

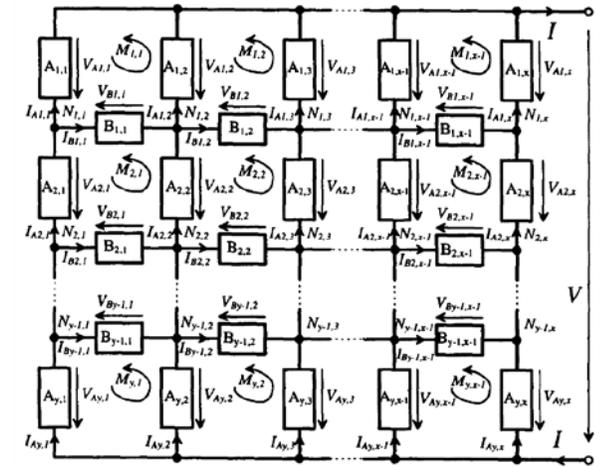
Bifacial PV System Mismatch Loss Estimation & Parameterization

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UNIVERSITAT ROVIRA I VIRGILI

Irradiance
Distribution

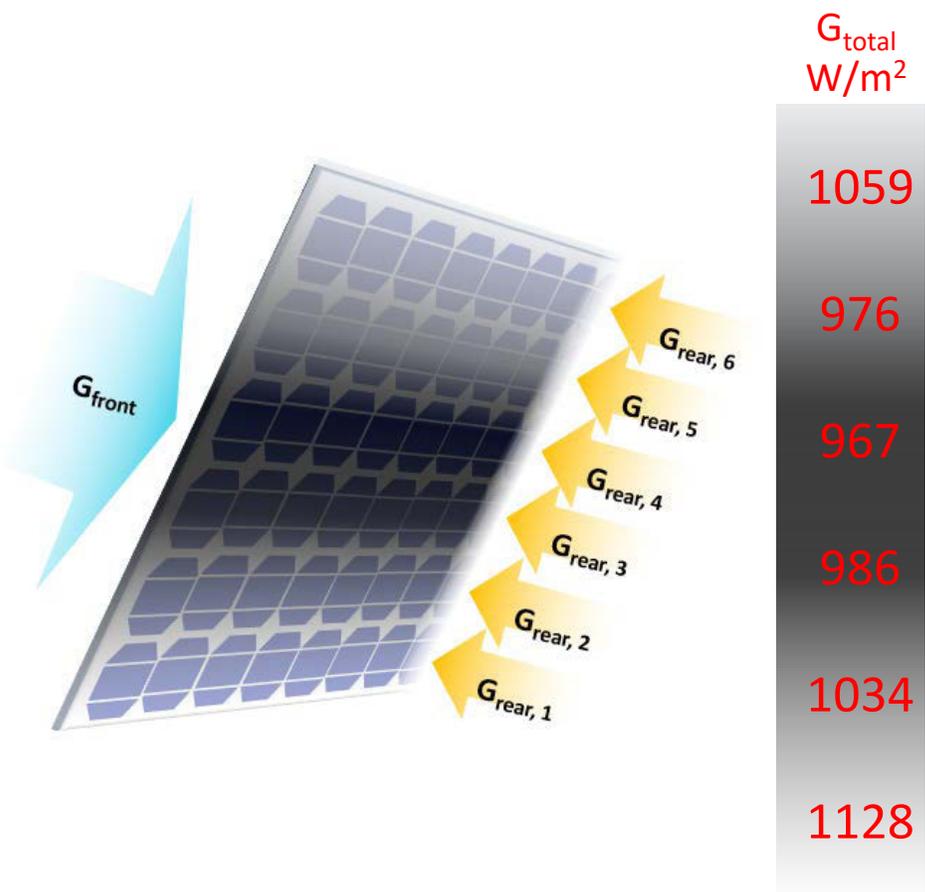


g. 4. General model for a connection of various elements in a photovoltaic assembly. (A: vertical elements, B: horizontal elements, M: meshes, N: nodes).

Power output
*Mismatch loss

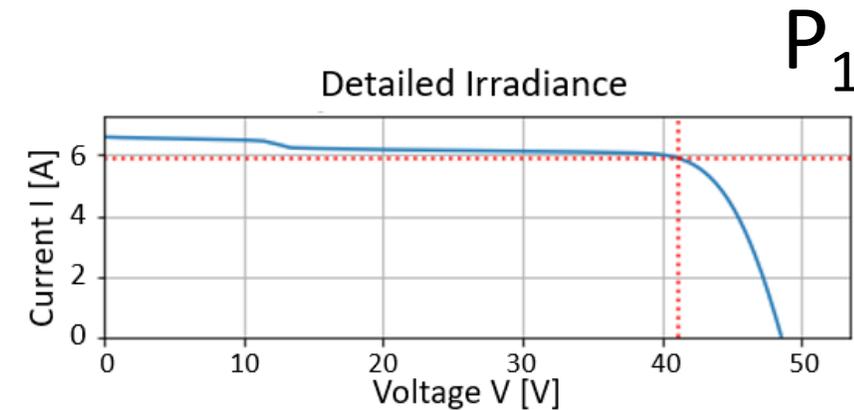
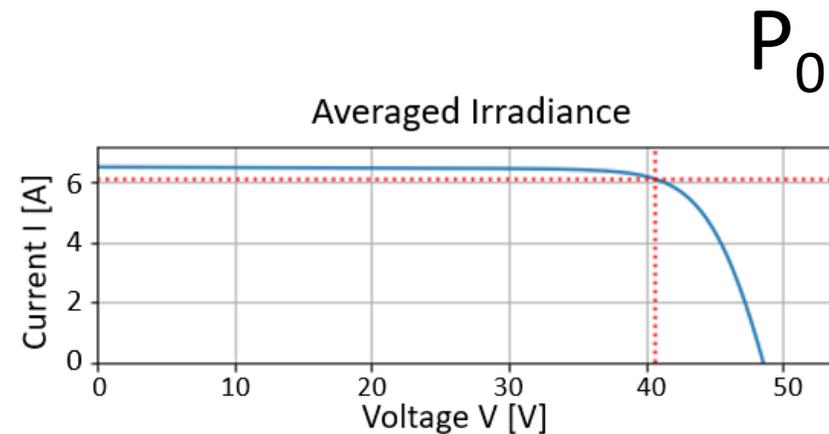
Reduced Order Model

Electrical Mismatch



Averaging Irradiance for the module
 $\sim 1031 \text{ W/m}^2$

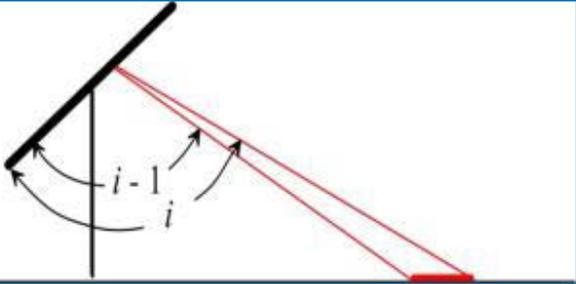
Detailed Irradiance value



Cairo, June 21st at 2 PM

$$L_{DC} = M = 1 - \frac{P_1}{P_0}$$

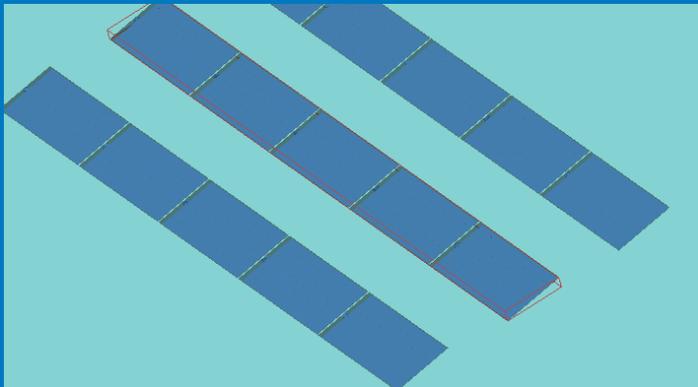
Irradiance Model



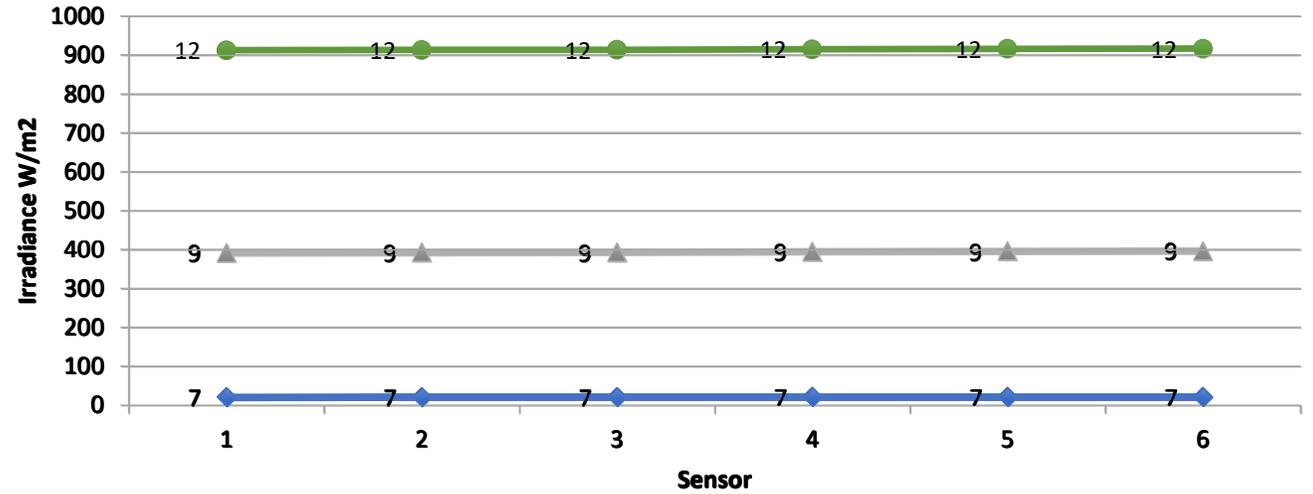
bifacialVF

or

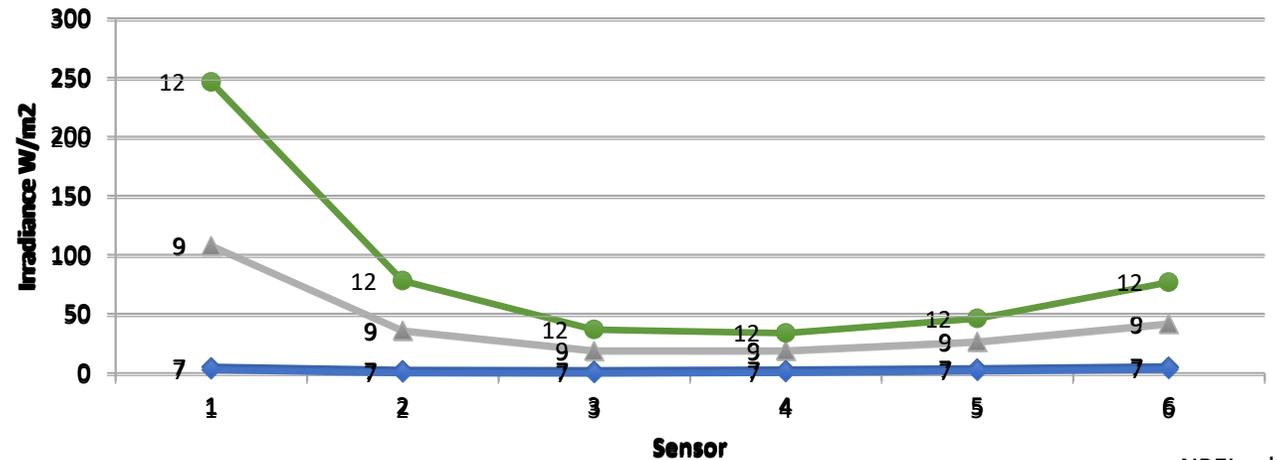
bifacial_radiance



Front Irradiance Spatial Distribution on Spring Equinox

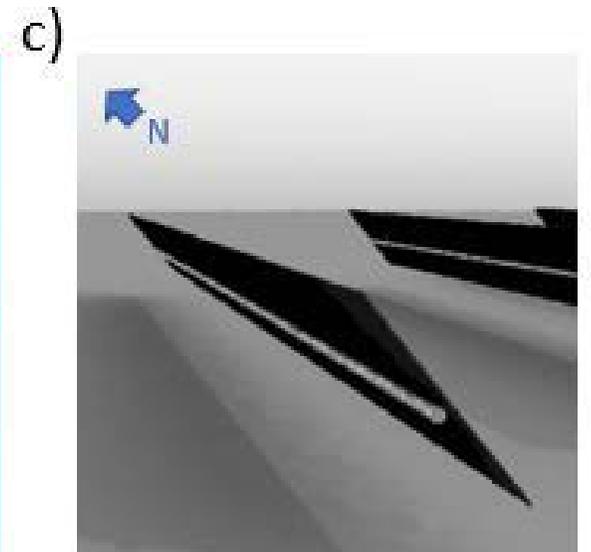
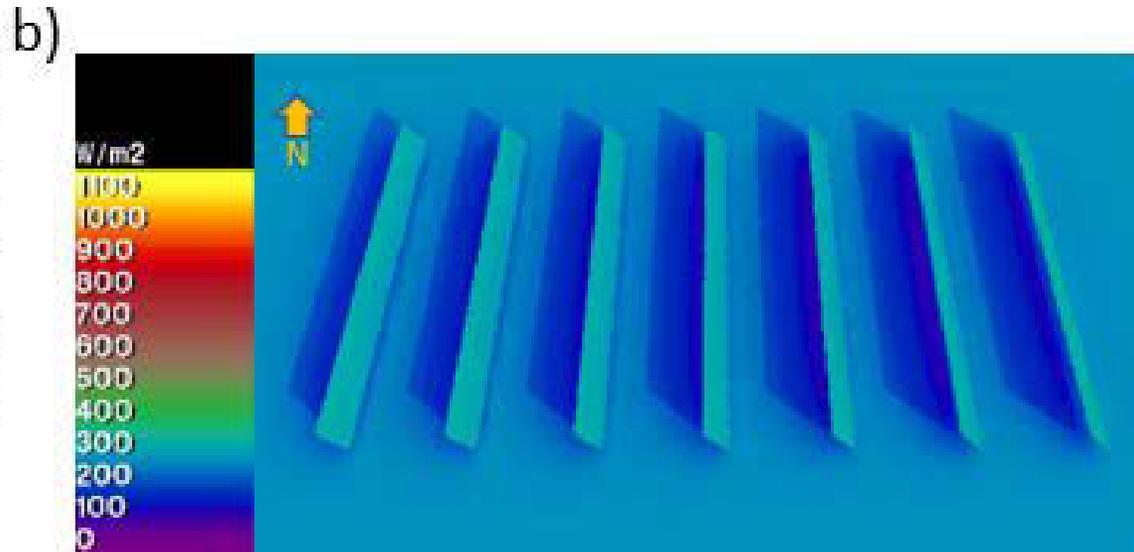
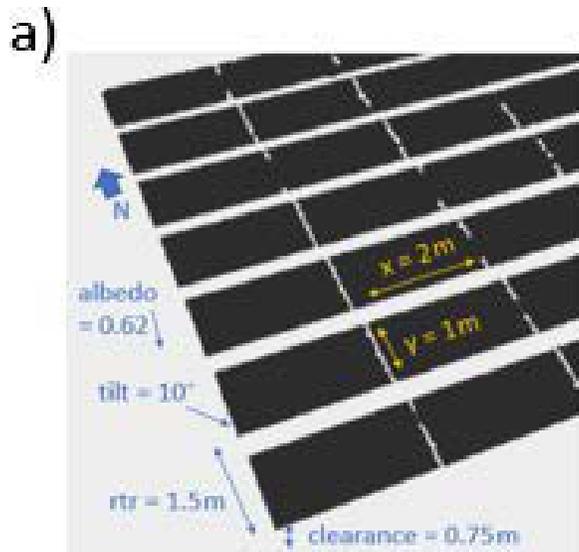


Back Irradiance Spatial Distribution on Spring Equinox



Scenarios

System	Height	Albedo	GCR	Tilt	# modules
a) Rooftop	0.15 – 1 m	0.62	0.67	10°	1-landscape
b) Tracking c) Tracking w TT	1.0 – 2.4 m	0.2	0.33	--	1-portrait

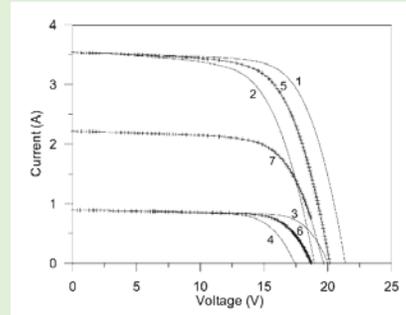


Electrical Model

PV Mismatch
SUNPOWER®

Cell > Module > String > System
2-diode system; Irrad. and
Temperature inputs

Bilinear Interpolation

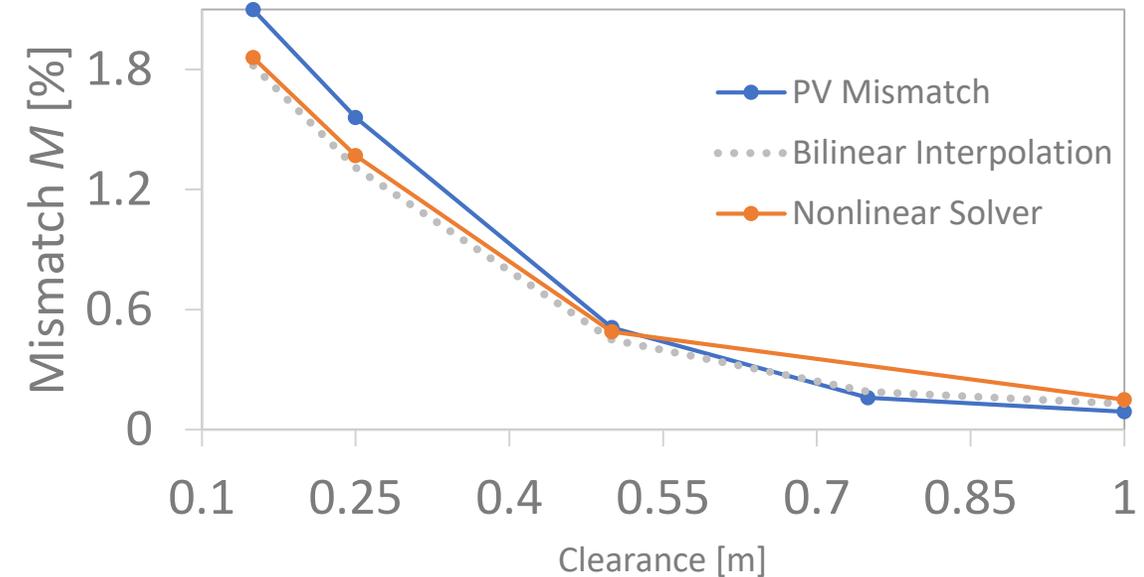


Nonlinear Solver

$$\begin{bmatrix} f_1 \\ \vdots \\ f_{n_s} \\ f_{n_s+1} \end{bmatrix} = \begin{bmatrix} I_{str} - I_{cell_1} - I_{by_1} = 0 \\ \vdots \\ I_{str} - I_{cell_{n_s}} - I_{by_{n_s}} = 0 \\ \sum_{j=1}^{n_s} V_{sub_j} - V_{str} = 0. \end{bmatrix}$$

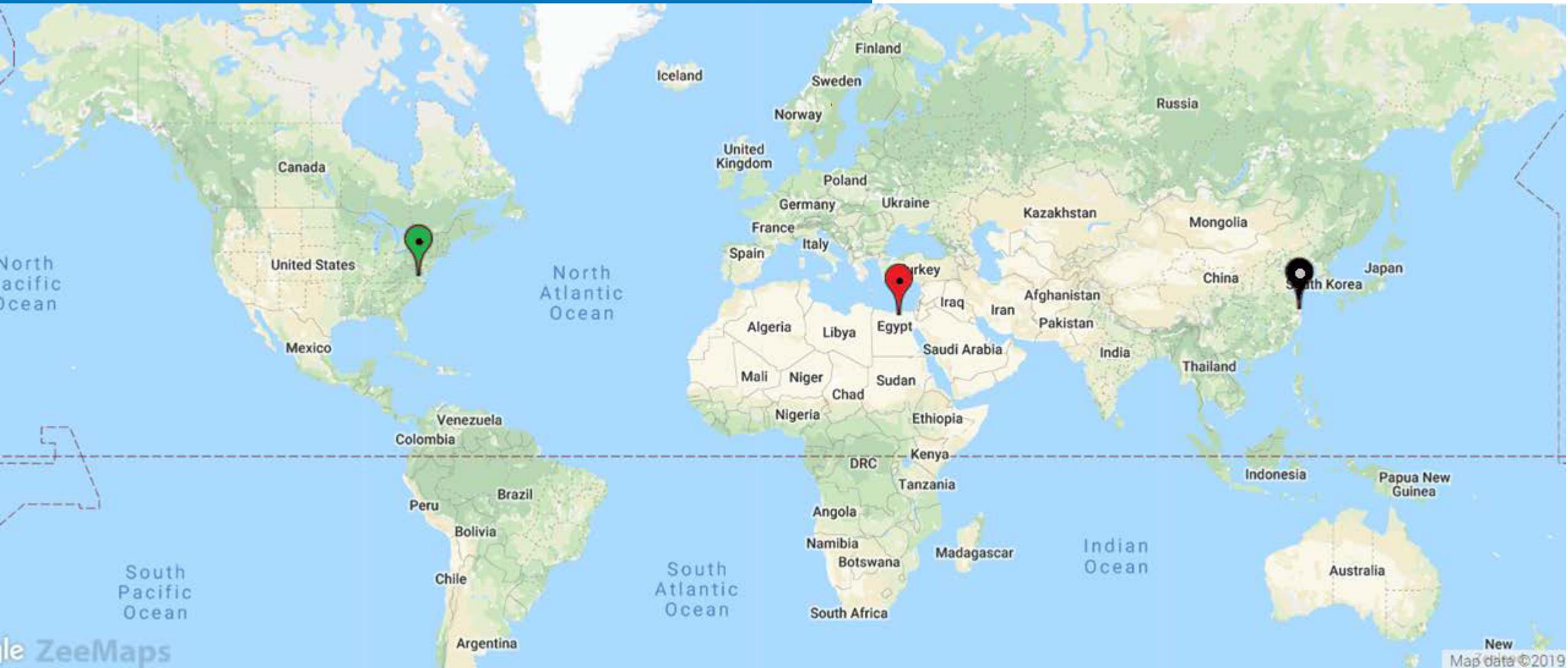
System of n_s+1 equations and n_s+1 unknowns.
Use Nonlinear Newton-Raphson solver

Outcome of calculated mismatch loss % was found to be similar.

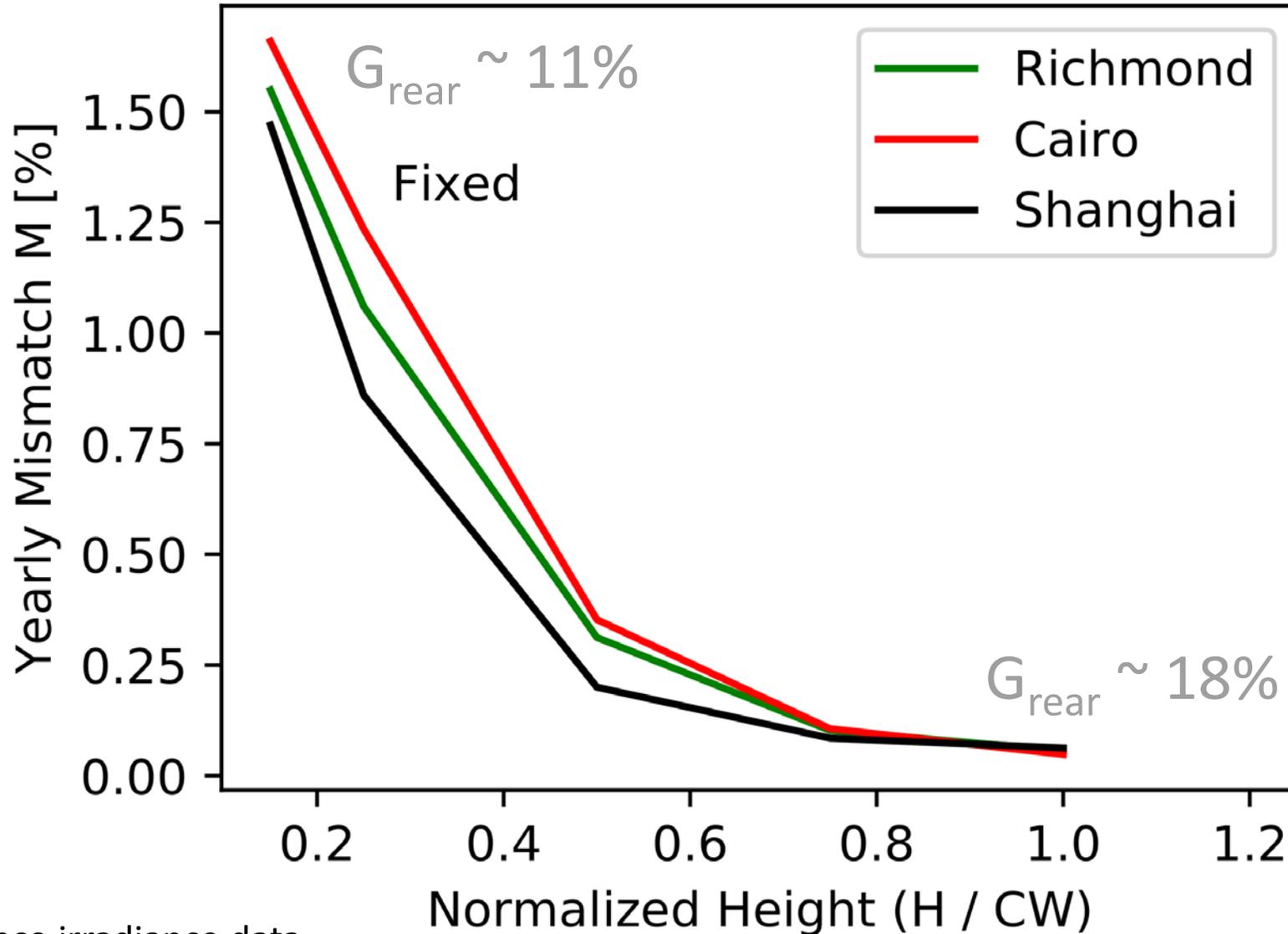


$$M = \left(1 - \frac{\sum_{h=0}^{8760} P_1}{\sum_{h=0}^{8760} P_0} \right) \times 100\%$$

Evaluating climate dependence

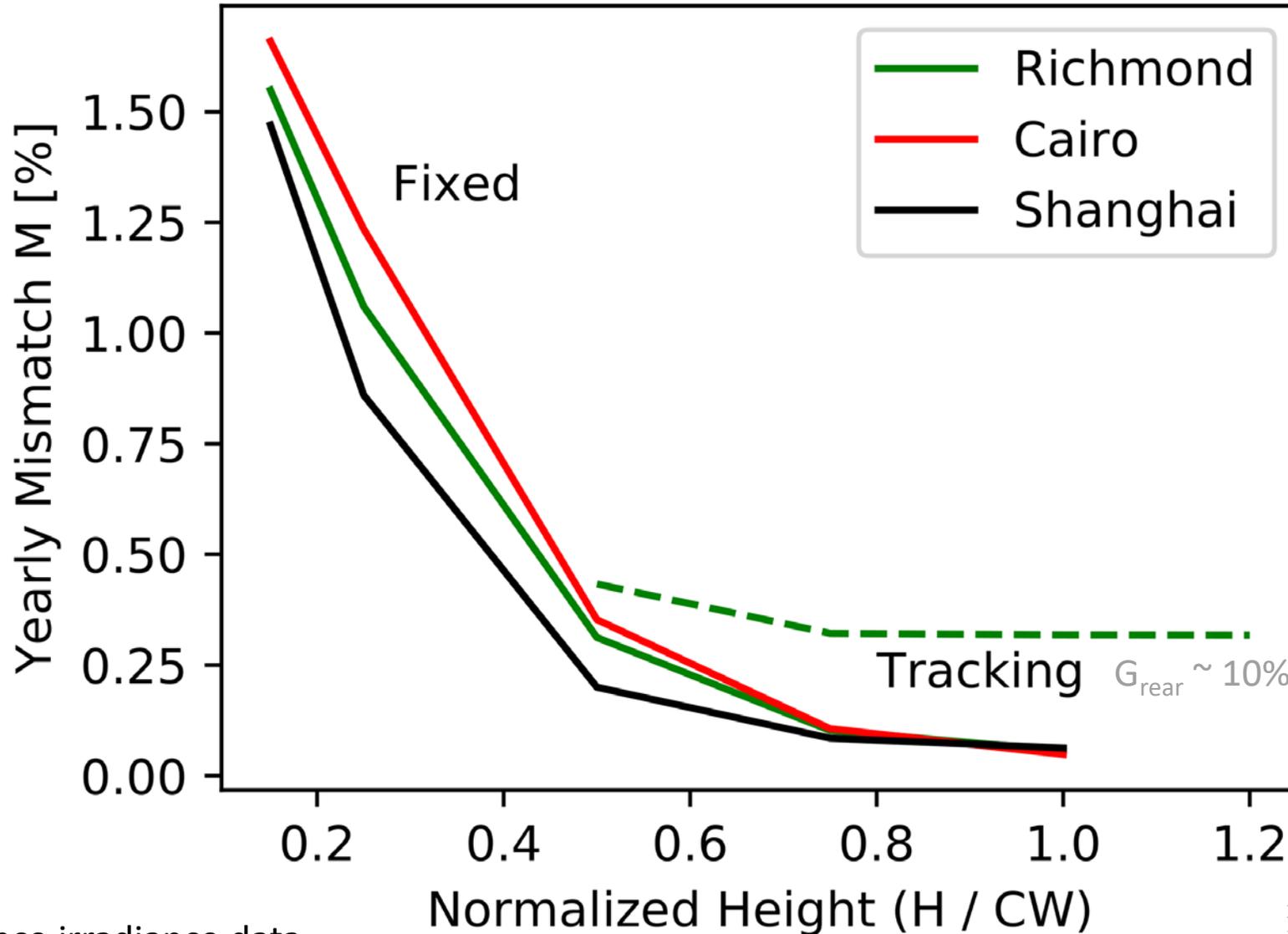


Slight climate dependence for high-albedo rooftop simulations



*bifacial_radiance irradiance data

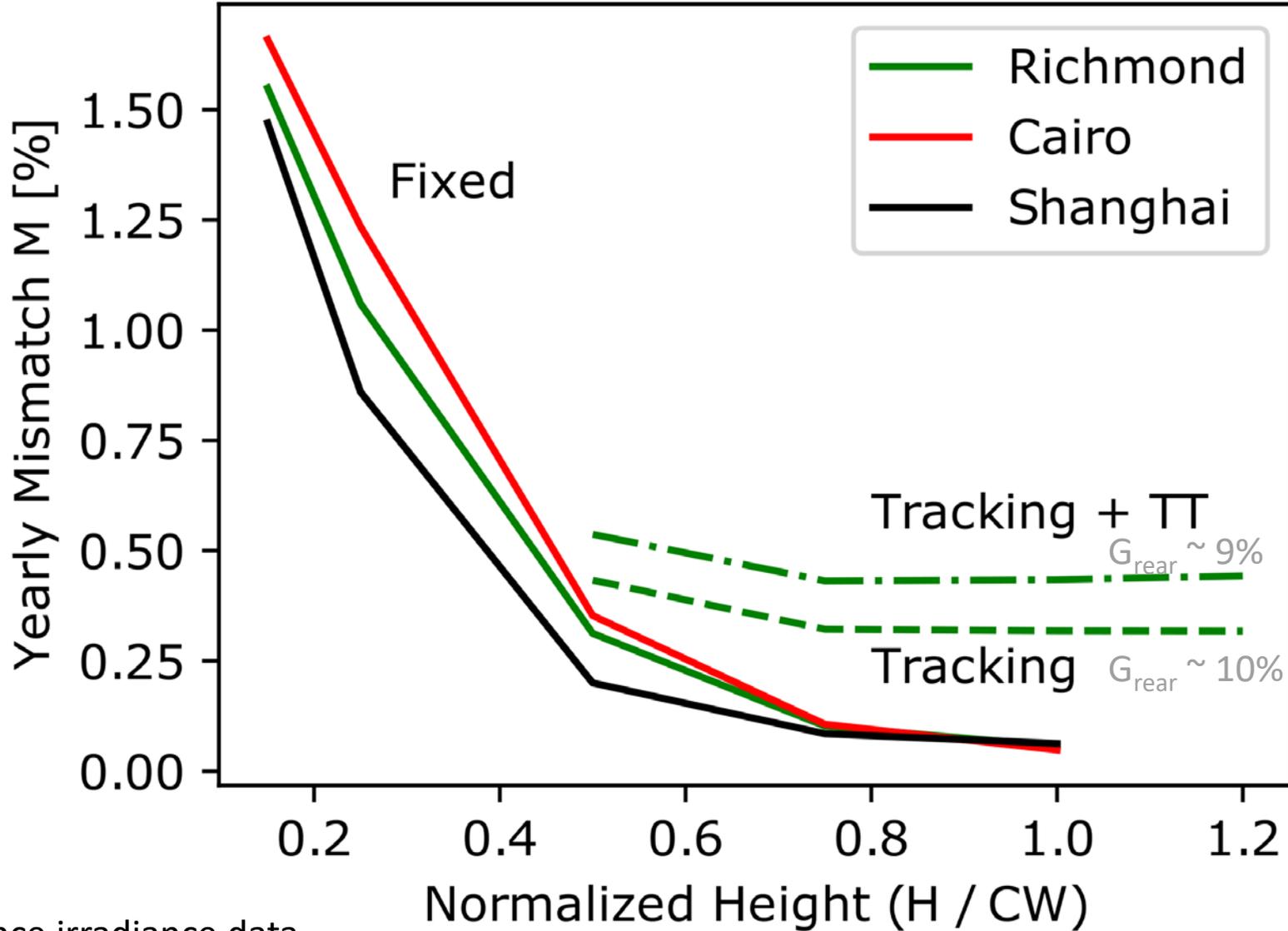
HSAT Mismatch losses are slightly higher



Annual mismatch loss is 0.3%–0.6%, matching the results of McIntosh et al (46th PVSC), which showed values of 0.3%–0.4% under similar conditions

*bifacial_radiance irradiance data

Torque tube increases mismatch by only 0.1%

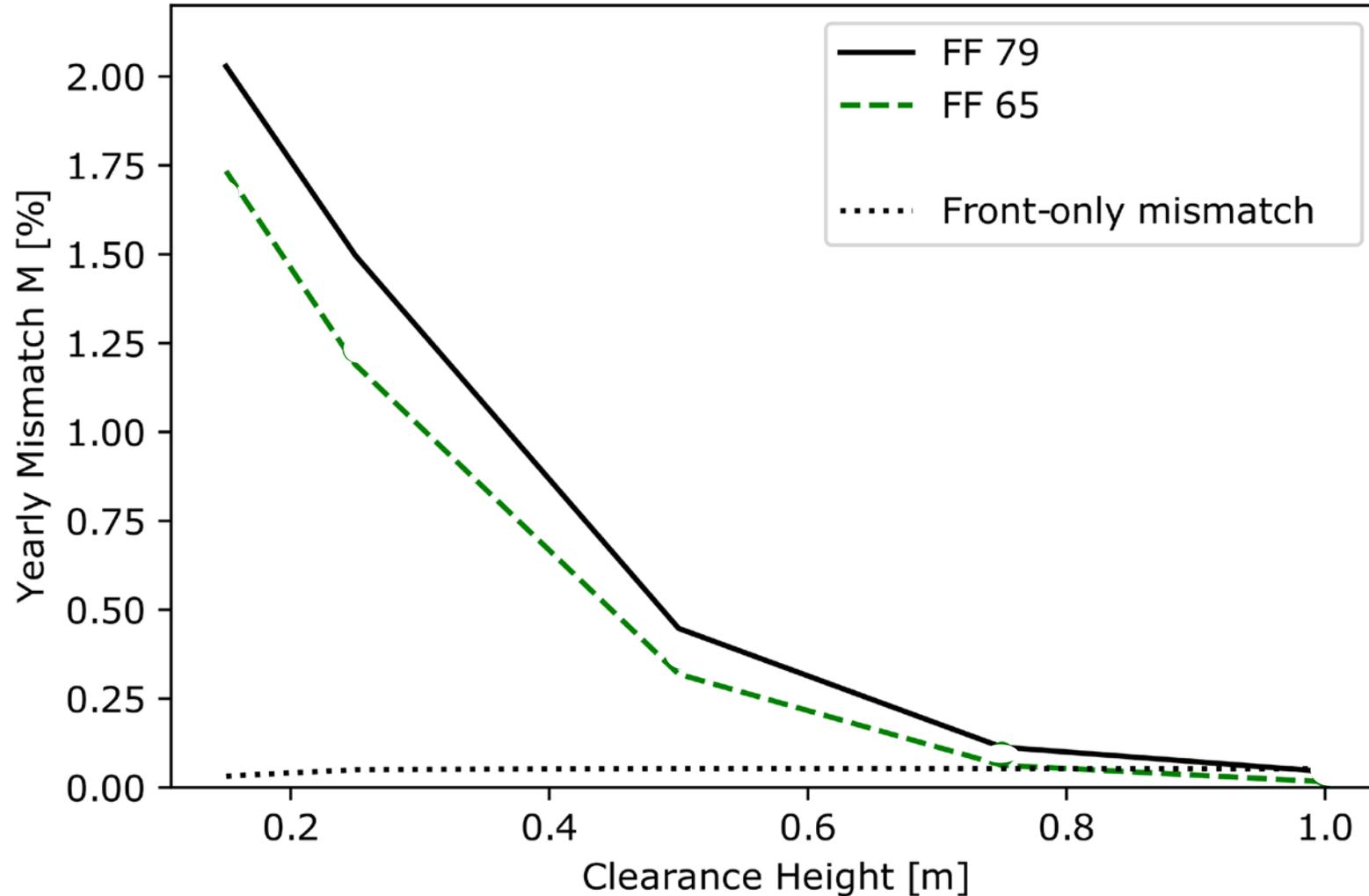


Torque tube:
10 cm diameter, 5 cm from the module (CW=2M), absorptive “black” material

*bifacial_radiance irradiance data

Fill Factor dependency

Richmond: Fill Factor dependence



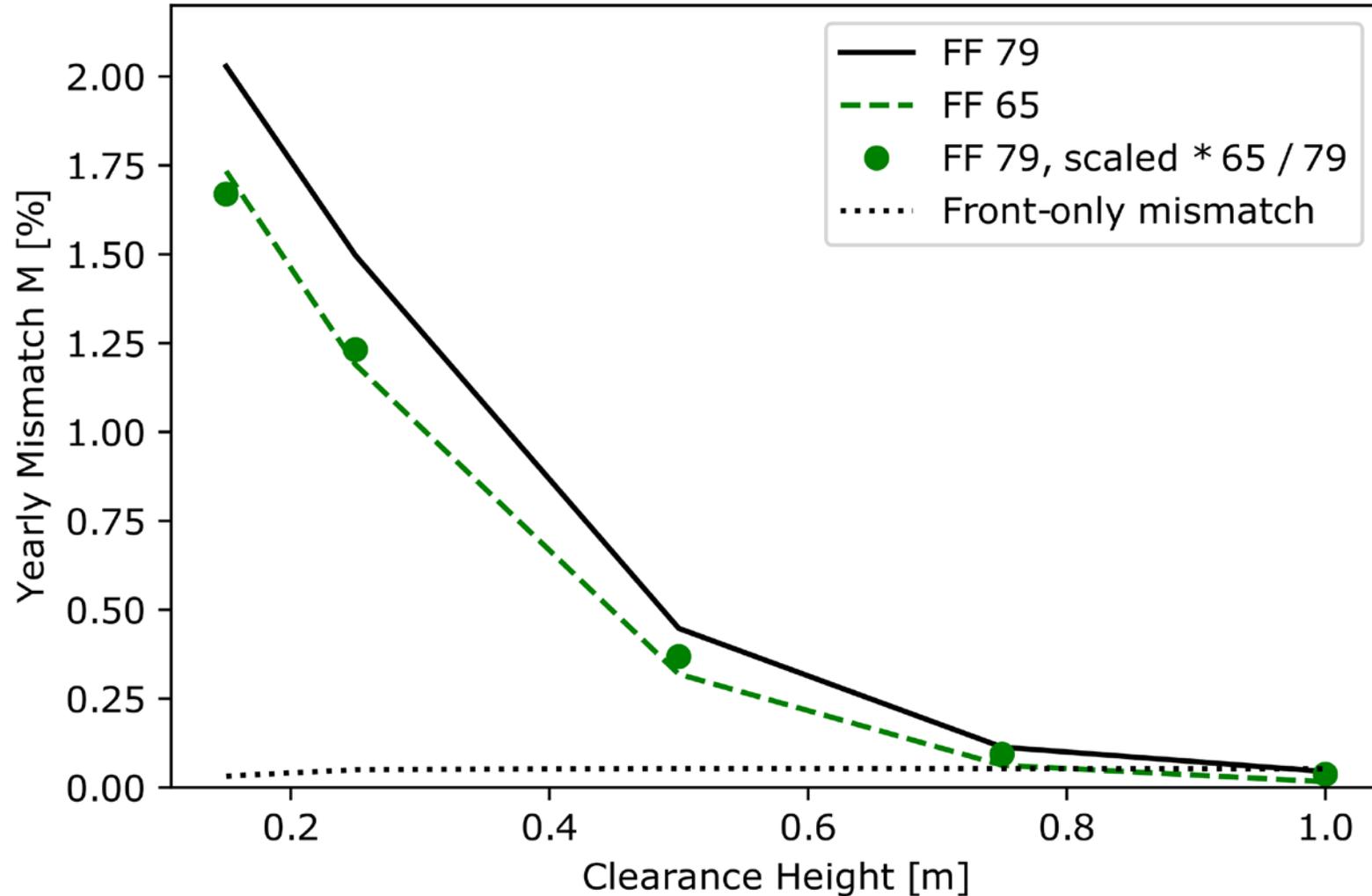
Lower Fill Factor modules are susceptible to reduced mismatch loss

*Fixed tilt cases shown with bifacialVF irradiance data

Fill Factor dependency

$$M[\%]_{FF1} = M[\%]_{FF0} \frac{FF_1}{FF_0}$$

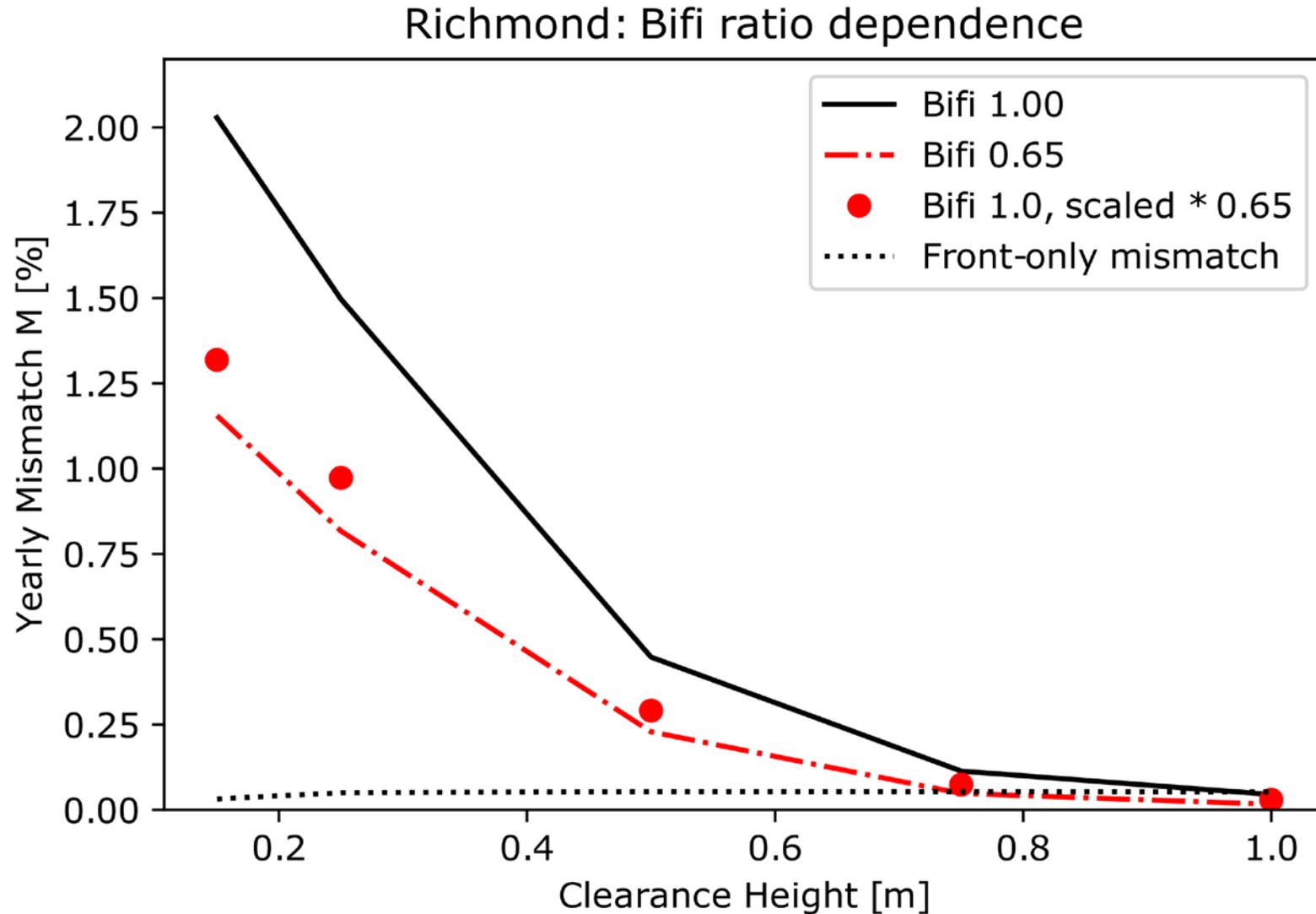
Richmond: Fill Factor dependence



*Fixed tilt cases shown with bifacialVF irradiance data

Bifaciality Factor dependency

$$M[\%]_{\phi_{Bifi,1}} = M[\%]_{\phi_{Bifi,0}} \frac{\phi_{Bifi,1}}{\phi_{Bifi,0}}$$



*Fixed tilt cases shown with bifacialVF irradiance data

Reduced-order model



Reduced Order Model – Irradiance distribution

Mismatch depends on the total irradiance distribution.

Two statistical approaches:

Stdev

$$\sigma [\%] = \frac{1}{\bar{G}_{total}} \sqrt{\frac{\sum (G_{total,i} - \bar{G}_{total})^2}{n-1}} \times 100\%$$

MAD Mean absolute difference

$$\Delta [\%] = \frac{1}{n^2 \bar{G}_{total}} \sum_{i=1}^n \sum_{j=1}^n |G_{total,i} - G_{total,j}| \times 100\%$$

$$G_{total} = G_{front} + \phi_{Bifi} G_{rear}$$

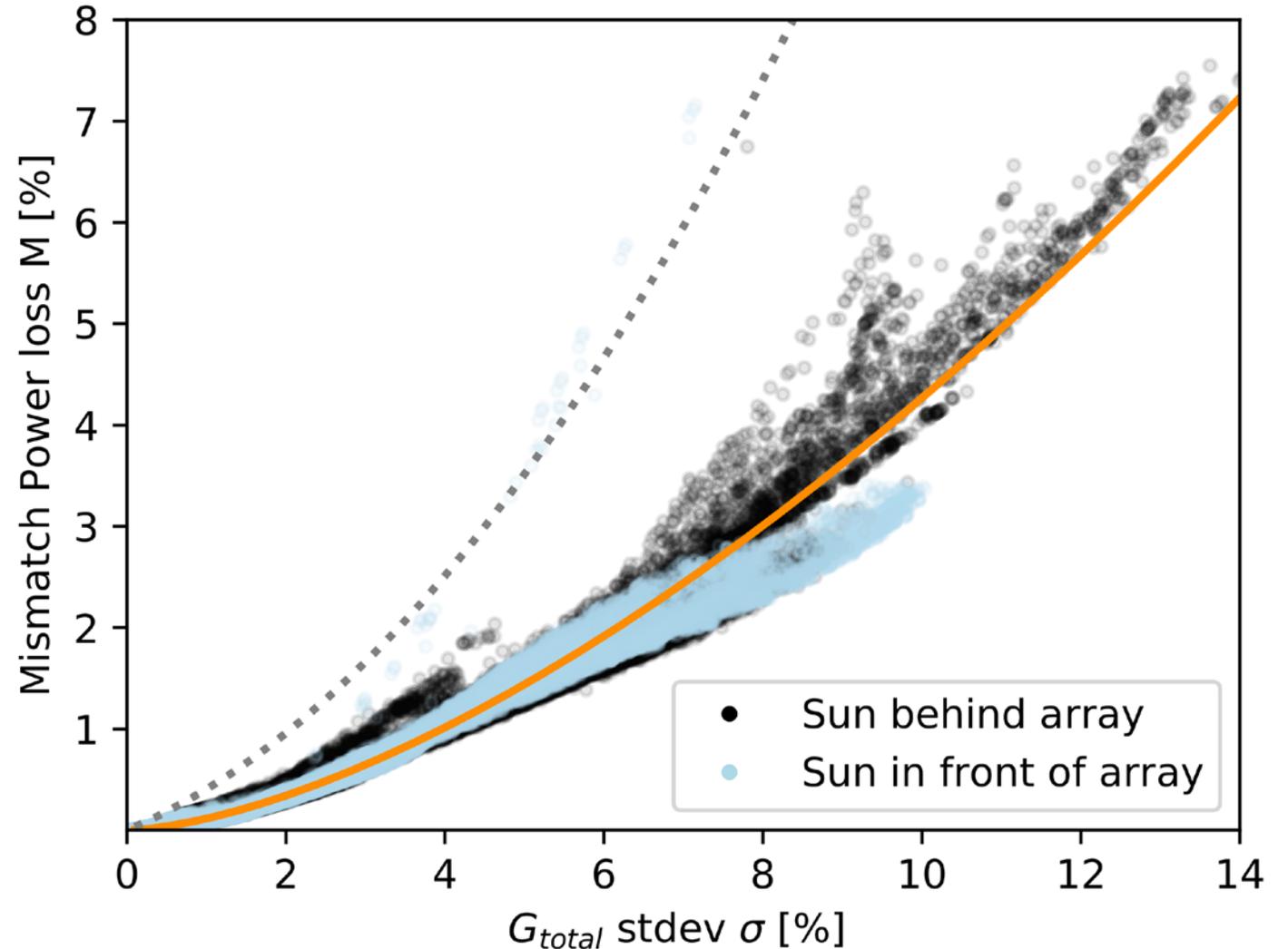
Reduced Order Model – fixed tilt

$$M[\%]_{Fit1} = e^{1.57 * \ln(\sigma[\%]) - 2.2}$$

Janssen et al, «Impact of inhomogeneous irradiance at the rear of bifacial panels on modelled energy yield» 33rd EUPVSEC

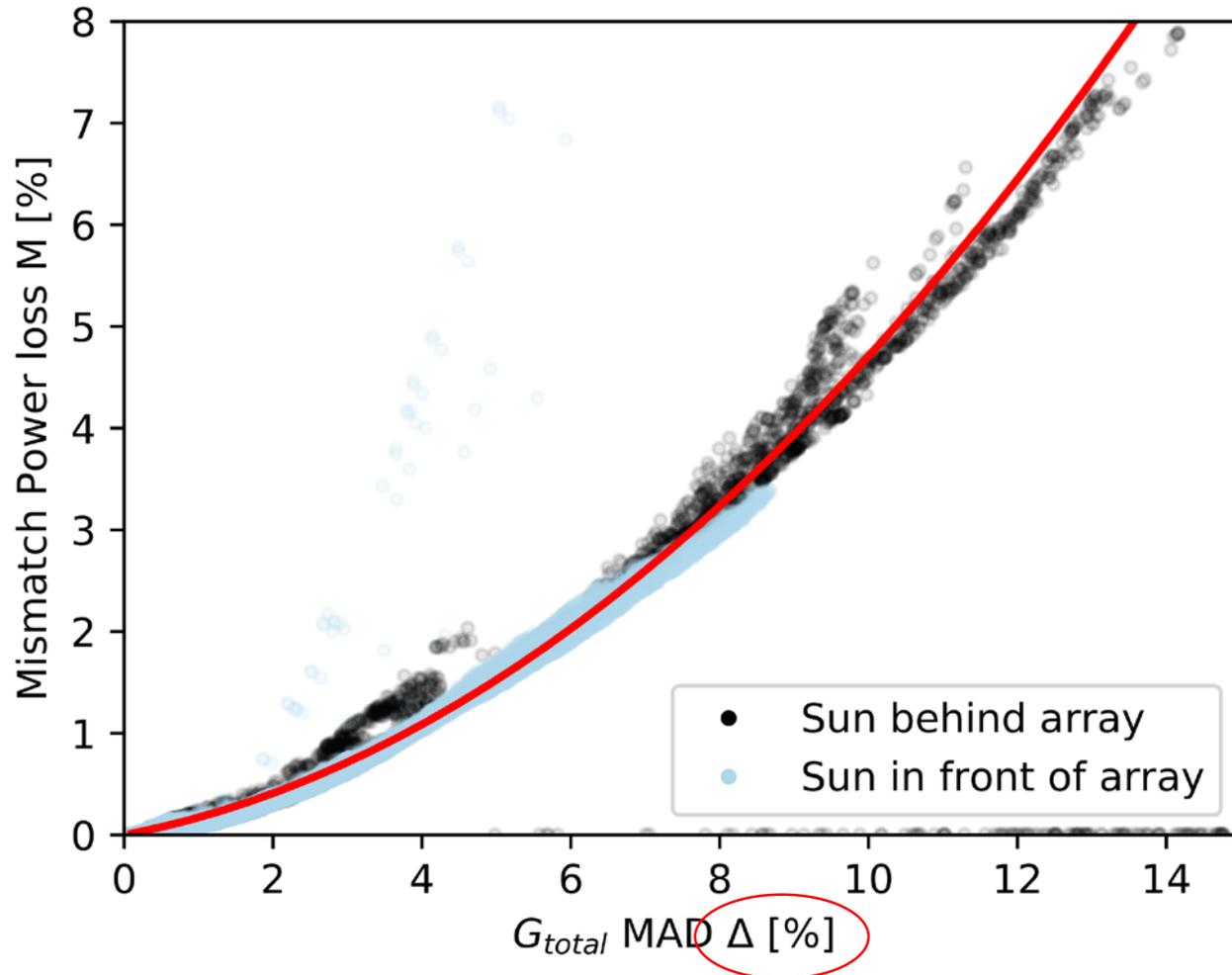
$$M[\%]_{Janssen} = 0.33 \sigma[\%] + 0.0745 \sigma[\%]^2$$

$$G_{total} = G_{front} + \phi_{Bifi} G_{rear}$$



* Fixed tilt results – 130k datapoints

Reduced Order Model: MADs fixed tilt



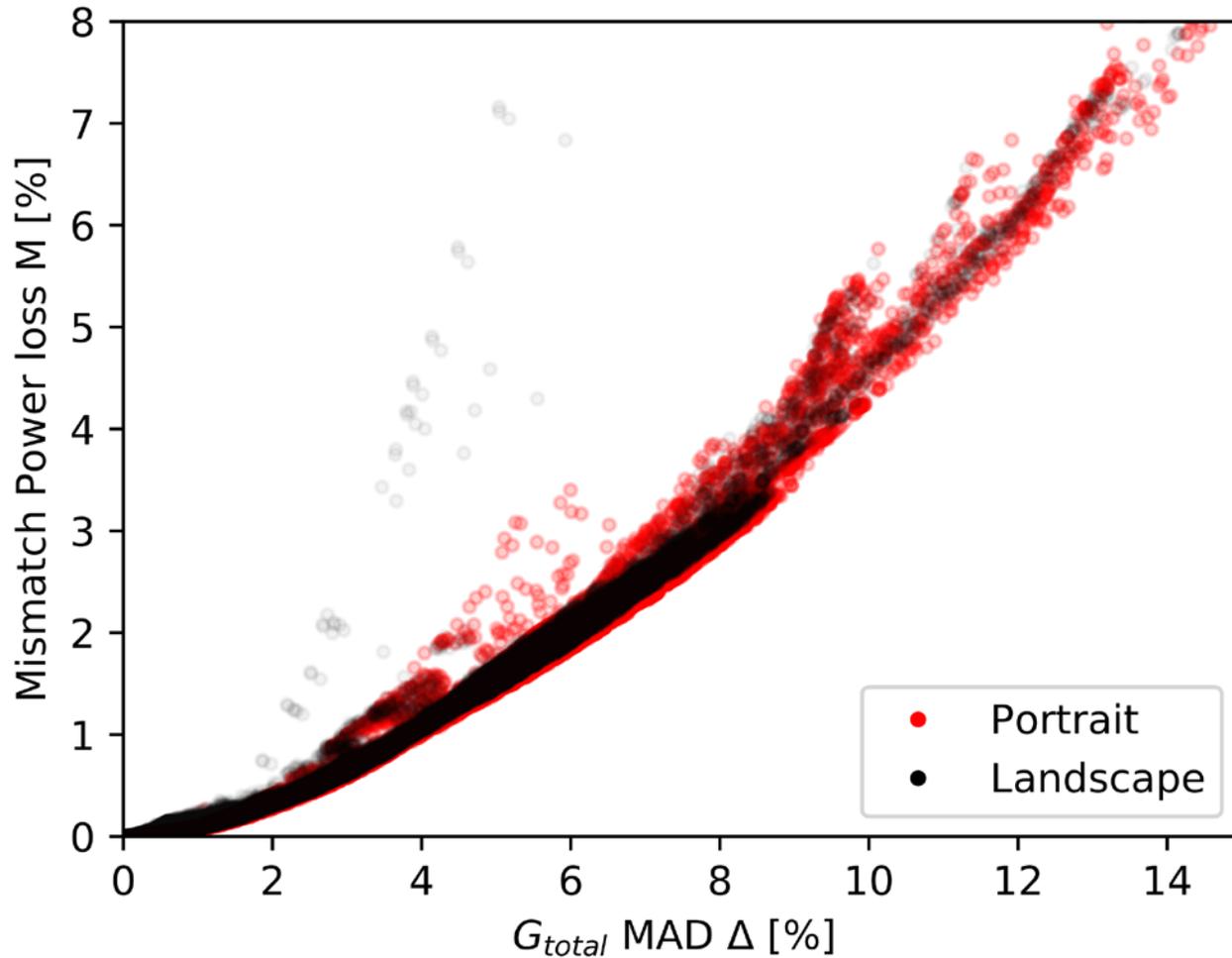
*Tighter distribution by using Δ instead of σ

$$M[\%]_{Fit2} = 0.142 \Delta[\%] + 0.032 \Delta[\%]^2$$

$\Delta = \text{Mean Absolute Difference } (G_{total})$

$$G_{total} = G_{front} + \phi_{Bifi} G_{rear}$$

Orientation of the module



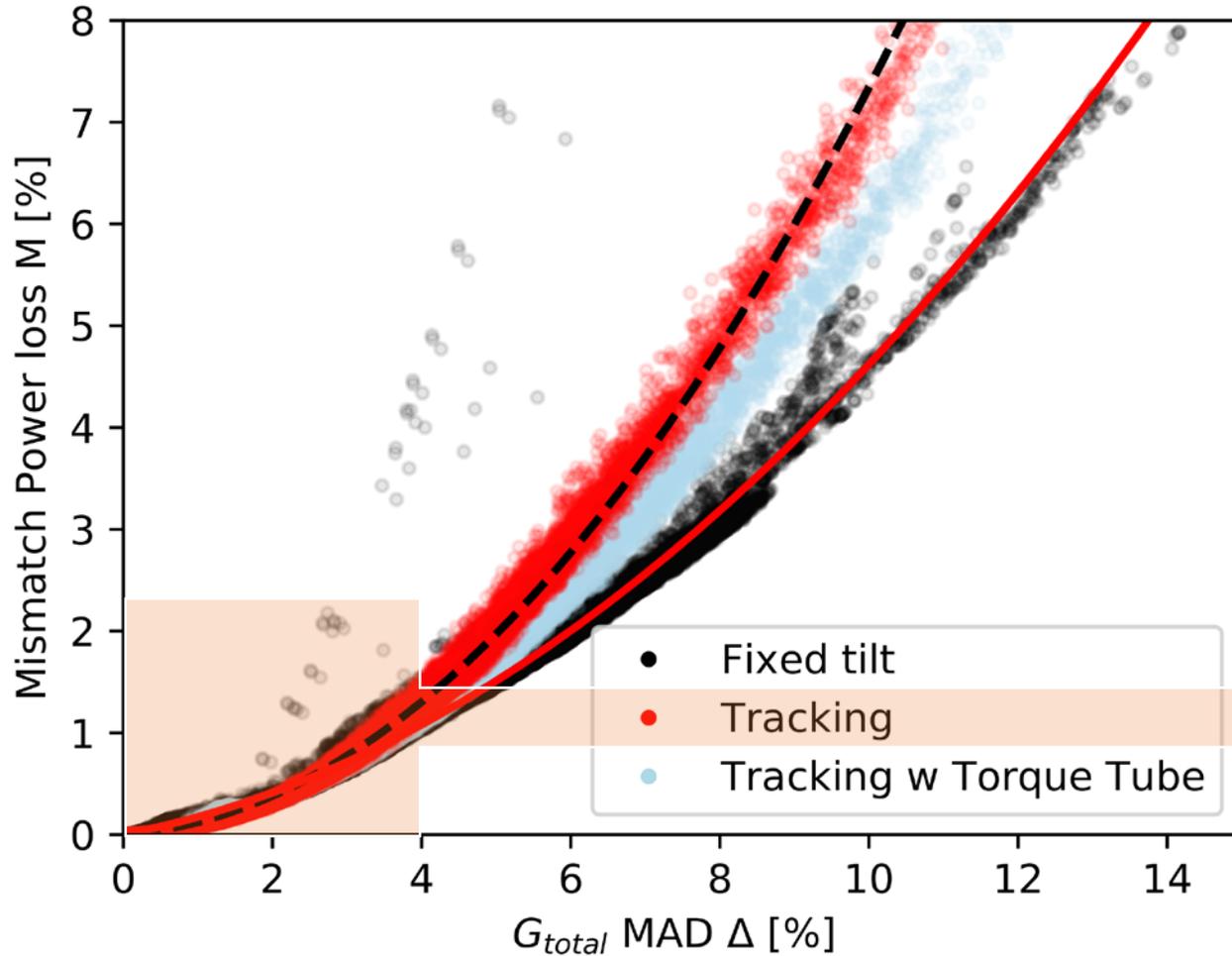
*No effect from landscape vs portrait orientation

$$\Delta = \text{Mean Absolute Difference } (G_{total})$$

$$G_{total} = G_{front} + \phi_{Bifi} G_{rear}$$

* With Tracking, ~90k datapoints

Tracking & Fixed Tilt



agreement is much better at $\Delta < 4$, where bulk of the energy is at.

$$\Delta = \text{Mean Absolute Difference } (G_{total})$$

$$G_{total} = G_{front} + \phi_{Bifi} G_{rear}$$

* With Tracking, ~90k datapoints

Reduced-order model

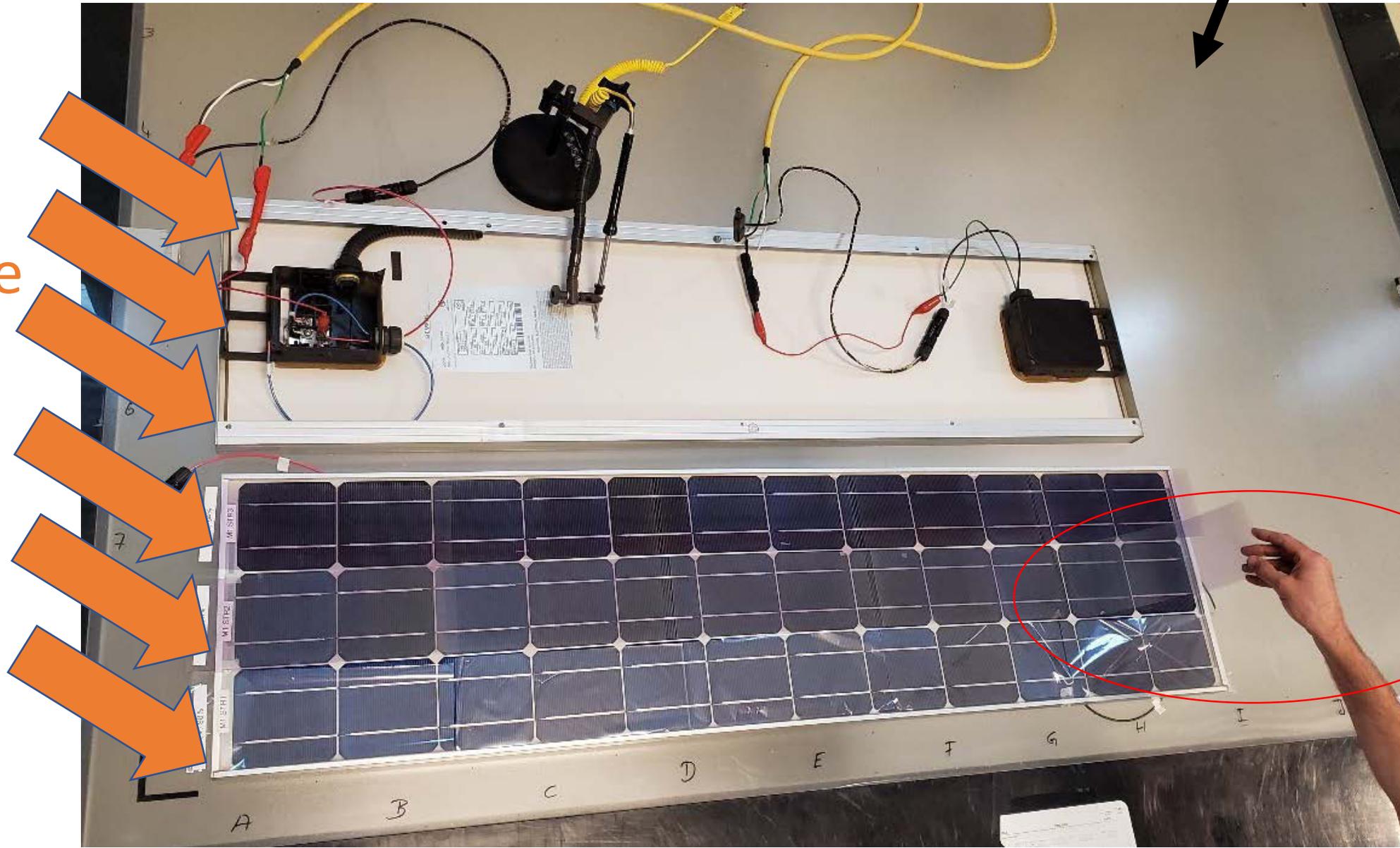
EXPERIMENTAL VALIDATION



Experimental Validation

Spire 4600 long-pulse flash I-V curve simulator.

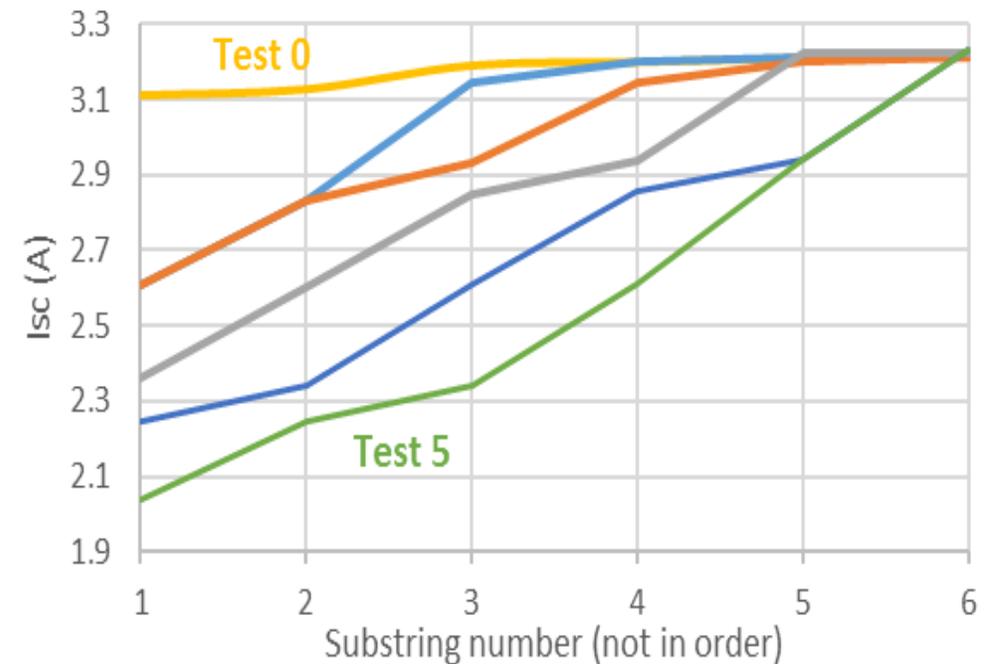
6 addressable
cell sub-
strings



Tests

Test#	M1 str1 (%)	M1 str2 (%)	M1 str3 (%)	M2 str1 (%)	M2 str2 (%)	M2 str3 (%)
0	-	-	-	-	-	-
1	90	-	84	-	-	-
2	90	-	84	-	-	90
3	90	7	84	-	-	90
4	90	75	84	70	-	90
5	64	75	84	70	-	90

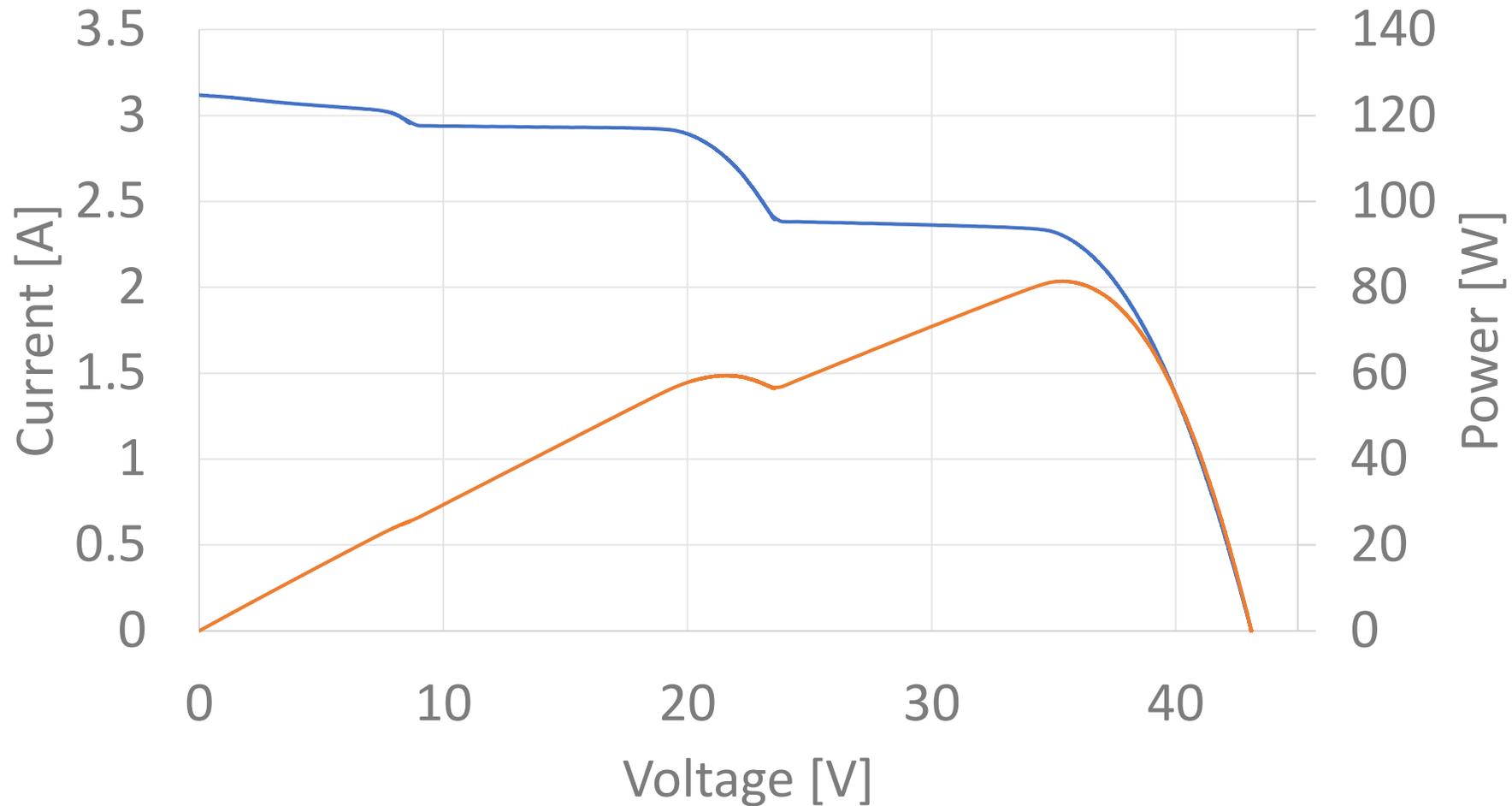
Measured substring I_{sc} for each of the shading tests



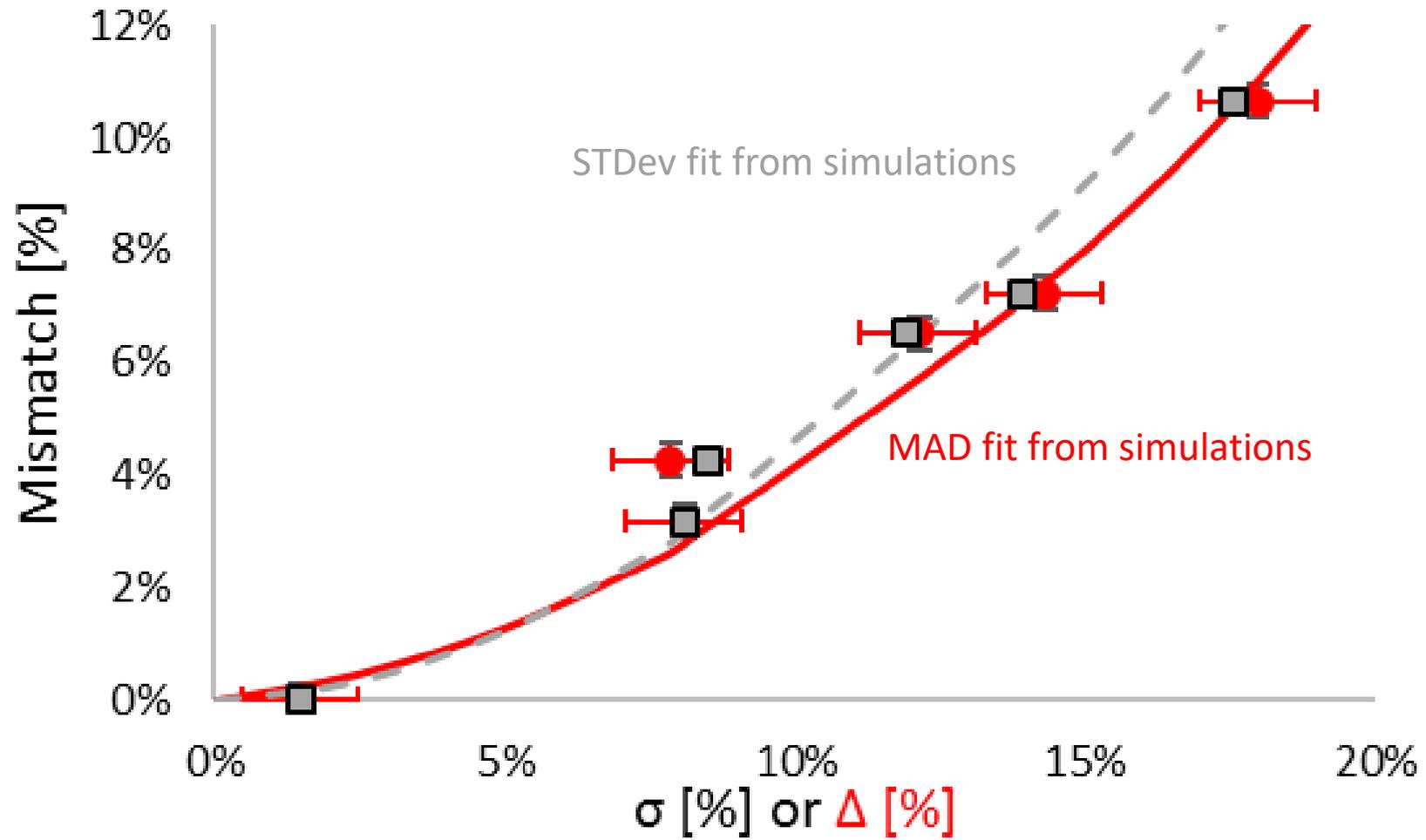
I_{sc} STD & MAD each vary from 1.5% - 18%

I-V curve measurements

Shading Test #3, IV curve 12% σ_{isc}



Measured mismatch loss



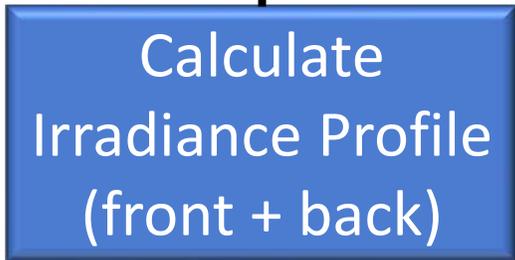
Reduced-order model



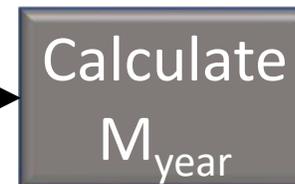
EXPERIMENTAL VALIDATION



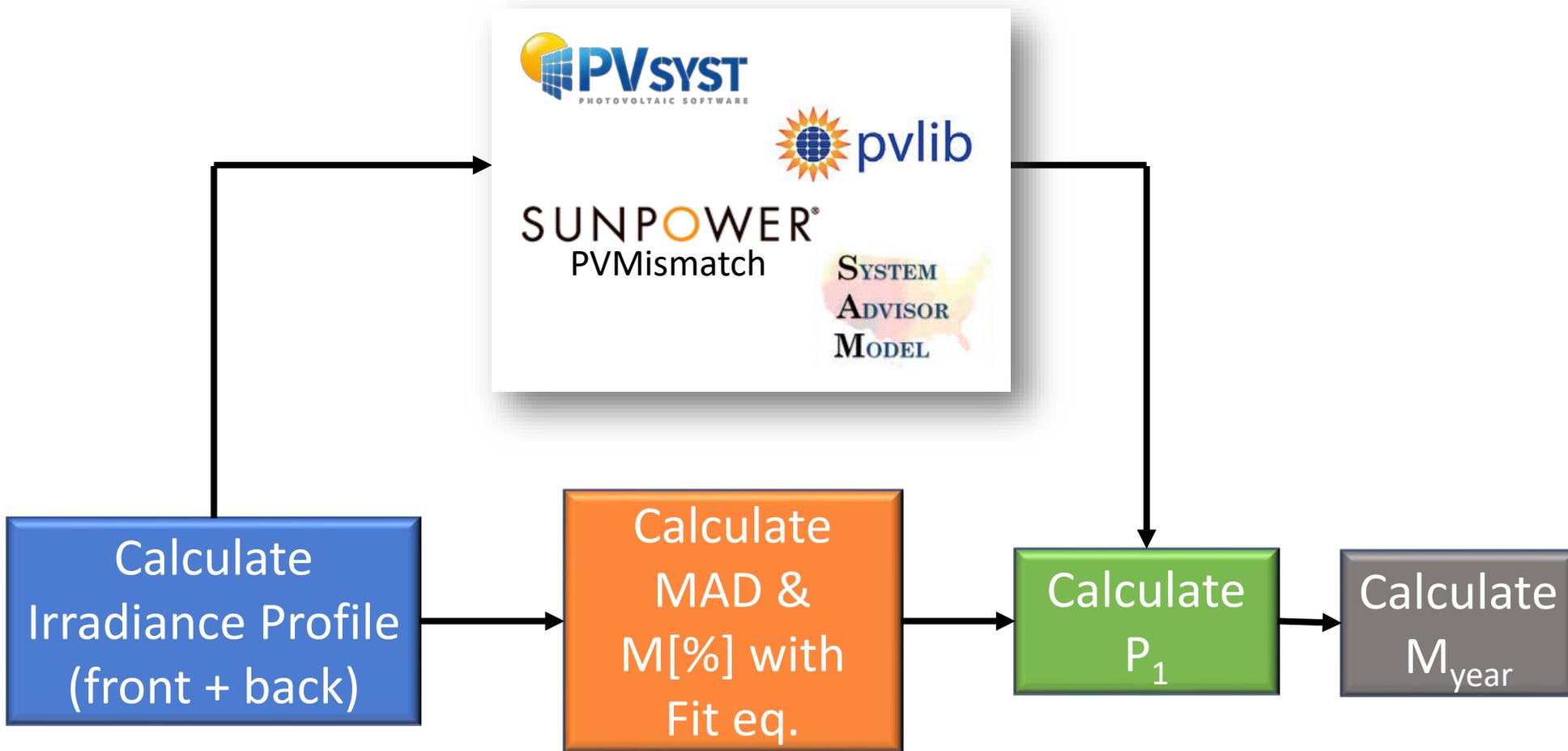
Calculate P_0 with preferred method



Calculate P_1 (cell-level mismatch)
with preferred method



Calculate P_0 with preferred method

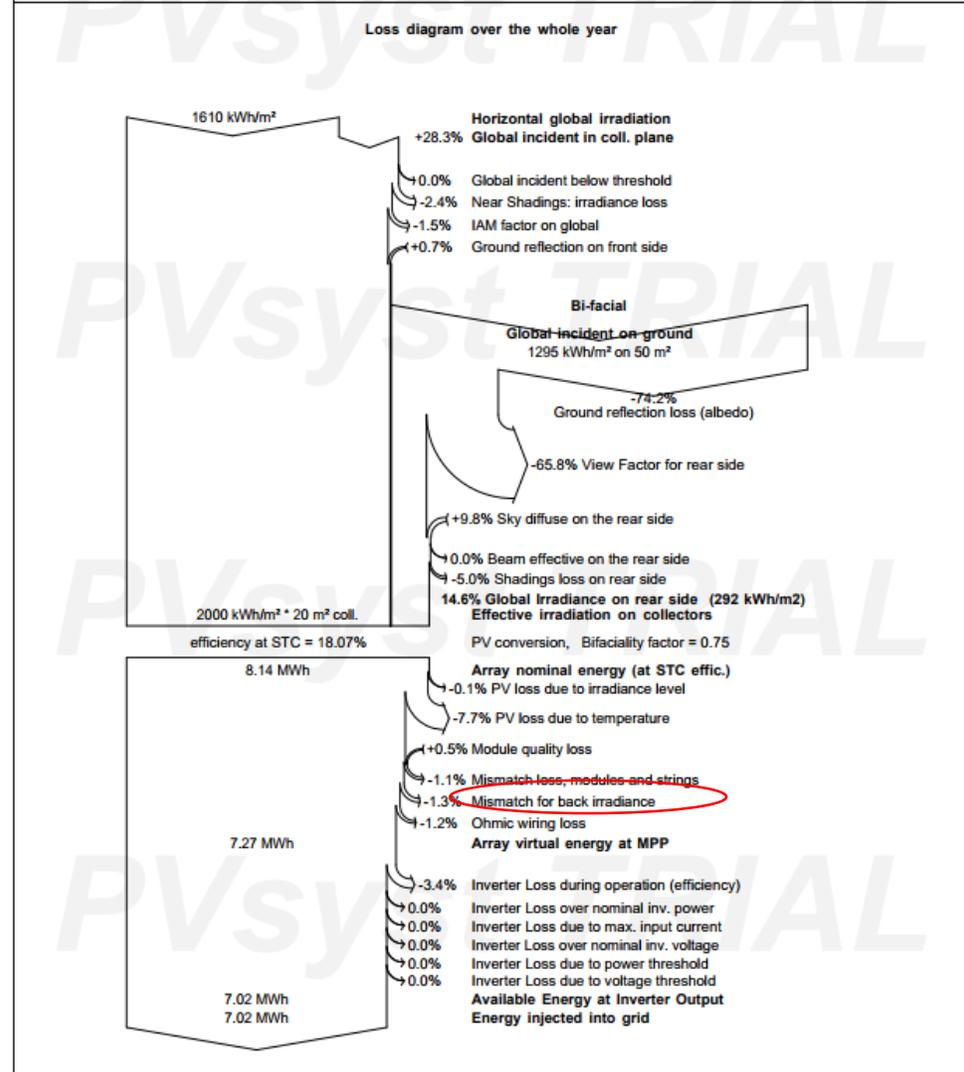


How to use this M parameter?

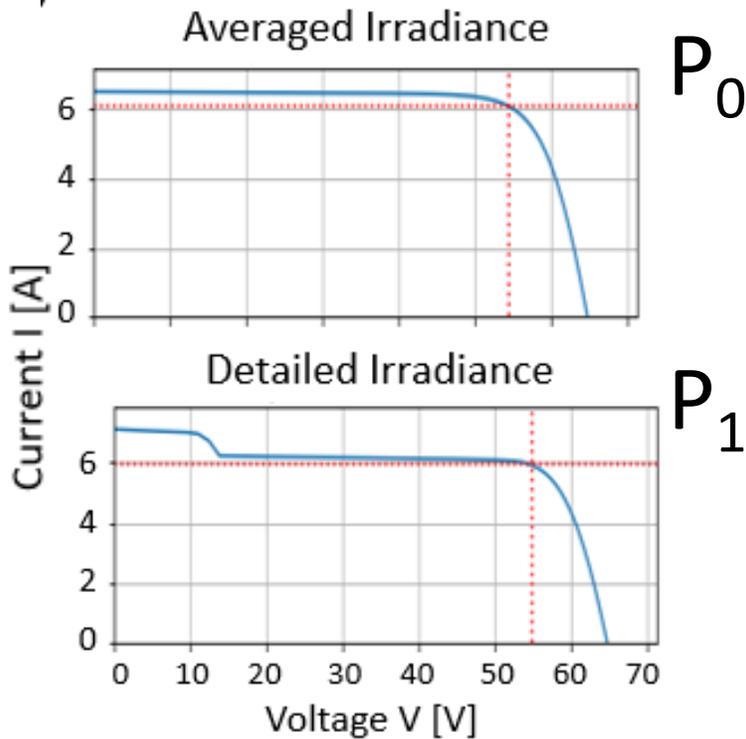
Connected System: Loss diagram
Tracking Mismatch Loss Exploration

Main system parameters	System type	Unlimited Trackers with backtracking		
PV Field Orientation	tilt			
PV modules	Model	LR6-60 HBD 305 M Bifacial	Pnom	305 Wp
PV Array	Nb. of modules	12	Pnom total	3660 Wp
Inverter	Model	4.2 kWac inverter	Pnom	4200 W ac
User's needs	Unlimited load (grid)			

- Mismatch loss factor a.k.a. rear mismatch loss, affects the Mismatch for back irradiance in the loss diagram



Shading Factor and Rear Electrical Mismatch Factors



P_0

$$P_0 = (G_{F_0} + G_{R_0} \cdot \varphi) \cdot \eta_0$$

P_1

$$P_1 = (G_{F_0} + G_{R_0} \cdot \varphi) \cdot \eta_0 \cdot (1 - M)$$

1%

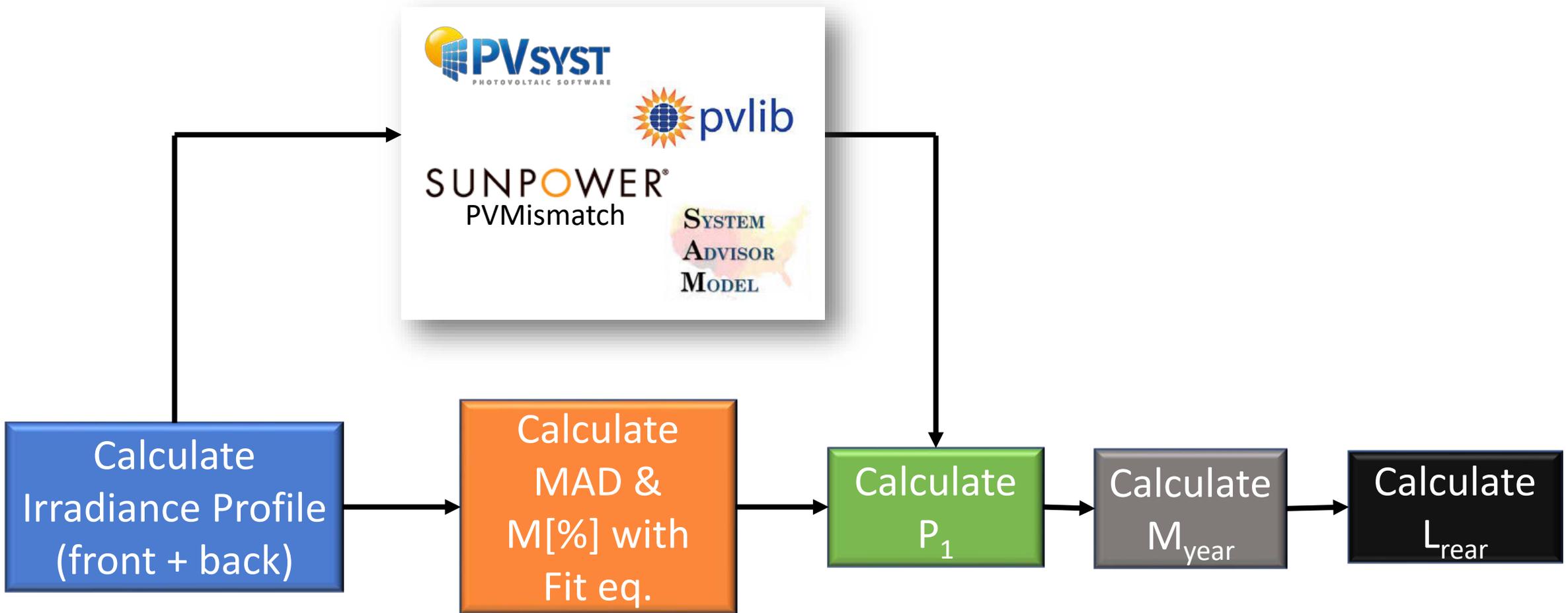
$$P_1 = (G_{F_0} + (1 - L_{Rear})G_{R_0} \cdot \varphi) \cdot \eta_0$$

$$L_{Rear} = L_{Inherent\ Mismatch} + L_{Structural\ Shading}$$

$$11\% \quad L_{Rear} = \frac{M}{BG} + M$$

10%

Calculate P_0 with preferred method



Conclusions

- Optical and cell-mismatch simulations were conducted on NREL's HPC to approximate bifacial fixed-tilt and tracking configurations in 3 climate zones.
- Annual mismatch loss was $M \leq 1\%$ for most configurations.
- For use in due diligence softwares, the value must be corrected by $\sim 10x$ to apply only to G_{rear} .
- Hourly values of $M[\%]$ can be much higher and follow an empirical relationship vs G_{Total} mean absolute difference Δ (spatial variation).
- Experiments with artificially applied mismatch confirm the empirical relationship, and adjustments for module FF and ϕ_{Bifi} are described.

*C. Deline, S. Ayala Pelaez, S. MacAlpine, C. Olalla "Estimating and Parameterizing Mismatch Power Loss in Bifacial Photovoltaic Systems", (*submitted*)

Slides to be open-published on NREL's database, link posted on:
https://github.com/NREL/bifacial_radiance/wiki



Learn to model bifacial fields

Oct. 17 | 9 AM MT (GMT -6)

Register
Today
(free)



This training will cover the use of `bifacial_radiance`, an open-source raytracing software developed and validated by NREL



More info:
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Thank you

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