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# **Effects of Reactive Power on Photovoltaic Inverter Reliability and Lifetime**

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## Introduction

- An inverter subsystem is critical for the overall PV system reliability
- An inverter system receives the largest amount of service calls for operation and maintenance [1]
- Physics of failure assessment using thermal cycling is used for determining

# **Development of in-house** inverter

• Two stage inverter rated at 1kW, with a synchronous DC-DC boost converter and H-bridge DC-AC inverter

• Inverter designed to operate in grid connected mode and has capability of reactive power support

## **Results of electrothermal** model

- Temperature measurements from the simulation verified with thermocouple measurements on the power switches of in-house inverter
- The temperature values from simulation matches the hardware measurements

# Lifetime model

- Rain flow counting used to record the number of device cycles, N<sub>i</sub>, under difference each junction in temperature,  $\Delta T_i$
- A simplified Coffin-Manson model is used to estimate the number of cycles to failure, N<sub>f</sub>

 $N_f = a \times (\Delta T_i)^{-n}$ (1)

### overall system reliability and lifetime

- Mission profile of ambient temperature solar irradiance translates into and junction temperatures of power switches
- New grid codes [2] require PV inverters to provide reactive power support
- A mission profile approach was used to study the impacts of reactive power on the inverter system reliability and lifetime



Photo by Ramanathan Thiagarajan, NREL Loss model

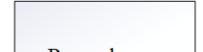
inverter model the Loss was OŤ developed in PLECS

# Workflow used to calculate lifetime of inverters

Loss model included semiconductor loss and con

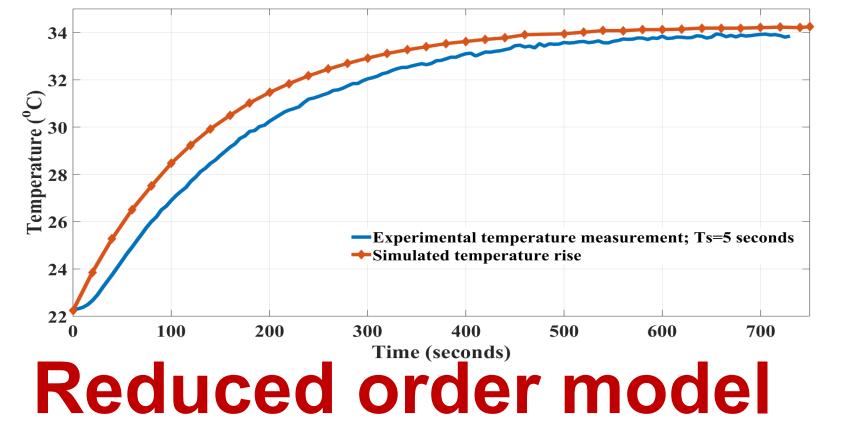


ses,	inductor	losses,	
ductior	n losses		



within 1°C accuracy at steady-state

- Model was validated by placing inhouse inverter inside thermal chamber
- was operated at 500W in Inverter ambient temperatures of 25°C, 35°C, and 45°C and hardware results matched simulation values

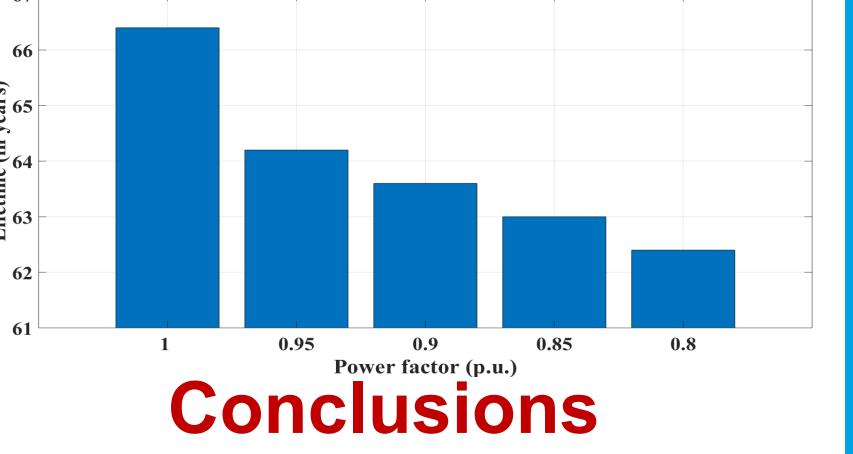


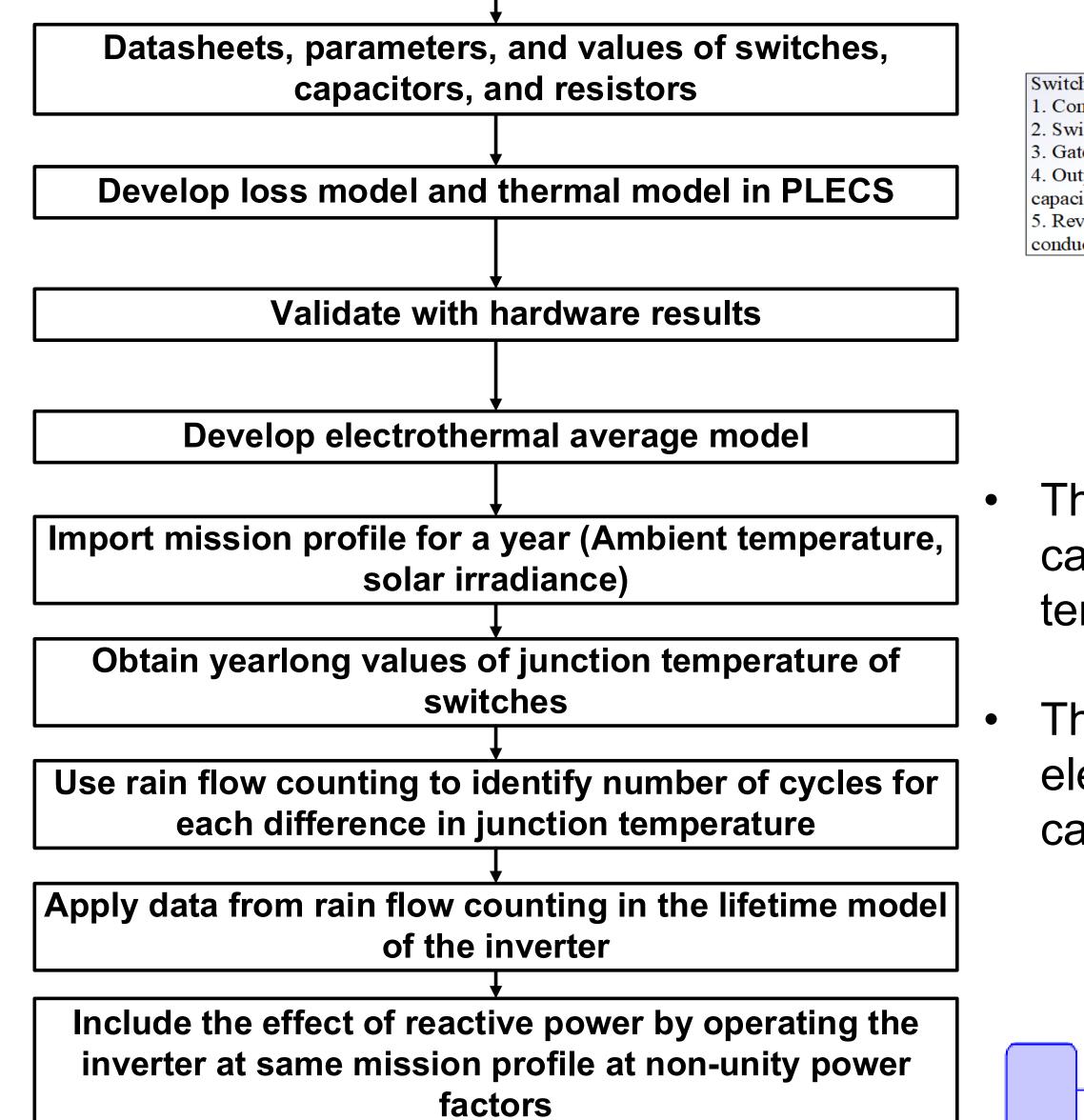
- Computational time of a switching model is large for year-long profile
- the reduced order Improved upon

- N<sub>f</sub> is related with the N<sub>i</sub> to estimate cumulative damage, Q for various  $\Delta T_i$  $Q = \sum_{i=1}^{n} \frac{N_i}{N_{ci}}$
- The reciprocal,  $\frac{1}{0}$  gives the number of mission profiles the device can survive, defined as Remaining Useful Lifetime

# Impact of reactive power

- Phoenix TMY reduced order model was repeated for non-unity power factors of 0.8 p.u. to 0.95 p.u.
- Results showed inverter lifetime decreasing as power factor moves away from unity

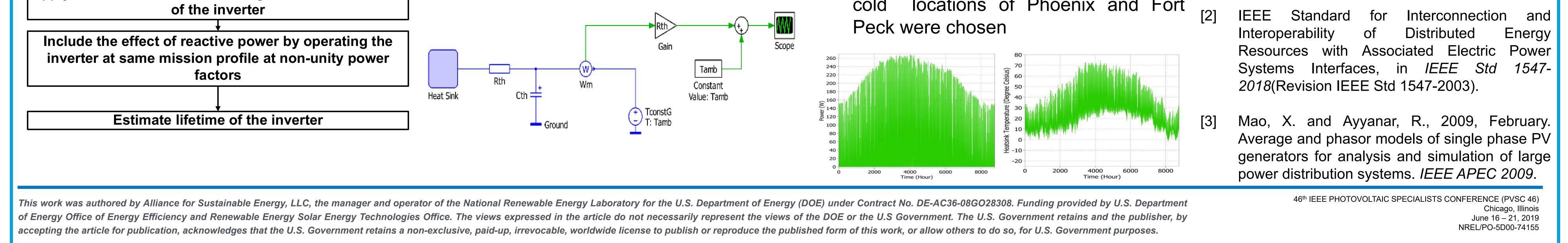




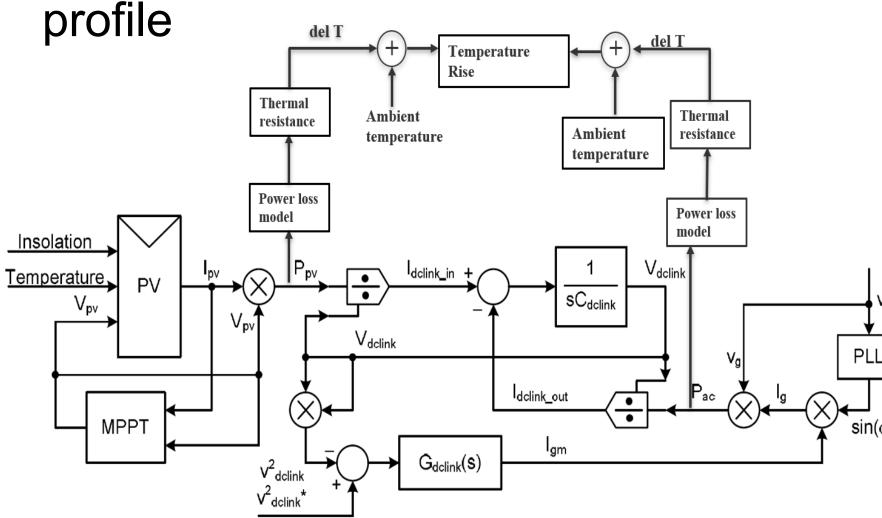
### Power losses . Conduction losses 2. Switching losses . Gate charge losse 4. Output Inductor Internal resistance 1. Conduction losses capacitance losses 1. Conduction losses . Conduction losses 2. Core losses 5. Reverse conduction losses

### **Thermal model**

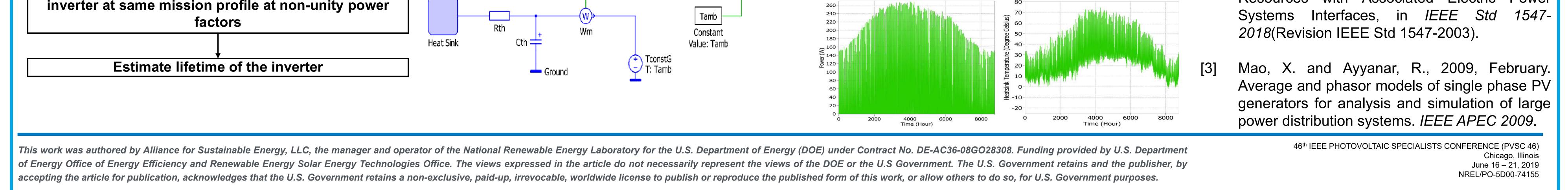
- translates the Thermal model losses calculated in loss model into increase in temperature of power device
- Thermal model described using lumped elements of thermal resistances and capacitances



developed in [3] with thermal model model OSS measure and to temperatures over a year-long mission



- To account for variations in temperature and irradiance at a location over many years, the Typical Meteorological Year (TMY) data was used
- Two representative extreme hot and locations of Phoenix and Fort cold



- Reduced order electrothermal model was developed from detailed switching model to translate mission profile data into junction temperature of switches
- Reduced order model was repeated for non-unity power factors
- Inverter lifetime reduces as the power factor moves away from unity References
- Golnas, A., 2012, June. PV system reliability: [1] An operator's perspective. 2012 IEEE PVSC.