

Smart Inverter Utility Experience in Hawaii

Andy Hoke, PhD, PE
National Renewable Energy Laboratory
Chair, IEEE P1547.1 Working Group
(Testing and Validation of IEEE 1547 DER Interconnection Requirements)

IEEE PES General Meeting Tutorial on Smart Inverters for Distributed Generators
August 4, 2019
Atlanta, Georgia

- 1. Background – why Hawaii?**
- 2. Selected technical challenges**
- 3. Case study – volt-var and volt-watt**
- 4. Case study – frequency-watt**

- Highest distributed PV capacity of any state (as percentage of load)
 - ~50% of peak load
 - High electricity costs for geographic reasons
 - Historical PV incentives
- First state to mandate a 100% renewables goal (100% by 2045)
 - Distributed PV will play a major role due to land constraints
- Peak island-wide inverter penetrations of 50%-80% in 2018 (depending on island)

Cumulative Solar Installations*

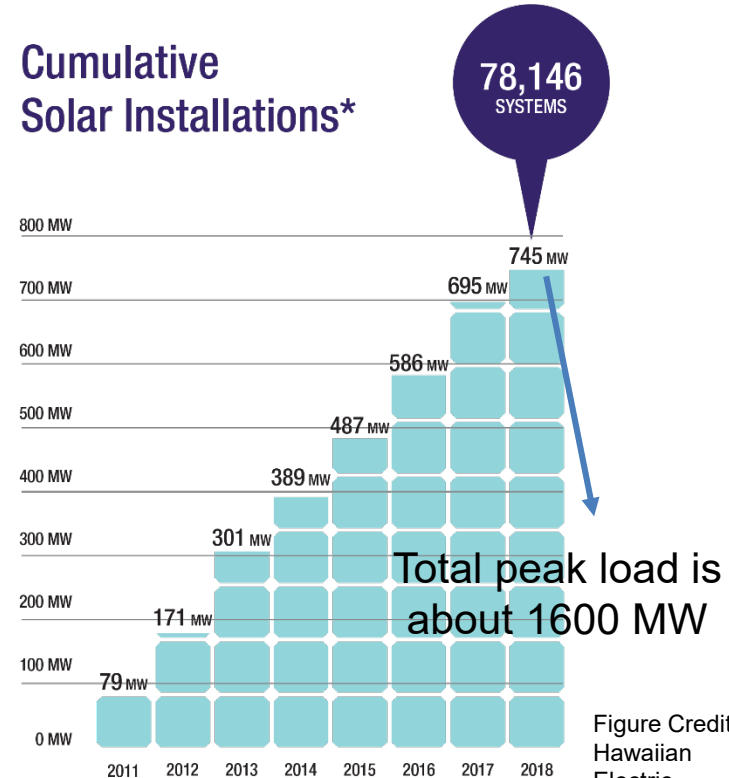
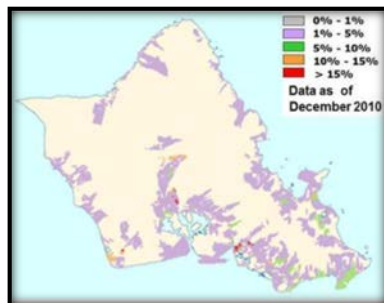


Figure Credit:
Hawaiian
Electric
Companies

*Systems installed or approved

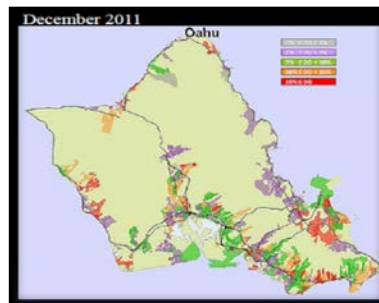
- Hawaii's Rule 14H (DER interconnection) has led the way in smart inverter functionality adoption in the U.S. (along with California's Rule 21)
- Hawaii required some advanced functionality even before it could be tested and certified under UL 1471 SA
- Advanced inverter functions currently required in Hawaii:
 - Voltage and frequency ride-through
 - Transient overvoltage mitigation (self-certification)
 - Volt-var control
 - Frequency-watt control
 - Soft-start
 - Ramp-rate control
 - Volt-watt (currently optional; under discussion for blanket activation)
 - Remote upgrade capability
- So far, no requirement for communications between utility and inverter

Distribution PV Penetration (Oahu Example)



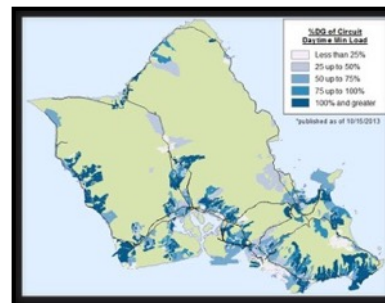
2010

Many feeders
> **1%**
Gross
daytime
minimum
load (GDML*)



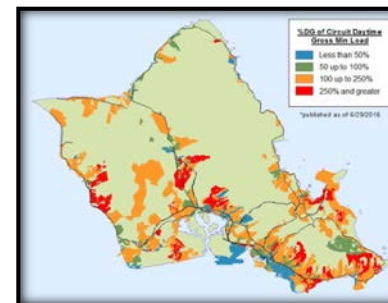
2011

Many feeders
> **15%**
GDML



2013

Many feeders
> **100%**
GDML



2016

Many feeders
> **250%**
GDML

*GDML = The minimum feeder load the utility would see during daylight hours if PV were not present
Slide courtesy of Adam Warren, NREL. (Modified)













Generating Facilities

These maps show existing and planned generating facilities and the maximum potential power in megawatts (MW) they can produce.

F FIRM GENERATION: Energy available on demand, which can be adjusted as needed.

V VARIABLE GENERATION: Energy that may not always be available or controllable.

BESS: Battery Energy Storage System

- | | |
|--|---|
|  BIOFUELS |  STORAGE |
|  BIOMASS |  WASTE TO ENERGY |
|  GEOTHERMAL |  WIND |
|  HYDRO |  COAL |
|  CUSTOMER-SITED SOLAR |  OIL |
|  GRID-SCALE SOLAR |  OIL (DEACTIVATED) |

O'AHU

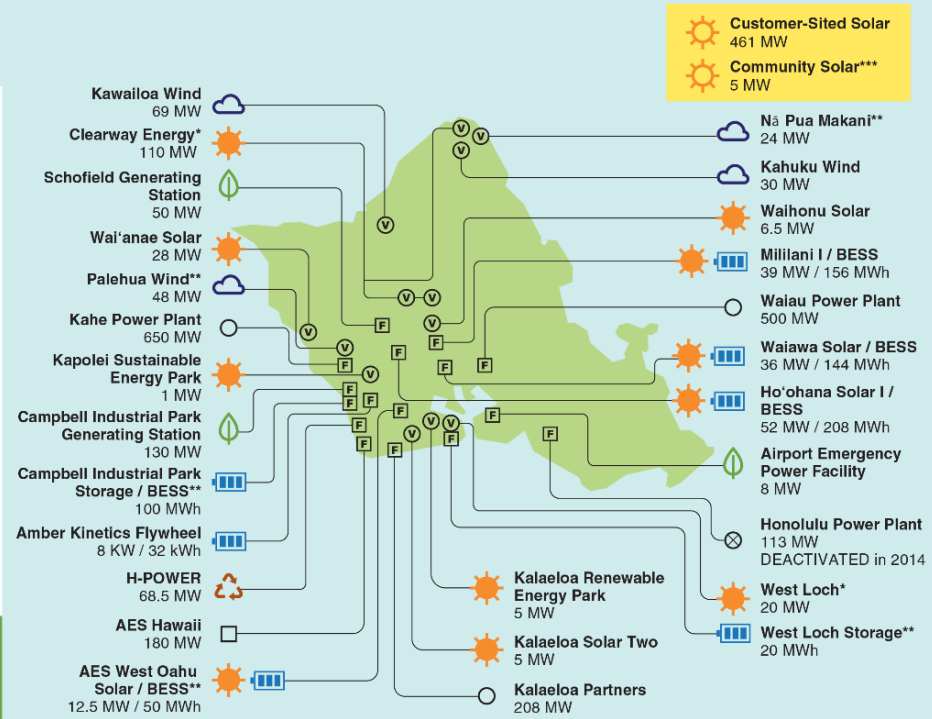
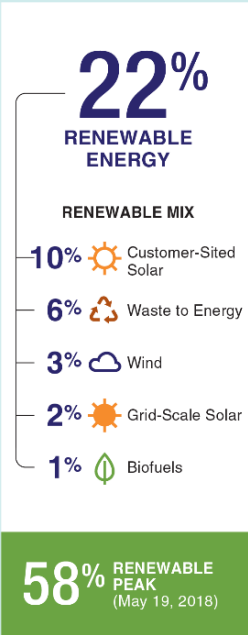


Figure Credit:
Hawaiian Electric Companies

System-Wide PV Penetration (Maui Example)













Generating Facilities

These maps show existing and planned generating facilities and the maximum potential power in megawatts (MW) they can produce.

F FIRM GENERATION: Energy available on demand, which can be adjusted as needed.

V VARIABLE GENERATION: Energy that may not always be available or controllable.

BESS: Battery Energy Storage System

- | | |
|--|---|
|  BIOFUELS |  STORAGE |
|  BIOMASS |  WASTE TO ENERGY |
|  GEOTHERMAL |  WIND |
|  HYDRO |  COAL |
|  CUSTOMER-SITED SOLAR |  OIL |
|  GRID-SCALE SOLAR |  OIL (DEACTIVATED) |

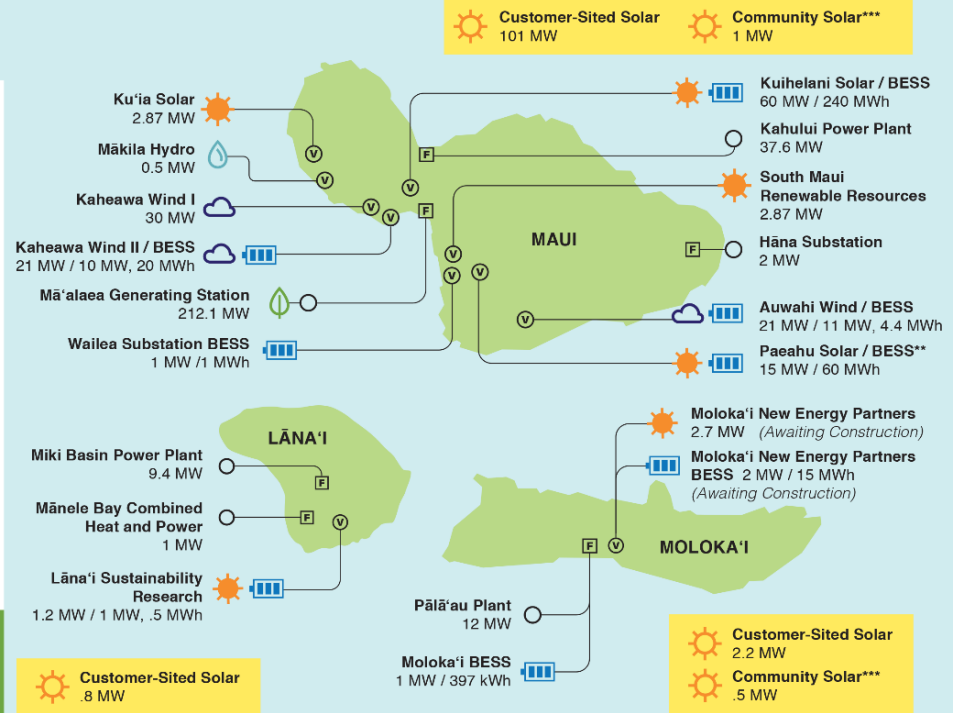
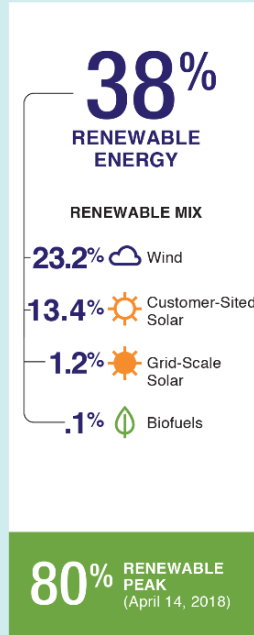
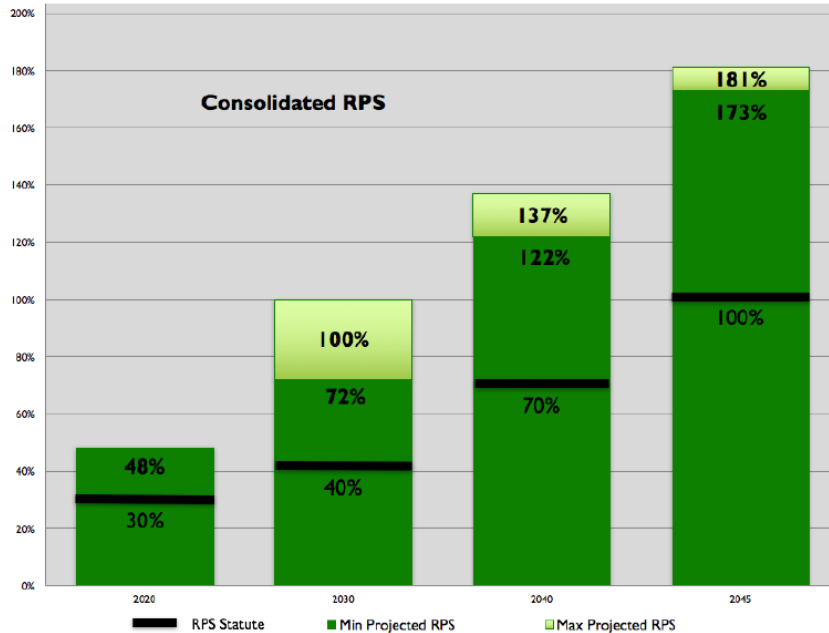


Figure Credit:
Hawaiian Electric Companies

Total renewable penetration:

$$\equiv \frac{\text{renewable kWh generated}}{\text{utility kWh sold}}$$



Total distributed PV

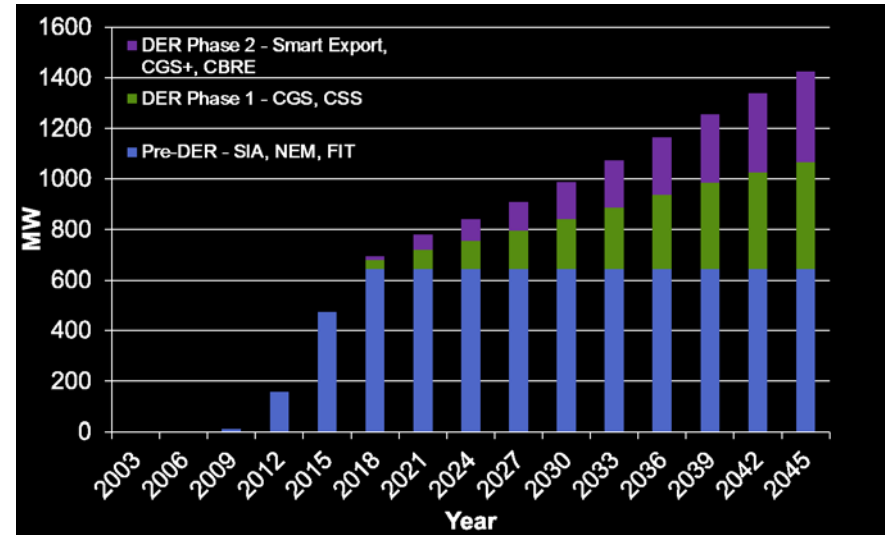


Figure Credits:
 Hawaiian Electric Companies

1. Background – why Hawaii?
- 2. Selected technical challenges**
3. Case study – volt-var and volt-watt
4. Case study – frequency-watt

Selected Technical Challenges

Existing and past challenges

- Steady-state voltage issues
- Islanding and transient voltage issues (GFOV/TOV, LROV/TrOV)
- Deterioration of frequency response (reduction of inertia, PFR, regulation)
- Lack of visibility and controllability of DER and grid-edge conditions
- Extremely difficult to change settings of legacy inverter fleet (due to logistical, cost, and policy challenges)
- ...

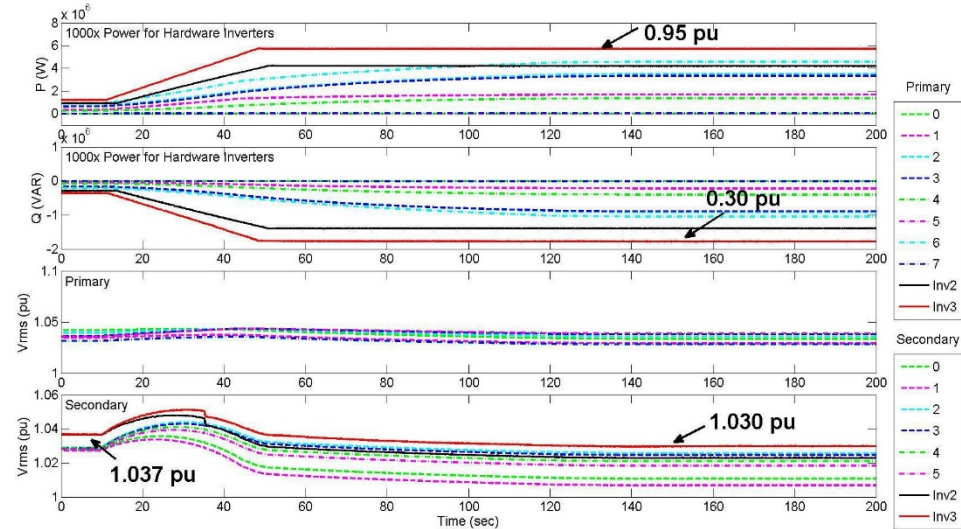
Emerging and future challenges

- Operation of very low inertia grids with 80-100% inverter-based generation at times
- Balancing load and variable generation across multiple timescales
- Control of thousands of individual customer-owned DERs
- Cybersecurity of DERs (manufacturer communications; possible future utility/aggregator comms)
- ...

- Activating relatively wide voltage and frequency ride-through capabilities was step #1 towards successfully operating a grid with high levels of PV
- “Legacy” inverters that don’t have ride-through capability (or can’t easily have ride-through enabled) are an ongoing system stability problem
 - *Lesson learned: require voltage and frequency ride-through capability and relatively wide trip settings early to avoid future problems when more DERs come online*
 - *This required compromises between transmission and distribution planners*
- By working with Enphase, Hawaiian Electric was able to retroactively widen voltage and frequency trip settings for many legacy DERs
 - This was a major effort and would be even harder in a market not dominated by one manufacturer
 - Would not have been possible without Enphase’s communication solution, which many other inverter manufacturers may not have

- In 2015 and 2016, HECO and NREL tested advanced functionality of several inverters:
 - V and F ride-through
 - Ramp rate control and soft start
 - Fixed power factor
 - Volt-var and volt-watt
- Tests conducted at NREL's ESIF*:
 - Baseline tests to characterize inverter responses (*pre UL1741 SA*)
 - Power HIL tests to validate inverter behavior while connected to a real-time simulation of HECO's system
- Conclusions:
 - Inverters largely performed as expected
 - Anomalous behavior was reported to manufacturers and fixed (firmware upgrade)
 - Smart inverter functions generally benefit grid operations

Example power HIL test of two inverters at fixed PF of 0.95 (absorbing) in volt-watt control mode



<https://www.nrel.gov/docs/fy17osti/67485.pdf>

*ESIF = Energy Systems Integration Facility, DOE's flagship lab for smart grid and related testing.

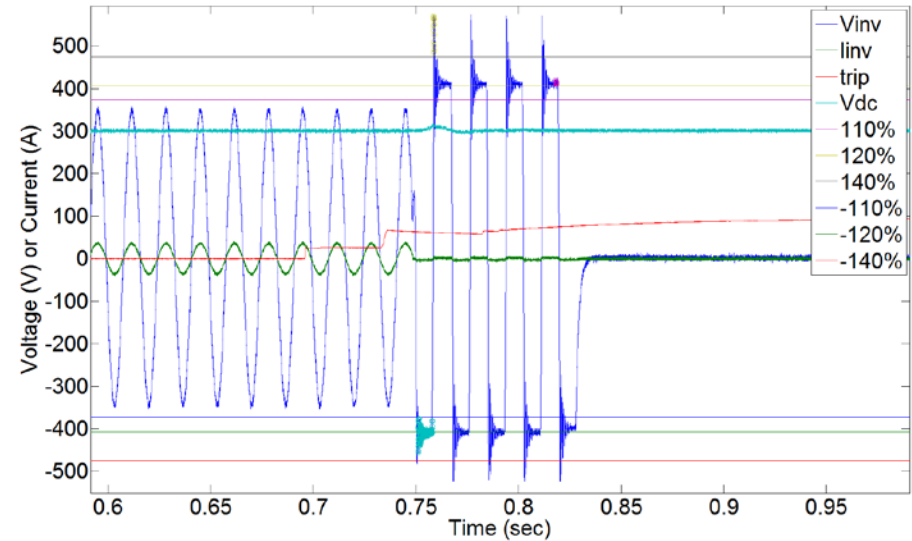
**HIL = Hardware-in-the-loop: A computer simulation running in real-time linked to actual hardware.

- As feeders began backfeeding substations, *load rejection overvoltage* became a concern
- SolarCity, HECO, and NREL collaborated to test several inverters' load rejection responses
- FIGII* developed consensus test procedure to quantify LROV response
- NREL evaluated load rejection response of five inverters in ESIF lab
- Typically, inverters disconnected very quickly, avoiding potentially damaging overvoltage

Outcomes:

- HECO required all inverters be tested for LROV prior to interconnection, and increased feeder PV limit from 120% of GDML to 250% of GDML
- LROV test now incorporated into draft IEEE 1547.1 (and so will become part UL 1741 in 2020)

Example LROV test waveform at 10:1 generation:load ratio



<http://www.nrel.gov/docs/fy15osti/63510.pdf>

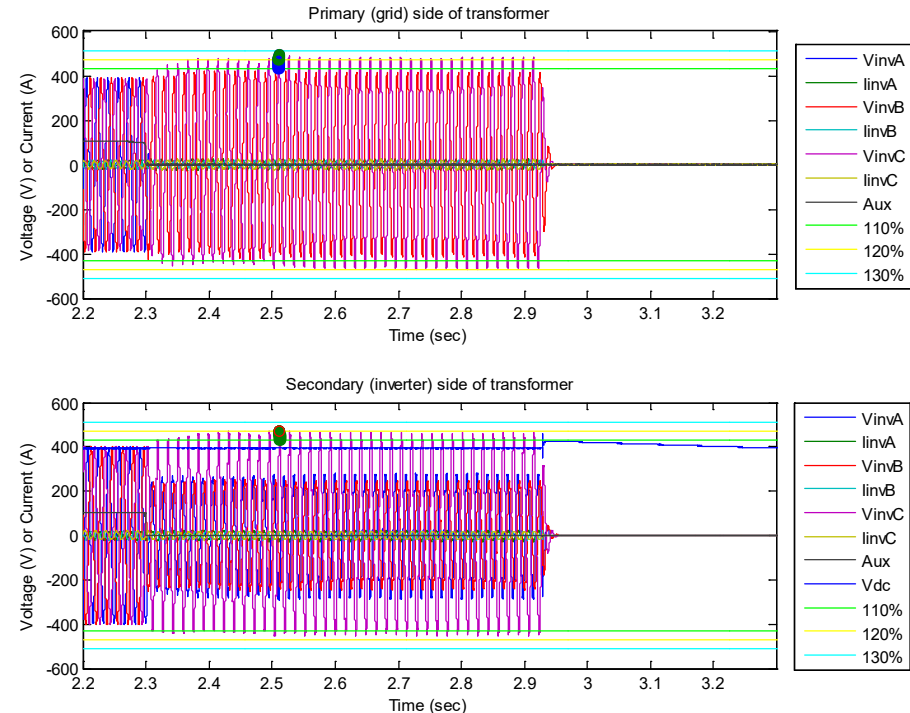
Solutions: GFOV

- As high-PV feeders began backfeeding substations, *ground fault overvoltage* became a concern
- SolarCity, HECO, and NREL collaborated to test several inverters' ground fault responses
- FIGII developed consensus test procedure to quantify GFOV response
- NREL evaluated three inverters in ESIF lab

Findings:

- Inverters do not maintain line-line voltages and typically disconnect quickly, avoiding potentially damaging overvoltage, but may remain connected briefly when fault is masked by transformer
- Where a GFOV may occur in a location that could be islanded with balanced real and reactive power, minimal wye-connected load, and no zero-sequence continuity to the DER location, an analysis may be needed to evaluate the possibility of damage to surge arrestors

Example GFOV test waveforms with fault masked by D:Y transformer



See [IEEE C62.92.6](http://www.ieee.org/standards/publications/62.92.6) for GFOV with inverters

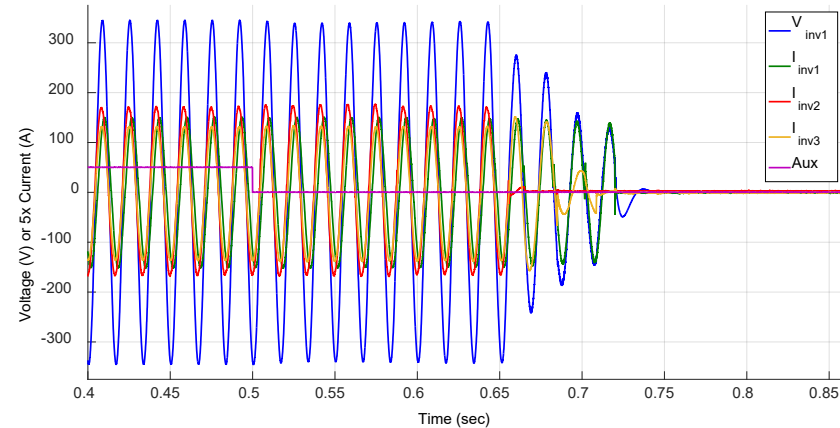
<http://www.nrel.gov/docs/fy15osti/64173.pdf>

- With rollout of ride-through (V and f) and other smart inverter functions, possible conflicts with inverter anti-islanding controls became a concern
- HECO, NREL and SolarCity tested the effects of ride-through, volt-var, and frequency-watt on three inverters' anti-islanding performance
- Tests included cases with multiple inverters connected at multiple neighboring locations on the same feeder

Outcomes

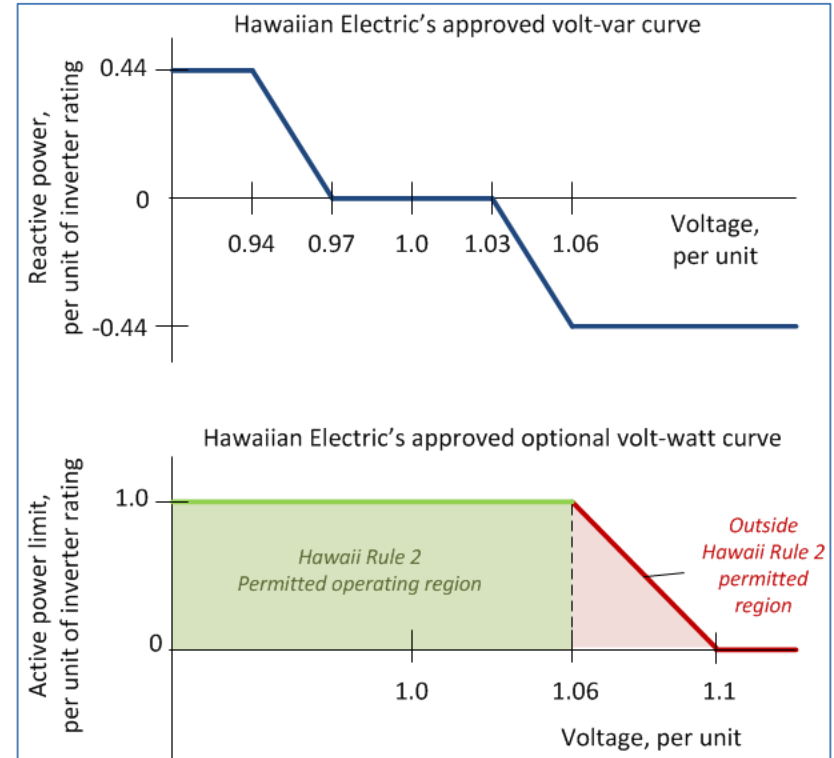
- No islands were found to extend beyond 0.7 seconds
- Volt-var and frequency-watt control had no statistically significant impact on island duration
- Ride-through tended to extend island duration by ~ 75 ms
- HECO relies on inverter anti-islanding in almost all cases. HECO recloser time settings are long enough to minimize the chance of out-of-phase reclosure

Example multi-inverter island test waveforms



1. Background – why Hawaii?
2. Selected technical challenges
- 3. Case study – volt-var and volt-watt**
4. Case study – frequency-watt

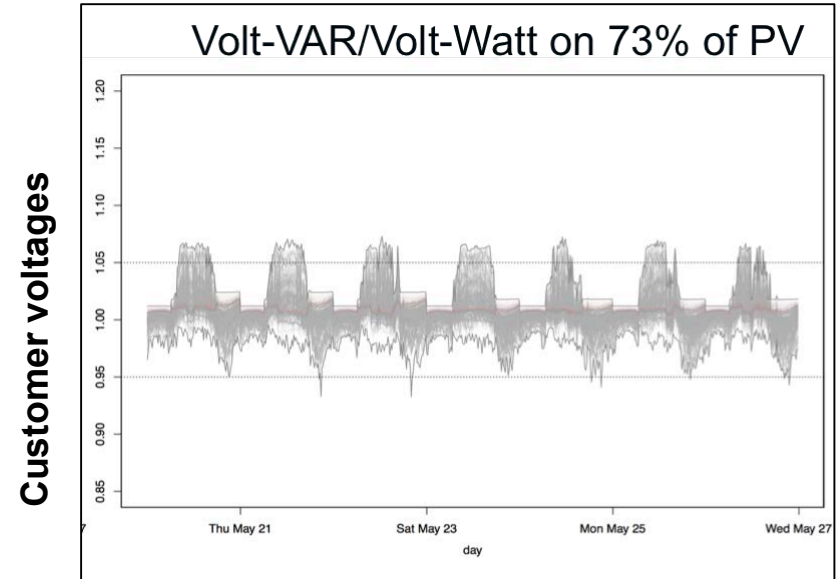
- PV at unity PF causes steady-state overvoltage issues in some locations
- Currently impractical to actively control thousands of individual PV systems
- Near-term solution: autonomous inverter responses
 - Fixed power factor operation
 - Volt-var control
 - Volt-watt control
- HECO initially required PV systems operate at 0.95 PF (absorbing vars)
- NREL, HECO, and industry collaborators expected volt-var control be more beneficial (to all) than fixed PF
- NREL and HECO conducted several studies
 - Detailed time-series simulation
 - Field pilot study
 - Lab testing at ESIF
 - Objective: Quantify impacts on utility and on customers (i.e. curtailment?)



Detailed feeder simulations:

- NREL and HECO performed detailed quasi-static time-series analysis of two HECO feeders to evaluate 0.95 PF, volt-var control, and volt-watt control
 - *Accurate analysis of volt-var and volt-watt requires modeling of secondary circuits*
- Volt-var was found to result in fewer voltage violations, fewer tap-changer operations, reduced losses, and less PV curtailment than fixed PF of 0.95
- PV energy curtailment due to volt-var and volt-watt was near zero in almost all cases, with a few outliers
- Also simulated cases with self-supply PV-battery systems.
 - Lower voltages
- HECO now requires volt-var for all new DERs

Example weekly simulation of feeder with 6.8 MW of distributed PV



<https://www.nrel.gov/docs/fy17osti/68681.pdf>

<https://www.nrel.gov/docs/fy19osti/72298.pdf>

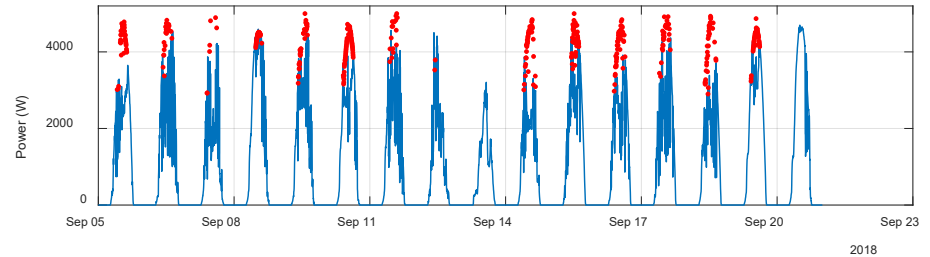
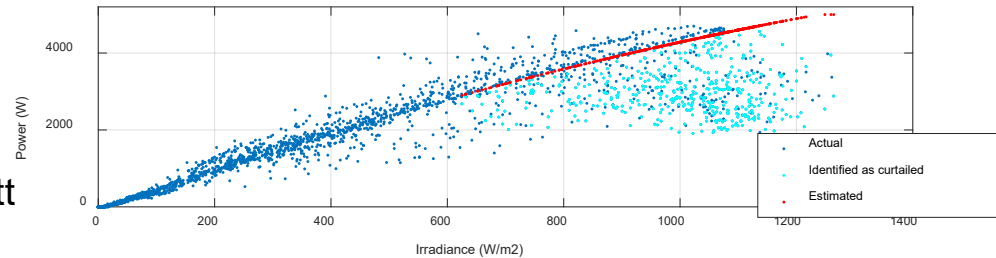
Pilot study:

- NREL and HECO installed monitoring, sensors, and communications to about 30 PV locations expected to have high voltage

Findings

- Voltages were typically lower than expected
 - Limited information available in planning studies leads to conservative assumptions
- PV energy curtailment due to volt-var and volt-watt was typically zero or near-zero
 - Curtailment of >1% identified in two cases
 - One location mitigated through conventional (wires) solution
 - Other location has ~1.1% curtailment. Mitigation needed?
- Large-scale deployment of sensing for accurate curtailment estimates is cost-prohibitive for residential-scale PV

Estimating PV curtailment due to volt-var and volt-watt using plane-of-array irradiance data during an unusual high-voltage period



<https://www.osti.gov/servlets/purl/1464444>

Case Study: Volt-Var and Volt-Watt Control

Conclusions:

- Volt-var and volt-watt control are useful tools for mitigating high customer voltages due to behind-the-meter PV
 - Volt-var curtailment impacts on PV production are typically near-zero (at least for the volt-var curve used in Hawaii)
 - If the sloping region of the volt-watt curve is outside ANSI Range B (1.06 pu), volt-watt provides a backstop against occasional high voltages while maintaining near-zero curtailment
- It is difficult to predict in advance exactly which locations will have high voltages, and periods of high voltage sometimes occur for a few days at a time due to feeder reconfigurations (utility switching)
- Volt-var and volt-watt are most beneficial if deployed system-wide

Ongoing work and next steps:

- HECO deploying AMI with all new PV systems
 - NREL receiving and analyzing AMI data in ESIF High Performance Computing (HPC) Center
 - NREL and HECO developing “non-wires alternatives toolbox” for mitigation of high voltages
- Most new PV systems in Hawaii now have integrated battery storage – daytime export is no longer economical in most cases
 - This helps maintain voltages within ANSI Range A
 - Leverage storage for other purposes?

1. Background – why Hawaii?
2. Selected technical challenges
3. Case study – volt-var and volt-watt
4. **Case study – frequency-watt**

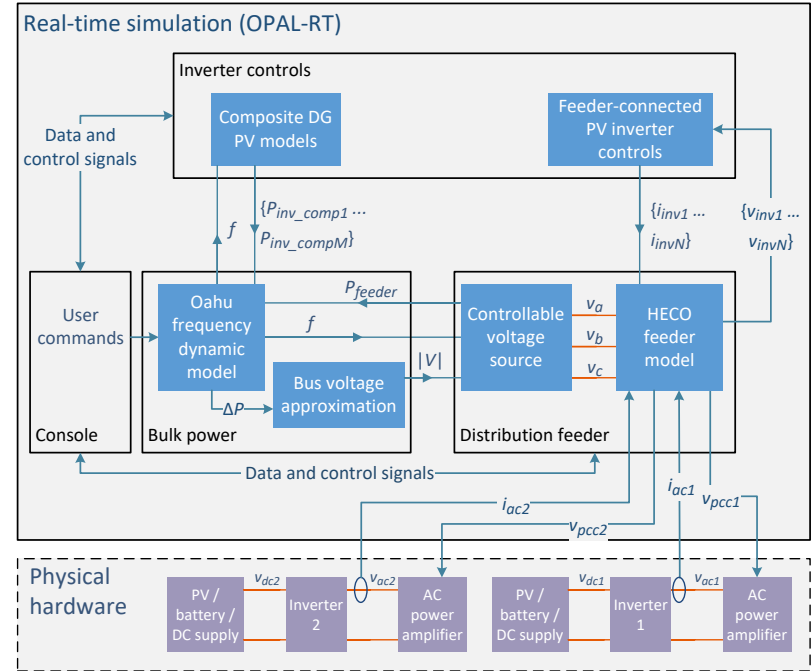
- As PV displaces conventional generation, system frequency stability is degraded
- DERs can help mitigate this by providing rapid frequency response (e.g. frequency-watt droop)

DOE GMLC project (HECO-NREL-SNL) examined ability of real hardware inverters to provide fast droop response

Approaches:

- Inverter hardware response characterization
- PSSE simulations
- Stability analysis
- Inverter controls development
- PHIL tests (at NREL ESIF)

PHIL Test Setup Including Real-time Model of Oahu Power System



<https://www.nrel.gov/docs/fy17osti/68884.pdf>

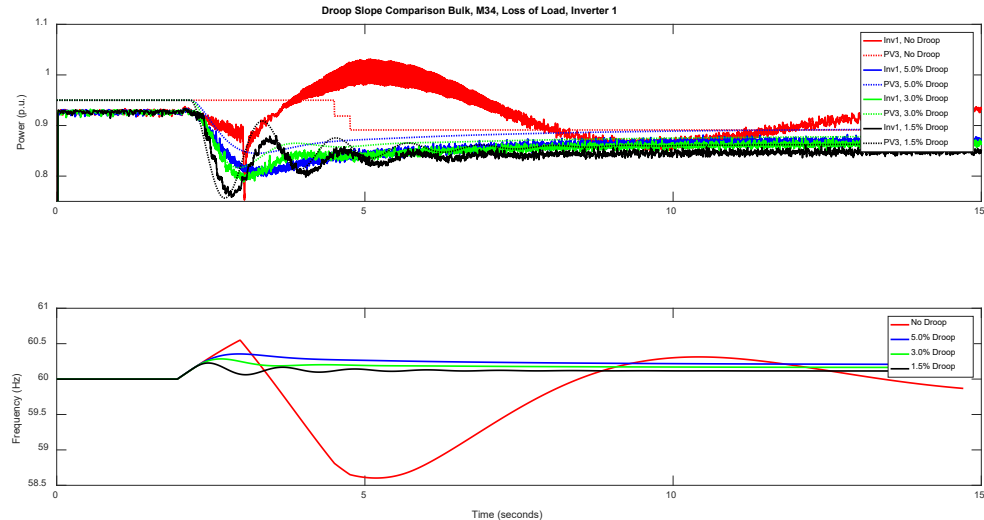
Findings:

- Many (but not all) off-the-shelf inverters can respond very quickly (sub-second) to frequency events
- At the time of testing (2017), most inverters only provided overfrequency response (even if headroom for underfrequency response available)
- *Fast response is needed to mitigate frequency events in low inertia systems*
- Under-frequency load-shedding (UFLS) can make DER frequency response less effective

Outcomes:

- IEEE 1547-2018 allows for very fast frequency droop if needed
 - Very fast response may not be needed/desired in all cases
- HECO now requires freq-watt for all new DERs

Example PHIL test of overfrequency event demonstrating DER inverters mitigating cascading event



<https://www.nrel.gov/docs/fy17osti/68884.pdf>

Conclusions

- Activating relatively wide voltage and frequency ride-through early is step #1 towards successfully operating a grid with high levels of PV
- Inverter anti-islanding controls were found reliable even with grid support active, and even in the multi-inverter, multi-PCC scenarios tested
- LROV concerns are easily mitigated through type-testing; GFOV is more complicated (but is not a problem if zero-sequence continuity is maintained)
- Power HIL tests validate the benefits of advanced inverter functions
- For feeders with very large numbers of distributed inverters, volt-var control is more beneficial to the utility and the customers than fixed PF
- Volt-watt control is beneficial as a backstop against high customer voltages, especially given limited grid-edge visibility
- Ensuring the correct inverter settings are deployed in field requires verification
- Smart inverters won't solve all your problems, but they can help!

Questions and possible next steps

- How to transition older “legacy” PV systems to advanced inverters?
- DER inverter fault response? Is “momentary cessation” okay if 100+ MW of distributed inverters do it?
- Grid services from DERs?
 - Bulk grid services? Local services? Aggregators? DERMS? ... Cybersecurity?
- Inverter data integration into utility systems?
 - Planning? Operations?
- Coordinated control of DERs?
- What other utility devices are needed in ultra-high DER world? D-STATCOMs? Synchronous condensers?
- What is the role of grid-forming inverters?
- Which of the above are appropriate for DERs vs larger utility-scale PV-battery plants?

Thank you!

Acknowledgements:

Many others contributed to the various projects mentioned here, especially Julieta Giraldez, Pete Gotseff, Nick Wunder, Austin Nelson, Rasel Mahmud, and Martha Symko-Davies at NREL; Earle Ifuku, Marc Asano, Reid Ueda, Reid Sasaki, Ken Fong, and Dean Arakawa at Hawaiian Electric; and Mohamed Elkhatab at Sandia. In addition, many members of industry contributed through Hawaiian Electric's Advanced Inverter Technical Working Group and other forums.

Thank you to NREL Energy Systems Integration Facility staff for facilitating hardware and PHIL testing.
Thank you to NREL Computational Sciences Center staff for computing and communications support.

Questions: Andy.Hoke@NREL.gov

NREL/PR-5D00-74091

This work was authored by the National Renewable Energy Laboratory, operated by Alliance for Sustainable Energy, LLC, for the U.S. Department of Energy (DOE) under Contract No. DE-AC36-08GO28308. Funding partially provided by U.S. Department of Energy Office of Energy Efficiency and Renewable Energy Solar Energy Technologies Office and Office of Electricity through the Grid Modernization Laboratory Consortium. Additional funding provided by The Hawaiian Electric Companies and SolarCity Corporation. The views expressed herein do not necessarily represent the views of the DOE or the U.S. Government. The U.S. Government retains and the publisher, by accepting the article for publication, acknowledges that the U.S. Government retains a nonexclusive, paid-up, irrevocable, worldwide license to publish or reproduce the published form of this work, or allow others to do so, for U.S. Government purposes.

- Advanced inverter testing including power HIL: <https://www.nrel.gov/docs/fy17osti/67485.pdf>
- Load rejection overvoltage testing: <http://www.nrel.gov/docs/fy15osti/63510.pdf>
- Inverter ground fault overvoltage testing: <http://www.nrel.gov/docs/fy15osti/64173.pdf>
 - GFOV analysis: <https://ieeexplore.ieee.org/abstract/document/7486059/>
 - Standard for GFOV with inverters: https://standards.ieee.org/standard/C62_92_6-2017.html
- Detailed time-series simulation of volt-var, fixed PF, and volt-watt: <https://www.nrel.gov/docs/fy17osti/68681.pdf>
- Frequency-watt testing and simulation including power HIL: <https://www.nrel.gov/docs/fy17osti/68884.pdf>
- Experimental Evaluation of PV Inverter Anti-Islanding with Grid Support Functions in Multi-Inverter Island Scenarios: <https://www.nrel.gov/docs/fy16osti/66732.pdf>
- Advanced Inverter Voltage Controls: Simulation and Field Pilot Findings: <https://www.nrel.gov/docs/fy19osti/72298.pdf>
- Energy System Integration, High Penetration PV: How High Can We Go? <http://www.nrel.gov/docs/fy16osti/65591.pdf>
- Control of utility-scale inverter-based plants for grid benefits (not discussed in above presentation):
 - Gevorgian, V. and B. O'Neill, *Advanced Grid-Friendly Controls Demonstration Project for Utility-Scale PV Power Plants*: <https://www.nrel.gov/docs/fy16osti/65368.pdf>
 - Gevorgian, V. et al. *Demonstration of Essential Reliability Services by a 300-MW Solar Photovoltaic Power Plant*: <http://www.nrel.gov/docs/fy17osti/67799.pdf>
- IEEE 1547-2018: <https://ieeexplore.ieee.org/document/8332112> (national DER interconnection standard)
- IEEE C62.92.6: https://standards.ieee.org/standard/C62_92_6-2017.html (GFOV and inverters)