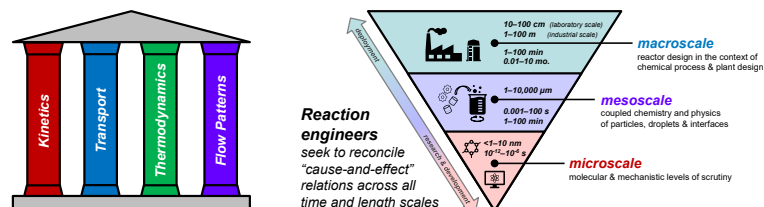


Electrochemical reaction engineering: a lost (and found) art

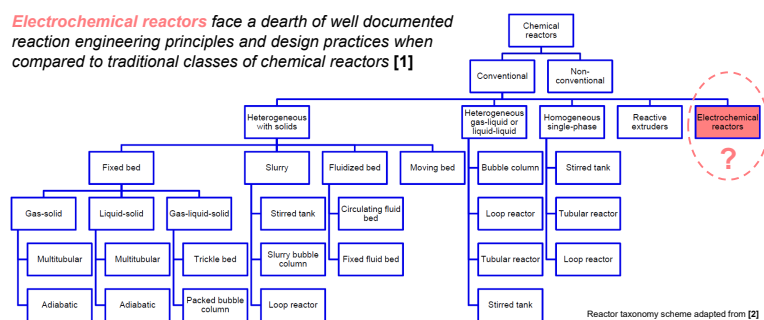
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What is reaction engineering?



Reactor taxonomy

Electrochemical reactors face a dearth of well documented reaction engineering principles and design practices when compared to traditional classes of chemical reactors [1]



Applying chemical engineering fundamentals

Mass balance

$$\left(\text{rate of mass input} \right) - \left(\text{rate of mass output} \right) + \left(\text{rate of mass production} \right) = \left(\text{rate of mass accumulation} \right)$$

$$\frac{dm_j}{dt} = \Delta\Phi_j + M_j R_j V + \frac{M_j I (FE)_{\text{overall}}}{n_j F}$$

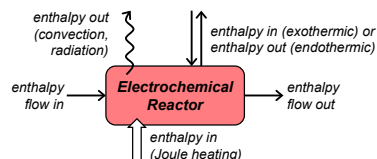
- m_j = mass of species j in the system
- $\Delta\Phi_j$ = net input of j into the system
- M_j = molar mass of j
- R_j = net mass rate of production of j per unit volume V by non-electrochemical reaction
- $\frac{M_j I (FE)_{\text{overall}}}{n_j F}$ = net mass rate of production of j by electrochemical reaction

Definitions applicable to any volume V of interest, such as a single electrode, a single electrochemical reactor, a reactor plus a separator, or a complete process. [1]

Energy balance

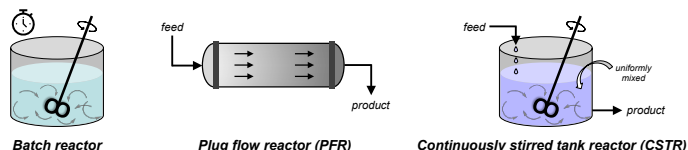
$$\left(\text{accumulation of thermal energy} \right) = \left(\text{enthalpy flow into the reactor} \right) - \left(\text{enthalpy flow out of the reactor} \right)$$

$$\sum m_j C_{p,j} \frac{dT}{dt} = I^2 R_e - \sum R_j \Delta H_j + \sum W_j C_{p,j} [T_i - T] - Q_L$$



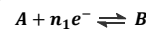
- $\sum m_j C_{p,j} \frac{dT}{dt}$ = accumulation of energy in the system
- $I^2 R_e$ = Joule (i.e., resistive) heat input
- $\sum R_j \Delta H_j$ = enthalpy change due to all reactions
- Q_L = enthalpic heat losses within the system
- $\sum W_j C_{p,j} [T_i - T]$ = enthalpy change from inlet to outlet for all components j with mass flow W_j , inlet temperature T_i and system temperature T [1]

Idealized chemical reactor archetypes



Illustrative design case: electrochemical CSTRs

Design equation for an eCSTR



Apply a mass balance under limiting current density:

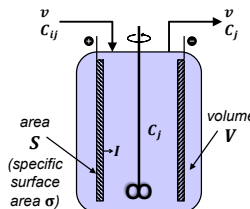
$$v(C_{Ai} - C_A) = \frac{i_1 S}{n_1 F}$$

$$\tau = \frac{V}{v} \quad \begin{matrix} \text{residence} \\ \text{time } \tau \end{matrix}$$

$$C_{Ai} - C_A = \frac{\sigma i_1}{n_1 F}$$

$$i_1 = i_L = n_1 F k_{LA} C_A$$

$$C_{Ai} - C_A = \sigma \tau k_{LA} C_A$$



Finally, solve for the exit concentration C_A and the fractional conversion X_A :

$$\frac{C_A}{C_{Ai}} = \frac{1}{1 + \sigma \tau k_{LA}}$$

$$X_A = 1 - \frac{C_A}{C_{Ai}} = \frac{\sigma \tau k_{LA}}{1 + \sigma \tau k_{LA}}$$

Three important reactor parameters influence the performance of an eCSTR:

- Specific electrode area σ
- Residence time τ
- Mass transfer coefficient of A, k_{LA}

Characteristic mixing timescales

Ideal mixing is achieved when the mixing time t_c is much smaller than the residence time τ [1]

Electrolyte recirculation time

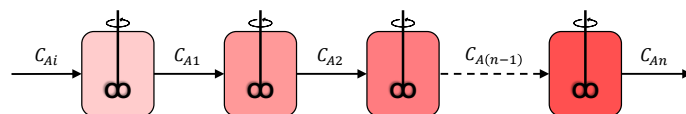
$$t_c = \frac{T_c d_v^2}{n_i d_i^2}$$

Ideal mixing criterion

$$\tau > \frac{100 d_v^2}{n_i d_i^2}$$

- t_c = electrolyte recirculation (mixing) time
- T_c = impeller coefficient (= 1 for turbine type)
- d_v = inner diameter of vessel
- d_i = outer diameter of impeller
- n_i = rotational speed of impeller

Cascades of eCSTRs



For Tafel reactions occurring in equal-size eCSTRs and operating at identical electrode potentials:

$$\frac{C_{An}}{C_{A(n-1)}} = \frac{1}{\left(1 + \frac{\sigma \tau k_f}{1 + Da}\right)} \quad \frac{C_{An}}{C_{Ai}} = \frac{C_{An}}{C_{A(n-1)}} \cdot \frac{C_{A(n-1)}}{C_{A(n-2)}} \cdots \frac{C_{A1}}{C_{Ai}} \quad \frac{C_{An}}{C_{A(n-1)}} = \left(1 + \frac{\sigma \tau k_f}{1 + Da}\right)^{-n}$$

where:

$$Da = \text{Damköhler number} = \frac{\text{surface reaction rate}}{\text{diffusive mass transfer rate}} \Rightarrow Da = \frac{k_{\text{forward}}}{k_{LA}}$$

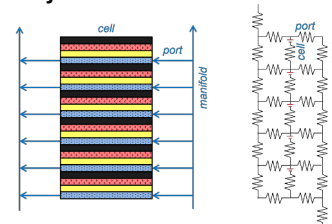
Engineering challenges beyond the laboratory

Stacks are multiple electrochemical cells configured to be electrically in series, but hydraulically in parallel [2]

- Require highly uniform distribution of liquid electrolyte, gaseous reactants and current to reconcile performance with lab cells

Shunt currents may pose integrity, efficiency and corrosion issues within an overall process [2]

- Ionically-conductive route(s) allow bypassing of reactive region
- Highly likely for electrolyte-based heat management strategies



Five-step methodology for electrochemical reactor scale-up

- Perform a single-cell mass balance**
 - Do mass balances inversely track with reactant conversion?
 - Are expected stoichiometries preserved (including e^-)? [2]
- Fundamental electrochemical measurements**
 - Validate thermodynamics (three-electrode cell, coulometry)
 - Measure intrinsic kinetics (rotating ring-disc electrode)
 - Propose and quantify a complete reaction network
 - Evaluate the adiabatic temperature rise (crucial for safety!)
- Quantify single-cell performance**
 - What is the per-pass conversion of the primary reactant?
 - What does the polarization curve look like?
 - Incorporate [ohmic losses] + [mass transfer losses] [2]
 - Develop a mathematical model of cell performance
- Validate performance across large-format single cells and miniature stacks**
 - Check for corrosion, particularly at electrode edges! [2]
 - Do product formation rates scale with total electrode area?
 - Develop coupled continuum models to link kinetics, transport phenomena and hydrodynamics of each system
- Model and validate large stack performance**
 - Re-evaluate cell model in an iterated repeat call routine [2]
 - Add shunt current losses and estimate overall efficiency
 - Optimize reactor inputs for a fixed design geometry
 - Current density (and ΔV between end cells)
 - Number of cells (total electrode area)
 - Flow rates and recycle ratios
 - Coolant flow rates (heat exchange requirements)