

# High-fidelity simulations of supercritical CO<sub>2</sub> based oxy-combustion with non-ideal equation of state

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# Power cycle

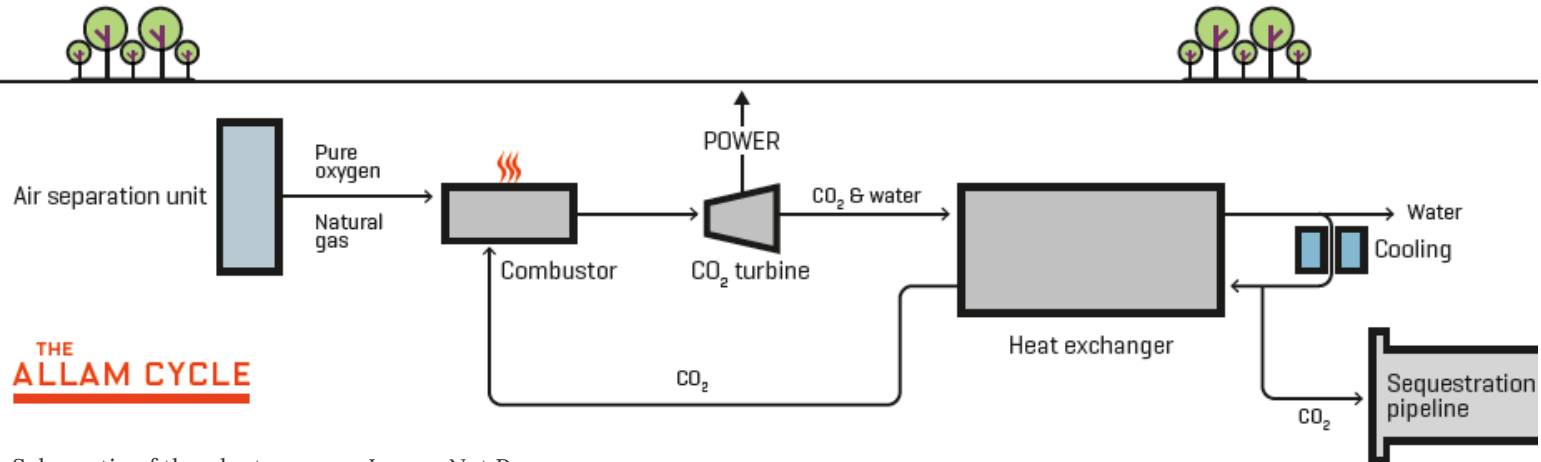
Capture ~100%  
of atmospheric  
emission

## High-temperature oxy-combustion of carbon fuels

- Oxygen is used instead of air, eliminating  $\text{NO}_x$  emissions

## High-pressure $\text{sCO}_2$ as working fluid ( $T_c = 304.13 \text{ K}$ , $P_c = 73.8 \text{ bar}$ )

- Produced  $\text{CO}_2$  can be recirculated within the same cycle loop
- The excess  $\text{CO}_2$  from the cycle can be used for other commercial purposes



Schematic of the plant process. Image: Net Power

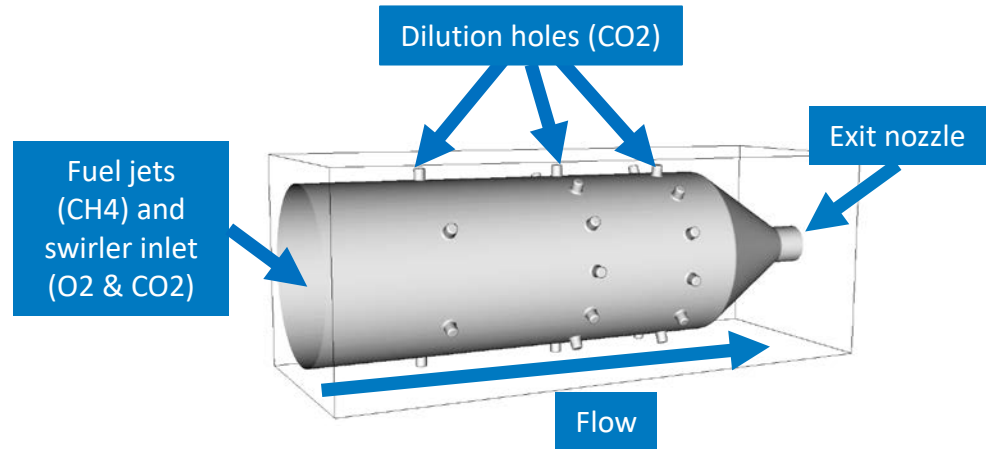
# sCO<sub>2</sub> based oxy-combustor

## sCO<sub>2</sub> combustor operating conditions

- 200–300 bar pressure
- 800–1000 K inlet temperature
- The percentage of sCO<sub>2</sub> should be more than 95% by mass

## Modeling challenges:

- Small scale turbulence
- Complex multi-inlet geometry
- Complex chemical kinetics
- Existing models were developed for lower  $T$ ,  $p$ ,  $Y(\text{CO}_2)$



# 2D case set up

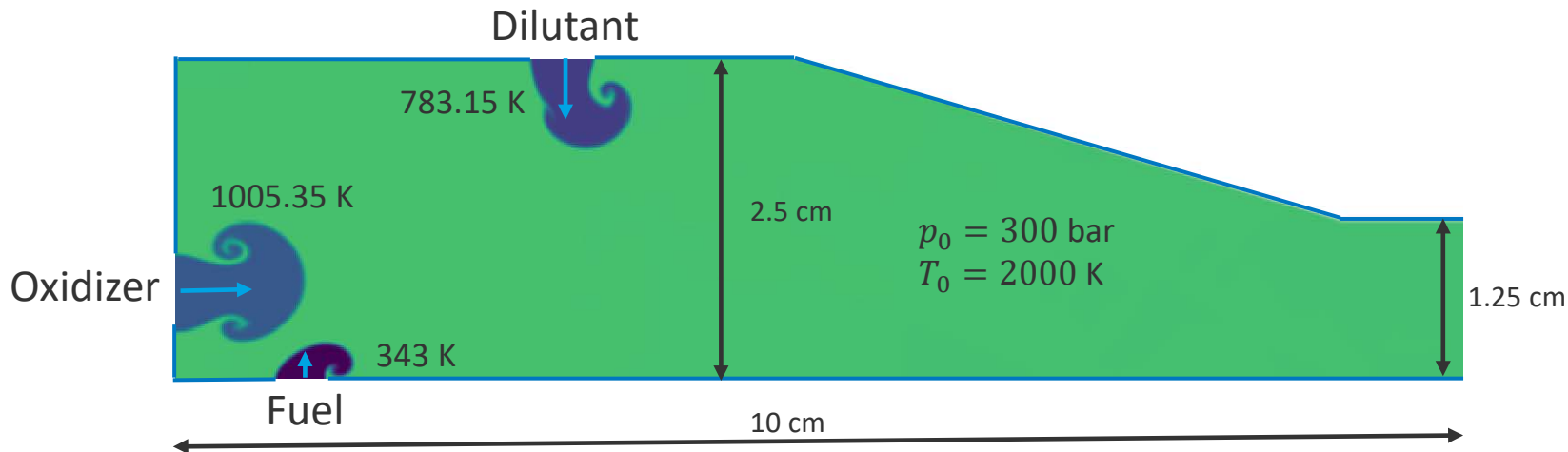
		$T$ [K]	$d$ [cm]	$\dot{m}$ [g/s]
Fuel	$\text{CH}_4$	343.15	0.4	101.2
Oxidizer	$0.8\text{CO}_2 + 0.2\text{O}_2$	1005.35	0.6	449.75
Dilutant	$\text{CO}_2$	783.15	0.5	337.32

Momentum ratio

$$\frac{\rho_{ox} U_{ox}}{\rho_f U_f} = \frac{\dot{m}_{ox} d_f}{\dot{m}_f d_{ox}} = 4$$

Equivalence ratio

$$\phi = \frac{1}{(F/O)_{st}} \frac{\dot{m}_f}{\dot{m}_{ox}} = 0.9$$



# PeleC

## PeleC

- Finite volume compressible solver
- for reacting flow

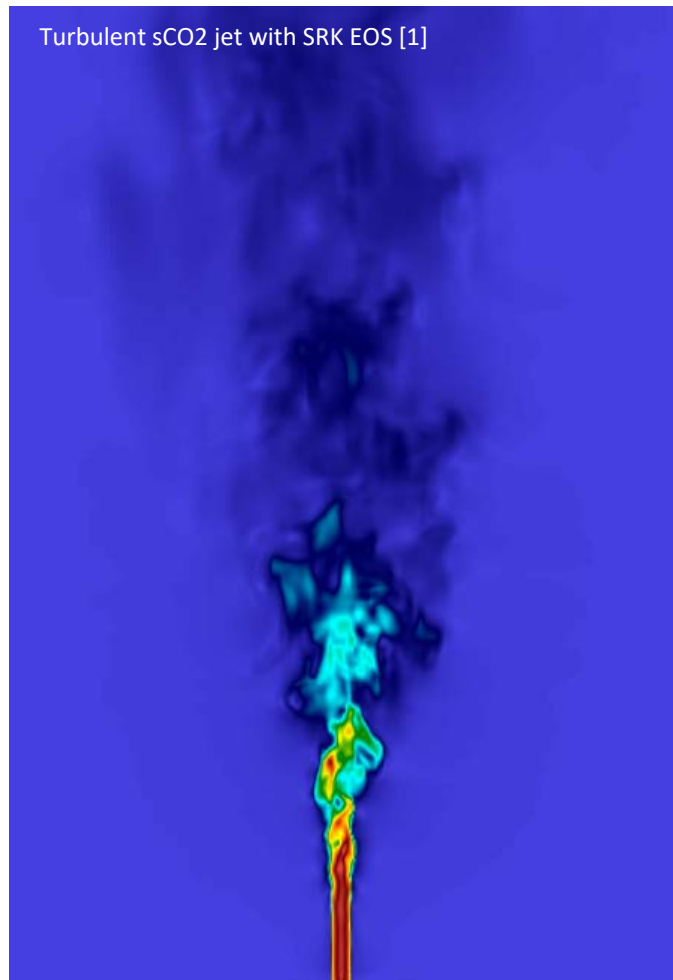
## AMReX

- Adaptive mesh refinement (AMR)

## PelePhysics:

- Models and parameters for thermodynamics
- Transport properties (viscosity, etc)
- Chemical reactions and finite rate chemistry integration (SUNDIALS)
- EOS: ideal gas mixtures and Soave-Redlich-Kwong (SRK)

Turbulent sCO<sub>2</sub> jet with SRK EOS [1]



# Equation of State

## Operating pressure 300 bar

- The supercritical condition for many of the reactants and products
- Intermolecular forces are not negligible
- The ideal gas assumption is not valid

## Ideal gas EoS

$$p = R_u T \sum \frac{Y_k}{W_k} \frac{1}{v}$$

### Assumptions:

- Negligible volume of particles
- No intermolecular forces
- Perfect elastic collisions with no energy loss

## Soave-Redlich-Kwong (SRK) EoS

$$p = R_u T \sum \frac{Y_k}{W_k} \frac{1}{v - b_m} - \frac{a_m}{v(v + b_m)}$$

$$a_m = a_m(T, Y_k) = \sum_{ij} Y_i Y_j \alpha_i \alpha_j; \quad b_m = b_m(Y_k) = \sum_k Y_k b_k$$

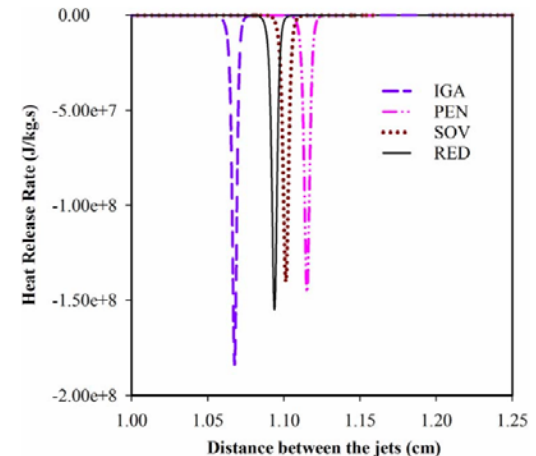
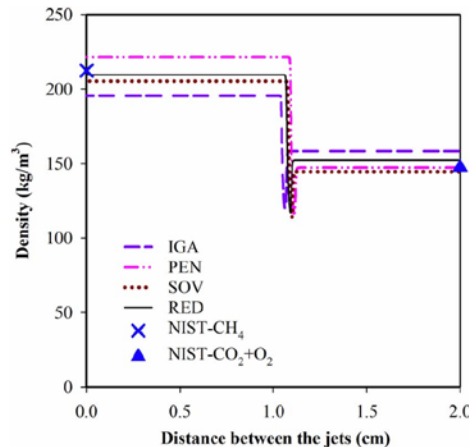
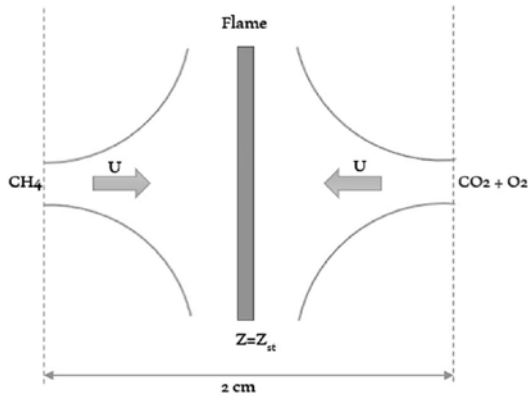
### Accounts for:

- Finite molecular dimensions
- Interactions between the molecules

# Influence of EoS

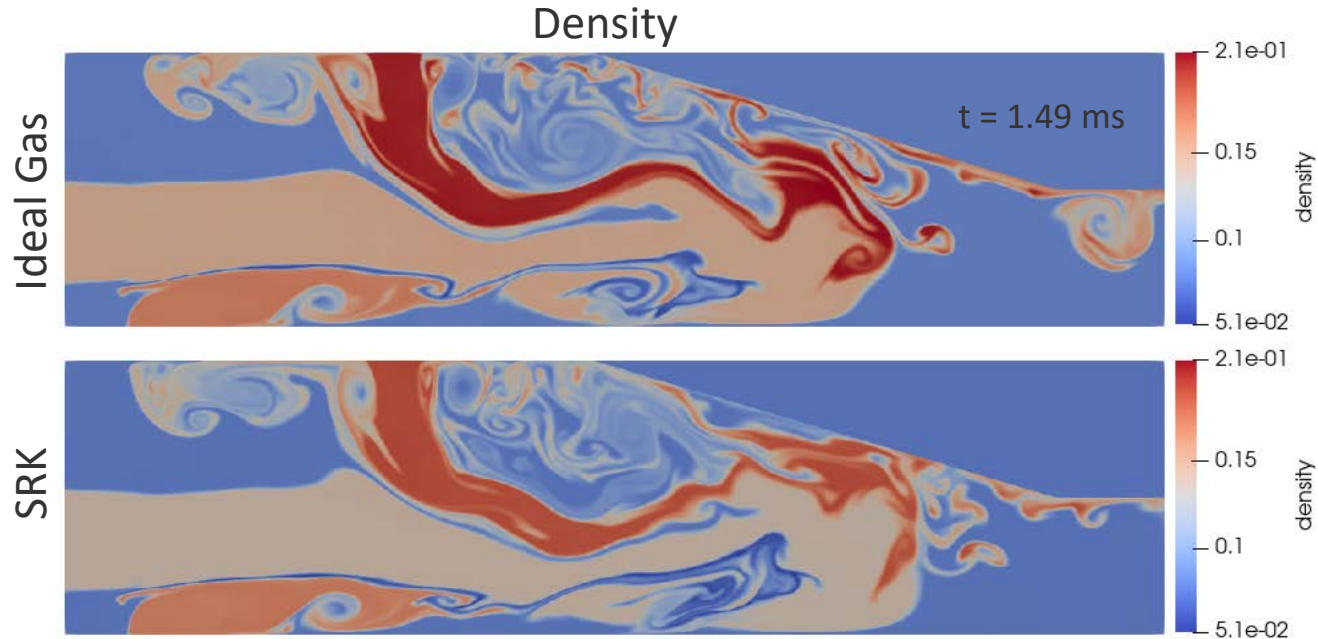
## [1] K.R.V. Manikantachari et al (2020).

- Simulating counter-flow sCO<sub>2</sub> flames
- $P = 300 \text{ atm}$ ,  $T_{ox} = 1000 \text{ K}$ ,  $T_f = 300 \text{ K}$ ,  $Y_{CO_2}$  in oxidizer = 0.96
- Non-ideal effects are significant for fuel jets.  $\sim 12\%$  difference in density
- Choice of EoS significantly influences momentum of jets, flame structure, heat release rate, etc.



# Preliminary results

CFL = 0.2, Mesh 1024x256

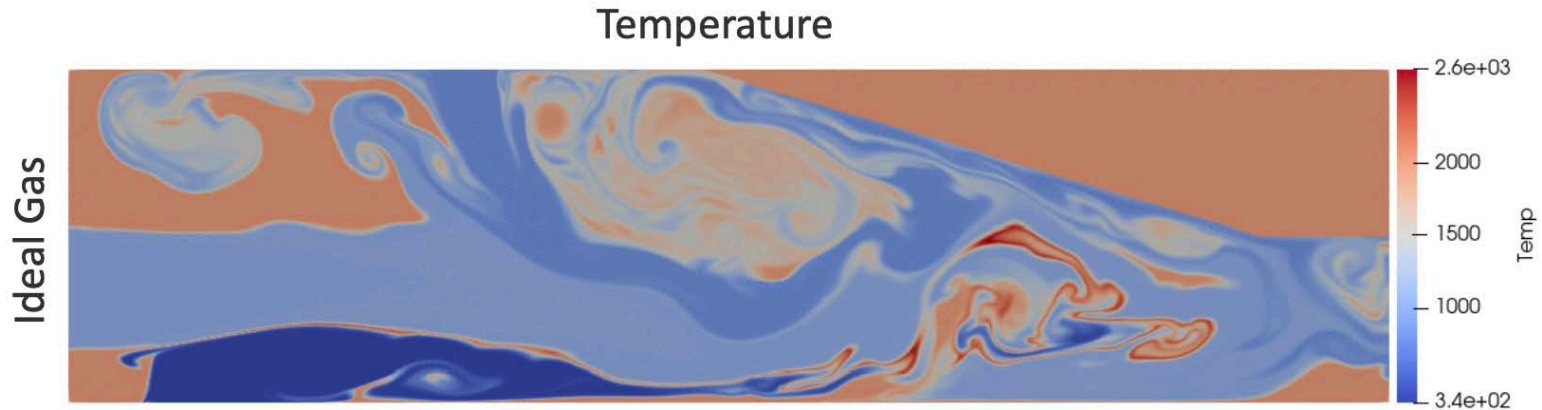


**The EOS is a crucial model for density estimation in a simulation.**



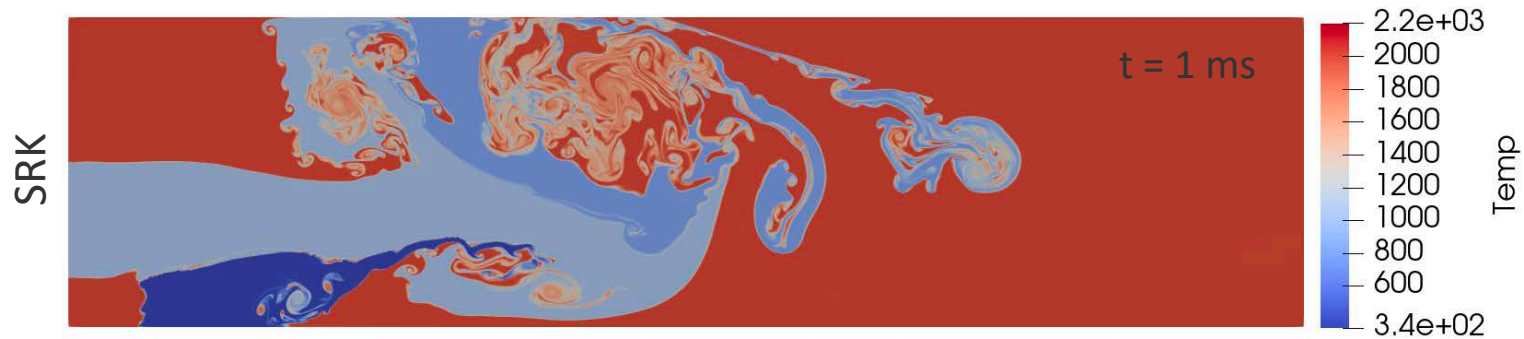
# Preliminary results

- Flame burns at oxygen-CH<sub>4</sub> interface
- Streams interacts with turbulence
- Forms recirculation areas



# Future plans

- **Higher resolution runs**
  - 2048x512 + 3 level AMR (0.61e-5 m)
  - Different % of CH4 in the fuel
  - Exit plane analysis





# Questions?

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[www.nrel.gov](http://www.nrel.gov)

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