

A Comparison of Ultimate Loads from Fully and Sequentially Coupled Analyses

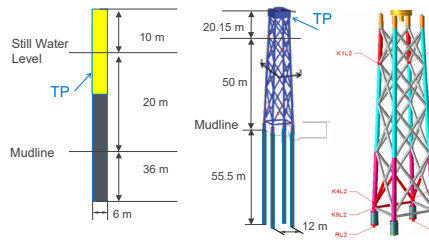
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INTRODUCTION

The design and analysis methods for offshore wind turbines must consider the aerodynamic and hydrodynamic loads and response of the entire system (turbine, tower, substructure, and foundation) coupled to the turbine control system dynamics. Although a **fully coupled** (turbine and support structure) modeling approach is more rigorous, intellectual property concerns can preclude this approach. In fact, turbine control system algorithms and turbine properties are strictly guarded and often not shared. In many cases, a partially coupled analysis using separate tools and an exchange of reduced sets of data via sequential coupling may be necessary. In the **sequentially coupled** approach, the turbine

and substructure designers will independently determine and exchange an abridged model of their respective subsystems to be used in their partners' dynamic simulations. Although the ability to achieve design optimization is sacrificed to some degree with a sequentially coupled analysis method, the central question here is whether this approach can deliver the required safety and how the differences in the results from the fully coupled method could affect the design. This poster summarizes the scope and preliminary results of a study conducted for the Bureau of Safety and Environmental Enforcement (BSEE) aimed at quantifying differences between these two modeling approaches through aero-hydro-servo-elastic simulations of two offshore wind turbines on a monopile and jacket substructure.

SUBSTRUCTURES



TURBINE PARAMETERS

Parameter	Value
Rating [MW]	5
International Electrotechnical Commission Class	1-B
Rotor Configuration	Upwind, 3 blades
Control	Variable speed, collective pitch
Drivetrain	Multistage gearbox
Rotor Hub Diameter [m]	120.3
Hub Height [m]	90
Cut-In, Rated, Cut-Out Wind Speeds [m/s]	3, 11.4, 25 m/s
Cut-In, Rated, Cut-Out Rotor Speeds [rpm]	6.9, 12.1 rpm
Rated Tip Speed [m/s]	80
Overhang, Shaft Tilt, Precone	5 m, 5°, 2.5°
Rotor Mass [tonnes]	110
Nacelle Mass [tonnes]	240
Acceptable System First Eigenfrequency Range [Hz]	(0.22, 0.3) Soft-stiff

Figure 3. Select substructures for this study: monopile (left, from the Offshore Code Comparison Collaboration [1]) and jacket (right, from Offshore Code Comparison Collaboration Continuation [2])

NREL 5-MW Turbine [3]

MODELING APPROACHES

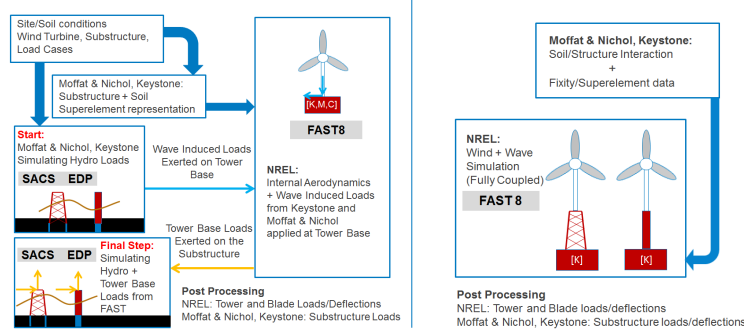


Figure 1. Sequentially coupled approach with NREL in the role of the turbine original equipment manufacturer (OEM) and Moffat & Nichol/Keystone in the role of the substructure OEM (left). For the fully coupled approach (right) the entire offshore wind system is modeled at NREL via FAST v8.

ENVIRONMENTAL CONDITIONS

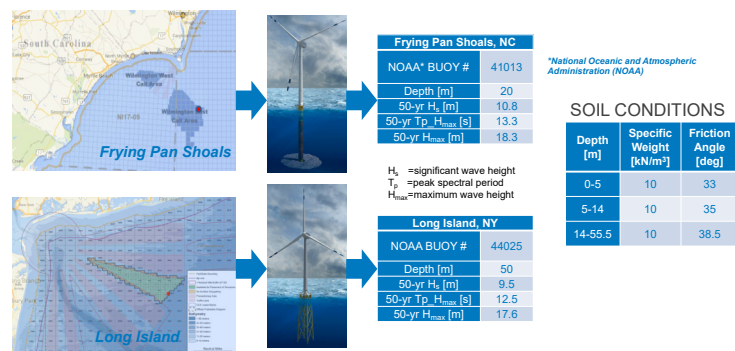


Figure 2. Geographical locations for the selected sites: Frying Pan Shoals, North Carolina (top, monopile location) and Long Island, New York (bottom, jacket location). Illustrations by Josh Bauer, NREL

MODEL-TO-MODEL VERIFICATION

Parameter	Monopile			Jacket		
	FAST	EDP	Delta (%)	FAST	SACS	Delta (%)
Tower Mass [kg]	237,001	43,821	-0.11	50,55	49,83	-1.43
Tower Z-CG abv. Still Water Line [m]	350,000	350,000	0.00	350,000	350,000	0.0001
Rotor Nacelle Assembly (RNA) Mass [kg]	89,571	89,57	0.00	89,57	89,57	0.0015
Substructure Mass (dry) [kg]	2,86E+05	285,432	0.03	6.74E+05	6.88E+05	-1.80
Substructure Z-CG (dry) abv. Still Water Line [m]	-5	-5	0.00	-21.90	-22.36	-2.08
Submerged Volume [m ³]	5.93E+02	595.49	0.00	497.36	497.31	0.01
Ballasted Volume [m ³]	0.00E+00	0.00	0.00	199.59	199.55	0.02
Buoyant Volume [m ³]				297.77	297.76	0.00
Eigenfrequency [Hz]	Monopile (Only Substructure)			Jacket (Only Substructure)		
	FAST	EDP	Delta %	FAST	SACS	Delta %
	2.75	2.76	-0.27	2.76	2.68	2.89
	2.75	2.76	-0.27	2.76	2.68	2.89
	5.93	5.93	0.02	5.90	5.25	-4.92
16.3	16.78	-2.98	5.41	-	-	
16.3	16.78	-2.98	7.63	7.43	2.71	

ACKNOWLEDGMENTS

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REFERENCES

[1] Jonkman, J., and W. Musial. 2010. *Offshore Code Comparison Collaboration (OCC) for IEA Task 23 Offshore Wind Technology and Deployment* (Technical Report). NREL/TP-5000-48191. National Renewable Energy Laboratory (NREL), Golden, CO (US). <http://www.nrel.gov/docs/11100/48191.pdf>.

LOAD CASES

Parameters	Design Load Case (DLC)-1.1 (Operational)		DLC-6.1a (Parked, 50-yr Extreme Conditions)	
	Monopile	Jacket	Monopile	Jacket
Wind Model	Normal Turbulence Model		Extreme Wind Turbulence Model	
Hub-Height Wind Speeds [m/s]	0	12 m/s	0	50 m/s at
Wind Direction [degrees]	0	0, 45	0	0, 45
Wave Model	Normal Sea State		Extreme Sea State	
Significant Wave Height H_s [m]/Peak Spectral Period T_p [s]	1.38/6.97	1.34/6.48	10.8/13.3	9.5/12.5
Wave Directions [degrees]	0, 45, 90, 135		Co-directional and 90° Misaligned	
Current Model	Normal Current Model		Extreme Current Model	
Subsurface Current Speed at SWL [m/s]	0.6		1.2	
Near-Surface Current [at -20 m]	0.084		0.349	
Tidal Conditions	Normal Water Level Range		Extreme Water Level Range	
Surge Tidal Offset [m]	1.25		2.5	
Simulation Length	10 min		10 min	
Yaw Misalignments [degrees]	0		0.20	
Number of Simulations	4	8	4	8

COMPARISON OF EXTREME LOADS

Monopile – DLC 1.1 (Operational)

	YawBearingFz	YawBearingMx	YawBearingMy	YawBearingMz	TowerBaseFz	TowerBaseMx	TowerBaseMy	TowerBaseMz	MSL_Mx	MSL_My	Mx_10m_depth	My_10m_depth	Fz_mudline	Fy_mudline	Mx_mudline	My_mudline	Mz_mudline			
Fully Coupled	3,568	5,274	5,653	5,974	981.4	282.6	5,900	23,330	72,470	5,974	25.9	81.9	28.9	91.9	1.4	0.6	8.7	34	103	6.0
Sequentially Coupled	4,328	5,014	5,842	6,036	1,012	271.8	7,245	22,120	72,900	6,036	24.6	82.3	27.7	92.2	1.4	0.6	9.7	32	104	6.0
Delta (%)	-21.4	-4.9	3.3	1.0	3.1	-3.8	22.8	-8.0	0.6	1.0	-4.8	0.6	-4.2	0.3	-2.8	-0.9	12	-4.5	0.6	0.1

Monopile – DLC 6.1a (Extreme Conditions)

	YawBearingFz	YawBearingMx	YawBearingMy	YawBearingMz	TowerBaseFz	TowerBaseMx	TowerBaseMy	TowerBaseMz	MSL_Mx	MSL_My	Mx_10m_depth	My_10m_depth	Fz_mudline	Fy_mudline	Mx_mudline	My_mudline	Mz_mudline			
Fully Coupled	3,429	2,697	3,941	6,086	1,057	860.9	5,764	65,050	62,680	6,086	72.9	73	83.9	89	3.5	3.6	8.6	114	112	6.1
Sequentially Coupled	3,526	2,642	3,943	5,661	1,008	893.8	5,981	69,260	58,550	5,661	78.0	67.6	88.4	80.4	3.5	3.2	8.5	102	97	5.7
Delta (%)	2.8	5.4	0.1	-7.0	-4.8	3.8	3.8	6.5	-6.6	-7.0	7.0	-7.0	5.4	-9.7	0.5	-12.7	-1.2	-10.3	-13.2	-7.5

Jacket – DLC 1.1 (Operational)

	YawBearingFz	YawBearingMx	YawBearingMy	YawBearingMz	TowerBaseFz	TowerBaseMx	TowerBaseMy	TowerBaseMz	RL_FZ	RL_FY	RL_FX	RL_MZ	RL_MY	RL_MX	RL_FZ	RL_FY	RL_FX	RL_MZ		
Fully Coupled	3,562	7,287	5,993	5,259	894.6	656.3	5,692	47,220	60,680	5,259	9,225	290	370	224	1,974	1,434	3,232	297	386	1,612
Sequentially Coupled	3,560	7,234	6,019	5,141	910.2	637.1	5,691	47,410	60,700	5,141	9,508	414	487	342	2,301	1,954	3,629	387	478	1,670
Delta (%)	-0.1	-0.7	0.4	-2.2	1.17	-2.9	0.0	0.4	0.0	-2.2	3.7	43.0	26	52.7	16.6	36.3	12.3	30.5	25.7	23.7

Jacket – DLC 6.1a (Extreme Conditions)

	YawBearingFz	YawBearingMx	YawBearingMy	YawBearingMz	TowerBaseFz	TowerBaseMx	TowerBaseMy	TowerBaseMz	RL_FZ	RL_FY	RL_FX	RL_MZ	RL_MY	RL_MX	RL_FZ	RL_FY	RL_FX	RL_MZ		
Fully Coupled	3,382	3,347	3,547	7,035	585.5	962.7	5,511	65,830	37,240	7,035	10,440	943	916	295	4,462	4,321	12,350	922.7	924.8	4,351
Sequentially Coupled	3,381	2,891	3,507	7,080	505.8	852.5	5,507	58,860	34,520	7,080	11,705	1,689	980	278	4,784	3,226	7,863	1,207	902.7	3,762
Delta (%)	0.0	-13.6	-1.1	0.6	-13.6	-11.4	-0.1	-10.6	-7.3	0.6	12.1	19.3	8.1	-5.8	6.8	21.6	-38.0	30.8	3.9	32.2

CONCLUSIONS

- Monopile:**
 - Turbine ultimate limit state (ULS) loads agree within 10%
 - Substructure ULS loads agree within 10%
 - Sequentially coupled approach not always conservative
- Jacket:**
 - Turbine ULS loads agree within 10%
 - Substructure ULS loads agree within 30%
 - Sequentially coupled approach not always conservative during extreme conditions

General Conclusions:

The sequentially coupled approach proved to be time consuming and required significant verification effort to minimize potential sources of errors related to data exchange and the specification of numerical model parameters. Additional research and targeted model verification is required to analyze and explain the observed differences.