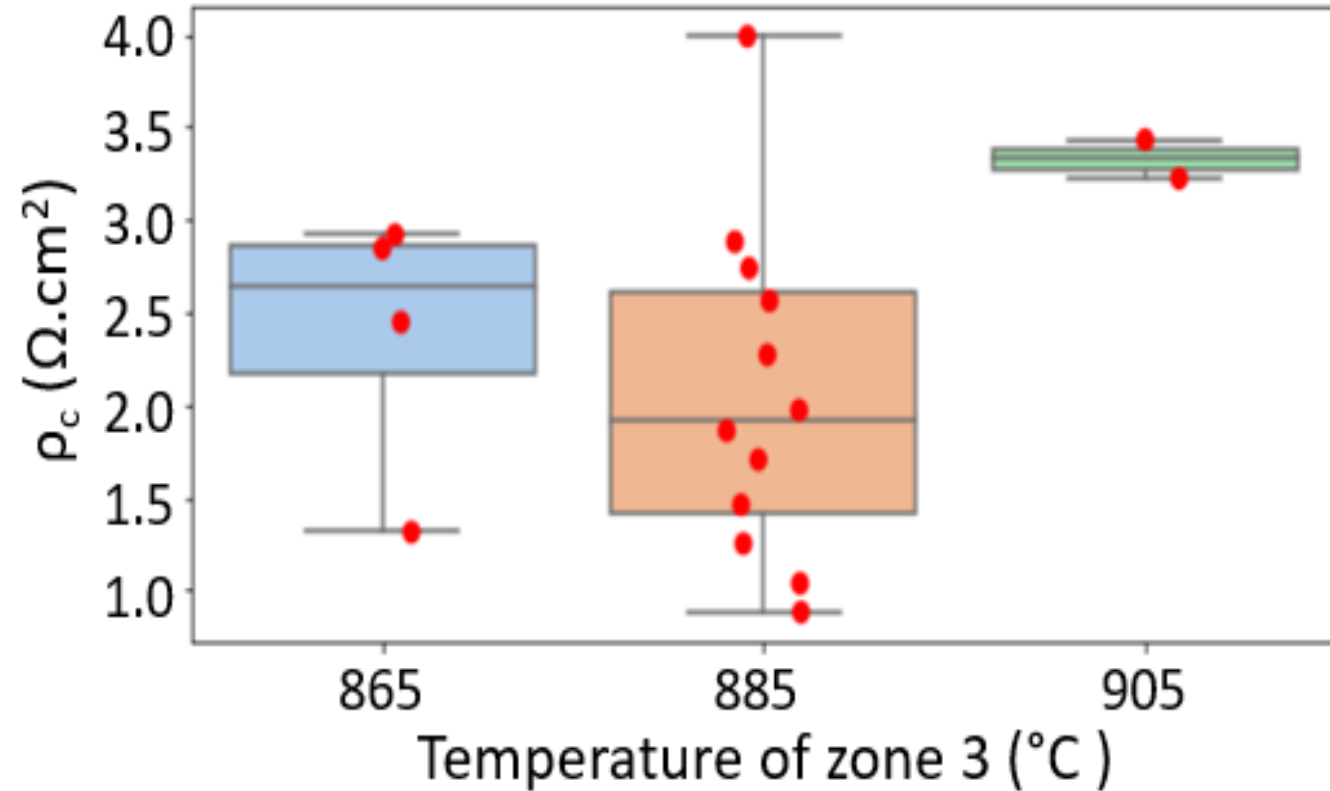
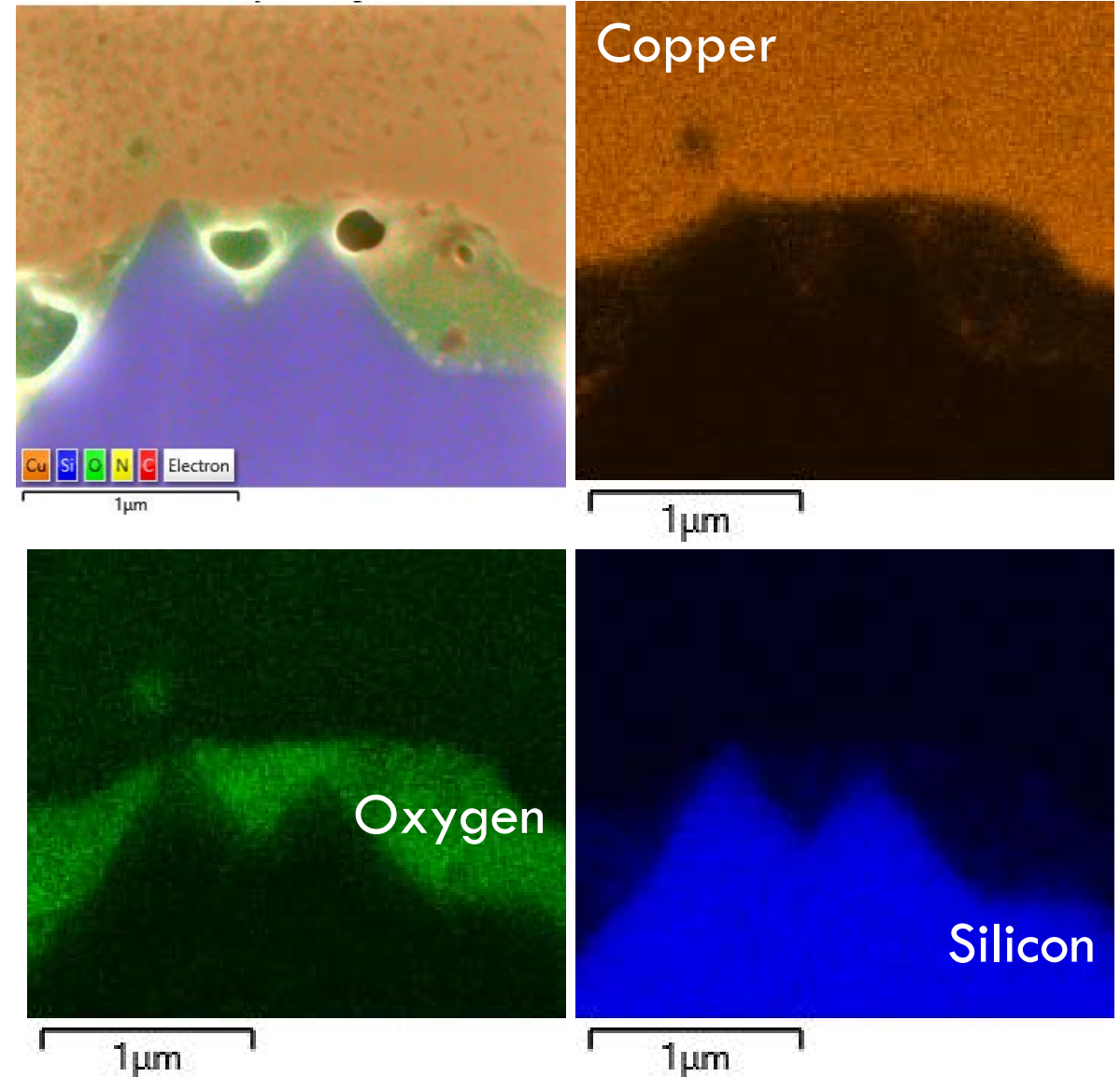


Fig. Contact resistance ( $\rho_c$ ) after firing at different temperatures for initial versions of the Cu paste (Firing done in a 3-zone furnace, Temperature of zone 1 & 2 was 450 $^{\circ}\text{C}$  with belt speed = 250 inch/min)

# Interface Studies by Energy Dispersive X-ray Spectroscopy (EDS)

## Observations:

- Thick oxide layer between Copper and Silicon
- This layer likely acts as Cu diffusion barrier
- Interface chemistry controls electronic properties



# Early pastes: J-V parameters for M6 sized PERC Cells

## Observations:

- Mean  $V_{oc}$  is  $\sim 5\text{mV}$  lower for  $630^\circ\text{C}$ , but the  $R_s$  is lowest and hence, FF and efficiency is highest

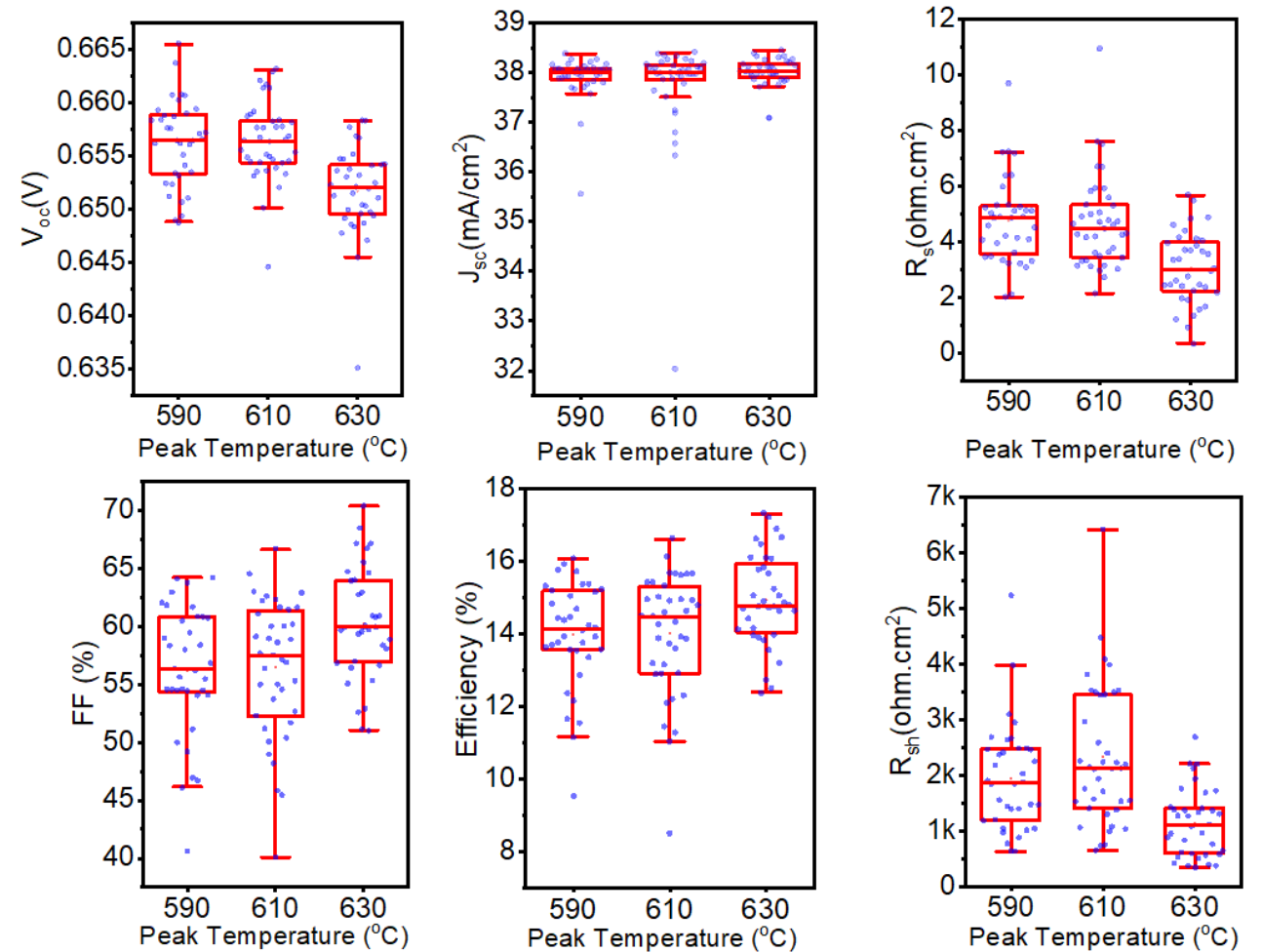
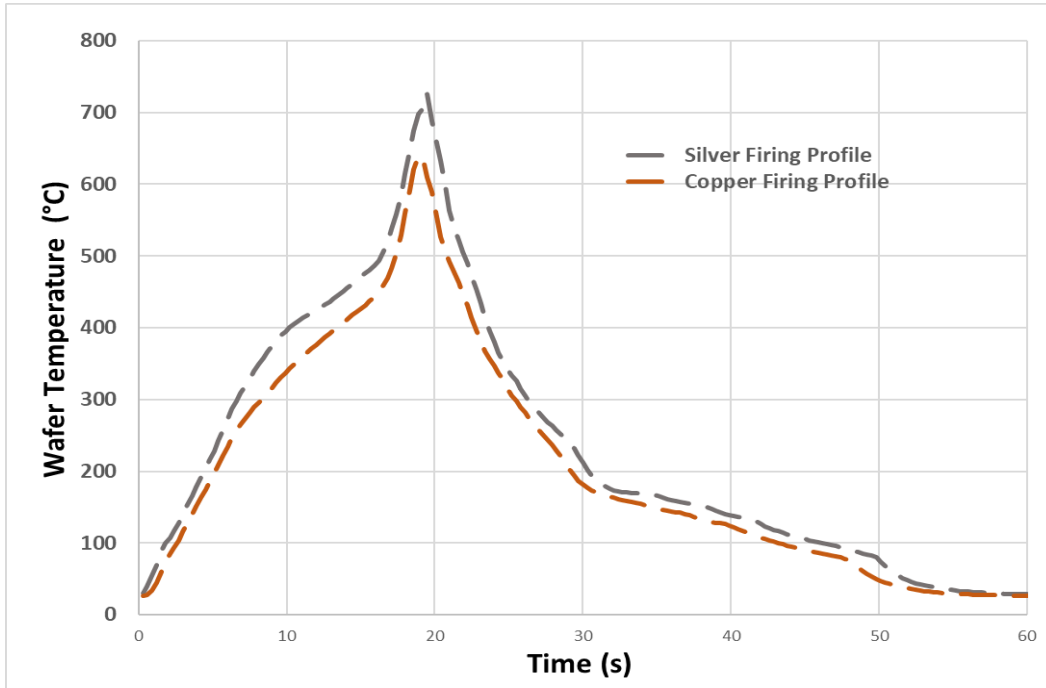


Fig. Distribution of IV parameters for M6 Size cells fired at three peak temperatures namely,  $590^\circ\text{C}$ ,  $610^\circ\text{C}$  and  $630^\circ\text{C}$

# 17+ Year Old Furnace (M2)



- Designed for smaller wafer sizes.
- Temperature uniformity limiting performance.

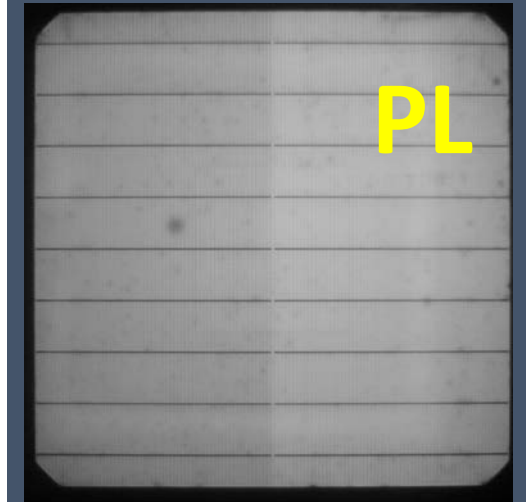
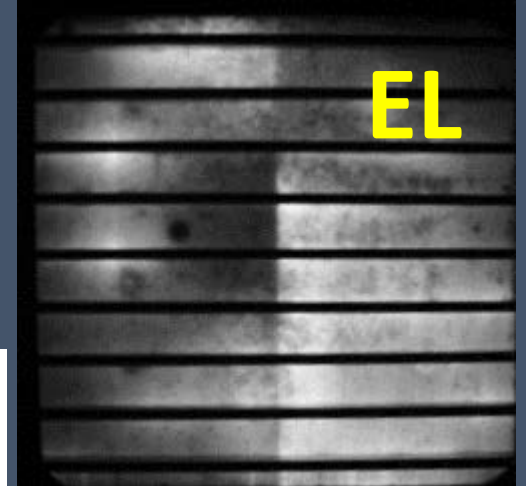
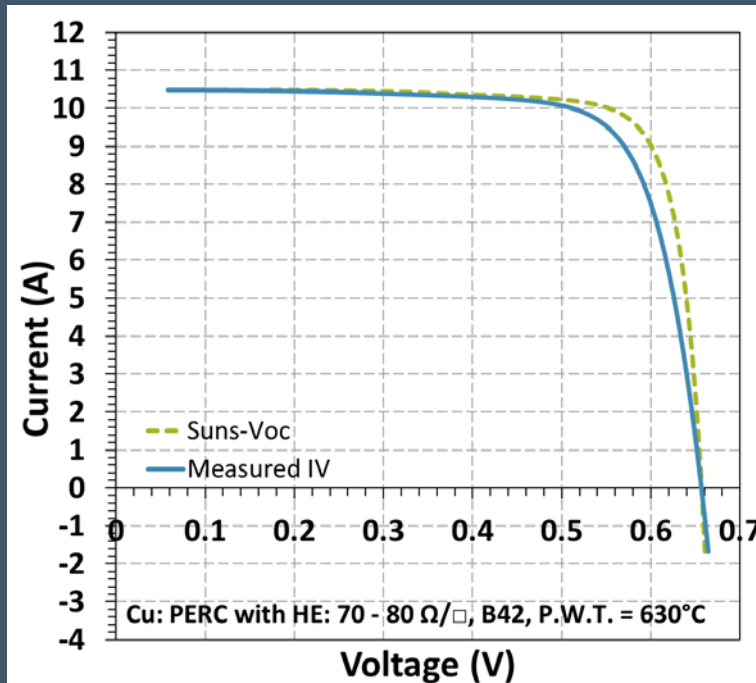
Champion Cell on M6 size wafer:

$$J_{sc} = 38.32 \text{ mA/cm}^2$$

$$V_{oc} = 0.657 \text{ V}$$

$$FF = 76.14\%$$

$$\eta = 19.17\%$$



# Biased PL imaging reveals firing non-uniformities; Series Resistance Mapping

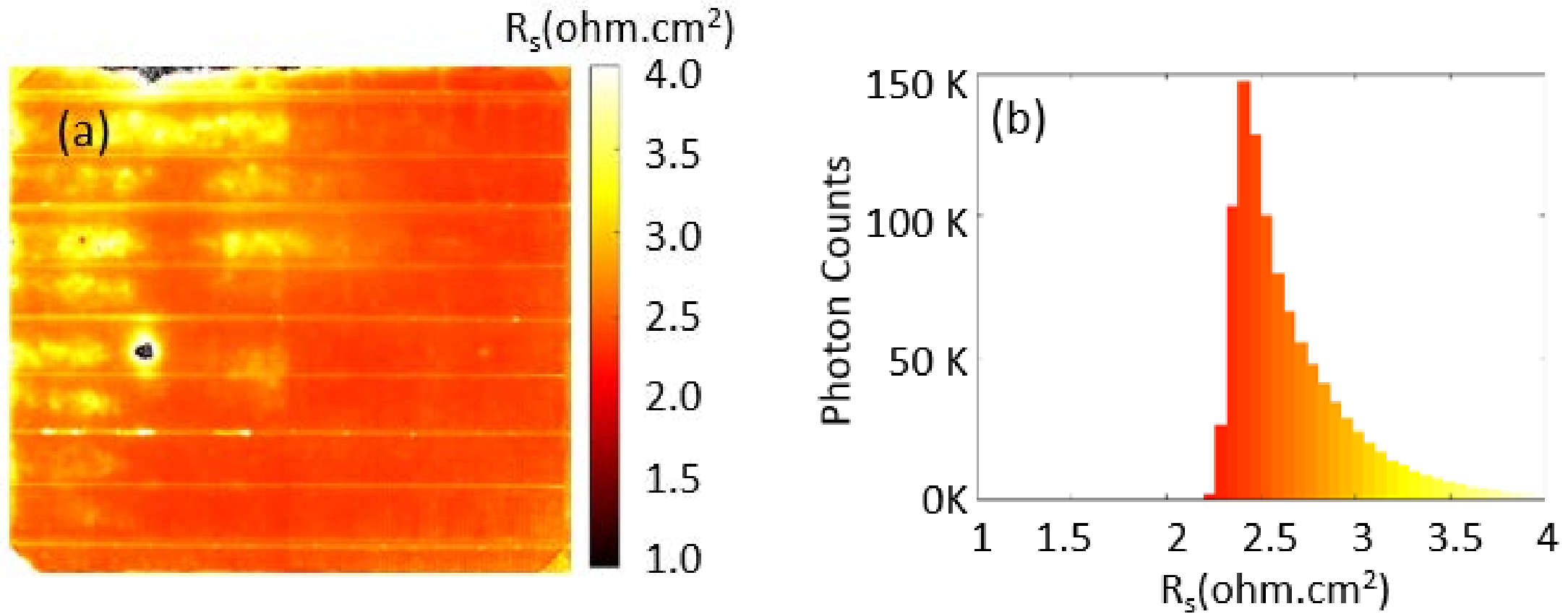


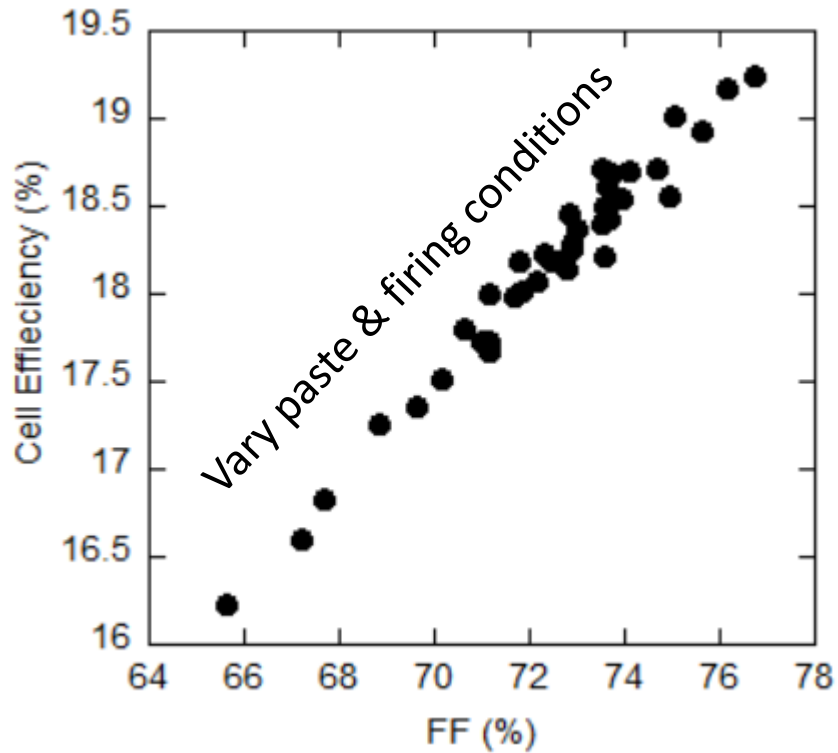
Fig. (a)  $R_s$  map obtained from biased PL images at two different intensities  
(b) Histogram showing the distribution of  $R_s$  over the entire surface

# Improved paste study: Initial Cell Efficiency correlates with Fill-factor variations.

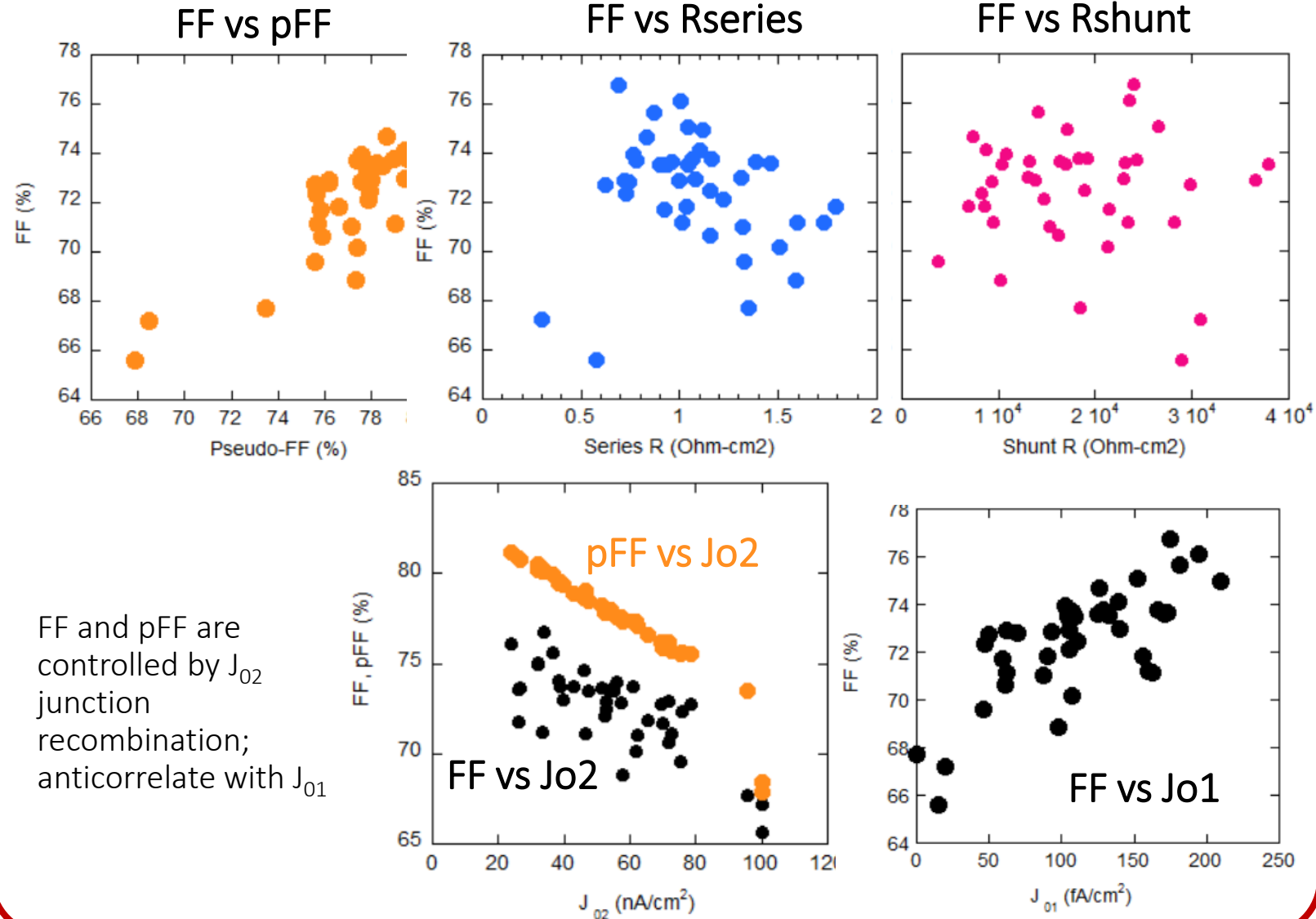
FF controlled by  $J_{O_2}$  and  $R_{ser}$

FF varies within 9% abs. in series studied.  
(12% relative,  $\gg$  than  $V_{oc}$ ,  $J_{sc}$ )

$V_{oc}$  varies within 10 mV (1.5% relative)  
Short circuit current varies within 1.5 % relative.



FF is affected by  $R_{series}$  between 0.3 and 1.7 Ohm-cm<sup>2</sup> and Pseudo-FF (varies  $\sim$  in the same range as FF plus 4% abs)





# Reliability Studies: earlier pastes, Damp Heat

## Observations:

- In Devices with Cu paste 1,  $V_{oc}$  degraded severely by 7.44% after 500 hrs of Damp heat (DH) testing.
- In Devices with Cu paste 2,  $V_{oc}$  degraded by 1.67% in the first 500 hours but didn't decay further in 1500 hours.

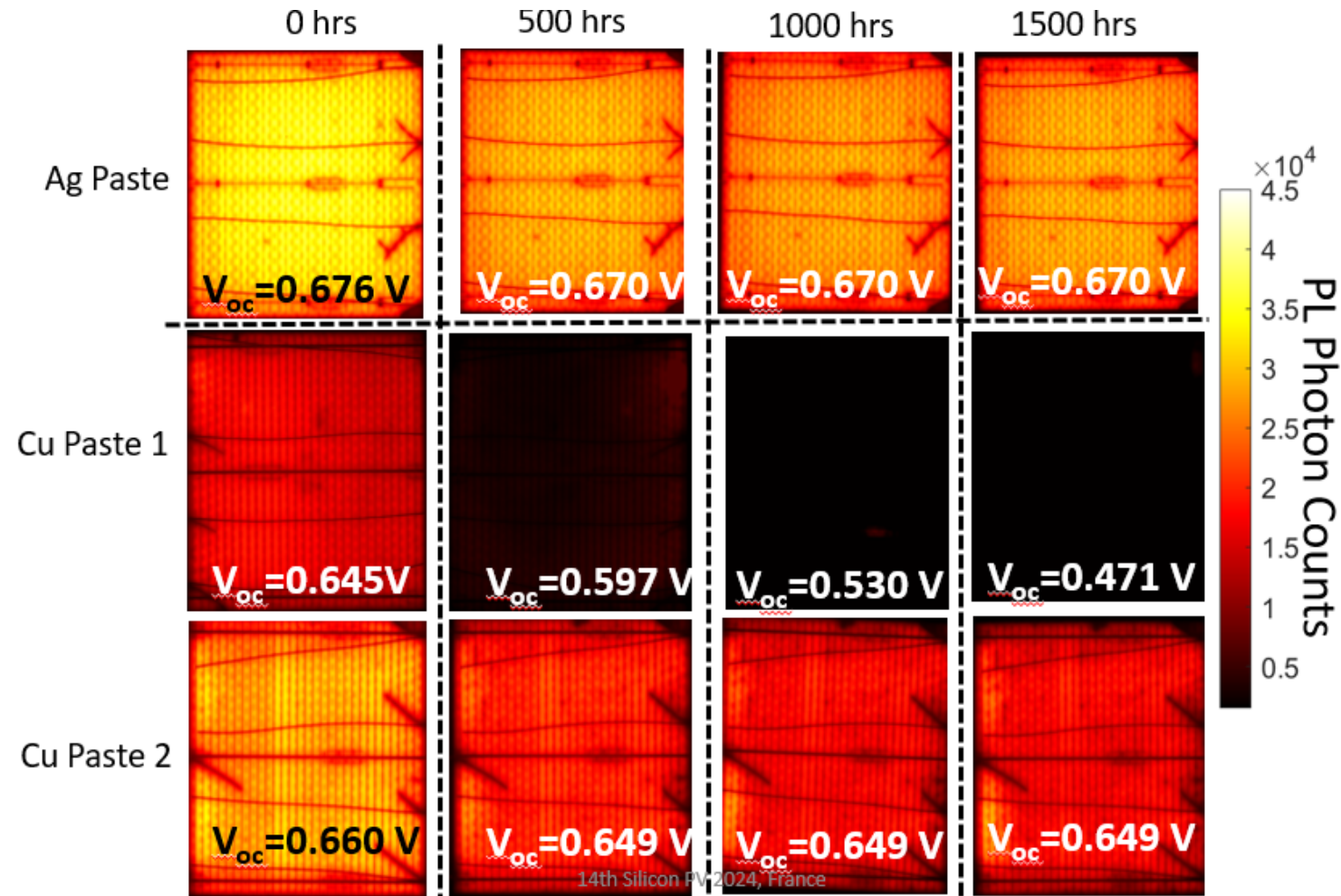


Fig. Open –Circuit PL imaging and  $V_{oc}$  degradation after DH (85 deg C/85% Humidity)- 4 cmx4cm modules

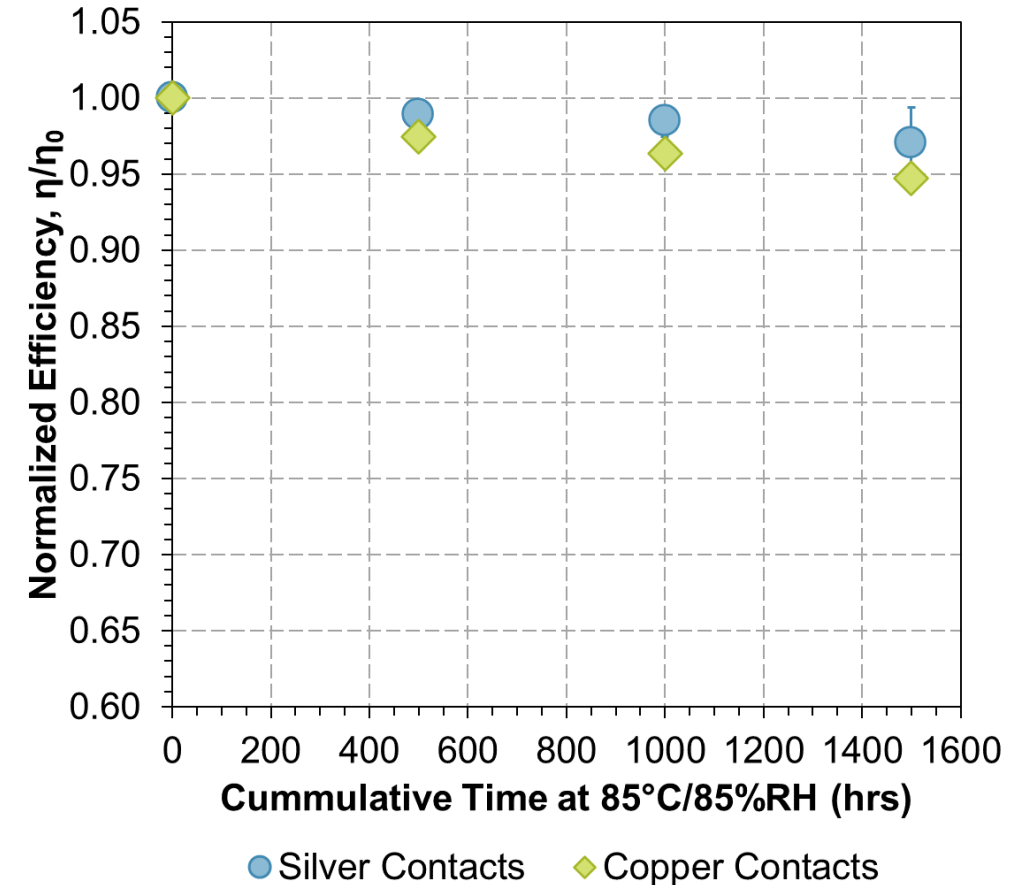
# Damp Heat – improved pastes

Copper contacts were compared to commercially sourced silver contacts in micro-modules.

Measured at NREL.

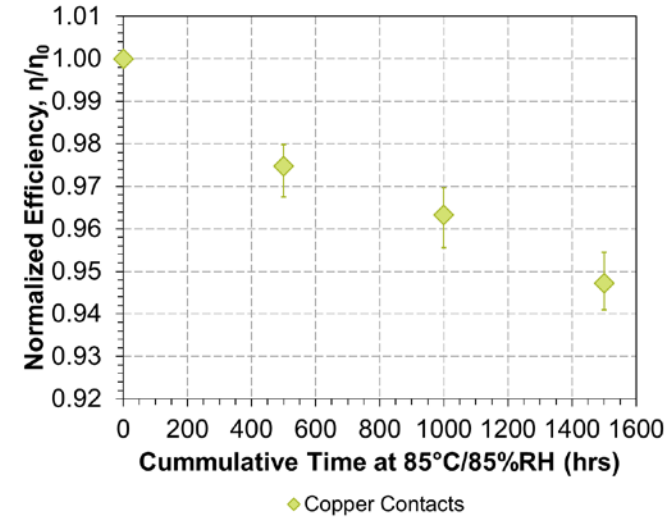
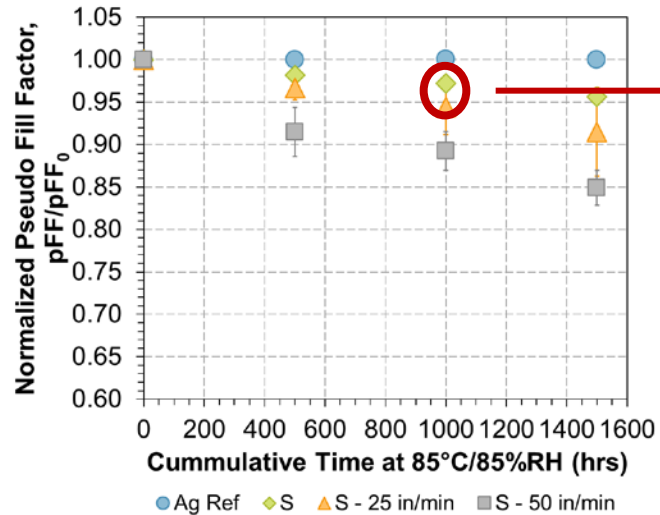
- 16 cm<sup>2</sup> cells encapsulated in to 6.4 cm × 8.3 cm micro-modules.
- 24 μm Screen Opening.
- Glass/Glass module structure with Thermoplastic Polyolefin (TPO).
- 5 micro modules per condition.
- Smart Wire Connection Technology (SnBiAg solder) used for the front.
- Manually soldered (SnPb) coated ribbons used on the rear.
- Modules used a desiccated polyisobutylene tape sealant on the edges.

|          | Cumulative Time at 85°C/ 85%RH |         |          |          |
|----------|--------------------------------|---------|----------|----------|
|          | 0 hrs                          | 500 hrs | 1000 hrs | 1500 hrs |
| Sample 1 |                                |         |          |          |
| Sample 2 |                                |         |          |          |
| Sample 3 |                                |         |          |          |
| Sample 4 |                                |         |          |          |
| Sample 5 |                                |         |          |          |

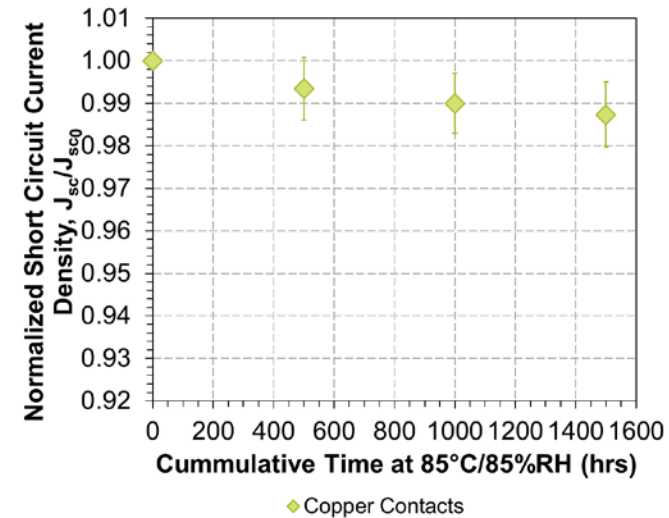
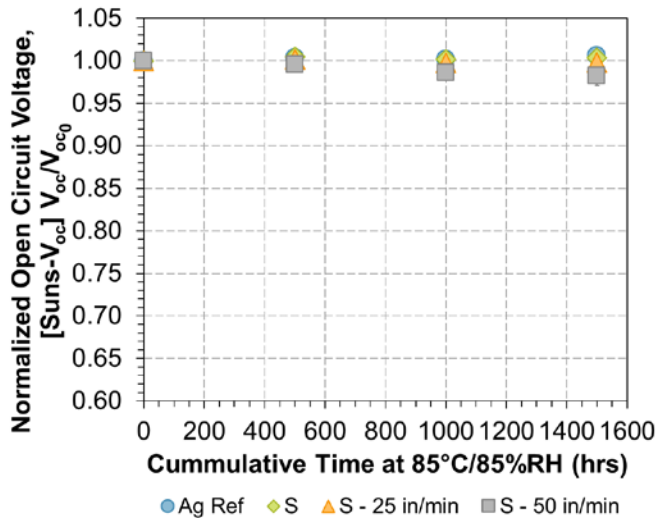


Yellowing of encapsulant for all (including silver contact) samples observed over time.

# Improved paste Cu-printed cells in a minimodule: Minimodules degrade 3.5% relative after 1000h Damp Heat Test



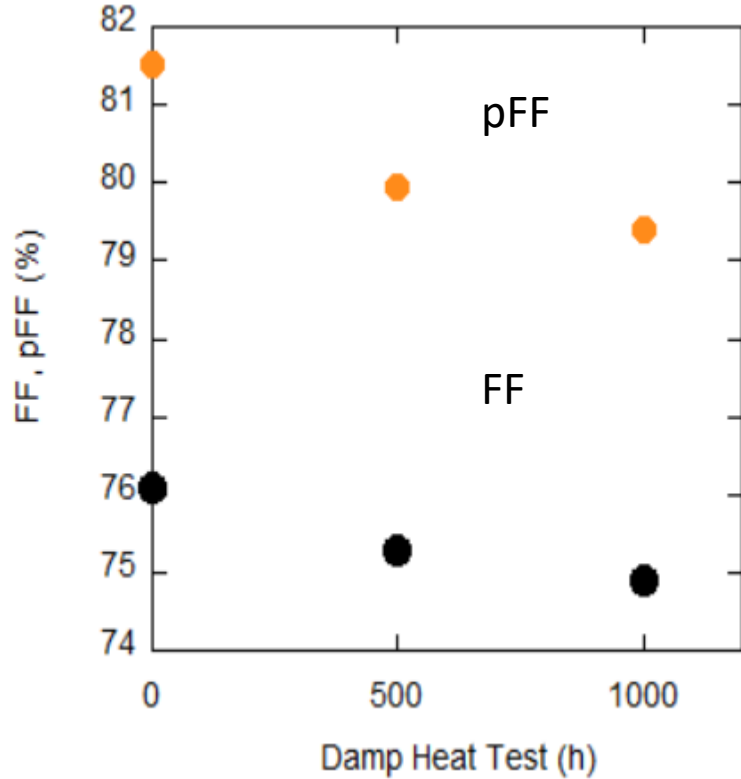
Efficiency dropped by 3.5% relative in 1000h DHT



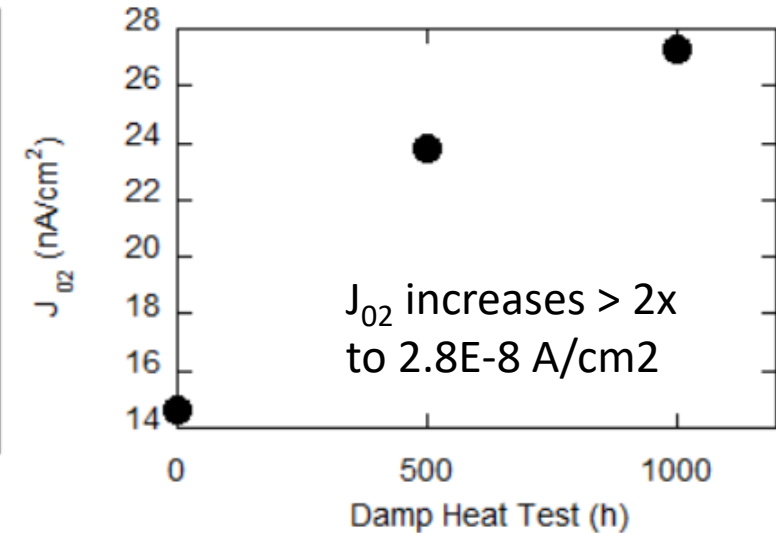
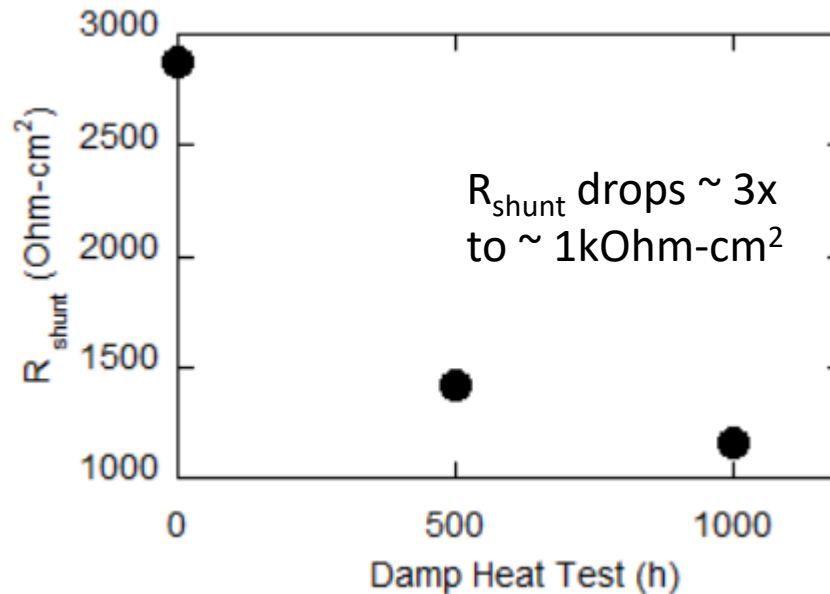
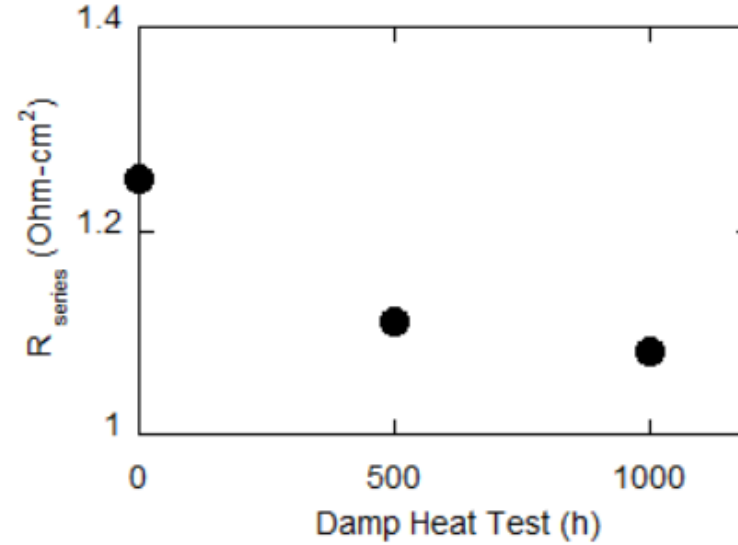
Jsc drops by 0.5 mA/cm<sup>2</sup> (2%)

# Minimodule degradation is governed by Fill-factor change. FF is again controlled mostly by $J_{O_2}$

Both FF and pFF degrade to similar extent (1% - 3% relative):  
FF/pFF ratio is almost constant



$R_{series}$  is  $\sim$  unchanged near 1.2 Ohm-cm<sup>2</sup>



# Conclusions

- ❑ Successful demonstration of large area selective emitter PERC solar cells using Cu fire-through paste with FF ~75% and ~19%
- ❑ Paste chemistry results in oxide-based Cu diffusion barrier, leading to good reliability of the devices: 1000h DHT → 3.5% efficiency drop. The additional series resistance still needs to be lowered.
- ❑ Printed and fired cell performance is governed mostly by pFF, especially  $J_{02}$ ; same for DHT degradation.
- ❑ Further improvement in printing and firing optimization for lower series resistance and higher FF.

**Acknowledgement:** This work was authored in part by the National Renewable Energy Laboratory, operated by Alliance for Sustainable Energy, LLC, for the **U.S. Department of Energy (DOE)** under Contract No. DE-AC36-08GO28308. Funding provided by U.S. Department of Energy Office of Energy Efficiency and Renewable Energy Solar Energy Technologies Office, DuraMat Open Call grant SUB-2022-10382. The views expressed in the article do not necessarily represent the views of the DOE or the U.S. Government. The U.S. Government retains and the publisher, by accepting the article for publication, acknowledges that the U.S. Government retains a nonexclusive, paid-up, irrevocable, worldwide license to publish or reproduce the published form of this work, or allow others to do so, for U.S. Government purposes.

Suchismita Mitra would like to thank the **Fulbright Commission**, the Institute of International Education (IIE) and the United States-India Educational Foundation (USIEF) for awarding the Fulbright Nehru Post-doctoral Fellowship.