

Numerical Simulations of the Supercritical Carbon Dioxide Round Turbulent Jet

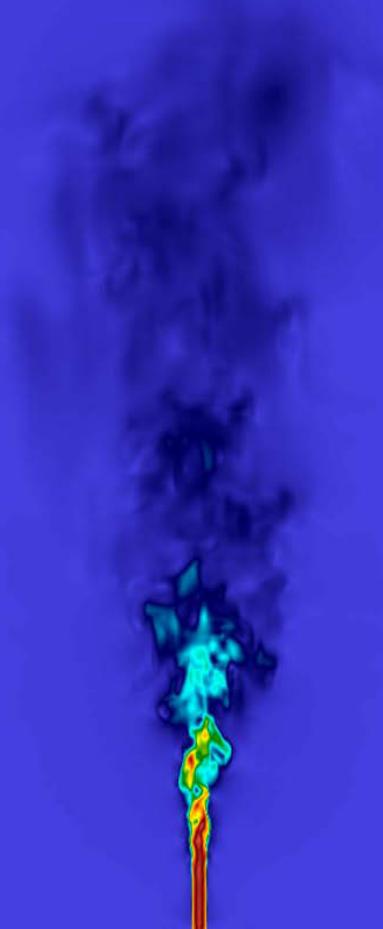
Julia Ream^{1,2}, Marc T. Henry de Frahan¹, Michael Martin¹,
Shashank Yellapantula¹, Ray Grout¹

¹ High Performance Algorithms and Complex Fluids Group, Computational Science
Center, National Renewable Energy Laboratory

² Applied and Computational Mathematics, Florida State University

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Overview

1. Introduction
2. Simulation Setup
3. Cases and Parameters
4. Ideal Gas Verification
5. sCO₂ Results
6. Future Work
7. Acknowledgements
8. Questions

Supercritical Carbon Dioxide (sCO₂)

Introduction

What are supercritical fluids?

- Fluids held above critical temperature and pressure
- Liquid-like density
- Gas-like viscosity
- Sensitive density, pressure, temperature relationship
- Critical point for CO₂: T=304 K, P=7.38 MPa

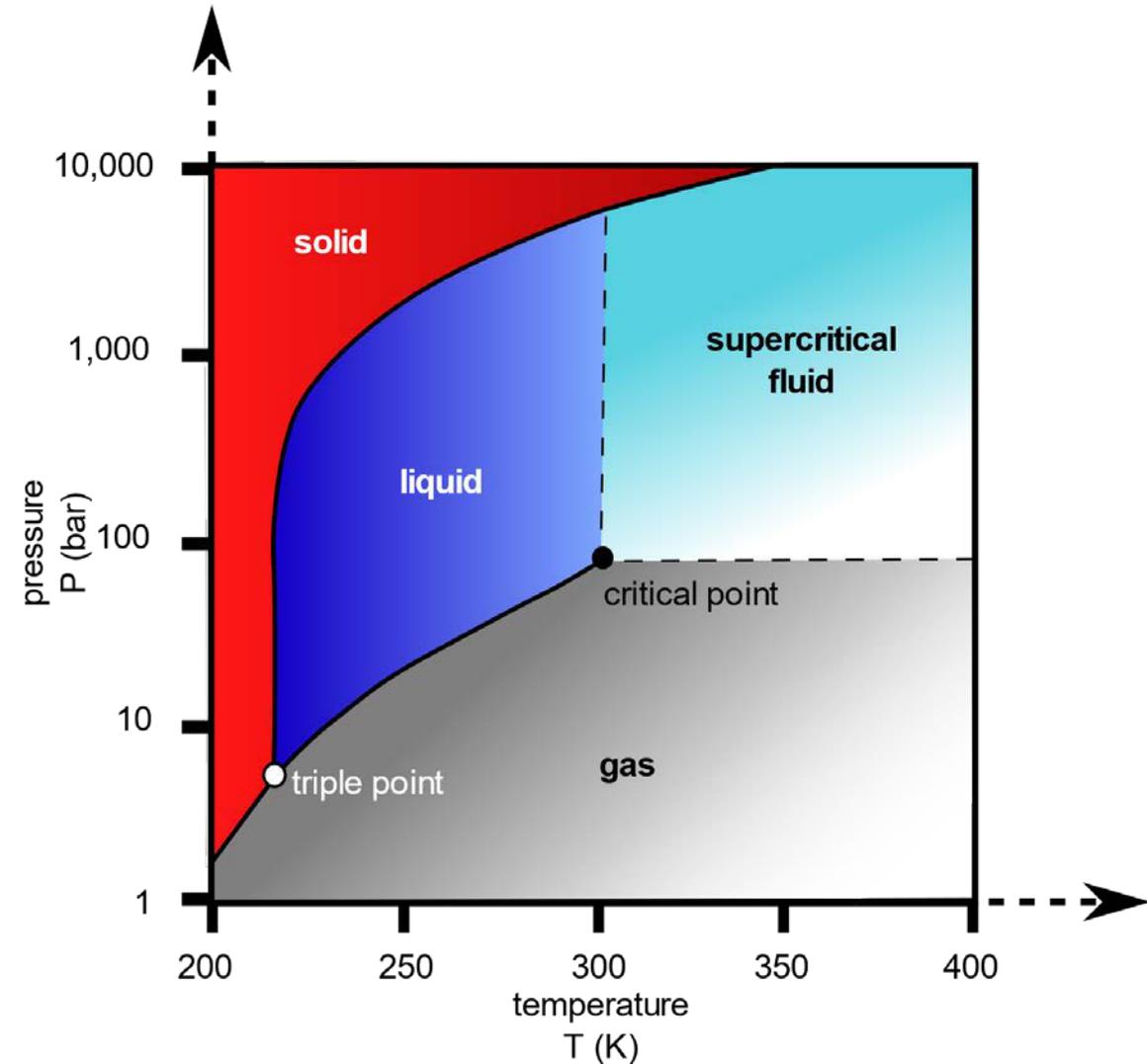


Fig. 1: Phase Diagram for Carbon Dioxide

Supercritical fluids are important for a wide range of applications

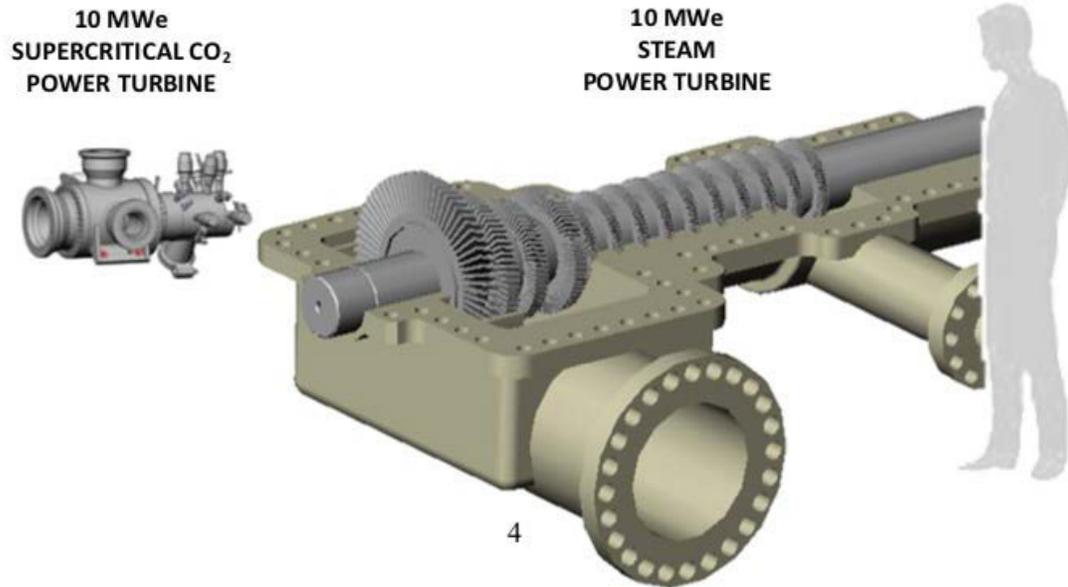


Fig. 2: 10 MWe sCO₂ power turbine compared to a 10 MWe steam turbine

- sCO₂ can be utilized in a variety of industries:
 - Closed-cycle gas turbines in advanced nuclear reactors
 - Carbon sequestration

Supercritical fluids are important for a wide range of applications

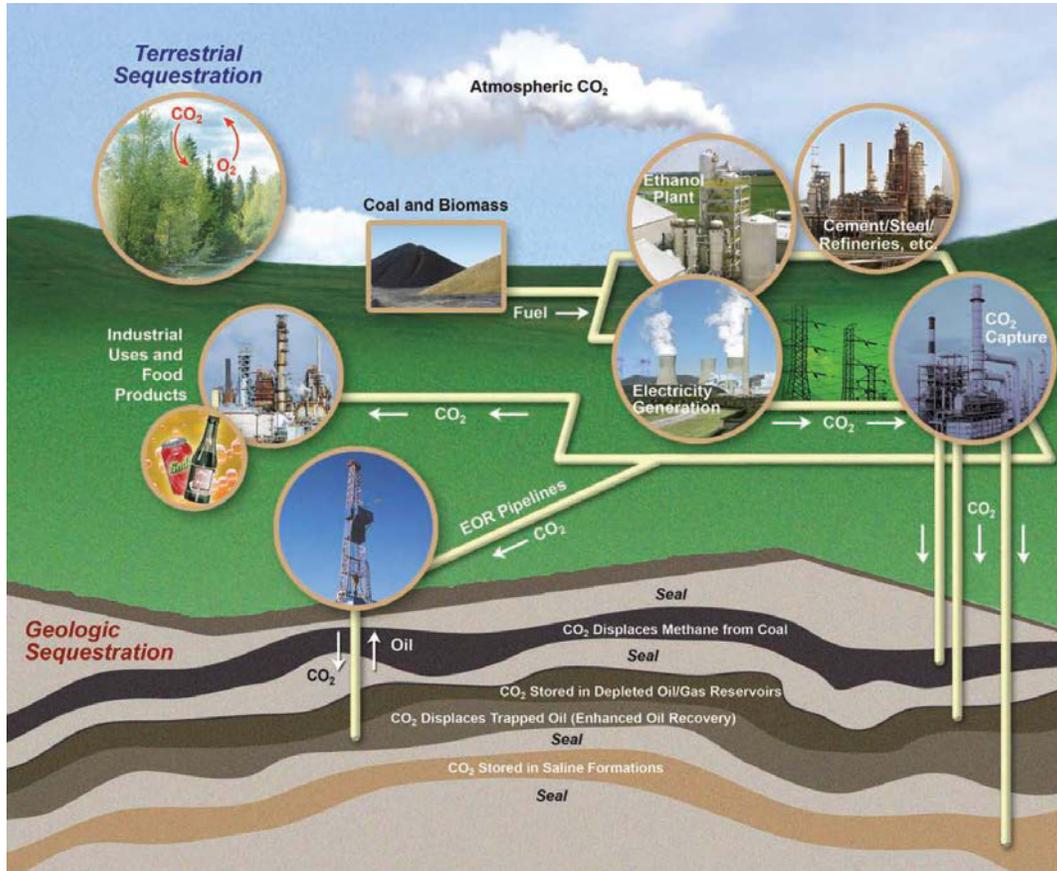


Fig. 3: Examples of Geologic Carbon Sequestration

- sCO₂ can be utilized in a variety of industries:
 - Closed-cycle gas turbines in advanced nuclear reactors
 - Carbon sequestration

Current Landscape

- sCO₂ promising fluid in many fields, yet many fundamental physical aspects still unknown
- Experimental challenges with critical parameters
- Current jet research oriented toward application-specific quantities of interest.

Project Scope

Goal: simulate flow field of turbulent sCO₂ jet in order to gain better understanding of underlying physics.

- Our hypothesis is that supercritical flows for canonical round turbulent jets exhibit different physical mechanisms than those of ideal gas.
- Understanding base mechanisms of supercritical flows can add to theory related to quantities of interest across all applications
- Specifically interested in investigating velocity profiles and Reynolds stresses compared to those of ideal gas case.

Numerical Simulations

Jet Setup

PeleC

- Built on AMReX and funded by the Exascale Computing Project (ECP) through the Department of Energy (DOE), PeleC is an adaptive-mesh compressible hydrodynamics code for reacting flows
 - Models turbulence-chemistry interactions motivated by conditions in internal combustion engines
 - Can additionally handle embedded boundary conditions, non-ideal EoS, and allows for implementation of adaptive mesh refinement (AMR)
- Utilizes 2nd order finite volume formulation using the Piecewise Parabolic Method (PPM) in space and a standard RK2 time integrator to approximate solutions to the compressible Euler equations.
- To learn more visit: <https://github.com/AMReX-Combustion/PeleC>

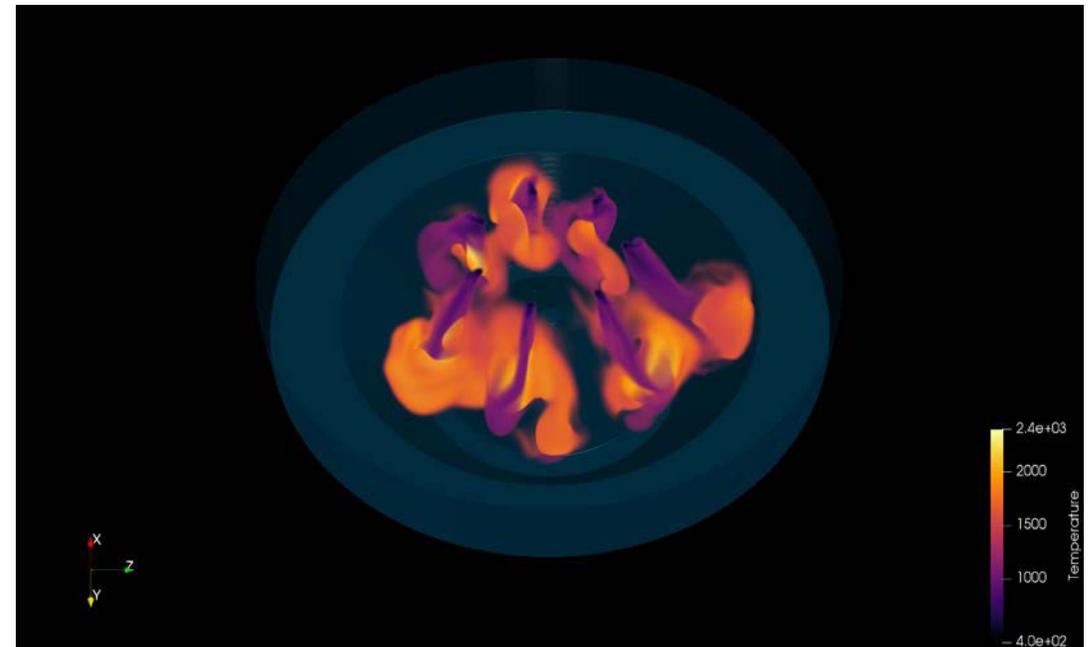


Fig 4: Injection of natural gas in a piston-bowl geometry performed using PeleC

Equations of State (EoS)

Gamma Law for Ideal Gas

$$P = (\gamma - 1)\rho\epsilon .$$

Used for Jet verification with air

Soave-Redlich-Kwong for Non-Ideal Gas

$$p = \frac{RT}{V_m - b} - \frac{a\alpha}{V_m(V_m + b)}$$

$$a = \frac{0.42747 R^2 T_c^2}{P_c}$$

$$b = \frac{0.08664 R T_c}{P_c}$$

$$\alpha = (1 + (0.48508 + 1.55171\omega - 0.15613\omega^2)(1 - T_r^{0.5}))^2$$

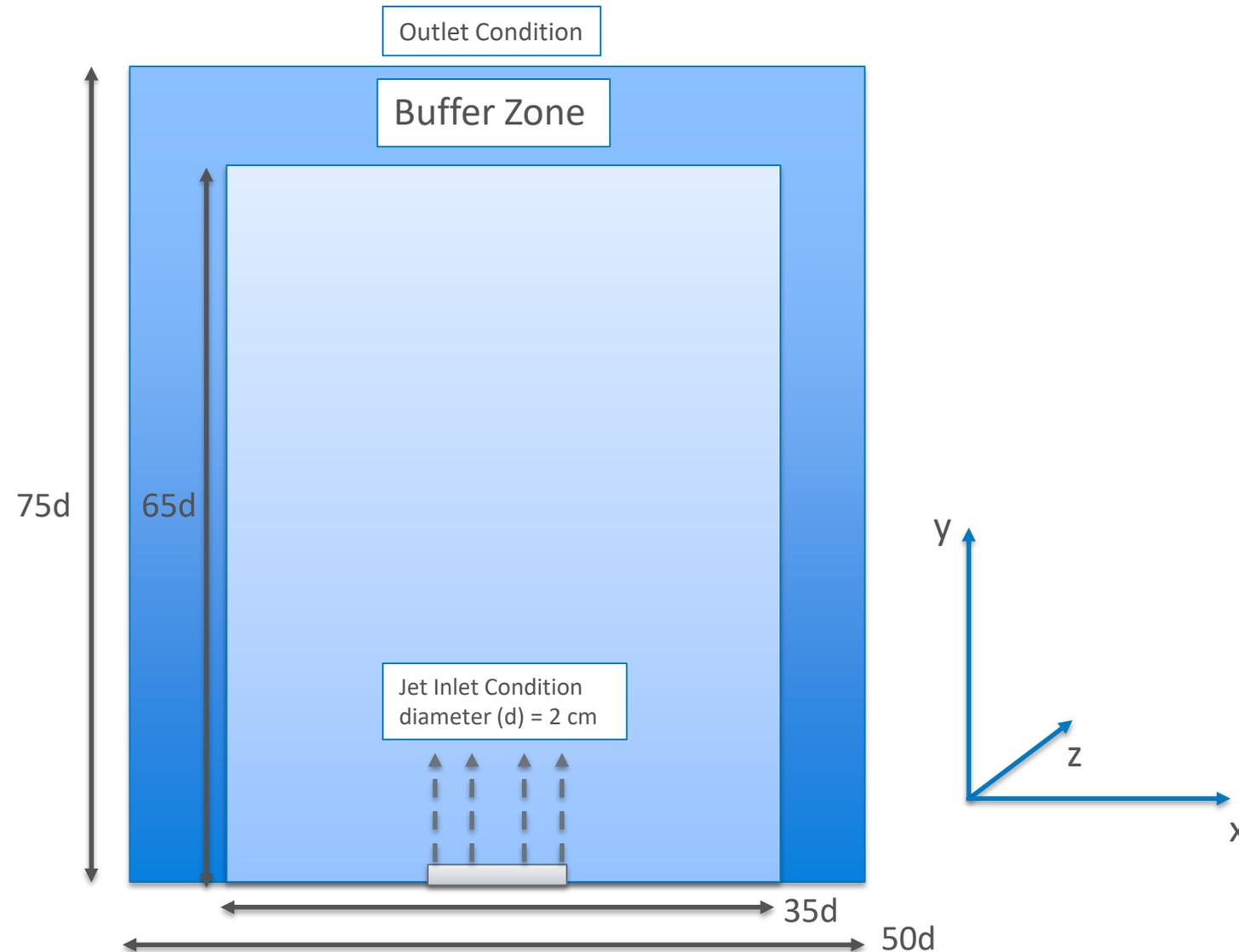
$$T_r = \frac{T}{T_c}$$

where ω is the acentric factor for the species.

More accurately handles drastic density and specific heat changes across critical point

Schematic

- 3D Simulation
- Slice at $z=0$ for visualizations
- Buffer zone implemented with adaptive mesh refinement (AMR)
- Ambient temperature and pressure set to match inlet condition



Boundary Conditions

Inflow

- diameter = 2 cm
- input velocity scaled to predetermined mean velocity + noise scaled by r.m.s. profiles calculated via direct numerical simulation (DNS)

$$v = \langle v_{\text{DNS}} \rangle + (v'_{\text{DNS}} + \beta v'_{\text{DNS}} r_1 \sin \theta_1) \cdot r_2 \sin \theta_2$$

$$u = u'_{\text{DNS}} + \beta u'_{\text{DNS}} r_3 \sin \theta_3$$

$$w = w'_{\text{DNS}} + \beta w'_{\text{DNS}} r_4 \sin \theta_4$$

$$r_i = \sqrt{-2.0 \log(X_i)}$$

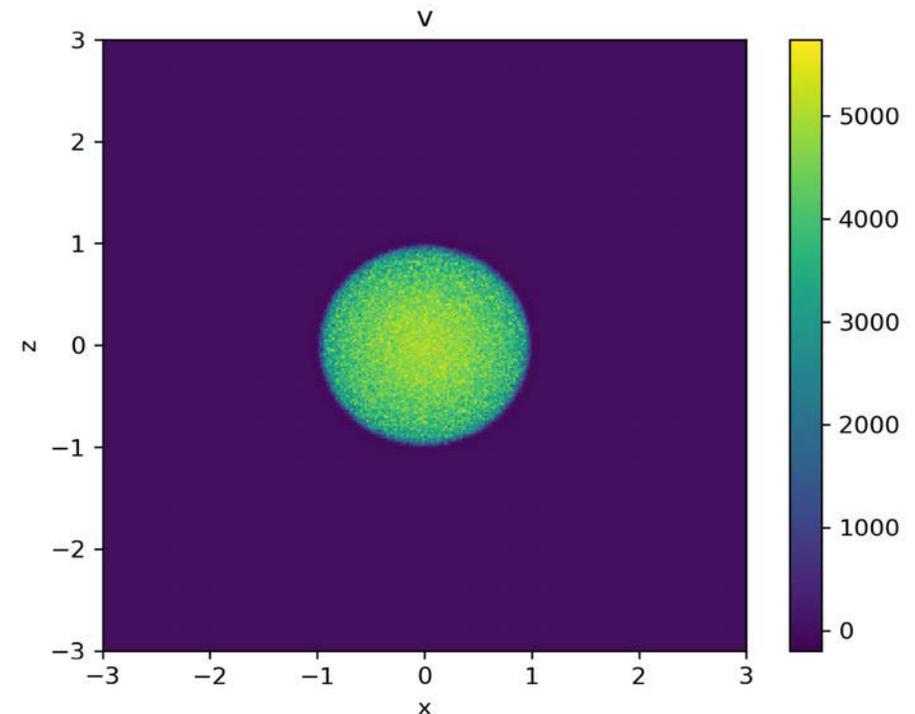
$$\theta_j = 2\pi X_j$$

X_n is a random number between 0 and 1



Outflow

- Impose zero gradient at boundary
- Do not implement AMR at boundary



Ideal Gas and Supercritical Fluid

Cases

Cases

Air

$$P_{\text{jet}} = P_{\text{ambient}} = .101325 \text{ MPa}$$

$$T_{\text{jet}} = T_{\text{ambient}} = 300 \text{ K}$$

$$V_{\text{jet}} = 5,000 \text{ cm/s}$$

$$\rho_{\text{jet}} \approx .001176 \text{ g/cm}^3$$

$$\text{Re} \approx 60,000$$

$$\text{M} \approx .144$$

- Initial # of cells (x ,y, z): 80, 120, 80
- AMR max level: 3
- Refine when: vorticity_{ERR} > 100

sCO₂

$$P_{\text{jet}} = P_{\text{ambient}} = 10.1325 \text{ MPa}$$

$$T_{\text{jet}} = T_{\text{ambient}} = 600 \text{ K}$$

$$V_{\text{jet}} = 10,000 \text{ cm/s}$$

$$\rho_{\text{jet}} \approx .08937 \text{ g/cm}^3$$

$$\text{Re} \approx 600,000$$

$$\text{M} \approx .262$$

- Initial # of cells (x ,y, z): 80, 120, 80
- AMR max level: 3
- Refine when vorticity_{ERR} > 100

We maintain a single phase fluid by staying far away from the critical point

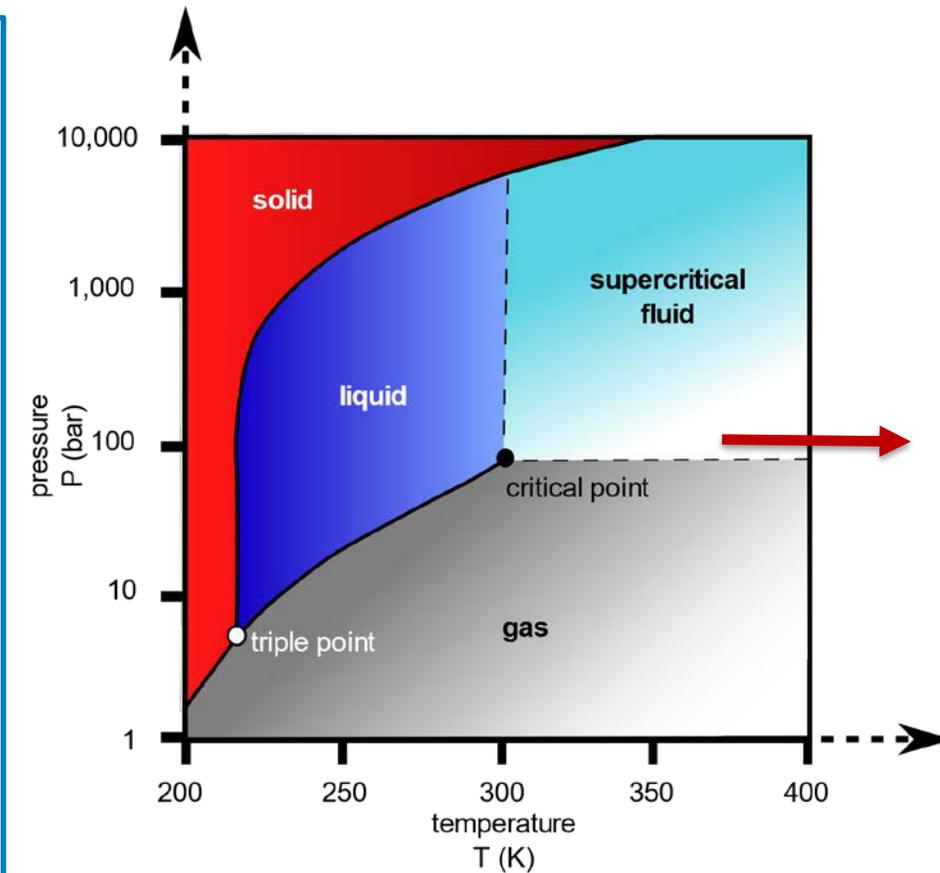


Fig. 5 : Phase Diagram for Carbon Dioxide

Checking the simulation with a familiar fluid

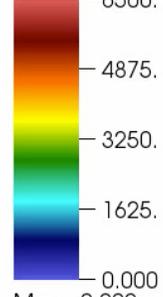
Ideal Gas

Air Jet

Note: Current simulations do not include a subgrid scale model; future ones will.

DB: Header
Cycle: 0

Pseudocolor
Var: magvel
6500.



Max: 0.000
Min: 0.000

Y-Axis

140
120
100
80
60
40
20

-40

-20

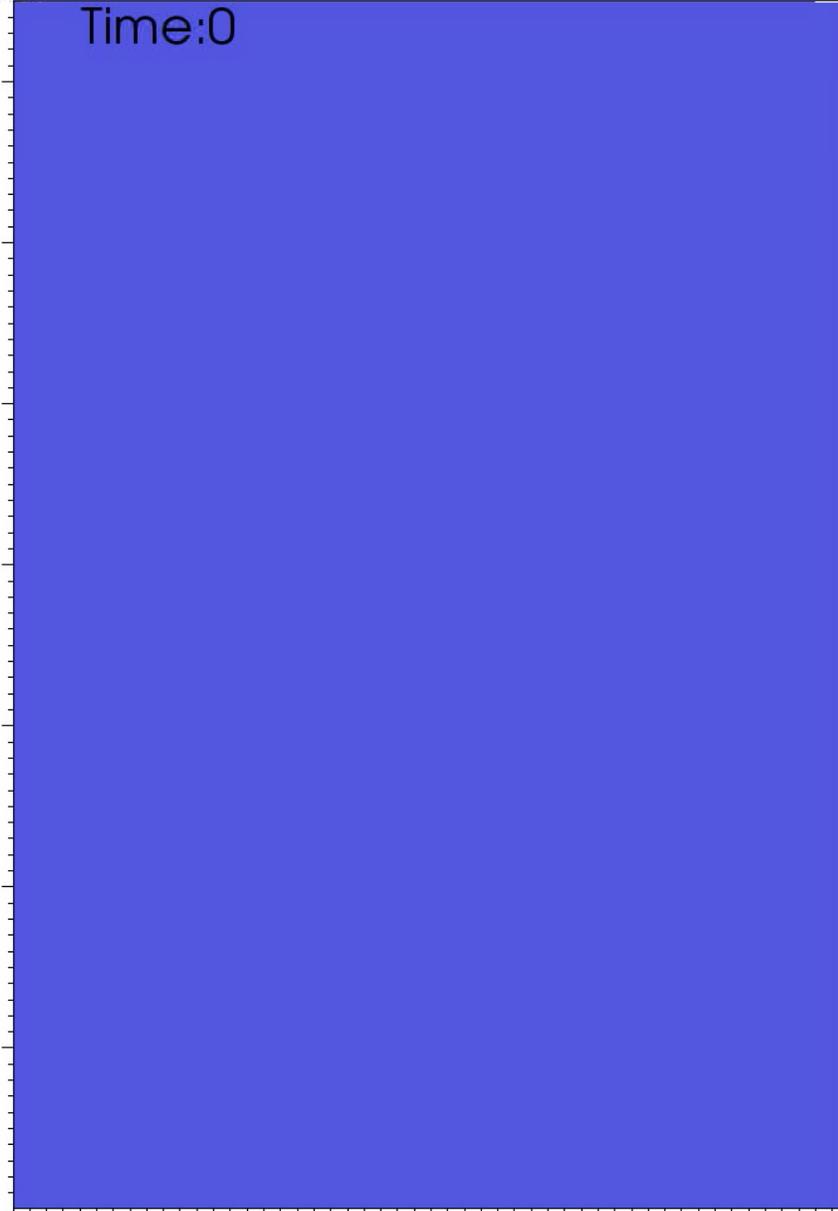
0

20

40

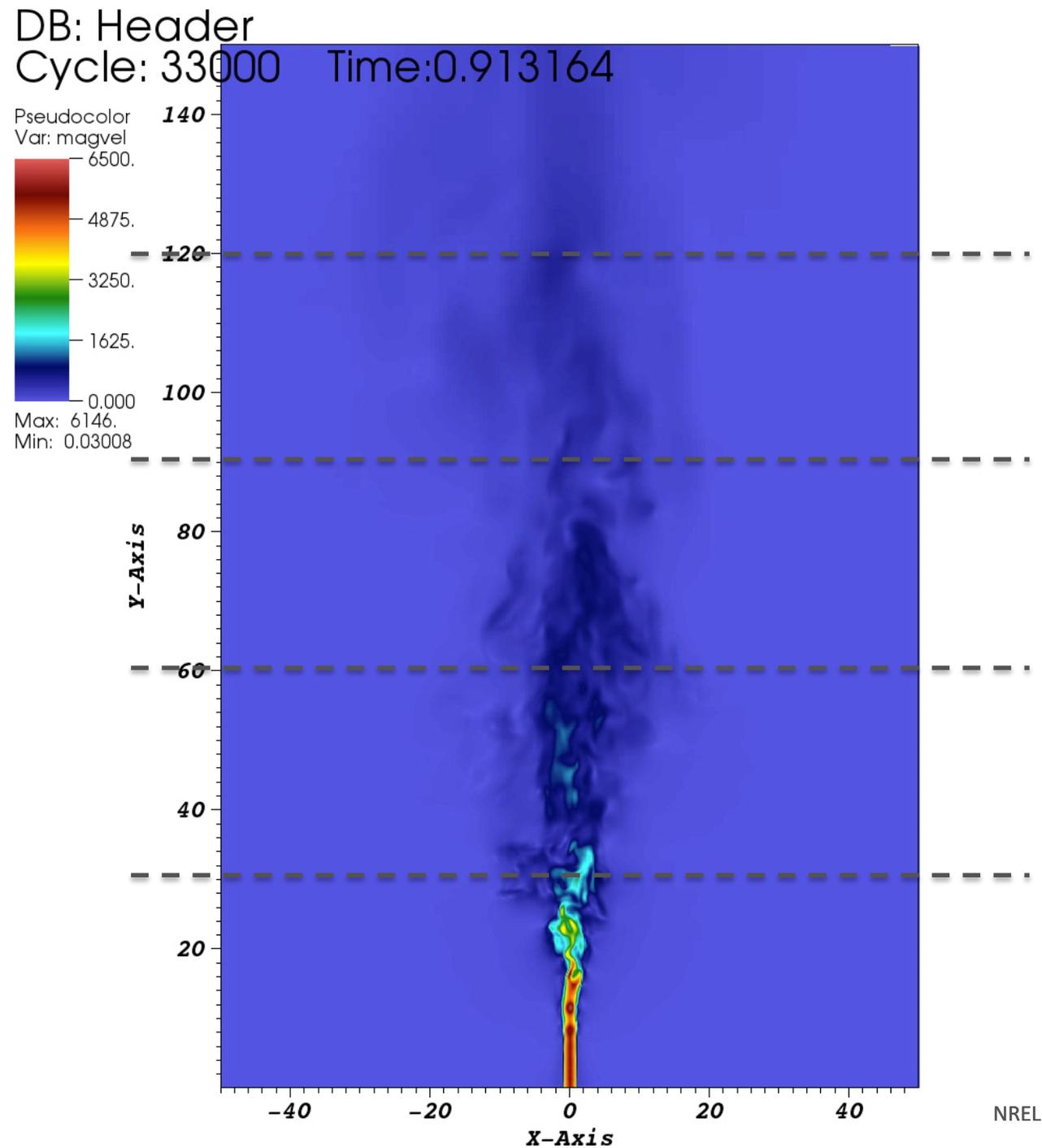
X-Axis

Time:0



Air Jet

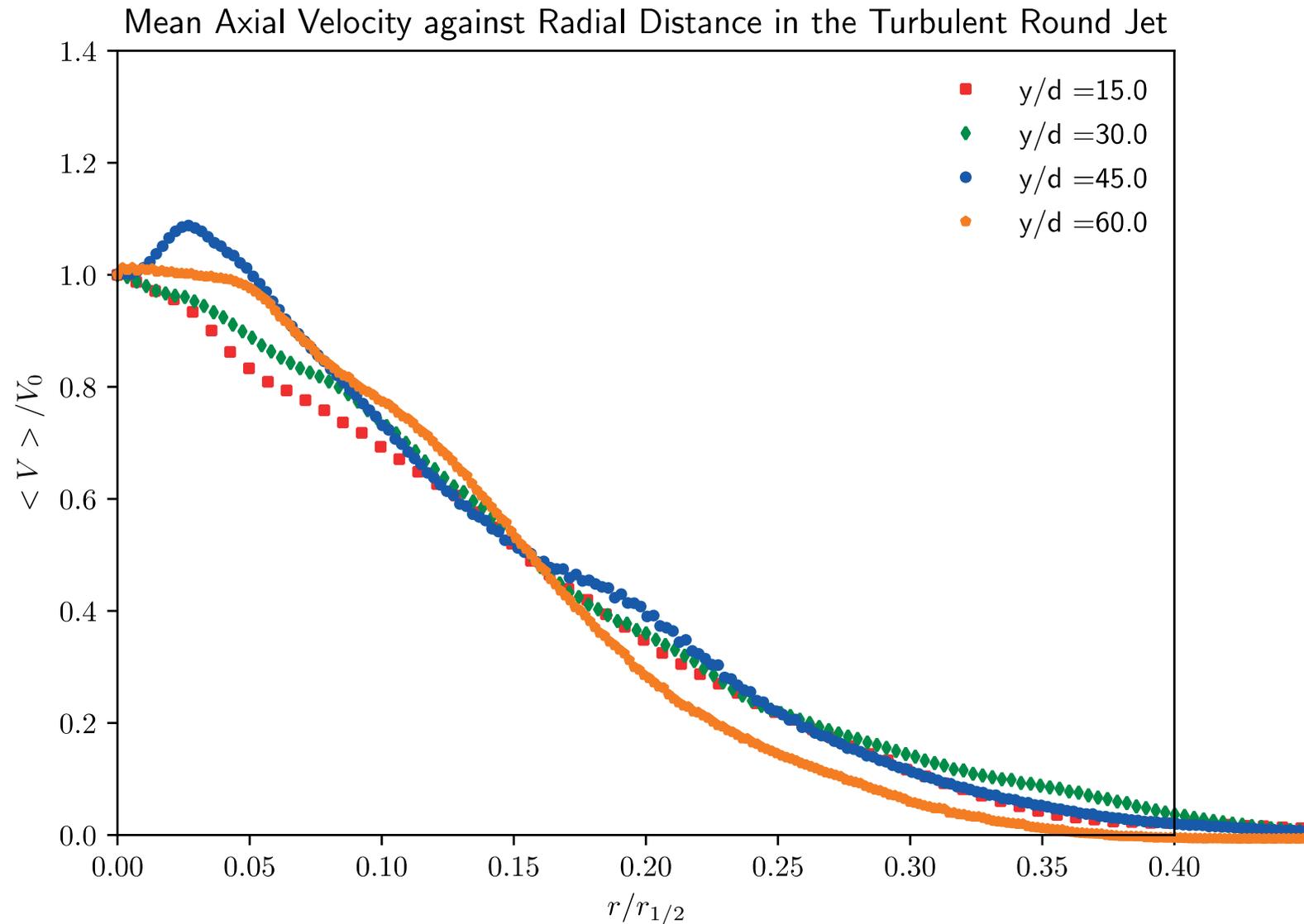
- Plots saved every 500 time steps
- Slices made every 30 cm in y direction from y = 30 to 120
- Means calculated with last 10 plot files



Air Jet: Velocity Profiles

- Profiles begin to collapse into one curve in self-similar region expected by theory

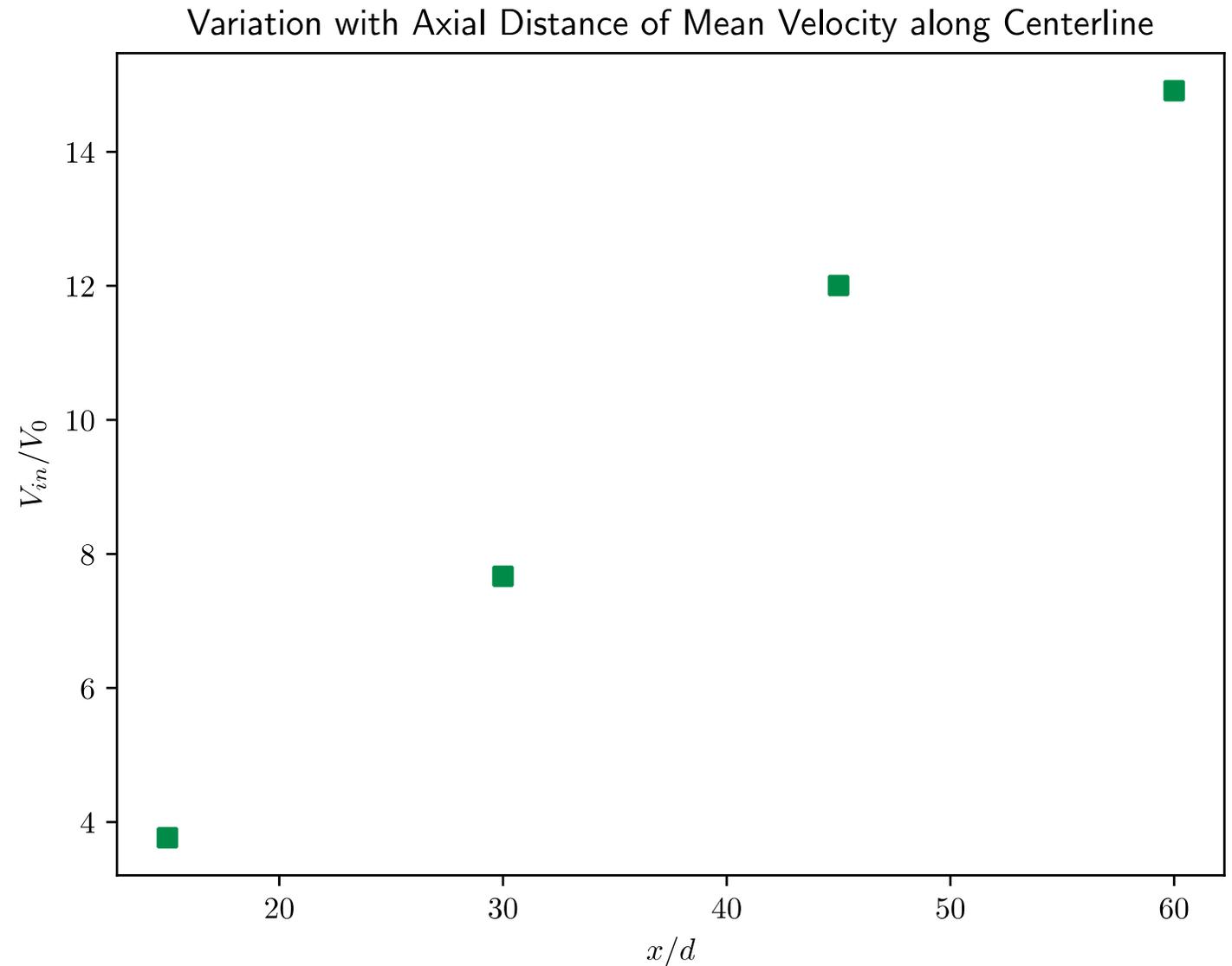
Note: Simulation has not yet reached statistically stationary steady state



Air Jet: Centerline Scaling

- Close to linear relationship
expected by theory: $V_0 \sim x^{-1}$

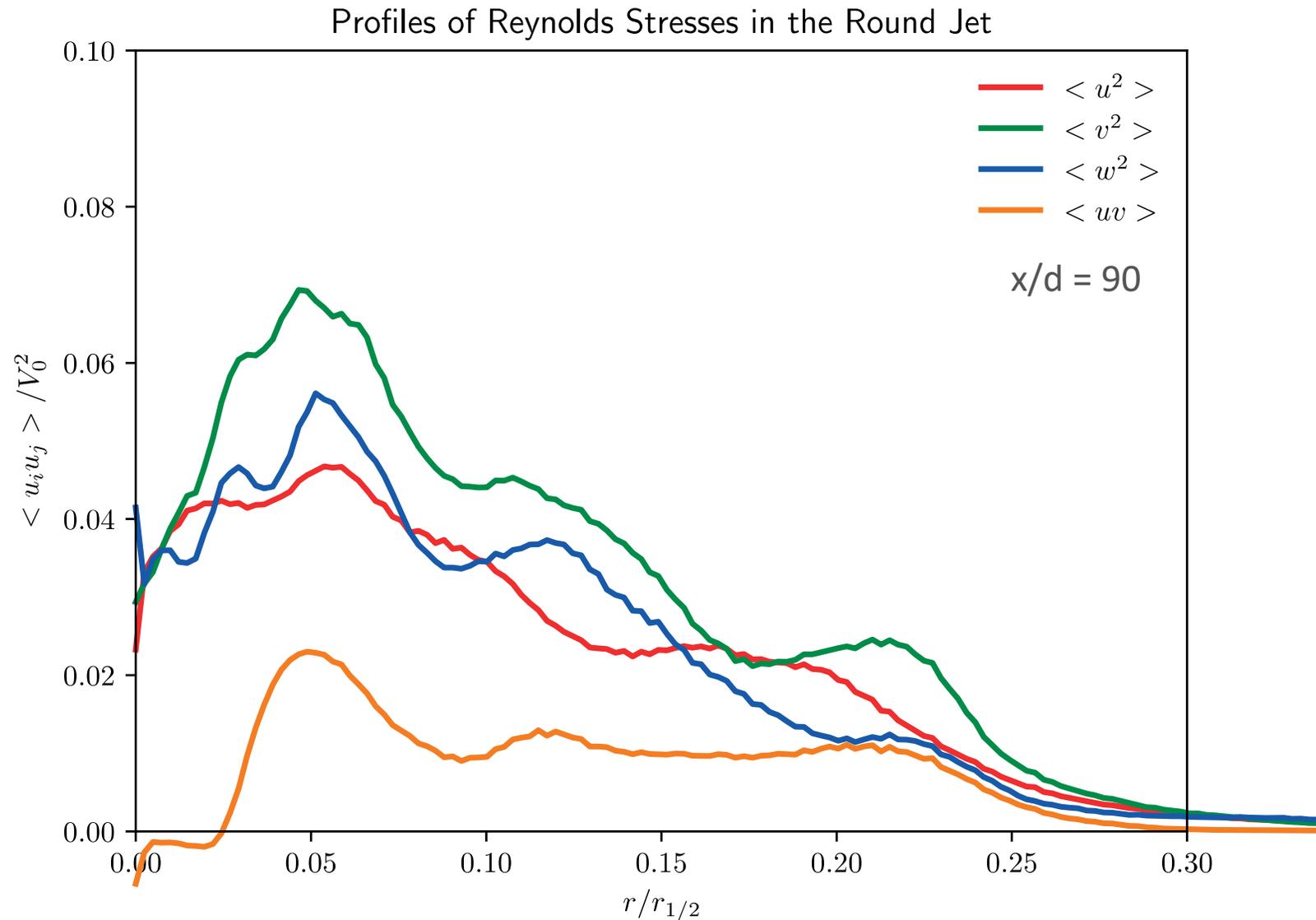
Note: Simulation has not yet reached
statistically stationary steady state



Air Jet: Reynolds Stresses

- Approaching profiles of Reynolds stresses expected from experimental results

Note: Simulation has not yet reached statistically stationary steady state



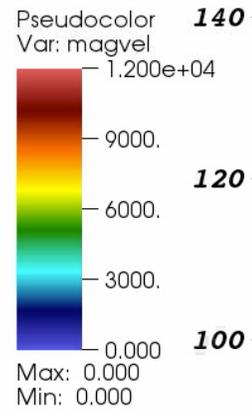
The Supercritical Round Turbulent Jet

Results

sCO₂ Jet

Note: Current simulations do not include a subgrid scale model; future ones will.

DB: Header
Cycle: 0



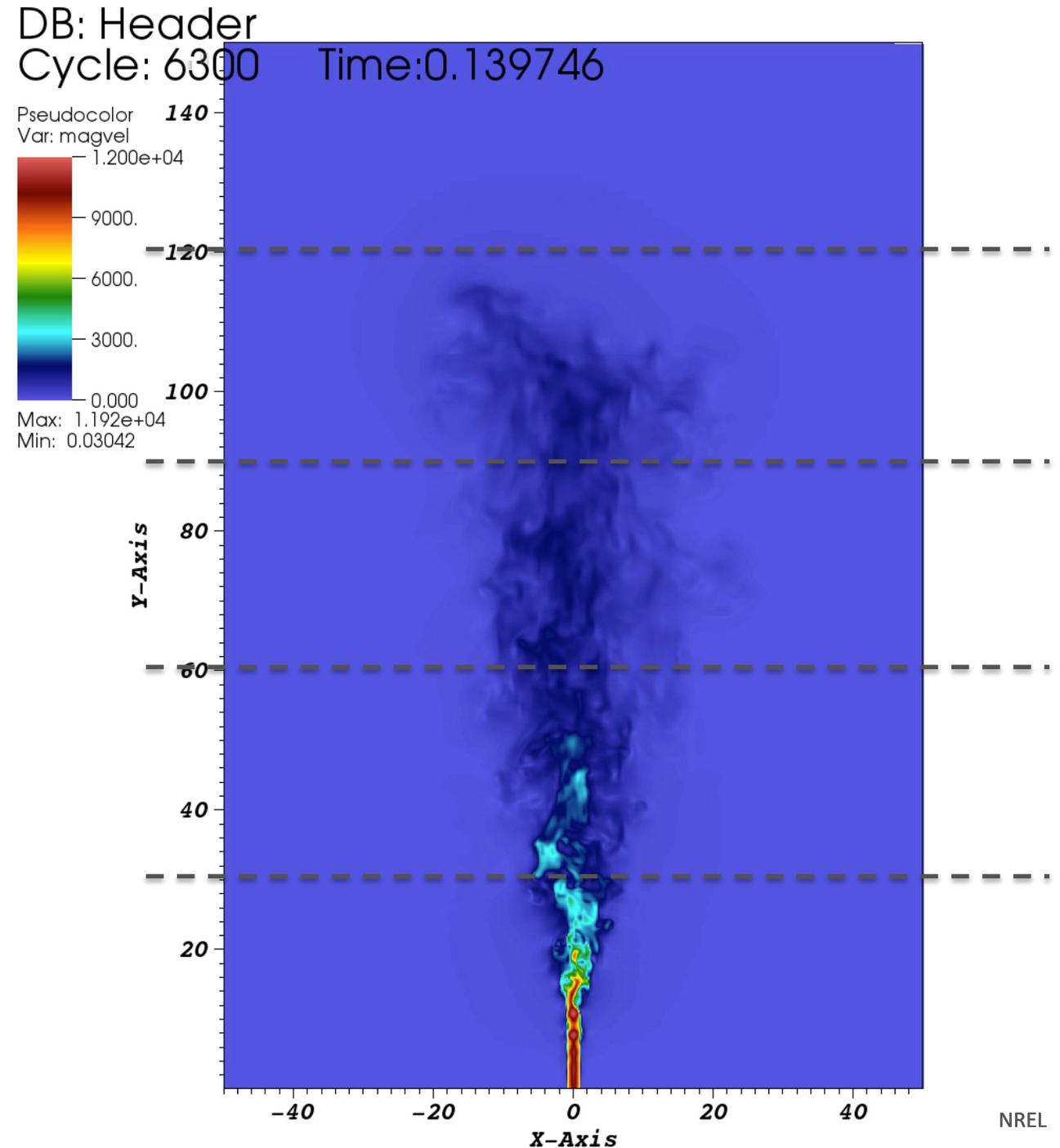
Y-Axis

80
60
40
20

-40 -20 0 20 40
X-Axis

sCO₂ Jet

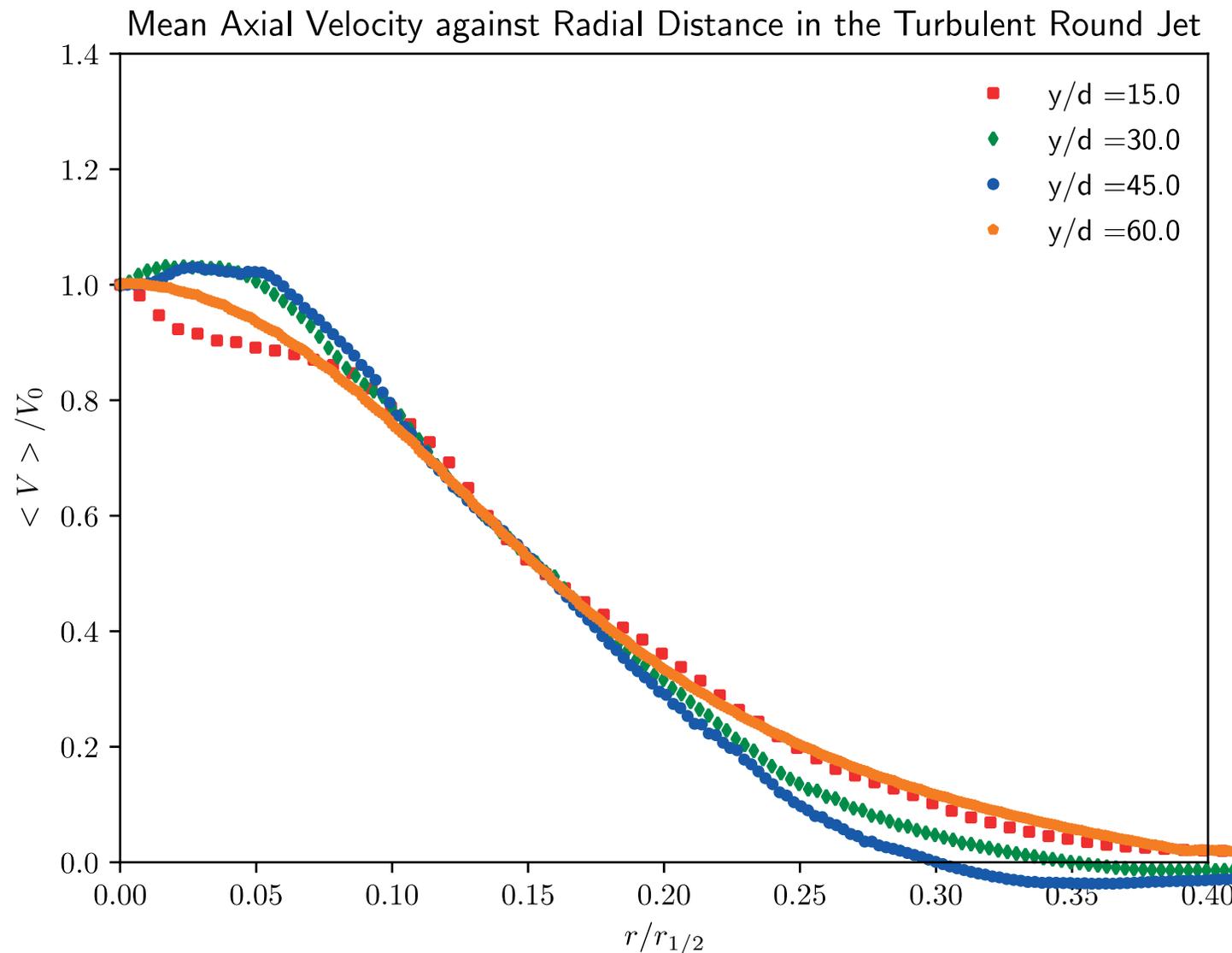
- Plots saved every 300 time steps
- Slices made every 30 cm in y direction from y = 30 to 120
- Means calculated with last 10 plot files



sCO₂ Jet: Velocity Profiles

- Profiles begin to collapse into one curve in self-similar region expected by theory.

Note: Simulation has not yet reached statistically stationary steady state

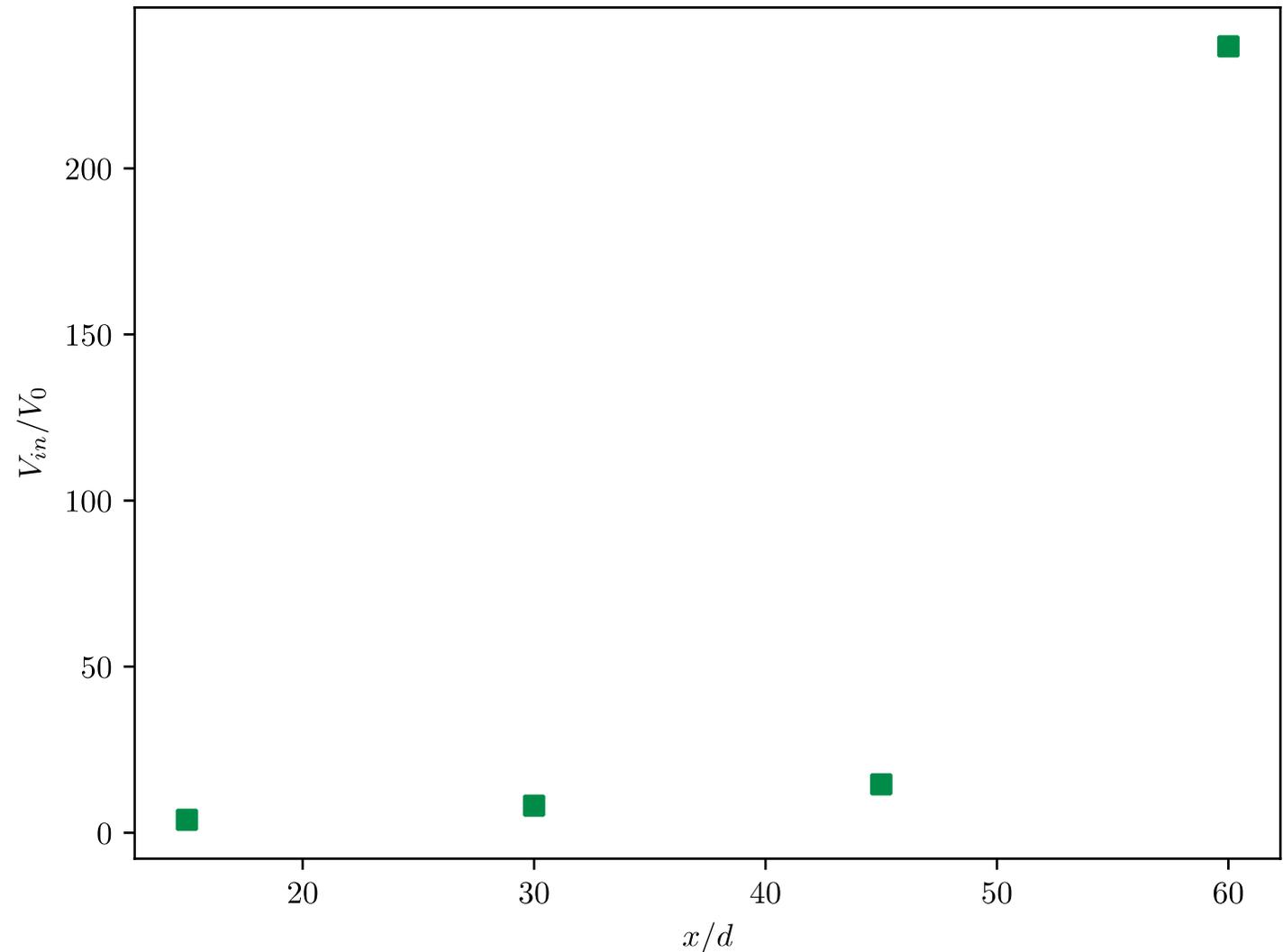


sCO₂ Jet: Centerline Scaling

- Jet has only just reached $x/d=60$ in simulation so relationship is still undetermined.

Note: Simulation has not yet reached statistically stationary steady state

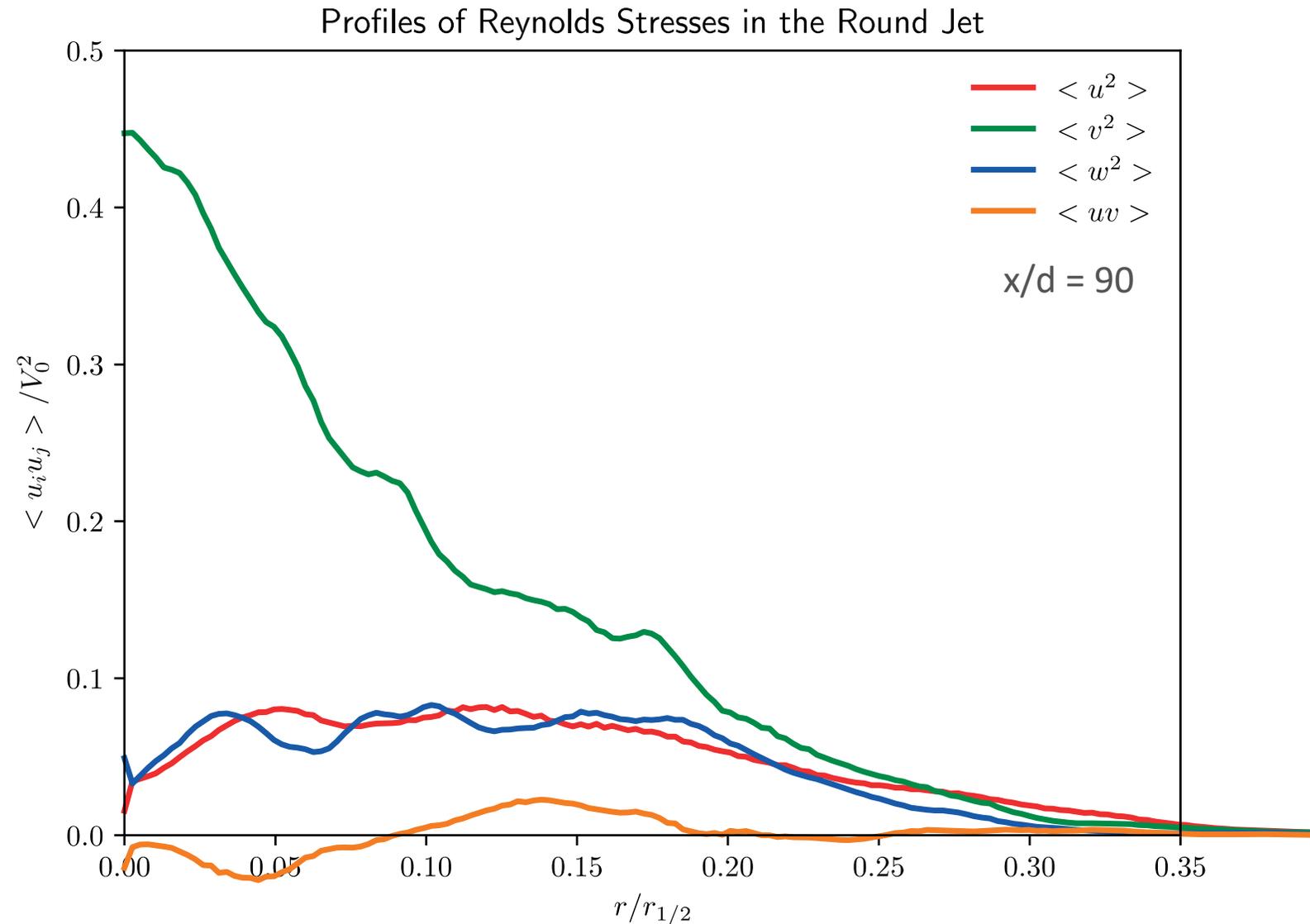
Variation with Axial Distance of Mean Velocity along Centerline



sCO₂ Jet: Reynolds Stresses

- General trends for Reynolds stresses match experimental data but magnitude is very high due to current time in simulation.

Note: Simulation has not yet reached statistically stationary steady state



Where will these results take us?

Next Steps

Future Work

So far, we've simulated an ideal gas case to verify jet setup and an sCO₂ case to establish that PeleC can handle simulations at supercritical conditions. Next, we will:

- Continue sCO₂ simulations to reach a statistically stationary state in order to improve accuracy of velocity profile and Reynolds stress information
- Incorporate subgrid scale models to perform Large Eddy Simulation (LES)
- Simulate sCO₂ jet injection into ambient air to incorporate more complicated dynamics and applications

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Questions?

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Julia Ream, jream@nrel.gov

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