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June 2016

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Prepared under Task No. WTLU.1000

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List of Abbreviations and Acronyms

ASHRAE	American Society of Heating, Refrigerating, and Air-Conditioning Engineers
CUNY	City University of New York
DC	direct current
DCAS	Department of Citywide Administrative Services
DOE	U.S. Department of Energy
EC	engine company
EE	energy efficiency
FDNY	Fire Department of New York
Ft	feet
Ft ²	square feet
ICE	interruption cost estimate
ITC	investment tax credit
K	thousand
kW	kilowatt
kWh	kilowatt-hour
LCOE	levelized cost of energy
LED	light-emitting diode
M	million
MACRS	modified accelerated cost recovery system
NPV	net present value
NREL	National Renewable Energy Laboratory
NYC	New York City
NYCHA	New York City Housing Authority
NYC-DOE	New York City Department of Education
NYC EM	New York City Emergency Management
NYPA	New York Power Authority
NYSERDA	New York State Energy Research and Development Authority
O&M	operations and maintenance
PPA	power purchase agreement
PV	photovoltaics
RE	renewable energy
RPR	reverse power relay
SCADA	supervisory control and data acquisition
SREC	solar renewable energy credit
TOD	time of day
W	watt

Executive Summary

Resilient PV, which is solar paired with storage (“solar-plus-storage”) that operates both on and off grid, provides value during normal grid operation and during power outages, as opposed to traditional solar PV, which functions only when the electric grid is operating. During normal grid operations, resilient PV systems help host sites generate revenue and/or reduce electricity bill charges. During grid outages, resilient PV provides critical emergency power that can help people in need and ease demand on emergency fuel supplies. The combination of grid interruptions during recent storms, the proliferation of solar PV, and the growing deployment of battery storage technologies has generated significant interest in using these assets for both economic and resiliency benefits. This report analyzes the technical and economic viability of solar and storage on three critical infrastructure sites in New York City (NYC): a school that is part of a coastal storm shelter system, a fire station that was flooded during Sandy, and a NYCHA senior center that serves as a cooling center during heat emergencies. This analysis differs from previous solar-plus-storage studies by placing a monetary value on resiliency and thus, in essence, modeling a new revenue stream for the avoided cost of a power outage. Analysis results show that resilient PV can be economically viable for NYC’s critical infrastructure and that it may be similarly beneficial to other commercial buildings across the city.

This report will help managers of city buildings, private building owners and managers, the resilient PV industry, and policymakers to better understand the economic and resiliency benefits of resilient PV. As NYC fortifies its building stock against future storms of increasing severity, resilient PV can play an important role in disaster response and recovery while also supporting city greenhouse gas emission reduction targets and relieving stress to the electric grid from growing power demands.

This analysis used the REopt modeling platform to optimally select and size resilient power options for the sites in the study. Four scenarios were modeled to reflect different priorities and constraints; each scenario was modeled with and without a resiliency revenue stream. The value of resiliency to a site in this analysis is equal to the estimated costs incurred due to grid interruptions. **In each case, the resilient PV system was able to capture revenue streams associated with displacing energy purchases from the grid, reducing peak demand charges, and shifting grid-purchased energy from high to low time-of-use cost periods.** In all cases, the model found the combination of energy assets that minimized the life cycle cost of energy for the site.

- 1. Scenario 1: Resilient PV sized for economic savings; no resiliency requirement imposed**
The model chose from solar and storage resources to size a system that is cost-effective^{*} for the host site.
- 2. Scenario 2: Resilient PV sized to meet resiliency needs**
The model chose from solar and storage resources to size a system that supports critical electric loads for short and long outages.
- 3. Scenario 3: Resilient PV and a generator (hybrid system) sized to meet resiliency needs**
The model chose from solar, storage, and diesel generator resources to size a hybrid system that supports critical electric loads for short and long outages.

¹ “Cost-effective” in this report means that the modeled system has a life cycle NPV that is equal to or greater than zero.

4. **Scenario 4: Generator sized to meet resiliency needs**

The model sized a diesel generator to support critical electric loads for short and long outages.

The results from the modeling indicate that resilient PV can provide both resiliency and economic benefits for the three sites analyzed in this study. The level of resiliency and/or economic savings the systems will provide depends on a number of factors including:

- Electricity rate of the host site
- Available space to accommodate solar energy
- The combination of technologies used
- The size and shape of the typical load and the critical load
- Whether or not the model includes a monetary value for resiliency.

If a technology solution is being implemented primarily to provide emergency power, the results of the analysis indicate that a hybrid system (Scenario 3) that includes resilient PV and a generator is the most cost-effective technology solution, when measured by lifecycle cost savings. The savings the battery (and sometimes PV) provides during normal grid-connected operation make the hybrid system more economical than a diesel generator alone. However, the hybrid system has a higher initial cost and is more complex than a stand-alone generator.

If lifecycle cost savings is the primary goal, and emergency power is secondary, the results of the study show storage (and sometimes PV) to be the best solution out of the options evaluated for the three sites analyzed under this study. These systems provide maximum cost savings over the project lifecycle with some resiliency benefit. A generator-only solution (Scenario 4), while having the least expensive initial cost, provided lower lifecycle cost savings because this type of asset does not provide value during normal, on-grid operations in this analysis.

The analysis also found that energy storage was cost-effective at all three locations. This is due to the high demand rates and the shape of the load profile at each of these sites. A modestly sized battery system can be strategically charged and discharged such that it shaves the monthly peak loads and therefore captures significant demand savings. It is expected that batteries would also be economically viable at other critical infrastructure sites with high demand rates and similarly shaped load profiles.

The three studied sites are all supplied by NYPA, with Con Edison providing electric delivery services. They have high demand charges and lower-than-average energy costs. For the smaller sites with limited roof space, the model did not always select solar as part of the lowest-cost solution. However, storage savings at these locations were used to offset the cost of solar to demonstrate how these technologies can be used in conjunction to create cost-effective systems. With NYC's commitment to deploying 100 MW of solar on city-owned buildings by 2025, this analysis demonstrates that solar paired with energy storage can support the city's solar deployment goals at buildings where energy costs are low and standalone solar may not always be cost-effective.

Lastly, the results showed that the inclusion of the cost of power outages can have a large impact on the economic viability of a resiliency solution. The net present value (NPV) of a system was always higher when resiliency was valued. Resiliency values were higher for the radial customer (the fire station in this analysis) which is likely to experience more frequent outages, and lower for the school shelter and cooling center, which are network customers on a more reliable grid. The resiliency value realized by the systems was higher for longer outages because there are more outage costs avoided during a long outage compared to a short outage. Currently, generators are responsible for providing the majority of NYC's emergency power needs during times of disaster. This analysis shows that cost-effective hybrid systems that include resilient PV and a generator can extend limited fuel supplies by reducing fuel consumption by approximately 9-36%. Furthermore, with and without a resiliency value, a hybrid system provides emergency power to the sites studied in this analysis at the lowest lifecycle cost.

While only three types of critical infrastructure were evaluated in this analysis, similar results could be expected at other critical infrastructure sites with similar loads and utility rate tariffs. Modestly sized resilient PV systems can achieve both economic savings during normal grid operation and limited emergency power supply during outages. When paired with a backup diesel generator, hybrid resilient PV systems can sustain critical loads for short and long outages (2 hours up to 2 days were modeled). This analysis is intended to initiate a conversation about the use of resilient PV on city buildings among policymakers who are working to increase resiliency while lowering greenhouse gas emissions and electricity costs.

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1 Introduction

Electricity system resiliency focuses on preventing power disruption and, when an outage does occur, restoring electricity supply as quickly as possible while mitigating the consequences of the outage. Resiliency in energy services has always been a top priority, especially for critical or high-value facilities such as emergency response centers, hospitals, and shelters. Currently, diesel or gas-powered generators are relied upon for the majority of emergency power needs, though renewable energy and other forms of distributed generation are starting to play a role in energy resiliency.²

The United States has seen an increase in the number of high-impact/high-cost natural disasters—seven of the ten costliest storms in U.S. history have occurred in the last ten years.³ These high-impact events have sometimes resulted in widespread and long outage durations, demonstrating that existing approaches to energy resiliency were not sufficient in some cases. This was due to a number of factors including lack of generators or other forms of backup power; lack of refueling options for backup diesel generators; unreliable operation of backup generators; interruptions in natural gas and other fuel supplies; and aging infrastructure.

According to the *NYC Hurricane Sandy After Action Report*, the need for generators after the storm far exceeded the available supply. The city deployed approximately 230 generators in total.⁴ Even when they were available, generators failed at several high-profile hospitals in NYC after the storm and called attention to the fact that the presence of a generator does not ensure emergency power. Generators are more susceptible to failure when equipment is outdated, improperly maintained, placed in flood-prone basements, or when fuel supplies are limited.⁵ NYC codes limit onsite fuel storage for tank-based diesel generators to 250 gallons.⁶ For a building with a 200-kW generator operating at half capacity, a 250-gallon fuel supply would be depleted in just under 30 hours.⁷ The average annual outage duration with storms in NYC over the past 5 years is about 22 hours for affected radial customers and just over 50 hours for affected network customers⁸, but in 2012 (the year of Superstorm Sandy), outage durations

² “Solar + Energy Storage = Resilient Power in Vermont.” 2014. Clean Energy Group.

<http://www.cleanenergygroup.org/solar-energy-storage-resilient-power-in-vermont/>.

³ Executive Office of the President. 2013. *Economic Benefits of Increasing Electric Grid Resilience to Weather Outages*. http://energy.gov/sites/prod/files/2013/08/f2/Grid%20Resiliency%20Report_FINAL.pdf.

⁴ NYC Mayor’s Office. 2013. *NYC Hurricane Sandy After Action Report*.

http://www.nyc.gov/html/recovery/downloads/pdf/sandy_aar_5.2.13.pdf.

⁵ Ornstein, C. 2012. “Why Do Hospital Generators Keep Failing?” ProPublica.

<https://www.propublica.org/article/why-do-hospitals-generators-keep-failing>.

⁶ Fire Department of the City of New York. 2014. *Study Material for the Citywide Certificate of Fitness Examination*. http://www.nyc.gov/html/fdny/pdf/cof_study_material/s_94_st_mat.pdf.

⁷ Based on Cat Model D200-2, a 200-kW generator that is 50% loaded and uses 8.6 gallons/hour.

⁸ There are two types of electric grid systems, radial and secondary network. Radial systems have a single high voltage feeder sending energy from the substation to numerous distribution transformers tapped along it. Cables and transformers on radial grids are often above ground. Network grids have multiple primary feeders feeding several parallel network transformers that feed energy into a low voltage grid (grid network type) or local building bus (spot network) where the consumer is connected. Spot networks are where one or multiple transformers are dedicated to one large energy consuming building. Cables and transformers on network grids are often below ground. Network grids are considered more reliable than radial grids as there are redundant sources of backup power in case of failures on the grid and underground equipment is less prone to weather-related damage.

reached 73 and 58 hours, respectively.⁹ Fuel supply in New York was scarce after Sandy for nearly a month as a result of refineries being shut down and other damages to the fuel supply chain serving New York.¹⁰ Local supplies were not sufficient to meet needs, resulting in FEMA providing more than 3.48 million gallons of fuel for Sandy recovery at a cost of \$6.37 million.¹¹

Long-duration outages can lead to lost output, wages, and inventory. **The estimated cost of U.S. weather-related outages in 2012 is \$27-52 billion dollars.**¹² For individuals who rely on electronic medical equipment, these outages can be lethal. Adding to costs associated with Superstorm Sandy, NYC was sued for violating the Americans with Disabilities Act, in part for failing to provide adequate emergency power.¹³ The cost of power outages varies from person to person and facility to facility, but the costs are real, and so is the value of avoiding an outage.

Resilient PV can serve as an alternative or supplement to existing forms of backup power, extending limited fuel supplies when paired with generators. A resilient PV system can be operated for economic gain during the 99.9% of the time that the grid is functional by offsetting bulk energy purchases, reducing peak demand charges, performing energy arbitrage¹⁴, and providing ancillary services. With appropriate inverters and controls these same systems can be islanded to form a microgrid, often along with diesel generators, to sustain critical electrical loads for the site during grid outages. A hybrid generator/PV/battery system can sustain longer outages for a given amount of diesel fuel by reducing the run-time (and therefore fuel consumption) of the diesel generator, thus increasing the energy resiliency of the site.¹⁵ For the three sites evaluated in this analysis, the hybrid generator/PV/battery system consumed 9% -36% less fuel than the standalone diesel generator during long outages. Additionally, resilient PV systems may provide a fast-acting backup power supply for small, highly sensitive critical loads like computers or communications equipment. Some resilient PV designs can re-energize critical loads within 10 to 20 milliseconds, compared to generators that may take 3-10 seconds to start.

Standalone resilient PV systems avoid problems associated with generators like noise and air quality issues while offering host sites a cost-savings opportunity and a reduced carbon footprint. Resilient PV hits an intersection point between resiliency and sustainability, two significant areas

⁹ “Electric Service Reliability Reports.” 2015. New York State Department of Public Service.

<http://www3.dps.ny.gov/W/PSCWeb.nsf/All/D82A200687D96D3985257687006F39CA?OpenDocument>.

¹⁰ NYC Mayor’s Office. 2013. *A Strong, More Resilient New York*.

http://www.nyc.gov/html/sirr/downloads/pdf/final_report/Ch_1_SandyImpacts_FINAL_singles.pdf.

¹¹ Office of Inspector General. 2015. *FEMA Has No Assurance that Only Designated Recipients Received \$6.37 Million in Fuel*. Department of Homeland Security. <https://www.oig.dhs.gov/assets/GrantReports/2016/OIG-16-04-D-Nov15.pdf>.

¹² Executive Office of the President. 2013. *Economic Benefits of Increasing Electric Grid Resilience to Weather Outages*. http://energy.gov/sites/prod/files/2013/08/f2/Grid%20Resiliency%20Report_FINAL.pdf.

¹³ Santora, M., and B. Weiser. 2013. “Court Says New York Neglected Disabled in Emergencies.” New York Times. <http://www.nytimes.com/2013/11/08/nyregion/new-yorks-emergency-plans-violate-disabilities-act-judge-says.html>.

¹⁴ Energy arbitrage is the process of charging batteries when energy prices are low, and discharging them when energy prices are high. This effectively shifts grid energy purchases to periods with lower energy prices.

¹⁵ 1 kW of PV in NYC generates 1274 kWh/year, or an average of 0.145 kWh/hour. As previously described, a 200-kW generator that is 50% loaded requires 8.6 gallons of fuel to generate 100 kWh. If the generator fuel curve were linear, a solar system would offset approximately 0.01247 gallons of fuel per hour per kW of solar installed. In this example, a 100-kW PV system installed alongside the 200-kW generator would displace about 14.5% of the hourly fuel consumption, saving about 1.25 of the 8.6 gallons used each hour.

of interest for NYC and much of the country. With the technical analysis offered in this report, those who plan for the city's emergency power needs have a template methodology to compare and contrast resilient power options and the opportunity to deepen collaboration across resiliency and sustainability programs.

Solar installations in New York are increasing rapidly. From 2011 to 2015, solar installations in New York increased 575%, and by 675% in NYC.¹⁶ The state is mandated to supply 50% of its electricity from renewables by 2030 and aims to deploy 3 GW of solar across the state by 2023. Energy storage can enable higher levels of intermittent renewables like solar, and studies show that the combined value of solar-plus-storage on commercial buildings is higher than deploying the technologies separately.¹⁷ In NYC, solar increased from a quarter of a megawatt in 2008 to nearly 50 megawatts in 2016, but few of these systems include backup power capabilities either through battery backup or inverters with emergency power plugs. Only a handful of commercial-scale solar-plus-storage systems exist in NYC today, and only a few of these systems are configured to provide emergency backup power. With NYC committed to deploy 100 MW of solar on city-owned buildings by 2025, this report highlights the unique opportunity that resilient PV systems can provide for critical infrastructure sites, many of which are owned by the city. The [NYSolar Smart Distributed Generation \(DG\) Hub](#), through projects like this analysis, is creating pathways for resilient PV to reach the market.¹⁸

¹⁶ “Solar Growth per Region.” 2015. NYSERDA. <http://www.nyserdera.ny.gov/-/media/Files/About/SUN-GEN-solar-growth-by-region.pdf>.

¹⁷ Sussman, M., and J. Lutton. 2015. “The Economics of Solar, Storage and Solar-Plus-Storage.” Greentech Media. <http://www.greentechmedia.com/articles/read/The-Economics-of-Solar-Storage-and-Solar-Plus-Storage>.

¹⁸ The DG Hub was formed by Sustainable CUNY in the aftermath of Hurricane Sandy, and received funding from the U.S. Department of Energy, NYSERDA, and NYPA in 2015 to work with partners to create strategic pathways for greater resiliency using solar and storage. Additional DG Hub resources can be found at www.cuny.edu/DGHub.

2 Methodology

The City University of New York (CUNY) and the National Renewable Energy Laboratory (NREL) worked with city partners to select three critical infrastructure sites at which to evaluate PV and battery opportunities. CUNY and NREL gathered preliminary utility and site data, and verified the data during site assessments. For each of the three critical sites selected, we modeled the economic and resiliency benefits of PV and battery systems at the three sites. This section documents the data collected and assumptions made for the modeling.

2.1 Selection of Critical Infrastructure Sites

CUNY and NREL, in coordination with the NYSolar Smart DG Hub software working group, identified a range of critical infrastructure facility types to consider: utilities, coastal storm shelters, transportation systems, telecommunication systems, water and wastewater treatment facilities, and healthcare facilities, among others.

CUNY sent a survey to the working group to determine the critical infrastructure facility types to focus on in the analysis. The potential sites included gas stations, nursing homes, hospitals, water treatment facilities, shelters, and stores selling emergency supplies. Site selection was based on the following factors:

- Evacuation zones and close proximity to flood plain
- Prone to outages
- No existing backup generation
- Non-hospital site that serves medical needs
- Roof age (20+ years of usable life remaining) with limited shading
- Space for PV and battery (20,000 sq. ft. for solar)
- Number of people the shelters supported during storms Irene and Sandy
- Support from the building staff
- Sites with high demand charges
- Sites where energy efficiency upgrades are being implemented or considered.

The three critical infrastructure facility types selected were fire stations, cooling centers, and coastal storm shelters. CUNY reached out to the New York Department of Citywide Administrative Services (DCAS), New York City Department of Education (NYC- DOE), New York City Fire Department (FDNY), and New York City Housing Authority (NYCHA) to help select the specific sites to be analyzed in the study. The sites selected were:

- NYC-DOE coastal storm shelter: Susan Wagner High School, 1200 Manor Road, Staten Island, New York, 10314
- FDNY fire station: Engine Company 309, 1864 East 48th Street, Brooklyn, New York, 11234
- NYCHA cooling center: Brownsville Senior Center, 528 Mother Gaston Blvd, Brooklyn, New York.

2.2 Site Overview

A summary of the three critical infrastructure sites is presented in this section.

2.2.1 NYC-DOE High School/Shelter

Description and Load Data

The Susan Wagner High School is located on Staten Island and served as a shelter (Figure 1) after Hurricane Sandy with approximately 1,000 beds in the cafeteria. The school lost power after Sandy and had diesel generators brought in for backup power.

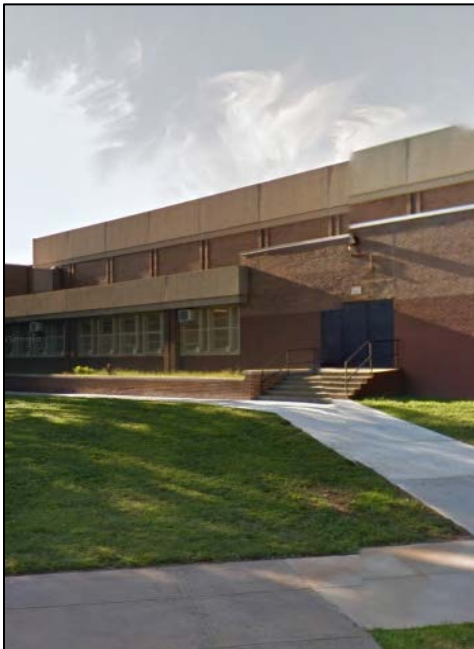
	Table 1. School Shelter Load Data				
	Data Source	DCAS			
	Data Type	15-minute interval; September 2014 – August 2015			
	Methodology	Interval data were synthesized by modeling the building based on DOE's secondary school commercial reference building and the New York City climate zone (ASHRAE climate zone 4A).			
	Load Size	Minimum Load	Maximum Load	Average Load	Peak Loads
		42 kW	588 kW	177 kW	May – October

Figure 1. Susan Wagner High School

Photo by Kari Burman, NREL

The annual energy profile is shown in Figure 2. Relative to May and September, peak loads do not increase during the summer months of June through August due to summer vacation.

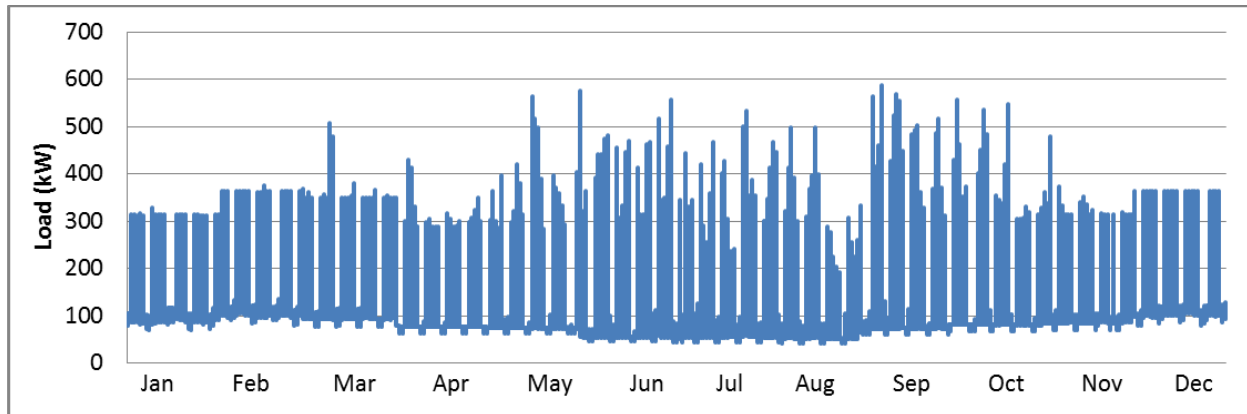


Figure 2. Susan Wagner High School annual energy profile 2014-2015

The composite daily load profile is shown in Figure 3. The peak load occurs during the mid-afternoon which would be expected for a school.

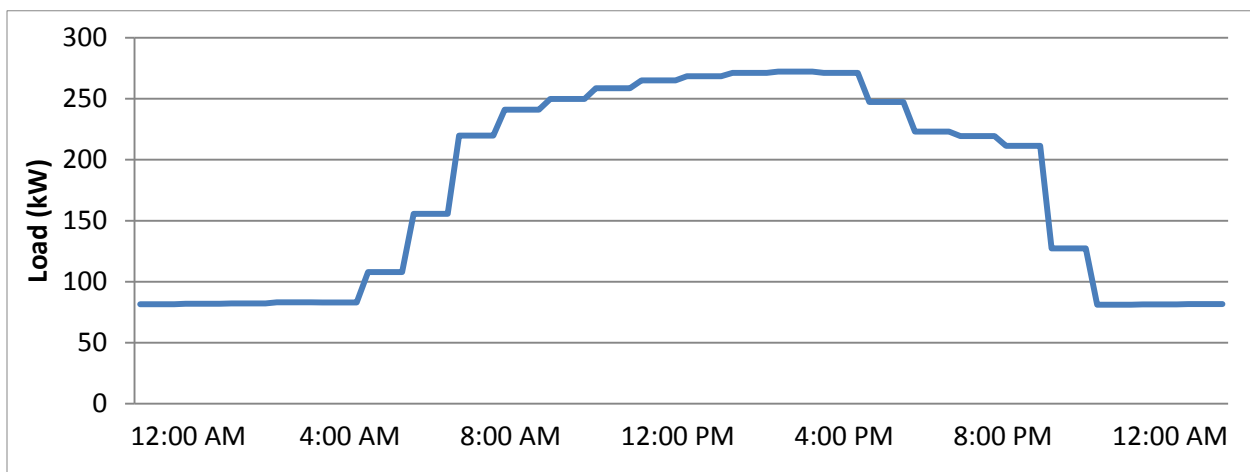


Figure 3. Susan Wagner High School composite daily load profile

Utility Rate Structure

The Susan Wagner High School is on the NYPA Service Tariff No. 100, Service Classification No. 91 for New York City Public Buildings-Schools, conventional, low tension service (see Service Classification No. 91, Appendix B, Table of Rates and Service). The tariff has an energy charge component (with different charges for summer and winter seasons) and a demand charge component. The demand component is split into a production charge and a delivery charge. For the production charge component, if metered demand in any given month is less than 75% of the maximum demand in the prior 12 months, billed demand is equal to 75% of the earlier maximum demand. For the delivery charge component, if metered demand in any given month is less than 39% of the maximum demand in the prior 18 months, billed demand is equal to 39% of the earlier maximum demand. Otherwise, the demand charges are the actual measured demand for the month.

The school is eligible for a net metering agreement. Since this site is on a spot network, however, additional smart grid equipment must be installed at NYC-DOE's expense if the PV system exports to the grid. Per Con Edison guidance, buildings on a spot network may either enable a reverse power relay (RPR) to prevent export at a cost of \$5,000 or implement a smart grid solution that allows export at a cost of \$50,000-100,000. If the school installed the maximum PV system size (210 kW), the energy exported from the system would be worth about \$500/year (\$12,500 over 25 years), which is less than the cost of the smart grid solution and negates the benefit of net metering. Therefore, in this analysis we assumed an RPR would be implemented at a cost of \$5,000 to prevent export.

Critical Load Data

NYC-DOE provided a list of equipment that would need to operate during an outage as well as an estimate of the number of hours each item would run. Since the shelter might need to operate year-round, we synthesized critical load profiles for summer, winter, and shoulder seasons (see Figures 4-6). The seasonal differences are primarily a result of air conditioning and auxiliary space heating loads. The summer (June-August) critical load includes air conditioning in limited rooms for shelter residents with special needs, while the winter (October-April) critical load includes space heating. The critical load in the shoulder season (September, May) includes neither. We estimated the total critical energy use was 352 kWh/day in the summer and 432 kWh/day in the winter, which is approximately 7-13% of typical load. Peak critical demand ranges from 33 kW in the winter and shoulder seasons to 36 kW in summer. See Appendix A for a full list of equipment and calculations.

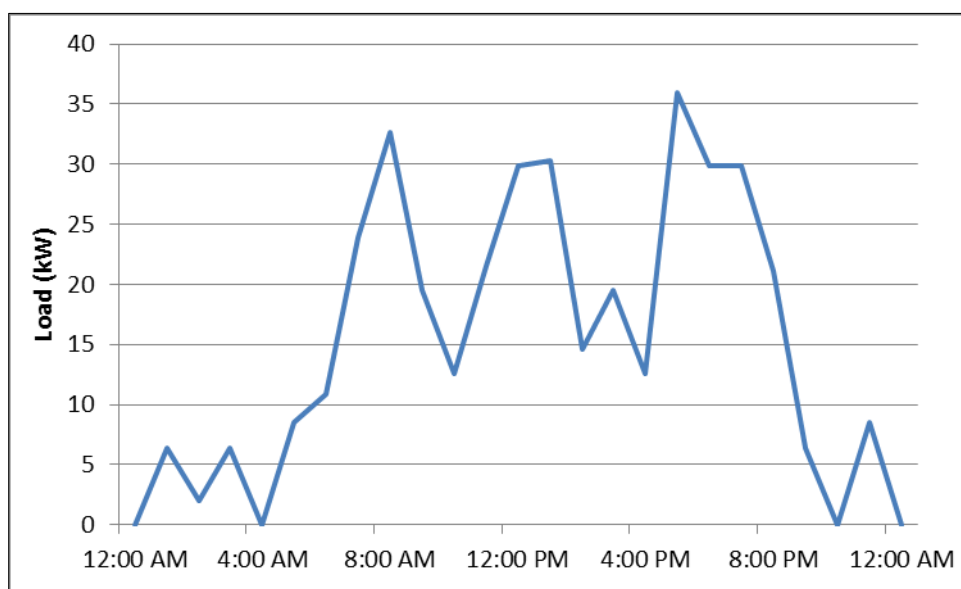


Figure 4. Critical load: summer daily profile

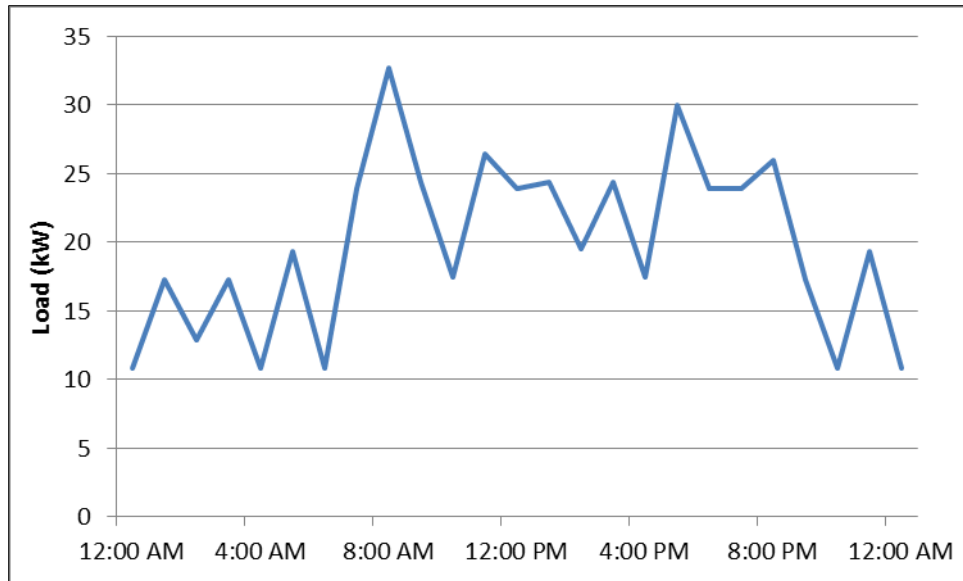


Figure 5. Critical load: winter daily profile

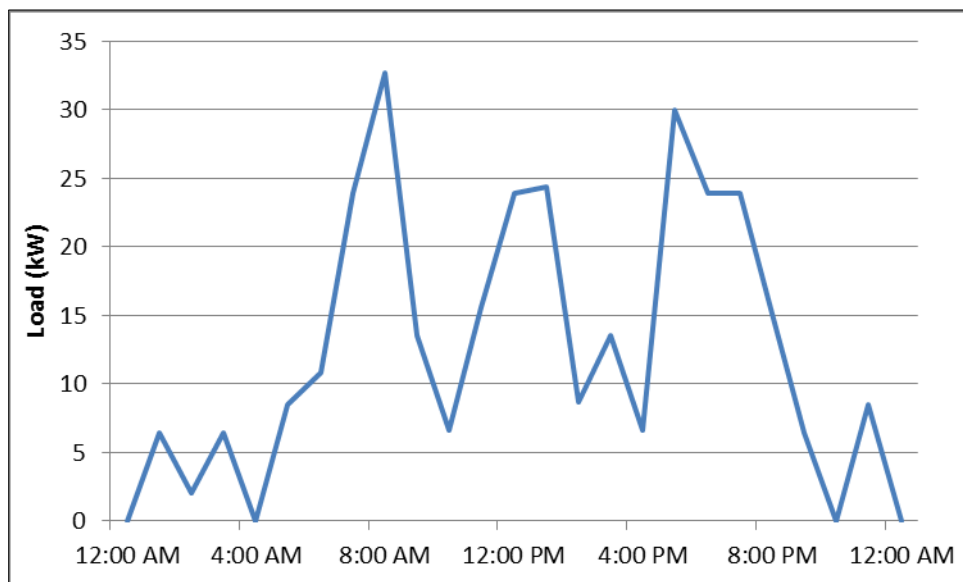


Figure 6. Critical load: shoulder season daily profile

Types of Existing Backup Power

There is no existing backup power/generation at the Susan Wagner High School. Backup diesel generators were brought in during the power outage after Hurricane Sandy.

PV Assessment

We visually inspected the roof areas of the high school to measure roof size, presence of rooftop equipment, and potential shading. The high school could accommodate PV systems on the roof areas designated in Figure 7. PV could also potentially be placed on carports in the parking lot, but this area was not considered in this analysis.

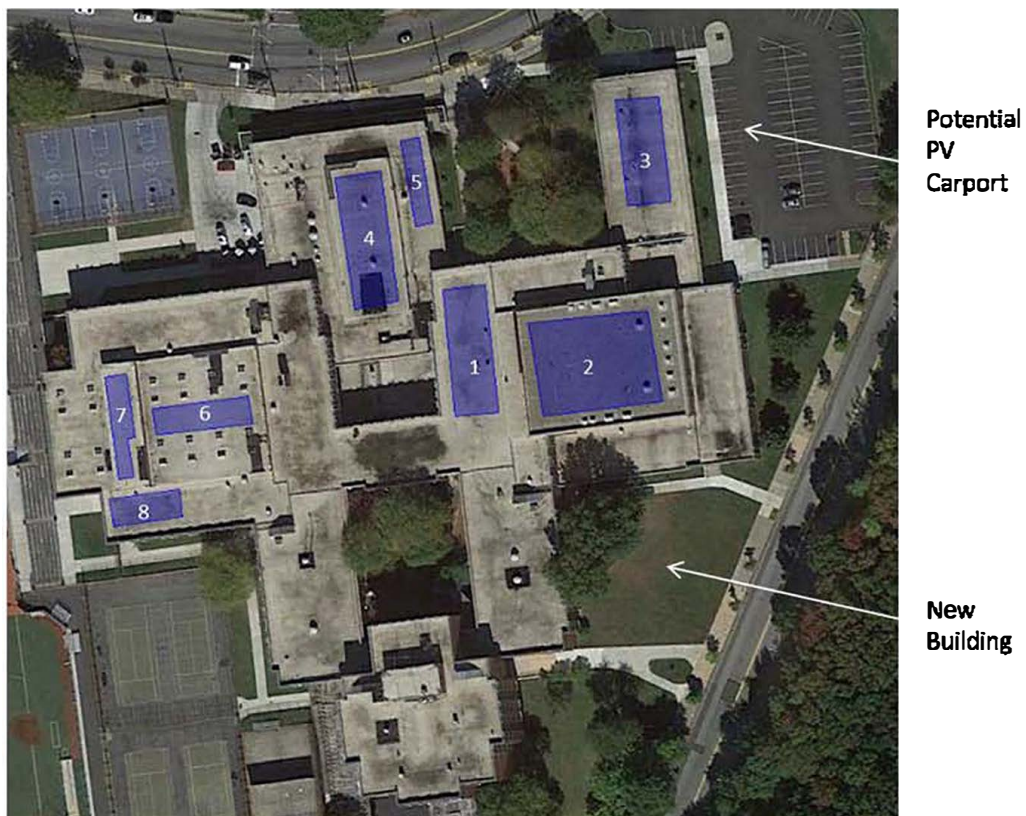


Figure 7. Susan Wagner High School/Shelter PV layout
 Source: © 2016 Google Earth, alterations by Kari Burman



Figure 8. Roof of the Susan Wagner High School, looking south in Area 1
Photo by Kari Burman, NREL

Table 2. DOE Roof Areas Identified for PV and Associated Details

Array location and areas (ft²)	Area 1: 3,626 ft ² Area 2: 7,373 ft ² Area 3: 3,000 ft ² Area 4: 3,960 ft ² Area 5: 1,050 ft ² Area 6: 1,722 ft ² Area 7: 1,320 ft ² Area 8: 1,272 ft ²
Available roof area (ft²)	23,323 ft ²
Maximum PV rated capacity (kW DC) excluding potential carport areas	210 kW (254,457 kWh/year, or 16% of annual building energy consumption) ¹⁹
PV tilt angle	10°
Roof fall-line azimuth	173°
Roof type	Flat
Roof condition	Fair
Roof installation date	New roof will be installed in FY16
Potential obstructions	Potential PV is designed around large equipment
Parapet wall height	3 feet
Solar availability (%)	PV was designated for areas with at least 90% solar availability

2.2.2 FDNY Engine Company 309

Description and Load Data

Engine Company (EC) 309, located at 1864 East 48th Street in Brooklyn, provides fire and emergency medical services. This facility lost power for about five days after Hurricane Sandy.

Recent renovations at the fire station included a new roof; it re-opened in July 2015. Because the building systems and the occupancy of the station changed, historical pre-renovation energy data for EC309 were not representative of future energy consumption. We used the one month of post-renovation energy data available (August 2015) and estimated the remaining months of the year based on energy data for EC315, a station of similar size and with similar August energy consumption and demand.

¹⁹ A 210-kW PV system would generate 254,457 kWh/year (estimated using PVWatts). The school's annual energy consumption is 1,556,800 kWh.

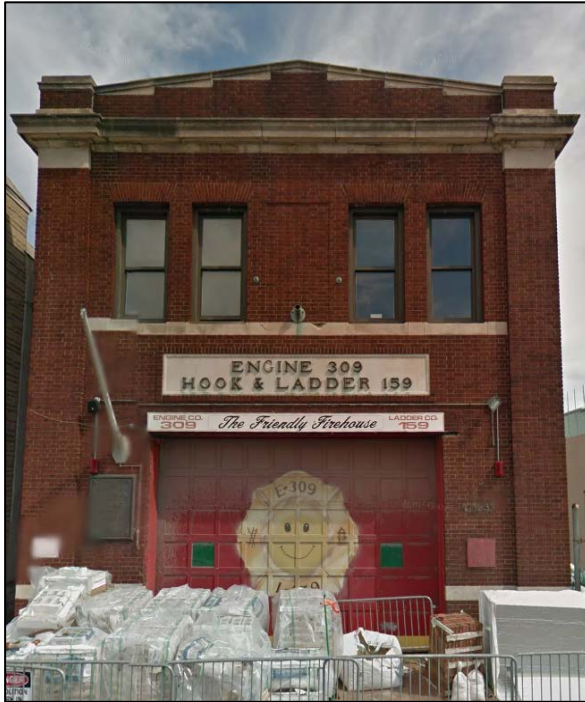


Table 3. Fire Station Load Data				
Data Source	DCAS			
Data Type	Energy and demand data			
Methodology	Interval data were not available for this site, so they were estimated from the monthly electric use of a similar station by modeling the building based on DOE's commercial reference buildings and the New York City climate zone (ASHRAE climate zone 4A). A fire station is not one of the DOE commercial reference building types, so we assumed 50% warehouse (for the garage area downstairs) and 50% midrise apartment (for the upstairs firefighter living quarters).			
Load Size	Minimum Load	Maximum Load	Average Load	Peak Loads
	2.86 kW	63.2 kW	15.2 kW	May – October

Figure 9. FDNY EC309 in Marine Park

Photo by Kari Burman, NREL

The annual electricity profile is shown in Figure 10.

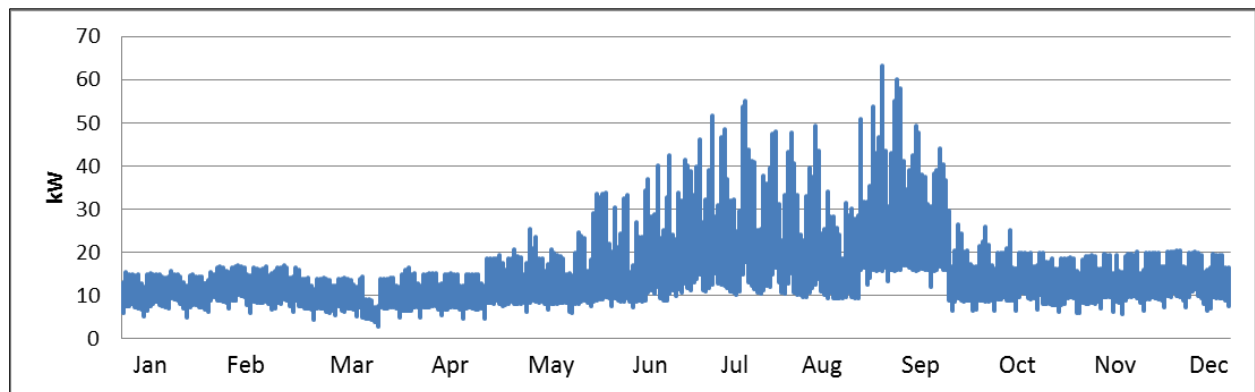


Figure 10. FDNY EC309 annual electricity profile

Peak loads occur during the hotter summer months of July-September. The composite daily load profile is shown in Figure 11. The daily peak load occurs around 4 p.m.

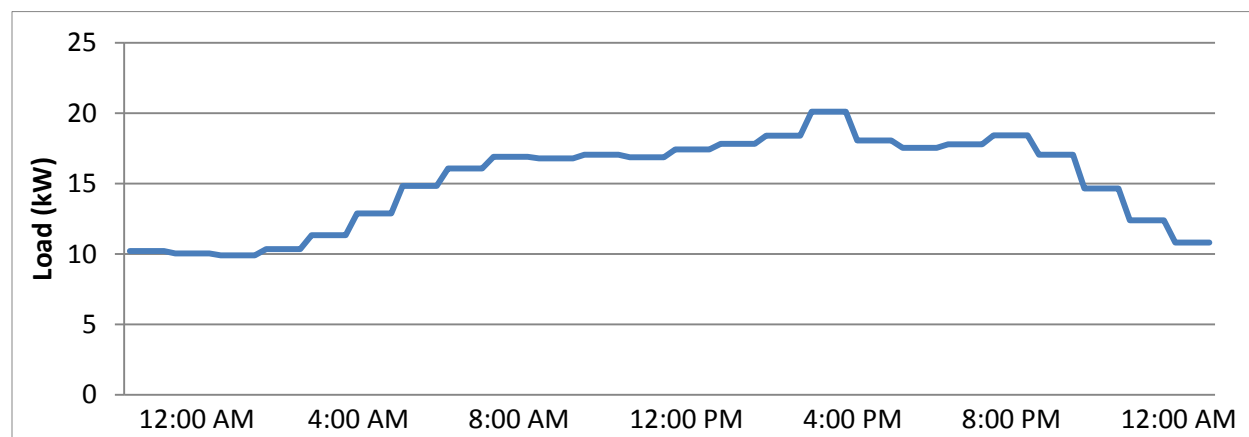


Figure 11. FDNY EC309 composite daily load profile

Utility Rate Structure

The fire station is on the NYPA Service Tariff No. 100²⁰, Service Classification No. 91 for New York City Public Buildings, conventional, low tension service (see Service Classification No. 91, Appendix B, Table of Rates and Services). The tariff has an energy charge component (with different charges for summer and winter seasons) and a demand charge component. The demand component is split into a production charge and a delivery charge. For the production charge component, if metered demand in any given month is less than 75% of the maximum demand in the prior 12 months, billed demand is equal to 75% of the earlier maximum demand. For the delivery charge component, if metered demand in any given month is less than 39% of the maximum demand in the prior 18 months, billed demand is equal to 39% of the earlier maximum demand. Otherwise, the demand charges are the actual recorded value for the month.

The fire station is eligible for a net metering agreement. This building is on a radial grid.

Critical Load Data

FDNY did not provide a specific list of critical loads, so we estimated the critical load by applying a percentage reduction to the typical load. The critical load level assumed for the fire station is 65% of typical load²¹, which is approximately 350 kWh/day in the summer and 170 kWh/day in the winter. This would include loads such as computers and communication equipment in the control center, lighting, and pumps to fuel trucks. The critical annual load profile is shown in Figure 12.

²⁰ NYPA. 2015. *Electric Service Tariff for New York City Governmental Customers*, Service Tariff No. 100, Date of Issue March 2015.

²¹ The NYC and San Francisco Solar Market Pathways teams conducted site visits at fire stations to determine critical loads. Critical loads were estimated by staff to be in the range of 65-100%; 65% was selected since backing up a larger load would likely be cost prohibitive.

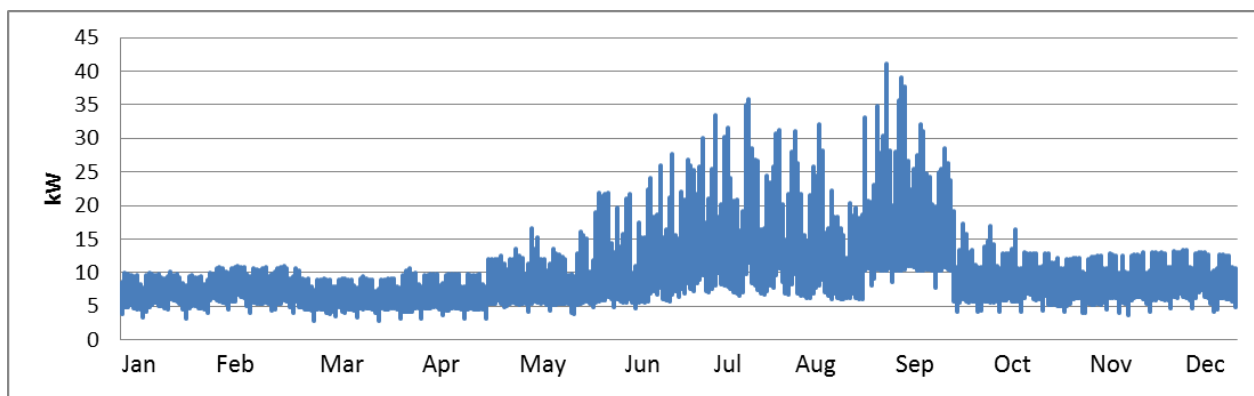


Figure 12. Annual critical load profile

Types of Existing Backup Power

There is no existing backup power/generation at this fire station at the time of the site visit.

PV Assessment

We visually inspected the roof areas of the fire station to measure roof size and identify the presence of rooftop equipment and potential shading. For buildings under 100 linear feet high, the New York City fire code²² requires a clear path on the roof of not less than six feet horizontal width from the front of the building to the rear of the building. An aerial view of the roof, with space available for PV, is shown in Figure 13 and a picture of the roof is shown in Figure 14. Table 4 shows the roof dimensions and PV capacity. This roof is estimated to be able to support approximately 10.2 kW-DC of PV.



Figure 13. FDNY: EC309 PV layout

Source: © 2016 Google Earth, alterations by Kari Burman

²² The New York City Fire Code, Chapter 504 and 512. 2014.
http://www.nyc.gov/html/fdny/apps/pdf_viewer/viewer.html?file=firecode_chap_05.pdf§ion=firecode_2014.



Figure 14. Roof of the fire station looking east from the west side

Photo by Allison Silverman, CUNY

Table 4. FDNY Roof Areas Identified for PV and Associated Details

Array location and areas (ft²)	Area 1: 891.3 ft ² Area 2: 251.6 ft ²
Available roof area (ft²)	1,142 ft ²
Maximum PV rated capacity (kW DC)	10.2 kW (12,362 kWh/year, or 9.2% of building annual energy consumption) ²³
PV tilt angle	10°
Roof fall-line azimuth	175°
Roof type	Flat
Roof condition	New
Roof installation date	2015
Potential obstructions	Large equipment that was previously on the roof (shown in the roof image above) was removed during the renovation
Parapet wall height	3 feet
Solar availability (%)	95%

²³ A 10.2-kW PV system would generate 12,362 kWh/year (estimated using PVWatts). The fire station's annual energy consumption is 133,812 kWh.

2.2.3 NYCHA Cooling Center

Description and Load Data

The Brownsville Senior Center (Figure 15) is located at 528 Mother Gaston Blvd in Brooklyn, New York. The senior center is located on the first floor of a seven story apartment building and may serve as a cooling center for up to 70 people during heat waves. The building lost power for about three days after Hurricane Sandy.



Table 5. Cooling Center Load Data				
Data Source	NYCHA			
Data Type	15-minute interval; January 2015 – September 2015			
Methodology	15-minute interval data were provided for January-September. October – December data were estimated based on previous months: March for October, February for November and January for December.			
Load Size	Minimum Load	Maximum Load	Average Load	Peak Loads
	21.5 kW	77.3 kW	30.5 kW	June – Sept.

Figure 15. NYCHA Brownsville Senior Center

Photo by Allison Silverman, CUNY

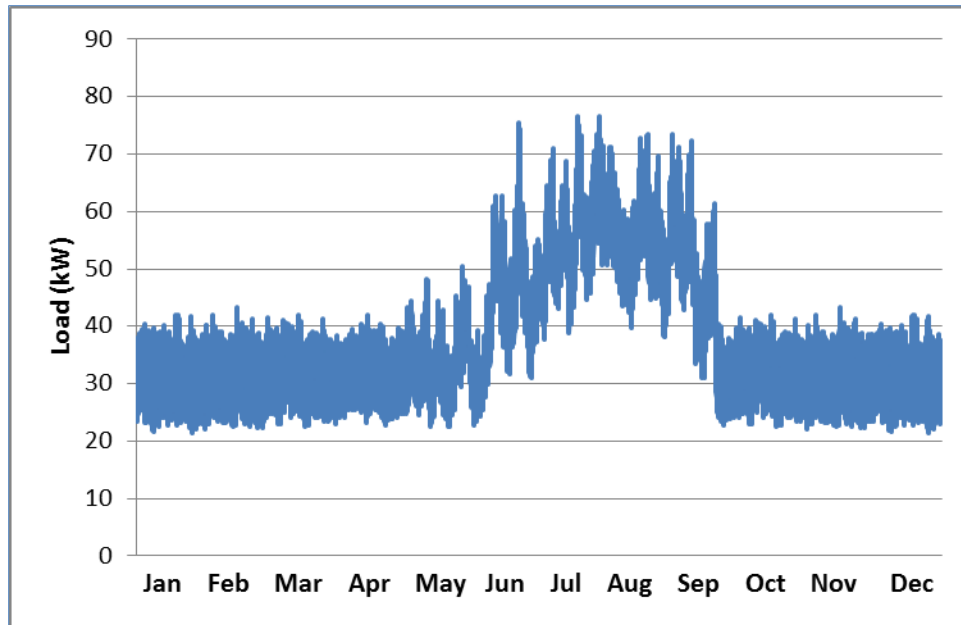


Figure 16. NYCHA Brownsville Senior Center annual load profile

A composite daily load profile for the entire apartment building was created by averaging the daily load profiles for the entire year (Figure 16 and Figure 17). The peak load occurs in the evening between 8 p.m. – 11 p.m., and the minimum load occurs in the morning between the hours of 5 a.m. - 9 a.m.

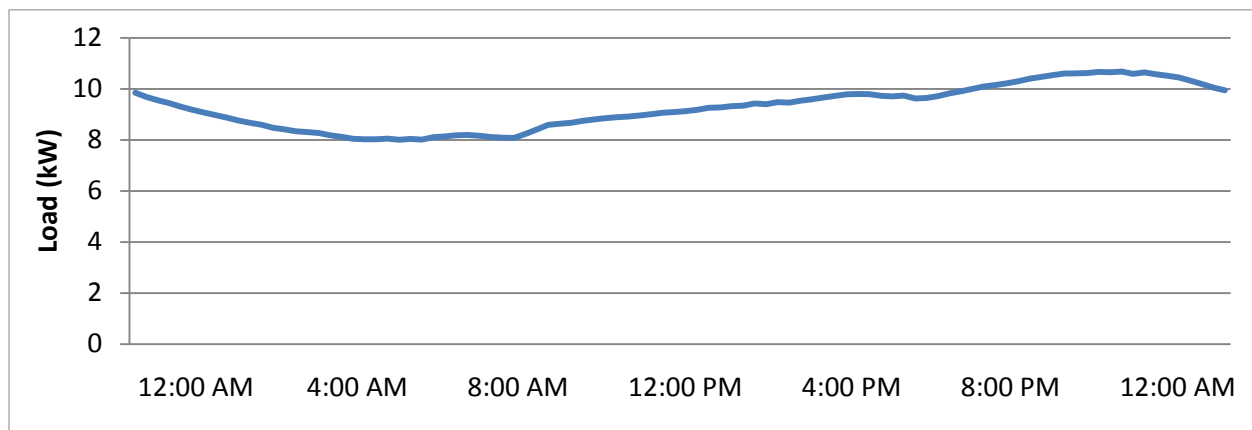


Figure 17. NYCHA annual composite daily load profile

Utility Rate Structure

The NYCHA Brownsville Senior Center is on the NYPA Service Tariff No. 100, Service Classification No. 68 for Multiple Dwellings-Redistribution, Time of Day (TOD), low tension service (see Service Classification No. 68, Appendix B, Table of Rates and Service). The tariff has an energy charge component (with different charges for summer and winter seasons) and on and off peak periods. It also has a demand charge component with different demand charges for summer and winter periods. The demand component is split into a production charge and a delivery charge. For the production charge component, if metered demand in any given month is

less than 75% of the maximum demand in the prior 12 months, billed demand is equal to 75% of the earlier maximum demand. For the delivery charge component, if metered demand in any given month is less than 39% of the maximum demand in the prior 18 months, billed demand is equal to 39% of the earlier maximum demand. Otherwise, the demand charges are based on the actual recorded value for the month.

The NYCHA Brownsville Senior Center is eligible for a net metering agreement. This building is on an area network.

Critical Load Data

The critical load profile for the NYCHA cooling center was synthesized by adding the individual component loads as specified by Brownsville staff. These components consist of air conditioners, a computer, lighting, fire alarm system, and refrigerator. The air conditioners are estimated to operate 8 hours/day during the grid outage and represent the majority of energy consumption in the critical load (~96 kWh/day). See Appendix A for a full list of critical loads and calculations. A graph of the synthesized critical daily load profile used in this analysis is shown in Figure 18. Since the cooling center would only operate during the summer, the critical load profile was developed for the summer season only.

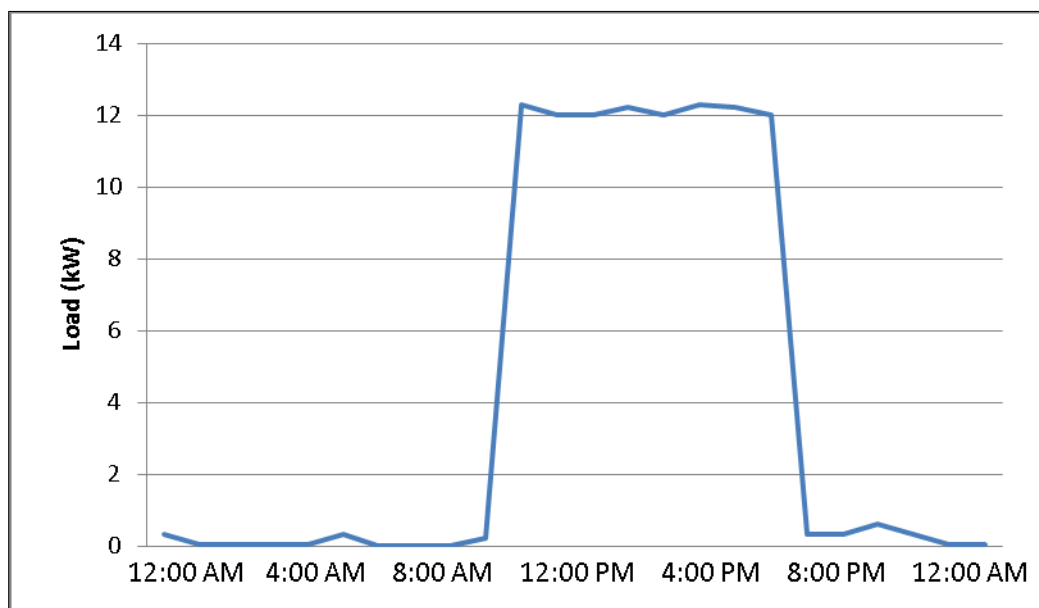


Figure 18. NYCHA Brownsville Senior Center daily critical load profile

Types of Existing Backup Power

There is no existing backup power at Brownsville Senior Center.

PV Assessment

We visually inspected the roof areas of the NYCHA Senior Center to measure roof size, presence of rooftop equipment, and potential shading. The Senior Center could accommodate PV systems on the roof areas designated in the figures below. Note that areas on the 6th floor were not

considered for PV due to shading from the 7th floor and elevator shaft in the center. This building is under 100 linear feet, so it must comply with the New York City fire code²⁴ which requires a clear path on the roof of not less than six feet horizontal width from the front of the building to the rear of the building. An aerial view of the roof with space available for PV is shown in Figure 19, and a picture of the roof is shown in Figure 20. Table 6 shows the roof dimensions and PV capacity. This roof can support approximately 9.2 kW-DC of PV.

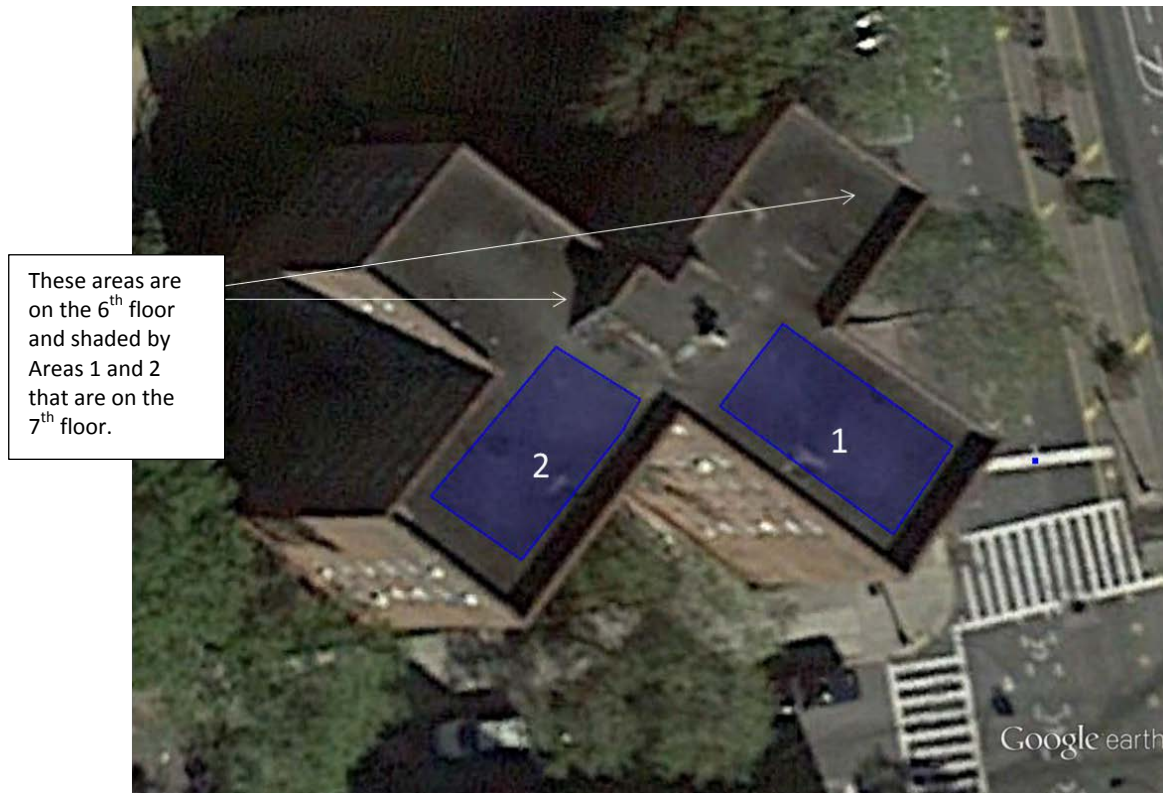


Figure 19. NYCHA Senior Center PV layout

Source: © 2016 Google Earth, alterations by Kari Burman



Figure 20. Roof of the NYCHA Senior Center/Cooling Center looking south

Photo by Allison Silverman, CUNY

²⁴ The New York City Fire Code, Chapter 504 and 512. 2014.
http://www.nyc.gov/html/fdny/apps/pdf_viewer/viewer.html?file=firecode_chap_05.pdf§ion=firecode_2014.

Table 6. NYCHA Roof Areas Identified for PV and Associated Details

Array location and areas (ft²)	Area 1: 511 ft ² Area 2: 511 ft ²
Available roof area (ft²)	1,022 ft ²
Maximum PV rated capacity (kW DC)	9.2 kW (11,137 kWh/year, or 3.4% of annual energy consumption) ²⁵
PV tilt angle	10°
Roof fall-line azimuth	Area 1: 125° Area 2: 212°
Roof type	Flat, built up roof
Roof condition	Fair
Roof installation date	Brownsville roof replacement is in the Capital Plan for 2017 (Design) and 2018 (Construction) to be funded from federal capital funds
Potential obstructions	No large equipment on the roof areas that are proposed for PV
Parapet wall height	3 feet
Solar availability (%)	95%

2.3 Modeling Description and Assumptions

REopt is NREL's software modeling platform for energy system integration and optimization.²⁶ The core of the model consists of a mixed-integer linear program with minimizing life cycle cost of energy as the objective function. The objective of the model is, therefore, to find the combination of energy assets that can supply electricity to the site at lowest cost, including capital, operating, fuel, and maintenance costs, over the analysis period (25 years in this case). For the purposes of this analysis, the model could select from among the utility grid, PV, batteries, or a diesel generator to meet the load, though not all technologies were available in every scenario. Each technology had specific operating constraint, capital cost, and operating cost assumptions which are described in the table below.

REopt is a time-series model that determines the optimal operation of each energy asset during every time step. For this analysis, the model was run with 8,760 one-hour time steps per year. Since the model is formulated as a mixed-integer linear program, it does not need to be programmed with a specific dispatch strategy for the dispatchable assets, but can, instead, find the operating strategy that minimizes overall life cycle cost. This dispatch strategy is one of the model outputs, along with the optimal selection and sizing of the components. Components are

²⁵ A 9.2-kW PV system would generate 11,137 kWh/year (estimated using PVWatts). The building's annual energy consumption is 325,138 kWh.

²⁶ Simpkins, T., D. Cutler, K. Anderson, D. Olis, E. Elgqvist, M. Callahan, and A. Walker. 2014. *REopt: A Platform for Energy System Integration and Optimization*. NREL/CP-7A40-61783. <http://www.nrel.gov/docs/fy14osti/61783.pdf>.

sized using continuous variables rather than discrete variables for sizing, so the exact sizes recommended may not be available in the market. For example, an 11-kW, 32-kWh battery may be recommended, but the closest commercially available size may be a 10-kW, 30-kWh battery.

The table below summarizes the modeling assumptions used at each site.

Table 7. Assumptions for the Analysis

PV Assumptions	
PV capital costs	<ul style="list-style-type: none"> • NYC-DOE School Shelter: \$3.45/W-DC based on projected third party financing prices for DCAS • FDNY Fire Station: \$3.88/W-DC based on DCAS historic PV contract prices • NYCHA Cooling Center: \$4.64/W-DC based on 2015 NYC Solarize contract pricing for 10-kW flat roof systems
PV cost details	<ul style="list-style-type: none"> • Costs are total installed costs including engineering, permitting, and interconnection. Additional potential costs are listed at the end of this section. • Costs include a grid-forming inverter that assists with regulation of both voltage and frequency during a grid outage. • A cost of \$5,000 is added to the capital cost of systems at the DOE site (in addition to the \$3.45/W PV capital cost) to pay for an RPR to prevent export to the spot network.
O&M cost	\$20/kW/year
PV system specifications	<ul style="list-style-type: none"> • Calculations assume standard modules in a fixed roof mount array with 14% system losses. • Systems are modeled with 10° tilt. • System azimuth varied by site (180° is a due-south orientation): <ul style="list-style-type: none"> ○ NYC-DOE: 173° ○ FDNY: 175° ○ NYCHA Area 1: 125°, Area 2: 212°.

Storage Assumptions	
Battery type	Lithium-ion nickel manganese cobalt oxide ²⁷
Minimum state of charge	20% ²⁸
State of charge at time of outage	100%
Round-Trip AC-AC Efficiency	92.5% ²⁹
Capital cost	Initial Cost: \$520/kWh, \$1000/kW ^{30,31}
Replacement cost	Assume battery is replaced once at year 12. Estimated replacement cost in 2037 is \$200/kWh, \$200/kW
Diesel Generator Assumptions	
Capital cost	\$1.50/W
Non-fuel O&M cost	\$0.02/kWh
Fuel cost	\$2.52/gallon ³²
Diesel fuel cost escalation rate	0.4%/year ³³
Fuel available	250 gallons
Minimum turndown	30%
Fuel curve slope (gal/kW/hr)	0.072119 ³⁴
Fuel curve intercept (gal/hr)	0.435884
Availability	Runs only during grid outages and scheduled maintenance testing. We assume the generators do not participate in peak load management.
Utility Assumptions	
Electricity costs	See Appendix C for tariff details.
Electricity cost escalation rate	1.52%/year ³⁵
Ownership and Financing	
Ownership model	NYC-DOE: Third party FDNY: Direct ownership

²⁷ DG HUB. 2015. "Resilient Solar Photovoltaics (PV) Systems."

<http://www.cuny.edu/about/resources/sustainability/SmartDGHUBEmergencyPower/DecHardwareFactSheet.pdf>.

²⁸ Ibid.

²⁹ Ibid.

³⁰ DG Hub Survey. 2015. www.cuny.edu/DGHub

³¹ Rocky Mountain Institute. 2015. "Defection Economics: PV, Batteries, and the Grid." Presented May 7, 2015.

³² https://www.eia.gov/dnav/pet/pet_pri_gnd_dcus_y35ny_a.htm

³³ National Institute for Standards and Technology (NIST). 2015. "Energy Price Indices and Discount Factors for Life-Cycle Cost Analysis- 2015." <http://energy.gov/eere/femp/downloads/energy-price-indices-and-discount-factors-life-cycle-cost-analysis-2015>

³⁴ Based on Homer Pro 50-kW generator

³⁵ National Institute for Standards and Technology (NIST). 2015. "Energy Price Indices and Discount Factors for Life-Cycle Cost Analysis- 2015." <http://energy.gov/eere/femp/downloads/energy-price-indices-and-discount-factors-life-cycle-cost-analysis-2015>

	NYCHA: Third party
Corporate tax rate	35%
Developer discount rate	10%
Off-taker discount rate	3.1%
Incentives	
Investment Tax Credit (ITC)	<ul style="list-style-type: none"> • Third-party ownership scenario: <ul style="list-style-type: none"> • 30% ITC applied to PV only; not applied to batteries because they are not charged at least 75% from PV • Direct ownership scenario: ITC not applied
Modified Accelerated Cost Recovery System (MACRS)	<ul style="list-style-type: none"> • Third-party ownership scenario: 5 year MACRS applied to PV • Direct ownership scenario: MACRS not applied
Net metering	NYC-DOE: No FDNY, NYCHA: Yes
NYSERDA NY-Sun incentive for PV systems under 200 kW	\$0.80/W for the first 50 kW and \$0.50/W for the next 51-200 kW ³⁶
Property tax abatement	None (government property)
Solar Renewable Energy Credit (SREC)	None
Value Streams	
Ancillary services	None ³⁷
Demand response	<ul style="list-style-type: none"> • NYC-DOE: The Susan Wagner High School participates in the DCAS (NYISO) demand response program. Based on historical data, DCAS estimates savings of \$100/kW reduced in each season (summer and winter). Because the potential savings from peak demand management are greater, and participating in the demand response program would reduce battery availability for peak demand management, in this analysis the potential demand response revenues are not included. • FDNY: No demand response; the system is too small to participate. • NYCHA: No demand response; the system is too small to participate.
Grid outage cost	<ul style="list-style-type: none"> • FDNY: \$917.43/hour • NYCHA: \$87.53/hour • NYC-DOE: \$68.97/hour (See Section 2.4)

The costs modeled in this analysis include the installed cost of the PV, battery, and/or diesel generator. There may be additional costs associated with integrating these systems that are not included in the analysis. This is due to a lack of validated cost data. These may include:

³⁶ See NY-Sun Nonresidential Block Structure, Block 3: <http://ny-sun.ny.gov/For-Installers/Megawatt-Block-Incentive-Structure>.

³⁷ NYISO ancillary services program requires 1 MW minimum. These sites are all <210 kW so aggregation to meet this threshold is unlikely.

- **Building physical characteristics:** Installation costs can vary based on the relative ease or difficulty of installing equipment and communication and controls. For example, ideal locations for electrical or communication and controls equipment may be mechanical and electrical rooms. If these spaces do not have enough room or working clearance, additional conduit runs or trenching may be necessary.
- **Structure to house batteries and environmental controls:** Environmental controls (cooling, ventilation, and filters) may be required to maintain the batteries within the manufacturer's recommended operating range. A shipping container or other structure to house the batteries may also be required if they cannot be stored inside the buildings.
- **Automatic transfer switch:** We assume a manual transfer switch would be installed to isolate the facility from the grid during a grid outage. This requires a person to physically flip a switch to transfer to the backup power system. The cost of the switch depends on the building voltage. An automated transfer switch could be included at additional cost. In either case, a brief outage will occur while the facility is switched from grid-connected mode to islanded mode, though in the case of the automated transfer switch, the outage would be of shorter duration (typically a few milliseconds to a few seconds).
- **Critical load isolation:** We did not include the cost of retrofitting the buildings with critical load panel(s). Depending on the electrical distribution infrastructure of the building, this cost can range from \$10,000 to \$100,000³⁸ or more for a building in NYC, including design/permit, electrician's fees for re-wiring, transfer switches, and new critical load panels. It may be more cost-effective to supply the entire building rather than modify the electrical system. In this case, some loads would need to be manually turned off during islanding events. In other cases, the building may have already installed a critical load panel.
- **Site controller:** Using resilient PV and hybrid systems during grid outages may add cost beyond what is presented in this analysis, depending on the level of system integration that is required. While most bi-directional inverters on the market are already enabled for island operation, they are controlled differently in island mode. Some commercially available microgrid controllers may be easily configured to provide both grid-connected and island functionality while others may require significant system integration engineering and additional hardware for proper islanded operation of all resources. Depending on the out-of-the-box capabilities of the site controller and the respective front end monitoring and control equipment on the PV inverter, battery, and diesel generator, this might add an additional \$20,000 or more³⁹ in system integration costs to a project. There may also be some additional hardware costs for communication cables and devices on the order of \$5,000-10,000.⁴⁰ If a standalone diesel generator is used to provide backup power, no additional monitoring or control costs are anticipated since controls are already built into the generator.

Additionally, it is important to note that actual demand savings may vary from predicted demand savings based on the actual battery control strategy used at the site. Because actual interval load data were not available for two of the three sites (the fire station and the school), load data were synthesized from models. There is some additional uncertainty in the results for these sites

³⁸ Email with energy company, 12/11/15.

³⁹ Email with energy company, 12/11/15.

⁴⁰ Conversation with Robert Butt, Senior Engineer, NREL, 12/14/15.

because hour-to-hour load variation in actual load profiles may be different from those developed by the models.

There may also be additional value streams not included in this analysis. For example, for systems meeting certain requirements, NYPA's peak load management program offers payments for capacity and energy reductions during demand response events.⁴¹

2.4 Value of Resiliency

Many organizations have trouble quantifying the price they are willing to pay for having a source of continuous, reliable electricity. The challenge of valuing resiliency causes most PV and battery systems to be designed and installed based upon their expected economic return during normal grid-connected operation. Although these systems will provide some measure of added resiliency, often no hard monetary value is assigned to the added resiliency, which is to say that the systems are expected to “pencil-out” before resiliency is considered.

This analysis modeled a resiliency value stream within the REopt model in order to demonstrate how valuing resiliency impacts system sizing and project economics. In this study, we assume that the value of resiliency to a site is equal to the costs they incur during an outage. The cost of power interruptions for a facility is a site-specific cost that depends on a number of factors including frequency, duration, timing of outages, activities that take place in the facility, and availability of backup systems. To calculate a site-specific outage cost, the facility could add up the damages that it will experience as a result of a grid outage. Some facilities such as government organizations involved in life safety may be exposed to other second- and third-order damages (i.e., inability to treat wastewater, inability to dispatch firefighters, inability to react to criminal activity).

In general, there are two approaches to determining the cost of a grid interruption: macroscopic or microscopic. In the macroscopic approach, the value is based on national or utility-wide estimates of outage costs that have been experienced in the past.⁴² This method requires relatively little data, but may not capture site-specific values well. In the microscopic approach, the value is based on a survey of the site-specific installation of outage costs.⁴³ This may be more accurate, but is much more time-consuming to determine.

To determine the value of resiliency for the facilities in this study, the team selected a macroscopic approach because it is widely applicable, replicable for other facilities, and could be applied without lengthy data collection activities at the site. The U.S. Department of Energy's (DOE) Interruption Cost Estimator (ICE) calculator was used⁴⁴ to calculate outage costs that were used as a proxy for the value of resiliency for grid outages at each site based on utility reliability metrics and site characteristics.

⁴¹ See, “The Power of Demand: Peak Load Management Program for Governmental Customers.” http://www.nyc.gov/html/dem/downloads/pdf/PLM_brochure.pdf.

⁴² Sullivan, M., J. Schellenberg, and M. Blundell. 2015. *Updated Value of Service Reliability Estimates for Electric Utility Customers in the United States*. Berkeley, CA: LBNL. http://eetd.lbl.gov/sites/all/files/lbnl-6941e_0.pdf.

⁴³ Sullivan, M., and D. Keane. 1995. *Outage Cost Estimation Guidebook* EPRI. <http://www.epri.com/abstracts/Pages/ProductAbstract.aspx?ProductId=TR-106082>.

⁴⁴ “Interruption Cost Estimate (ICE) Calculator.” 2015. DOE. <http://icecalculator.com/>.

The ICE calculator requires several inputs (Figure 21) to calculate outage costs, including reliability data. The New York State Department of Public Service releases a reliability report each year that includes the following values with and without major storms included:⁴⁵

SAIFI is the average number of interruptions a customer experiences in a calendar year.

SAIDI is the average outage duration across all customers served.

CAIDI is the average outage duration per utility customer affected (in hours).

These values are reported by all regulated utilities in the country. A best-fit linear trend line shows that Con Edison grid outage duration and frequency with storms have been increasing over the past 14 years (see Figure 22).

Reliability Inputs	
SAIFI <input type="text"/>	
Please enter SAIDI or CAIDI (in minutes):	
SAIDI <input type="text"/>	CAIDI <input type="text"/>
Number of Customers	
Non-Residential <input type="text"/>	
Residential <input type="text"/>	

Figure 21. Screenshot of DOE ICE Calculator inputs

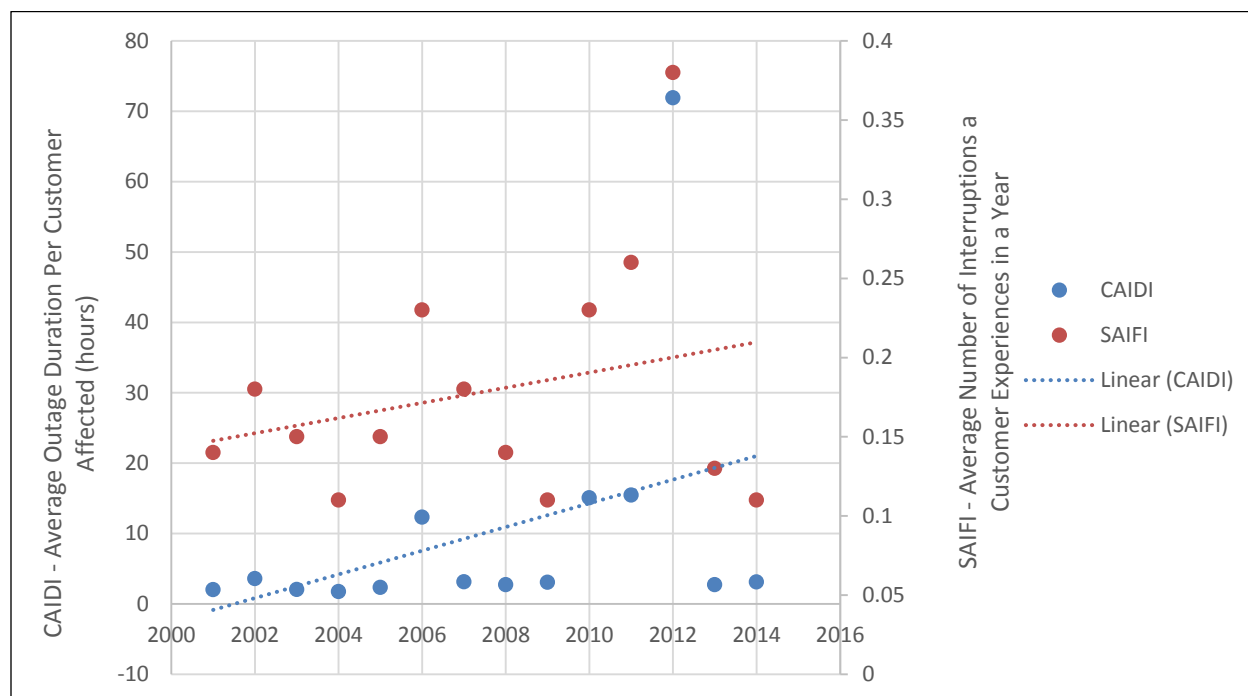


Figure 22. Con Edison system-wide grid reliability with storms

⁴⁵ “Electric Service Reliability Reports.” 2015. New York State Department of Public Service. <http://www3.dps.ny.gov/W/PSCWeb.nsf/All/D82A200687D96D3985257687006F39CA?OpenDocument>.

To appropriately represent the increasing frequency and duration of outages due to storms, the average reliability metrics from the past five years were used instead of the full 14-year data set. The frequency of outages (SAIFI) depends on if the facility is on the network or the radial grid. The values are summarized in the following table.

Table 8. Con Edison Five-Year Average SAIFI Values for Radial and Network Customers

Grid Segment	SAIFI
Radial	0.77
Network	0.04

Two outage duration values (CAIDI) are evaluated: “with storm” grid statistics (hereafter referred to as a long duration outage) and “without storm” grid statistics (hereafter referred to as a short duration outage); they are summarized in Table 9.⁴⁶ This establishes a lower and upper bound for grid outage duration for both the network and the radial grid, and establishes short and long outage cases for the analysis scenarios.

Table 9. Con Edison CAIDI Values for Radial and Network Customers

Grid Type	CAIDI (hours/year)	Technical Analysis Scenario
Radial		
Average year without storms (five-year average)	1.99	Short
Average year with storms (five-year average)	21.88	Long
Network		
Average year without storms (five-year average)	7.25	Short
Average year with storms (five-year average)	50.96	Long

The facility specific costs of interruptions (i.e., annual value of resiliency) are developed using the U.S. DOE ICE Calculator.⁴⁷ The ICE Calculator takes inputs of SAIFI, CAIDI, number of customers, customer class (residential, non-residential), location (state), average energy usage (MWh)⁴⁸, industry type, backup capabilities, and distribution of outages by time of day (percentage). Using the reliability metrics shown above, an outage cost vs. duration table is developed for each of the facilities in the study (see cost curve tables in Appendix B). The “Unit Cost of Interruption” is averaged over the 16-hour range that the ICE Calculator is able to analyze to provide an average hourly cost of interruption.

⁴⁶ The National Electric Code (NEC) requires that emergency and standby power systems supply power within a specified number of seconds and for a specified amount of time. The outage durations in this analysis are derived from Con Edison historical outage data, rather than from the NEC.

⁴⁷ “Interruption Cost Estimate (ICE) Calculator.” 2015. DOE. <http://icecalculator.com/>.

⁴⁸ Critical load that is supported during a grid outage.

Table 10 summarizes the hourly cost of interruptions, or value of providing resiliency, for the facilities included in the study. Additional information is provided in Appendix B.

Table 10. Value of Resiliency for Study Facilities

Site	Value of Resiliency Provided (\$/hour/year)	Annual Cost of Short Duration Outage (2 or 7 hours)	Annual Cost of Long Duration Outage (22 or 51 hours)
NYC-DOE School Shelter (network)	\$ 68.97	\$ 500.19	\$ 3,515.15
FDNY Fire Station (radial)	\$ 917.43	\$ 1,823.85	\$ 20,071.51
NYCHA Cooling Center (network)	\$ 32.02	\$ 232.15	\$ 1631.74

Due to variation in load, solar resource, and battery state of charge, the amount of time a given resilient PV system can sustain the load during an outage varies by time of day and time of year. For each site, a series of 8760 simulations were performed to calculate the number of hours a resilient PV system could sustain the critical load for outages beginning during every hour of the year. The average number of hours the system can be expected to maintain the load was calculated from the results of these 8,760 simulations, and is defined as a resiliency metric R . Parametric sweeps were performed to calculate a range of R values for various PV and storage sizes, and then a multi-variate regression analysis was conducted to calculate regression coefficients for the PV and storage components. For Scenario 1, the value of resiliency was incorporated into the optimization of system size based on the regression coefficients, hourly cost of interruptions, and expected annual outage duration.⁴⁹

2.5 Analysis Approach

NREL's REopt model was used to size and dispatch PV, battery, and/or generator systems in four scenarios including both economic and resiliency benefits:

- Scenario 1: Resilient PV sized for economic savings; no resiliency requirement imposed**

The model chose from solar and storage resources to size resilient PV systems that are cost-effective for the host site while grid-connected, and then evaluated the resiliency benefits these systems provided.

- Scenario 2: Resilient PV sized to meet resiliency needs**

The model chose from solar and storage resources to size resilient PV systems capable of sustaining critical electric loads for short and long outages, and then evaluated the grid-connected economic benefit that these systems provide during normal grid operations.

- Scenario 3: Resilient PV and a generator (hybrid system) sized to meet resiliency needs**

The model chose from solar, storage, and diesel generator resources to size hybrid systems capable of sustaining critical electric loads for short and long outages, and then

⁴⁹ Simpkins, T., K. Anderson, D. Cutler, and D. Olis. 2016. "Optimal Sizing of a Solar-Plus-Storage System For Utility Bill Savings and Resiliency Benefits," accepted for publication in *Proc. 7th Conf. on Innovative Smart Grid Technologies*, Minneapolis, MN.

evaluated the grid-connected economic benefit that these systems provide during normal grid operations.

4. **Scenario 4: Generator sized to meet resiliency needs**

The model sized a diesel generator to support critical electric loads for short and long outages.

In this analysis, cost-effective means that the modeled system has an NPV that is equal to or greater than zero, and thus provides lifecycle cost savings to the site. Building owners may have other measures of cost-effectiveness such as lowest initial capital cost. While initial cost is presented in our results, systems are selected based on maximizing lifecycle cost savings, not lowest first cost.

Given NYC's commitment to install solar on city-owned buildings in order to reduce emissions, when the cost-optimal system did not include solar as part of the solution in Scenarios 1-3, any positive life cycle cost savings attainable by a battery-only system were used to offset the cost of solar and incorporate it into the recommended system, up to the point that NPV reached zero or all available space for solar was filled. This allows NYC to understand the combined impacts of solar and storage for cost savings and resiliency when installed together, and demonstrates how storage can facilitate implementation of PV systems that would not be cost-effective on their own.

In each scenario, the resilient PV system was able to operate for financial benefits during grid-tied operation and was also able to serve the critical loads during grid outages. The generator was only able to operate during the outage. We modeled each scenario both with and without a resiliency value to understand the impact of valuing resiliency has on system sizing (for scenario 1) and economics (for all scenarios). We modeled Scenarios 2-4 with two different outage lengths (a short and long duration outage, described in Section 2.4) to demonstrate how system sizing and economics change with varying outage lengths.

Since the solar resource and critical load are both time-varying, the size of the resilient PV system required to sustain the critical load will be different depending on when the outage begins. For example, an outage occurring in the spring when loads are lower may require a smaller system than one occurring in the summer when loads are higher. To properly account for the stochastic nature of the critical load and the solar resource, the model should be run multiple times with the outage beginning at a different point in the year each time. The largest system required to sustain the critical load during this series of model runs would then represent the worst case, and could be assumed to meet the load during any of the other outages. Given the computational complexity of the model, for the purposes of this analysis we selected the period with the highest load and lowest solar generation to represent the worst case outage.

In this analysis, we assume the battery is fully charged at the time the outage occurs. Some outage events can be forecasted due to extreme weather, and in these cases the building owner may choose to charge the battery prior to the outage. Some outages cannot be predicted, and in this case, the assumption that the battery is fully charged is optimistic. A more thorough stochastic examination of the impact of battery state of charge is recommended for future work, but is not part of the scope of this analysis.

We also assume that the battery will be replaced once during the 25 year project lifecycle, and the replacement cost is amortized into the upfront capital cost. The lifetime of the battery will depend on number of cycles and depth of discharge. A lithium ion battery may be expected to last ten to twelve years based on calendar degradation. A battery may not last the entire twelve years, however, if it experiences an excessive number of deep charge / discharge cycles. Rather than include this effect in the model, we simply assume that the battery will last twelve years based on calendar degradation and then post-process the dispatch using the rainflow algorithm to verify the assumption⁵⁰.

Each scenario is described in more detail below.

Scenario 1: Resilient PV Sized for Economic Savings; no Resiliency Requirement Imposed

In the first scenario, resiliency is not included as a design constraint; the optimal system configuration is based on achieving lowest life cycle cost assuming the grid is always available. In Scenario 1.1, system revenues are the utility savings, incentives, and tax benefits. Scenario 1.2 and 1.3 add a short and long outage resiliency value to the potential economic value streams.

Once the optimal sizes for the PV and/or battery system were determined based upon the revenue streams available, a series of simulations was conducted to assess the added resiliency benefit that such a system could achieve. The length of time for which the critical load could be sustained varies based on the state of charge of the battery, the solar resource, and the size of the critical load during the outage. For this analysis, we evaluated a “best case” and “worst case” outage period to show the maximum and minimum amount of resiliency the system could be expected to provide, where the best case was the period of lowest load and highest solar generation and the worst case was the period of highest load and lowest solar generation.

Scenario 2: Resilient PV Sized to meet Resiliency Needs

In the second scenario, we introduce resiliency as a design constraint. Rather than designing exclusively to maximize utility savings and policy incentives, we now require that the model identify a system that can sustain the critical load during specified outage lengths. Although the system is explicitly designed to sustain the specified outages, it can also be used for economic gain in normal operation, the same as in the first scenario. This scenario illustrates the incremental cost required when resiliency is added as a design constraint as well as the incremental benefit of avoiding outage costs. We look at a short (Scenario 2.1) and a long (Scenario 2.2) outage length, and evaluate each with and without assigning a value to resiliency.

Scenario 3: Resilient PV and a Generator (Hybrid System) Sized to meet Resiliency Needs

The third scenario is essentially the same as the second except that the candidate pool of technologies now includes a diesel generator in addition to the PV and battery. The model is constrained to operating the diesel generator only during grid outages while the PV and storage can operate both during outages and when the grid is operational.

⁵⁰ S.D. Downing, and D.F. Socie, *Simple Rainflow Counting Algorithms*; International Journal of Fatigue; 1982.

Scenario 4: Generator Sized to meet Resiliency Needs

The fourth scenario considers a diesel-only case which is essentially the same as the second and third scenarios except that the candidate pool of technologies now includes only a diesel generator. Generators in this analysis were unable to participate in demand response due to small system sizes and the complexities of siting and operating a generator for demand response. Scenario 4 is included for completeness and to provide a cost comparison of the various options for ensuring resiliency of the site.

The scenarios are summarized in Table 11.

While energy efficiency, natural gas generators, combined heat and power and other distributed generation resources may also offer economic and resiliency benefits, these were not modeled due to time and funding limitations.

Table 11. Scenarios

Scenario	Description	Outage Length	Resiliency Valued
1.1	Resilient PV sized for economic savings; no resiliency requirement imposed	N/A	No
1.2	Resilient PV sized for economic savings; no resiliency requirement imposed	Short – not required	Yes
1.3	Resilient PV sized for economic savings; no resiliency requirement imposed	Long – not required	Yes
2.1.a	Resilient PV sized to meet resiliency needs	Short	No
2.1.b	Resilient PV sized to meet resiliency needs	Short	Yes
2.2.a	Resilient PV sized to meet resiliency needs	Long	No
2.2.b	Resilient PV sized to meet resiliency needs	Long	Yes
3.1.a	Resilient PV + generator sized to meet resiliency needs	Short	No
3.1.b	Resilient PV + generator sized to meet resiliency needs	Short	Yes
3.2.a	Resilient PV + generator sized to meet resiliency needs	Long	No
3.2.b	Resilient PV + generator sized to meet resiliency needs	Long	Yes
4.1.a	Generator only sized to meet resiliency needs	Short	No
4.1.b	Generator only sized to meet resiliency needs	Short	Yes
4.2.a	Generator only sized to meet resiliency needs	Long	No
4.2.b	Generator only sized to meet resiliency needs	Long	Yes

3 Results

A summary of REopt results for each of the four scenarios is presented in this section for all three sites. See Appendix D for comprehensive results for each site.

The costs presented in this section may not include additional integration costs, such as critical load isolation or those that result from physical building characteristics, as outlined in Section 2.3. Any increases in cost would impact project economics.

3.1 NYC-DOE High School/Coastal Storm Shelter

Scenario 1: Resilient PV Sized for Economic Savings; no Resiliency Requirement Imposed

A high-level summary of system sizing and costs for Scenario 1 are below in Table 12.

Table 12. School Shelter Scenario 1 Results

School Shelter			
Scenario 1: PV + Storage Sized for Economic Savings			
	System 1.1: No resiliency value included	System 1.2: Short-duration resiliency value included	System 1.3: Long-duration resiliency value included
PV Size (kW-DC)	50	50	50
Battery Size (kWh)	74	74	74
Battery Size (kW)	35	35	35
Total Capital Cost	\$205,716	\$205,716	\$205,716
NPV	\$51,560	\$58,650	\$58,650
Simple Payback (years)	14.3	13.9	13.9

System 1.1 is a traditional economic analysis that does not include a resiliency value stream. This system would save the school \$51,000 over 25 years, which represents about 1% savings over the base case life cycle cost (see Appendix D). Because the resiliency value for network grid customers is relatively low, allowing the system to capture resiliency benefits in Systems 1.2 and 1.3 does not change the system size, but does reduce the payback period by 0.4 years and increases the NPV by about 14% (\$7,000).

Though this site can accommodate over 200 kW of solar, the economically optimal size solar array selected by the model is 50 kW-DC due in part to the NY-Sun incentive modeled at \$0.80/W for the first 50 kW and \$0.50/W for the next 51-200 kW. Unlike the other two sites modeled in this analysis, solar at the school shelter was selected as an economically optimal solution without requiring storage savings to offset solar costs. This is due to a lower cost of solar assumed for larger systems at this site and ample roof space. The assumed third-party ownership of the system at this site also allows the school to benefit from the federal tax incentives the developer would capture.

For all three cases, savings are attained by managing demand during peak periods. This is shown in Figure 23 where the battery is strategically discharged to reduce peak loads.

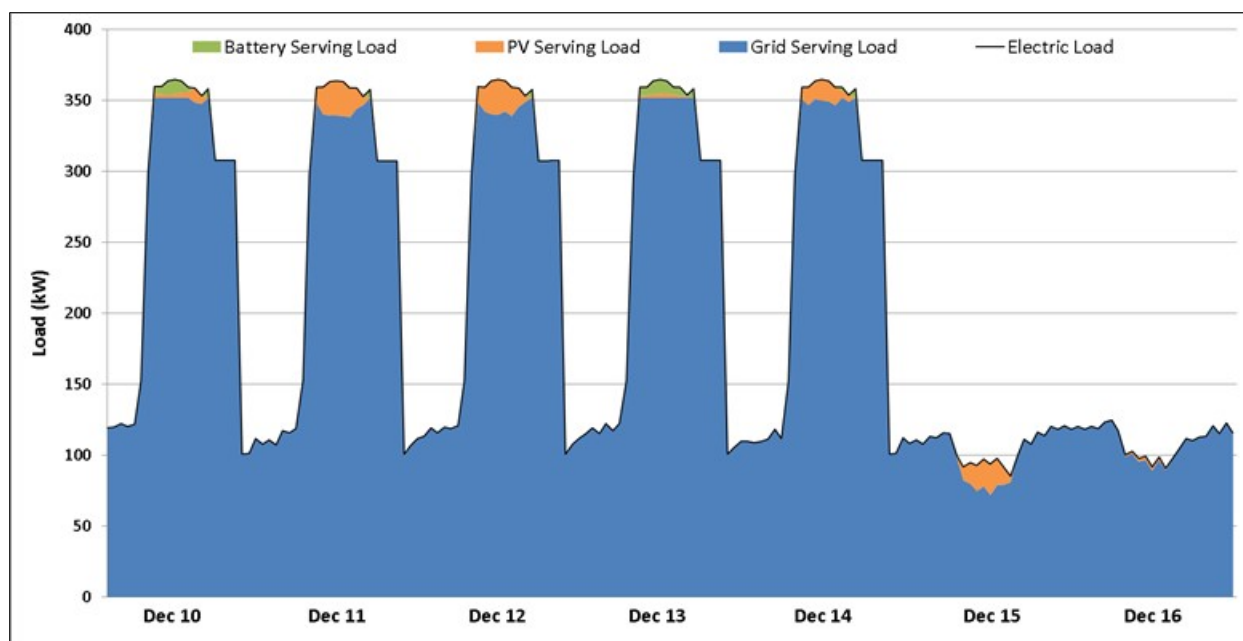


Figure 23. PV and battery combine to reduce peak demand

Because the school is on a spot network⁵¹, exported energy can be problematic, so net metering savings were not factored into the analysis. A reverse power relay could be installed to prevent export at an estimated cost of \$5,000. The school could alternatively implement a smart grid solution⁵² to allow export. However, the smart grid solution costs \$50,000-100,000, and the exported power for the maximum solar array (210 kW) is only worth about \$500/year (\$12,500 over 25 years), so in this case, the reverse power relay to prevent export is a better economic choice.

The school participates in both the summer and winter DCAS demand response programs through NYPA. Potential revenues are approximately \$100/kW of demand reduced in each season. Historically, the school has committed 25 kW of demand response in the summer (for revenue of approximately \$2,500) and 10 kW in the winter (for revenue of approximately \$1,000).

⁵¹ A spot network is a utility installation designed with multiple high-voltage feeders and transformers tied to a common bus to ensure reliable electric service for large electric load users. The network protectors on these transformers are designed with an automatic safety feature where the network protector will open when energy feeds back from the low-voltage bus toward the high-voltage feeder, which is indicative of a fault on the high-voltage cable. If a PV system were installed on a spot network and solar production were to exceed building load at any given time, the network protectors would sense the export of PV power as conditions analogous to those during a high-voltage feeder fault and would open automatically, causing the electricity service to that building to go out.

⁵² There are two options when installing PV on a spot network. First, a reverse power relay can be installed to trip solar inverters offline whenever incoming power drops below a certain minimum amount in order to prevent any possibility of back feed of power to the network protectors. This costs approximately \$5,000-10,000. Second, if export of solar is desired, a smart grid solution including lightening the sensitivity of the network protectors to prevent them from opening under normal PV export conditions, installing SCADA monitoring and communications equipment, and anti-islanding relays can be installed. This costs approximately \$50,000-100,000.

The school could potentially use the battery to increase its commitment to the demand response program. In theory, if the battery were fully charged each time the demand response call was issued, and the required demand reduction period was short enough that the battery could discharge at full capacity for the whole window, the 35-kW battery could potentially save the school \$3,500 in the summer and \$3,500 in the winter for a total of \$7,000/year.

These potential revenues are significant, but less than the savings the battery provides by managing peak demand. The battery saves the school about \$14,000/year through peak demand management. If the battery is being used for peak demand management, it is unlikely the full battery capacity will be available to participate in demand response programs. Some of the battery capacity could be re-allocated away from peak management toward demand response in order to capture demand response revenues, but this would likely reduce peak demand management revenues.

It may be possible to use the battery for peak demand management while also allocating a portion of its capacity to demand response. Optimizing the use of the battery for simultaneous peak demand management and demand response requires detailed modeling of the demand response program, including the expected date and length of demand response calls and the payment available for each of those calls. This is beyond the scope of this analysis. For purposes of this analysis, we assume that the battery will be used for peak demand management rather than demand response since peak demand management provides a higher value stream.

Next, we evaluated the length of time that the 50-kW PV and 35-kW/74-kWh battery system could sustain the critical load during a short outage of 7 hours and a long outage of 51 hours. For the short outage, under the worst case scenario (low PV and high load), the system can support the full critical load for 3.1 hours, or 46% of the critical load for the entire 7 hours. Under the best case scenario (high PV and low load), the system can power additional loads beyond those designated as critical. For the long outage, under the worst case scenario (low PV and high load), the system can support the full critical load for 6 hours, or 12% of the critical load for 51 hours. Under the best case scenario (high PV and low load), the system can support the full critical load for 31 hours, or support 50% of the critical load for 51 hours; see Table 13.

Table 13. Percent of Critical Load System Can Support

	System 1.1: No resiliency value captured	System 1.2: Short-duration resiliency value captured	System 1.3: Long-duration resiliency value captured
7-Hour Outage (Worst)	46%	46%	46%
7-Hour Outage (Best)	285%	285%	285%
51-Hour Outage (Worst)	12%	12%	12%
51-Hour Outage (Best)	50%	50%	50%

Scenario 2: Resilient PV Sized to meet Resiliency Needs

A high-level summary of system sizing and costs for Scenario 2 are below in Table 14.

Table 14. School Shelter Scenario 2 Results

School Shelter				
Scenario 2: PV + Storage Sized for Resiliency				
	System 2.1A: Short outage; resiliency not valued	System 2.1B: Short outage; resiliency valued	System 2.2A: Long outage; resiliency not valued	System 2.2B: Long outage; resiliency valued
PV Size (kW-DC)	50	50	200	200
Battery Size (kWh)	203	203	985	985
Battery Size (kW)	68	68	158	158
Total Capital Cost	\$306,282	\$306,282	\$1,244,758	\$1,244,758
NPV	\$21,870	\$30,570	-\$523,480	-\$462,330
Simple Payback (years)	12.0	11.7	18.4	17.5

A cost-effective resilient PV system in Scenario 2 is possible with and without resiliency valued for short outages. Without resiliency valued, a system sized to cover the short outage would save the school \$21,000 over 25 years. This number increases by 40% to \$30,000 when a resiliency value stream is added.

In order to support a long outage, the size of the PV system increases by 300% and the battery capacity (kWh) increases by 385%. The battery provides most of the energy to sustain the critical load, though the PV system provides some as well (see Figure 24). The NPV for both systems supporting a long outage is negative, again demonstrating that adding a resiliency value does not always have a large impact for network grid customers.

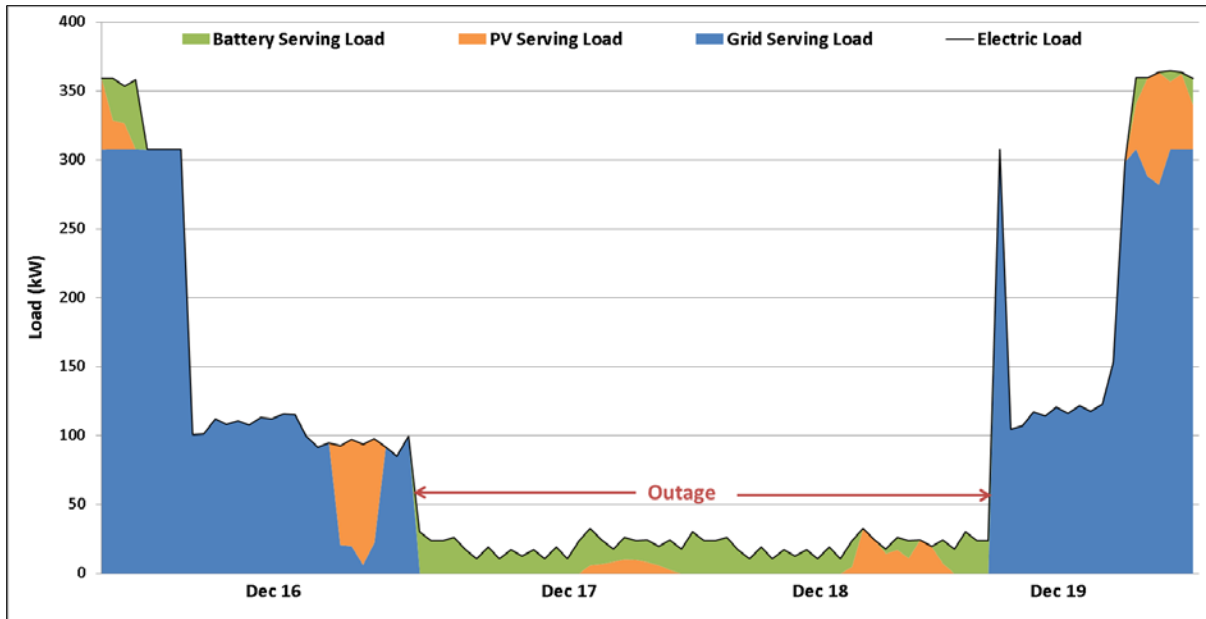


Figure 24. PV and battery support the critical load during a 51-hour outage

Scenario 3: Resilient PV and a Generator (Hybrid System) Sized to meet Resiliency Needs

A high-level summary of system sizing and costs for Scenario 3 are below in Table 15.

Table 15. School Shelter Scenario 3 Results

School Shelter				
Scenario 3: PV + Storage + Generator Sized for Resiliency				
	System 3.1A: Short outage; resiliency not valued	System 3.1B: Short outage; resiliency valued	System 3.2A: Long outage; resiliency not valued	System 3.2B: Long outage; resiliency valued
PV Size (kW-DC)	50	50	50	50
Battery Size (kWh)	118	118	87	87
Battery Size (kW)	48	48	39	39
Diesel Generator Size (kW)	10	10	18	18
Diesel Fuel Used (gallons/yr)	8	8	88	88
Total Capital Cost	\$255,974	\$255,974	\$244,331	\$244,331
NPV	\$23,650	\$32,350	\$17,380	\$78,530
Simple Payback (years)	14.5	14.1	15.5	12.7

The results for Scenario 3 demonstrate that all four systems are cost-effective. By integrating a diesel generator into the PV and battery system, the school can sustain a longer outage period at much lower cost than if they were to use a PV and battery system alone. The school can save \$17,000 - \$78,000 over the 25-year life of the system, depending on the length of outage the system is sized for and whether or not resiliency is valued. The resiliency value stream increases the NPV somewhat, especially in the long outage scenario (3.2B).

The size of the PV system remains at 50 kW across all four systems, again likely due to the reduction in the NY-Sun incentive above 50 kW. However, the battery size decreases and generator increases when moving from the short to long outage. This is because a much larger battery would be required to sustain a long outage (as seen in 2.2.B). Peak demand management provides diminishing returns, and the savings from demand charge management do not offset the costs of a larger battery. The cost of additional fuel for the generator is relatively small (about \$200 for 80 gallons), so the model elects to use the generator instead. The PV and battery allow a smaller generator to cover the critical load (see Figure 25). The amount of fuel required to support a long outage increases ten-fold over short outage systems.

The capital cost for short-duration systems is slightly higher than long-duration total capital cost due to the larger battery size; however, the payback period is shorter for the short-duration systems. Third-party ownership was modeled for this site since NYC-DOE would likely use a PPA to implement the system, so upfront funding would not likely be a concern.

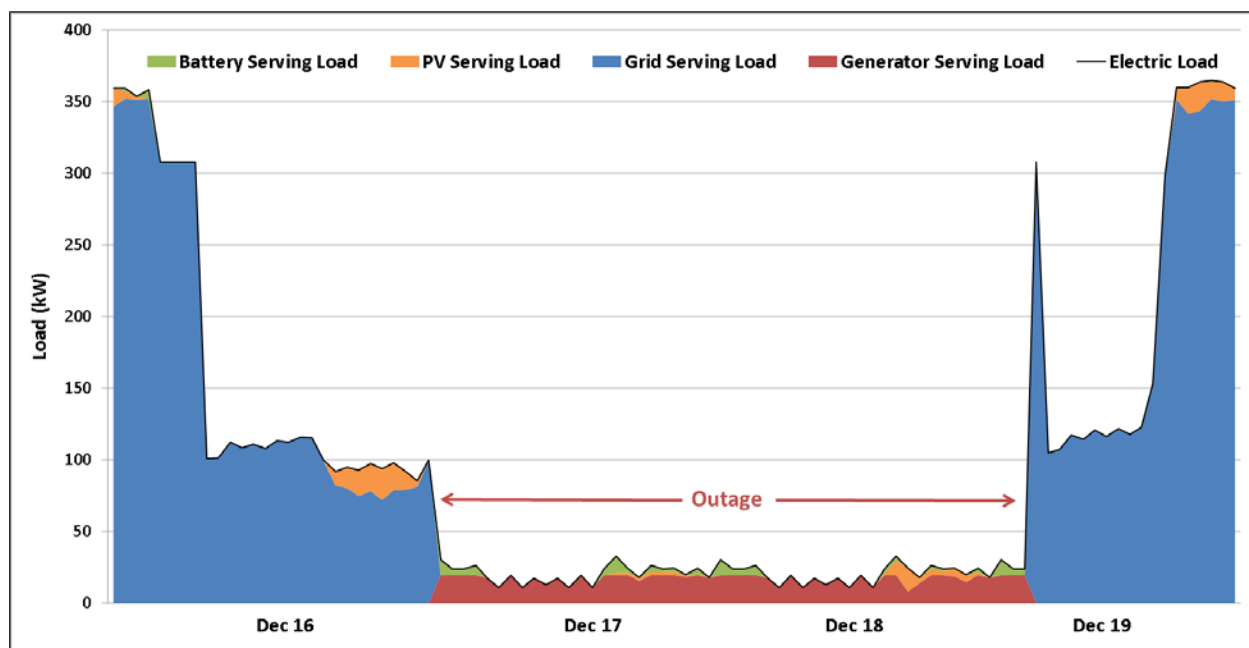


Figure 25. PV and battery reduce the size of generator required to meet the critical load during a 51-hour outage

Scenario 4: Generator Sized to meet Resiliency Needs

A high-level summary of system sizing and costs for Scenario 4 are below in Table 16.

Table 16. School Shelter Scenario 4 Results

School Shelter				
Scenario 4: Generator Sized for Resiliency				
	System 4.1A: Short outage; resiliency not valued	System 4.1B: Short outage; resiliency valued	System 4.2A: Long outage; resiliency not valued	System 4.2B: Long outage; resiliency valued
Diesel Generator Size (kW)	30	30	33	33
Diesel Fuel Used (gallons/yr)	15	15	98	98
Total Capital Cost	\$44,850	\$44,850	\$48,900	\$48,900
NPV	-\$61,470	-\$52,770	-\$63,550	-\$2,400
Simple Payback (years)	None	None	None	14.9

The NPV for all four systems in Scenario 4 is negative, and only system 4.2B has a simple payback when resiliency is valued. System size and capital cost do not increase much when moving from short to long outages, but the amount of fuel required increases by 83 gallons (550%).

Discussion of School Shelter Results Across All Scenarios

Table 17 compares the NPV and simple payback for the three scenarios (2-4) that size systems for resiliency. The highest NPV and quickest payback in each column is highlighted in green, as is the row with the most green cells, to represent the system with the best economics overall. Looking across all the systems sized to support resiliency needs, Scenario 3 has the highest NPV and shortest payback period for systems designed to support long outages. Scenario 4 has the lowest upfront capital cost of all the scenarios, but NPV is negative in all four cases.

Table 17. School Shelter NPV and Payback Comparison of Scenarios 2, 3, and 4

School Shelter				
Most Cost-Effective Option for Outage Coverage				
	Short outage; resiliency not valued	Long outage; resiliency not valued	Short outage; resiliency valued	Long outage; resiliency valued
Scenario 2: PV+Storage NPV	\$21,870	-\$523,480	\$30,570	-\$462,330
Scenario 2: PV+Storage Payback	12.0	18.4	11.7	17.5
Scenario 3: Hybrid NPV	\$23,650	\$17,380	\$32,350	\$78,530
Scenario 3: Hybrid Payback	14.5	15.5	14.1	12.7
Scenario 4: Generator NPV	-\$61,470	-\$63,550	-\$52,770	-\$2,400
Scenario 4: Generator Payback	N/A	N/A	N/A	14.9

3.2 FDNY EC309

Scenario 1: Resilient PV Sized for Economic Savings; no Resiliency Requirement Imposed

A high-level summary of system sizing and costs for Scenario 1 are below in Table 18.

Table 18. Fire Station Scenario 1 Results

Fire Station			
Scenario 1: PV + Storage Sized for Economic Savings			
	System 1.1: No resiliency value captured	System 1.2: Short duration resiliency value captured	System 1.3: Long duration resiliency value captured
PV Size (kW-DC)	10	10	10
Battery Size (kWh)	43	43	213
Battery Size (kW)	16	16	31
Total Capital Cost	\$69,413	\$69,413	\$172,741
NPV	\$22,365	\$54,132	\$324,250
Simple Payback (years)	15.9	10.5	6.1

System 1.1 is a traditional economic analysis that does not include a resiliency value stream. This system would save the fire station \$22,000 over 25 years, which represents about 5.1% savings over the base case life cycle cost. When the system is able to capture a resiliency value for a short duration outage (approximately 2 hours/year in this case), the system size remains the same, but the payback period is reduced by 5.4 years. System 1.3 is able to capture a resiliency value for a long duration outage (approximately 22 hours/year), which increases the battery storage size by 495% and reduces the payback period by an additional 4.4 years.

For all three cases, savings are attained by managing demand during peak periods. This is shown in Figure 26, where the battery is strategically discharged to reduce peaks.

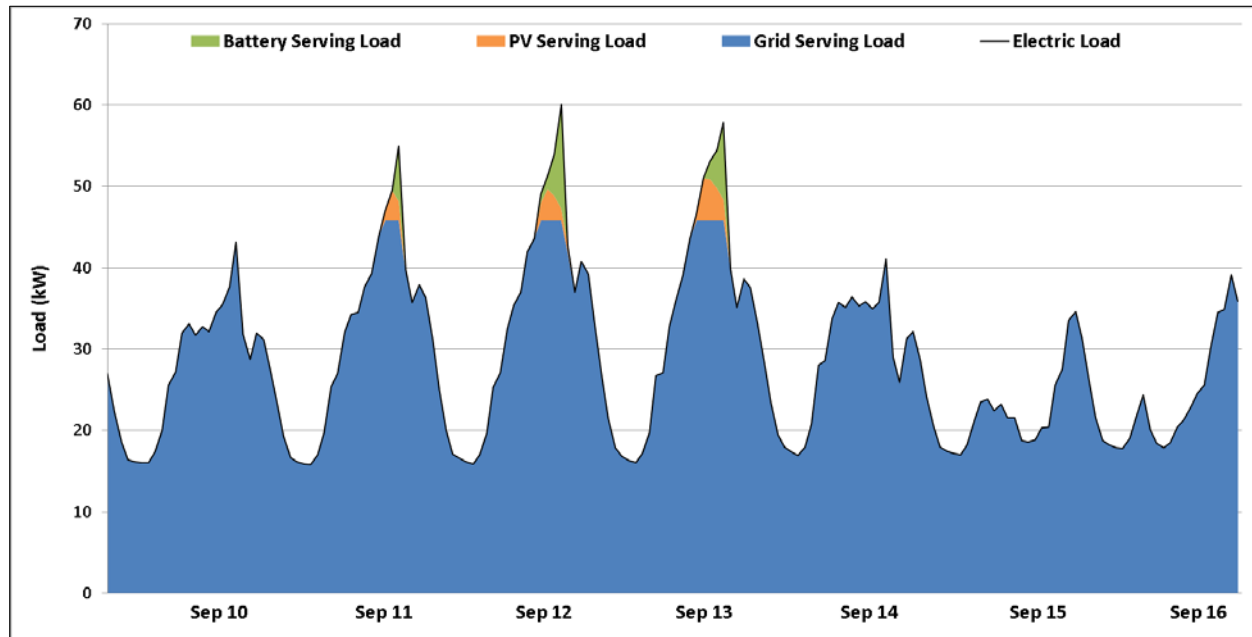


Figure 26. PV and battery combine to reduce peak demand at the fire station

Next, we evaluated the length of time that the PV and battery system could sustain the critical load during a short outage of 2 hours and a long outage of 22 hours. Because the PV and battery in this scenario are relatively small compared to the load, the battery cannot always sustain the full critical load. Systems 1.1 and 1.2 do not have an inverter large enough to support the full critical load in the worst case scenario. However, these systems could support 41% of the critical load for a 2-hour outage under the worst case scenario (low PV and high load), and could support additional loads (beyond just the critical load) under the best case scenario (high PV and low load). The systems could support 2% of the critical load for a 22-hour outage under the worst case scenario and 73% under the best case scenario. System 1.3 could support 77% of the load for a 2 hour outage and 47% for a 22 hour outage under the worst case scenario. Under the best case scenario, additional loads in excess of the critical load can be supported; see Table 19.

Table 19. Percent of Critical Load System Can Support

	System 1.1: No resiliency value captured	System 1.2: Short-duration resiliency value captured	System 1.3: Long-duration resiliency value captured
2-Hour Outage (Worst)	41%	41%	77%
2-Hour Outage (Best)	732%	732%	1181%
22-Hour Outage (Worst)	2.4%	2.4%	47%
22-Hour Outage (Best)	73%	73%	264%

Scenario 2: Resilient PV Sized to meet Resiliency Needs

A high-level summary of system sizing and costs for Scenario 2 are below in Table 20.

Table 20. Fire Station Scenario 2 Results

Fire Station				
Scenario 2: PV + Storage Sized to Meet Resiliency Needs				
	System 2.1A: Short outage; resiliency not valued	System 2.1B: Short outage; resiliency valued	System 2.2A: Long outage; resiliency not valued	System 2.2B: Long outage; resiliency valued
PV Size (kW-DC)	0	10	10	10
Battery Size (kWh)	136	131	613	613
Battery Size (kW)	41	40	40	40
Total Capital Cost	\$111,930	\$138,828	\$389,706	\$389,706
NPV	-\$12,070	\$10,149	-\$256,158	\$93,118
Simple Payback (years)	20.7	16.9	N/A	13.6

Cost-effective PV+storage systems sized to meet resiliency needs were only possible when a resiliency value stream was included. The addition of a resiliency value stream for system 2.1B results in a positive NPV of \$10,000, and allows PV to be incorporated into the solution. Without the resiliency value stream, the system has an NPV of negative \$12,000 (system 2.1A) and no PV. The impact that valuing resiliency can have is seen even more clearly when the systems are required to support a long outage. The NPV of system 2.2A is negative \$256,000, while the NPV of system 2.2B is positive \$93,000.

A large amount of battery capacity is required because the PV system can only supply on average 14% of the daily energy required. Therefore, the battery has to store the remaining 86% of the energy required in advance of the outage. Since solar resources are limited to 10 kW, sustaining a long outage requires a significant increase in battery capacity. Battery sizing for a 2-hour outage requires 131-136 kWh of battery capacity while a 22-hour outage requires 613 kWh of battery capacity, representing an increase of approximately 368%; see Figure 27.

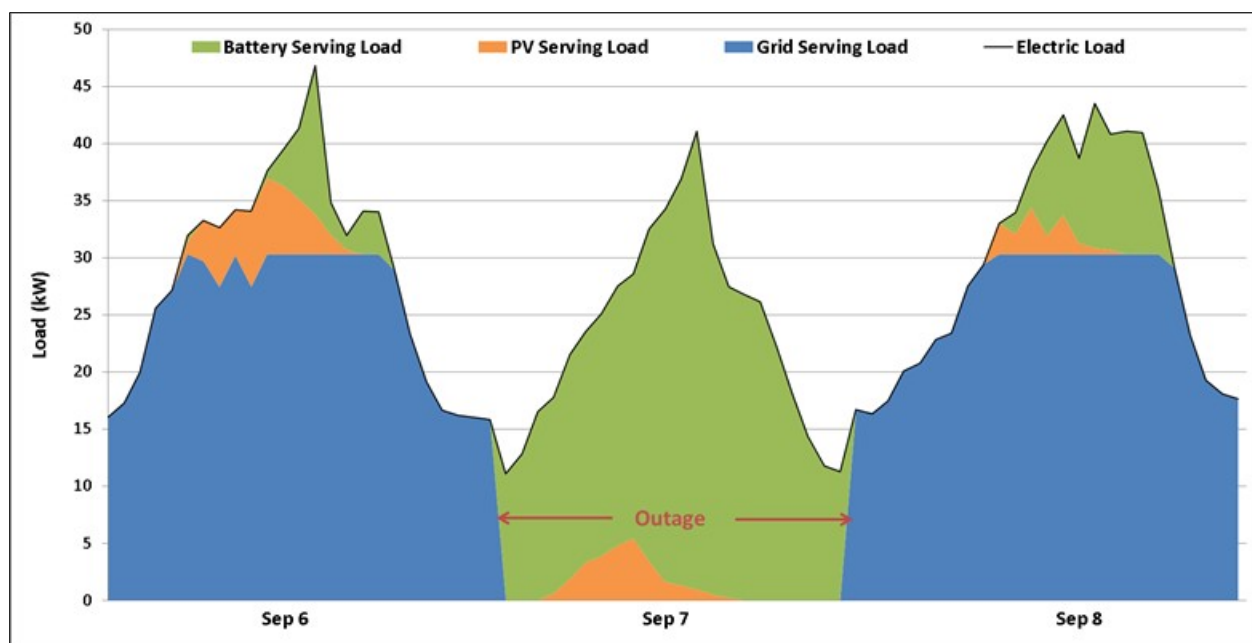


Figure 27. During a 21-hour grid outage on September 7th, the PV (orange) and battery (green) sustain the critical load

Scenario 3: Resilient PV and a Generator (Hybrid System) Sized to meet Resiliency Needs

A high-level summary of system sizing and costs for Scenario 3 are below in Table 21.

Table 21. Fire Station Scenario 3 Results

Fire Station				
Scenario 3: PV + Storage + Generator Sized to Meet Resiliency Needs				
	System 3.1A: Short outage; resiliency not valued	System 3.1B: Short outage; resiliency valued	System 3.2A: Long outage; resiliency not valued	System 3.2B: Long outage; resiliency valued
PV Size (kW-DC)	4	10	1	10
Battery Size (kWh)	73	74	61	66
Battery Size (kW)	18	18	17	20
Diesel Generator Size (kW)	23	22	26	24
Diesel Fuel Used (gallons/yr)	4	4	43	41
Total Capital Cost	\$102,328	\$120,505	\$89,381	\$121,164
NPV	\$0	\$25,384	-\$1,679	\$344,848
Simple Payback (years)	19.3	15.4	19.8	4.7

Adding a resiliency value stream provided savings that were used to offset the cost of adding additional solar to the system, increasing the PV system size from 4 kW to 10 kW and reducing the generator size by 1 kW in system 3.1B. When a resiliency value is included in the long outage scenario (3.2B), the payback period drops significantly over all the other systems in Scenario 3 to 4.7 years. This hybrid system is estimated to cost approximately \$121,000 to install (though there may be additional integration costs, described in Section 2), and would save FDNY approximately \$344,000 over the 25-year life cycle compared to the base case of doing nothing. When resiliency is not valued for a long outage, system 3.2A would cost FDNY under \$2,000 over the 25-year life cycle of the system. Assuming FDNY values resiliency at \$2,000 or more over 25 years, System 3.2A would also be cost-effective. By pairing resilient PV with the generator, the size of generator required to sustain the critical load is reduced from 41 to 24kW (see Figure 28).

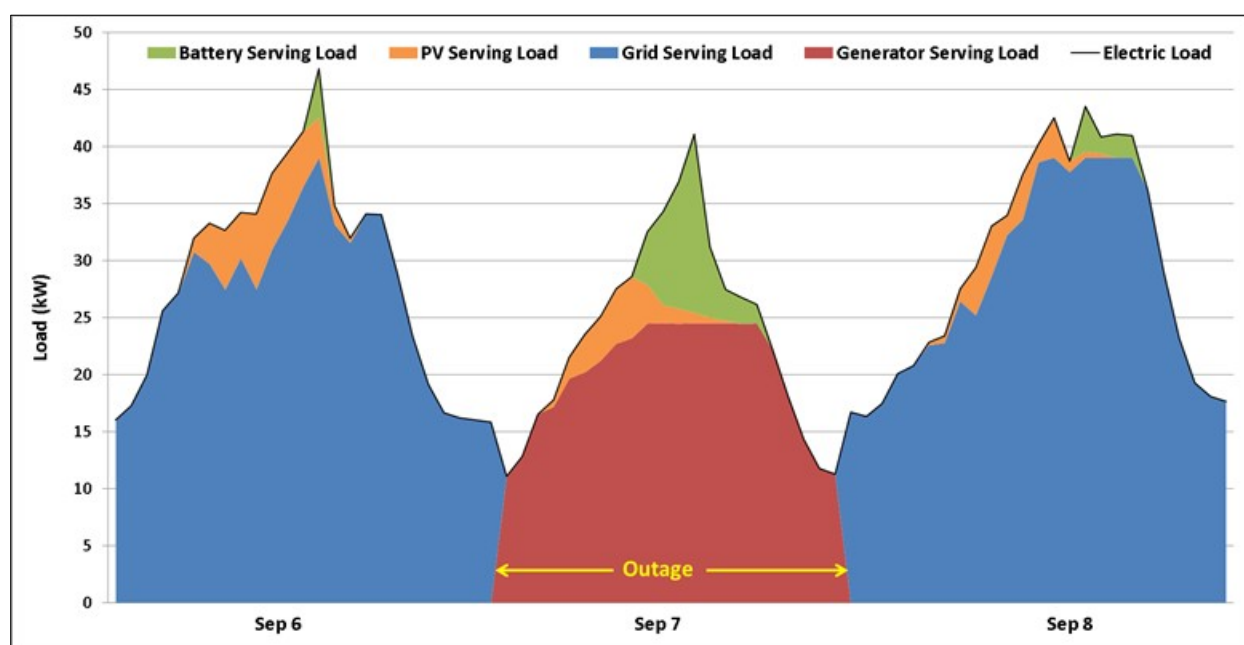


Figure 28. During a 21-hour grid outage on September 7th, the PV (orange) and battery (green) meet peak loads to reduce the size of generator required to sustain the critical load

Scenario 4: Generator Sized to meet Resiliency Needs

For comparison, we also evaluated the cost of a conventional diesel-only backup system. A high-level summary of system sizing and costs for Scenario 4 are below in Table 22.

Table 22. Fire Station Scenario 4 Results

Fire Station				
Scenario 4: Generator Sized to Meet Resiliency Needs				
	System 4.1A: Short outage; resiliency not valued	System 4.1B: Short outage; resiliency valued	System 4.2A: Long outage; resiliency not valued	System 4.2B: Long outage; resiliency valued
Diesel Generator Size (kW)	41	41	41	41
Diesel Fuel Used (gallons/yr)	7	7	47	47
Total Capital Cost	61,620	61,620	61,620	61,620
NPV	-\$51,731	-\$19,964	-\$52,896	\$296,380
Simple Payback (years)	None	None	None	3.0

The size of the generator stays consistent at 41 kW across all 4 systems, but the amount of fuel increases from 7 gallons to 47 gallons when the outage duration is increased from 2 hours to 22 hours. The only system in Scenario 4 that is cost-effective is 4.2B, which includes a resiliency value for a long duration outage.

Discussion of Fire Station Results Across All Scenarios

Table 23 compares the NPV and simple payback for the three scenarios that size systems for resiliency. The highest NPV and quickest payback in each column is highlighted in green, as is the row with the most green cells, to represent the system with the best economics overall. With and without resiliency valued, and for both short and long outages, the hybrid system consistently resulted in the highest NPV and typically, the shortest payback.

Table 23. Fire Station NPV and Payback Comparison of Scenarios 2, 3, and 4

Fire Station				
Most Cost-Effective Option for Outage Coverage				
	Short outage; resiliency not valued	Long outage; resiliency not valued	Short outage; resiliency valued	Long outage; resiliency valued
Scenario 2: PV+Storage NPV	-\$12,070	-\$256,158	\$10,149	\$93,118
Scenario 2: PV+Storage Payback	20.7	N/A	16.9	13.6
Scenario 3: Hybrid NPV	\$0	-\$1,679	\$25,384	\$344,848
Scenario 3: Hybrid Payback	19.3	19.8	15.4	4.7
Scenario 4: Generator NPV	-\$51,713	-\$51,713	-\$19,964	\$296,380
Scenario 4: Generator Payback	N/A	N/A	N/A	3.0

In the hybrid systems, the PV and battery provide demand savings during normal grid-tied operation and also sustain part of the critical load during outages, reducing the size of the generator required. The generator-only scenarios all required a 41-kW generator while the generator sizing for the hybrid systems ranged from 22-26 kW. Compared to the resilient PV systems in Scenario 2, the hybrid systems in Scenario 3 use a significantly reduced battery size (131 – 613 kWh vs. 61 – 74 kWh). Reliance on diesel fuel is reduced only minimally between Scenario 4 and Scenario 3; however, there is no reliance on diesel fuel in Scenario 2.

3.3 NYCHA Cooling Center

Scenario 1: Resilient PV Sized for Economic Savings; no Resiliency Requirement Imposed

A high-level summary of system sizing and costs for Scenario 1 are below in Table 24.

Table 24. Cooling Center Scenario 1 Results

Cooling Center			
Scenario 1: PV + Storage Sized for Economic Savings			
	System 1.1: No resiliency value captured	System 1.2: Short duration resiliency value captured	System 1.3: Long duration resiliency value captured
PV Size (kW-DC)	7	8	8
Battery Size (kWh)	25	25	25
Battery Size (kW)	7	7	7
Total Capital Cost	\$46,286	\$50,120	\$50,538
NPV	\$413	\$1,683	\$1,862
Simple Payback (years)	15.6	14.1	11.1

System 1.1 is a traditional economic analysis that does not include a resiliency value stream. This system would save the cooling center \$413 over 25 years, which presents essentially a breakeven case over the life of the system. When the system is able to capture a resiliency value for a short outage (approximately 7 hours/year in this case), the size of the battery remains the same and the additional revenue is used to offset the costs of a slightly larger 8-kW PV system. NPV increases and payback period is shortened by approximately one year. System 1.3 is able to capture a resiliency value for a long outage (approximately 51 hours/year), which results in a slight increase in battery size (less than 1 kWh) and reduces the payback period by an additional 3 years.

These savings are attained primarily by managing demand during peak periods. This is shown in Figure 29, where the battery is strategically discharged to reduce peaks.

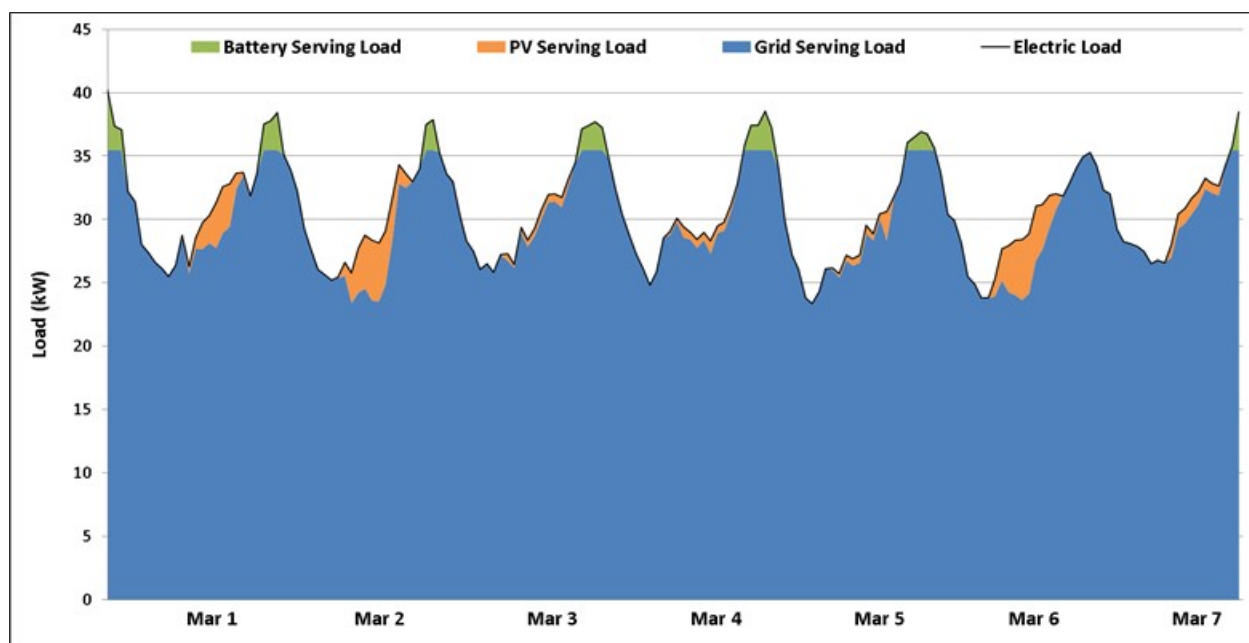


Figure 29. The battery (green) is discharged in the evening to shave the peak demand

Next, we evaluated the length of time that the PV and battery system could sustain the critical load during a short outage of 7 hours and a long outage of 51 hours. Because the PV and battery in this scenario are relatively small compared to the load, the battery cannot always sustain the full critical load. The best case outage scenarios assume that the outage starts in the evening when the air conditioners are off. In this case, the systems can power the lights, computer, fire alarm, and refrigerator through the night. However, they are too small to support the four air conditioners, which each draw 3 kW and together consume 12 kW each hour. The systems could, at most, support two air conditioners for four hours, or one air conditioner for eight hours.

Under the worst case scenario (low PV and high load), these systems do not have an inverter large enough to support the full critical load. However, they could support 31-32% of the critical load for a 7-hour outage. Under the best case scenario (high PV and low load), the systems could support additional load beyond the critical load during a 7-hour outage. During a 51-hour outage, the systems could support 13% of the critical load under the worst case scenario and 20-22% under the best case scenario; see Table 25.

Table 25. Percent of Critical Load System Can Support

	System 1.1: No resiliency value captured	System 1.2: Short-duration resiliency value captured	System 1.3: Long-duration resiliency value captured
7-Hour Outage (Worst)	31%	32%	32%
72-Hour Outage (Best)	2996%	3138%	5138%
51-Hour Outage (Worst)	13%	13%	26%
51-Hour Outage (Best)	20%	22%	22%

Scenario 2: Resilient PV Sized to meet Resiliency Needs

A high-level summary of system sizing and costs for Scenario 2 are below in Table 26.

Table 26. Cooling Center Scenario 2 Results

Cooling Center				
Scenario 2: PV+Storage Sized to Meet Resiliency Needs				
	System 2.1A: Short outage; resiliency not valued	System 2.1B: Short outage; resiliency valued	System 2.2A: Long outage; resiliency not valued	System 2.2B: Long outage; resiliency valued
PV Size (kW-DC)	2	2	9	9
Battery Size (kWh)	104	104	230	230
Battery Size (kW)	12	12	12	12
Total Capital Cost	\$74,907	\$74,907	\$167,006	\$167,006
NPV	-\$45,555	-\$41,516	-\$181,636	-\$153,244
Simple Payback (years)	14.9	14.3	25.5	20.4

None of the systems in Scenario 2 are cost-effective. This site has a relatively high cost of PV and a low value of resiliency. The larger systems required to sustain the longer network outages cannot capture enough savings to cover their higher capital cost.

The battery size remains consistent at 12 kW for all four systems because the peak critical load at this site is 12 kW. Battery capacity varies across the four systems, with much more battery storage required for the long outage. The large battery is required because the PV system can only supply about 36 kWh of the 124 kWh of energy required each day (29%). Therefore, the battery has to provide most of the energy required (see Figure 30).

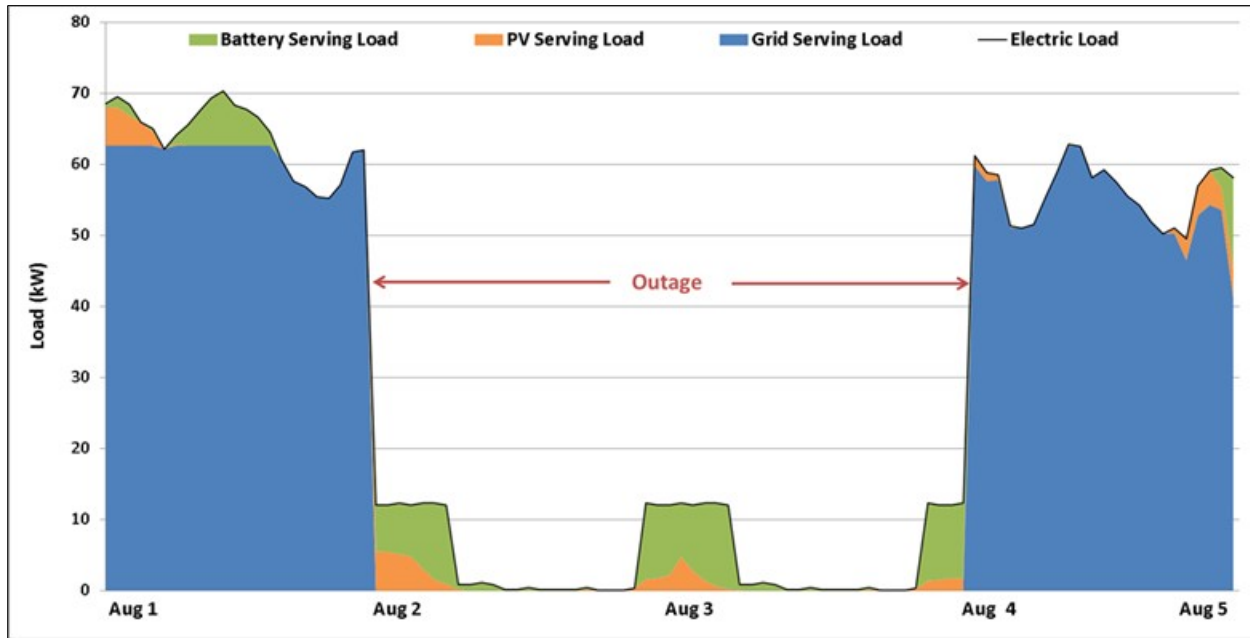


Figure 30. During a 51-hour grid outage in August, PV production is marginal and the battery (green) sustains most of the critical load

Scenario 3: Resilient PV and a Generator (Hybrid System) Sized to meet Resiliency Needs

A high-level summary of system sizing and costs for Scenario 3 are below in Table 27.

Table 27. Cooling Center Scenario 3 Results

Cooling Center				
Scenario 3: PV+Storage+Generator Sized to Meet Resiliency Needs				
	System 3.1A: Short outage; resiliency not valued	System 3.1B: Short outage; resiliency valued	System 3.2A: Long outage; resiliency not valued	System 3.2B: Long outage; resiliency valued
PV Size (kW-DC)	0	2	0	9
Battery Size (kWh)	25	28	25	35
Battery Size (kW)	7	7	7	8
Diesel Generator Size (kW)	9	9	10	7
Diesel Fuel Used (gallons/yr)	8	7	41	30
Total Capital Cost	\$33,798	\$42,261	\$34,376	\$70,893
NPV	\$430	\$0	\$1,008	\$9,329
Simple Payback (years)	11.4	12.2	11.3	12.3

All of the systems in scenario 3 were cost-effective. Solar is only cost-effective when a resiliency value is included. Adding in a resiliency value stream allows for the addition of a small PV system in System 3.1B and a larger PV system in 3.2B. It also increases the NPV by \$8,000 for a long outage.

The PV and battery are synergistic, and adding a larger PV system results in a larger battery. Adding solar in System 3.2.B reduces diesel fuel use by 25% during the long duration outage, compared to the battery-generator system in System 3.2.A.

The battery provides demand savings during normal grid-tied operation and also sustains part of the critical load during the outage to reduce the size of diesel generator required and reduce run-time of the diesel generator; see Figure 31. In summary, the hybrid scenario consistently outperforms scenario 2 and 4 in economics, while achieving the desired resiliency for both short and long duration.

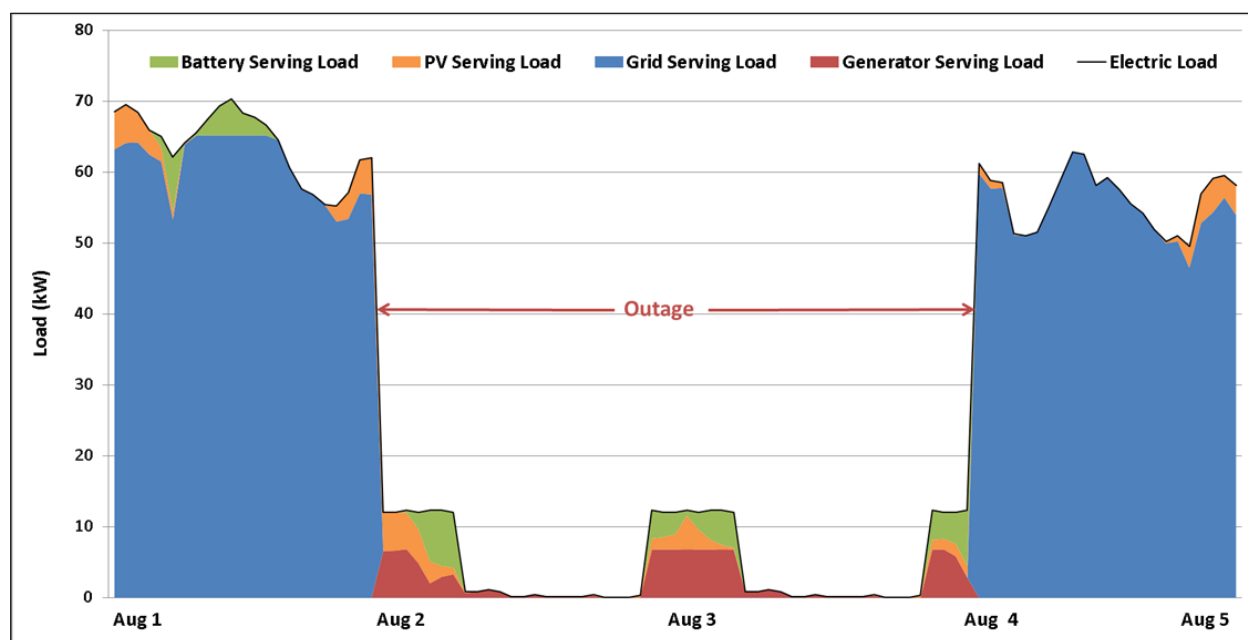


Figure 31. During the 51-hour outage in August, the PV and battery reduce the size of diesel generator required to meet the critical load, as well as reducing run-time of the diesel generator

Scenario 4: Generator Sized to meet Resiliency Needs

A high-level summary of system sizing and costs for Scenario 4 are below in Table 28.

Table 28. Cooling Center Scenario 4 Results

Cooling Center				
Scenario 4: Generator Sized to Meet Resiliency Needs				
	System 4.1A: Short outage; resiliency not valued	System 4.1B: Short outage; resiliency valued	System 4.2A: Long outage; resiliency not valued	System 4.2B: Long outage; resiliency valued
Diesel Generator Size (kW)	12	12	12	12
Diesel Fuel Used (gallons/yr)	9	9	48	48
Total Capital Cost	\$18,600	\$18,600	\$18,600	\$18,600
NPV	-\$25,411	-\$21,372	-\$24,246	\$2,562
Simple Payback (years)	None	None	None	11.0

For comparison, we also evaluated the cost of a conventional diesel-only backup system. A diesel generator is only cost-effective in Scenario 4 for a long outage when resiliency is valued. The NPV of \$2600 is relatively low and the payback period is 11 years.

The size of the generator remains consistent across all four systems at 12 kW, so the capital cost is the same for all four systems as well. When resiliency is not valued, the cost of a system that supports a short and long outage is equivalent, but the amount of fuel required increases from 9 to 48 gallons.

Discussion of Cooling Center Results Across All Scenarios

To compare cost-effectiveness across the systems designed primarily to support resiliency needs (Scenarios 2, 3, and 4), the NPV and payback periods are listed in Table 29. The cells highlighted in green represent the best NPV and best payback period for each column. Scenario 3 again presents the best economic system option to cover both short and long outages.

Table 29. Cooling Center NPV and Payback Comparison of Scenarios 2, 3, and 4

Cooling Center				
Most Cost-Effective Option for Outage Coverage				
	Short outage; resiliency not valued	Long outage; resiliency not valued	Short outage; resiliency valued	Long outage; resiliency valued
Scenario 2: PV+Storage NPV	-\$45,555	-\$181,636	-\$41,516	-\$153,244
Scenario 2: PV+Storage Payback	14.9	25.5	14.3	20.4
Scenario 3: Hybrid NPV	\$430	-\$1,008	\$0	\$9,329
Scenario 3: Hybrid Payback	11.4	11.3	12.2	12.3
Scenario 4: Generator NPV	-\$25,411	-\$24,246	-\$21,372	\$2,562
Scenario 4: Generator Payback	N/A	N/A	N/A	11.0

Recommendations

Currently, there is no established resiliency value stream; therefore, it is up to the individual facility and its larger agency to determine how resiliency is valued. The level at which resiliency is valued will influence the type of emergency power system that the facility should implement. Whether or not these three facilities assign an economic value to resiliency, if they want to deploy an emergency power system, a hybrid system (Scenario 3) is recommended. If emergency power is viewed as a secondary benefit to the economic benefits that a resilient PV system can provide, a Scenario 1 system is recommended. Scenario 1 systems will allow the host site to see a return on its investment while receiving some degree of emergency power in the event of an outage, depending on when the outage occurs.

4 Conclusion

This analysis modeled resilient PV systems designed for economic savings and examined the amount of emergency power these systems are capable of providing. The analysis also modeled resilient PV and hybrid systems designed to support emergency power needs, which could then be used for economic savings during normal grid operations. Finally, the analysis looked at generator-only systems designed to support emergency power needs in order to compare this traditional resiliency solution with resilient PV and hybrid solutions. The results for these sites indicate that:

- Resilient PV and hybrid systems can be NPV-positive with and without a resiliency value stream included.
- For NYPA customers, the economics of resilient PV are better than standalone solar PV, primarily due to the battery's ability to reduce utility demand charges.
- Project economics for all modeled systems are greatly improved for radial customers when a resiliency value stream is included due to higher frequency of outages that occur on radial systems vs. network grids.
- Project economics for all modeled systems are moderately improved for network customers when a resiliency value stream is included.
- Resilient PV sized for cost savings (i.e., not for resiliency) will provide limited resiliency benefits.
- The level of resiliency provided by resilient PV systems sized for utility cost savings depends on when the outage occurs, state of charge of the battery, and load size.
- Resilient PV and hybrid systems designed to support short long outages result in systems that are larger and more costly than systems sized for cost savings.
- In some cases, inclusion of a value for avoiding utility power outages can more than offset the additional costs incurred by sizing resilient PV for resiliency rather than utility cost savings alone.
- Generators as a resiliency solution are not NPV-positive except when resiliency is valued for long outages.
- Though generators are the most widely used form of emergency and stand-by power, solar-plus-storage and hybrid systems can offer the same benefits at a better lifecycle cost. However, generators have a lower initial cost.

Scenario 1 results show that a modestly sized battery system can be strategically charged and discharged such that it shaves the peak loads and, therefore, captures significant demand savings. Since the capacity of these batteries is small, they can generally only support the critical load for a few hours, much less than the five-day outage period desired by many of the onsite staff interviewed for this project. Similarly, small roof space at two of the sites offered nominal energy savings during grid operations, and extended the duration of outage that could be served by a battery by a few hours. When resiliency isn't prioritized or valued, a Scenario 1 system can support emission reduction targets and lower electricity costs.

The results from the second scenario show that it would take a battery of considerable size and increased solar resources to sustain the critical load for an extended outage. Inclusion of a resiliency value stream can make resilient PV economically viable, but without it, the increased system size can push the NPV negative. The results from the third scenario indicate that a hybrid system is generally the more economical system configuration for sustaining outages. The battery and PV reduce the size of the diesel generator required, and the diesel generator provides the extra energy and power required during long outage periods. The savings the battery and PV provide during normal grid-connected operation make the hybrid system more economical than a diesel generator alone, as seen in the fourth scenario. However, hybrid systems are a more complex solution with a higher first cost compared to a stand-alone diesel generator.

The size of resilient PV systems that these three sites—and other critical infrastructure sites in NYC—should deploy will depend on the priorities of the site and the degree to which resiliency is or is not valued. For city-owned buildings, solar deployment for emissions reductions is a priority. Knowing that 100 MW of solar will be installed on city buildings, it is worth noting that this analysis finds adding storage can improve project economics for NYPA customers by reducing demand charges. The incorporation of storage into NYC’s solar deployment goals will add resiliency benefits that standalone solar can not otherwise provide. Adding storage to city solar deployments could also be an opportunity to align the city’s sustainability and resiliency goals.

For critical infrastructure, interest in resilient PV may be driven by resiliency benefits rather than emissions reductions. Following Hurricane Sandy, the Mayor’s generator and boiler task force deemed restoring power to NYCHA’s 80,000 affected residents was the next-highest priority after meeting immediate life safety needs. Rather than relying solely on generators to supply emergency power needs, hybrid systems can offer NYCHA (and other sites) an option that is more cost-effective and reduces reliance on a single technology. Regulatory changes may be necessary in order to permit resilient PV as a code-compliant option for emergency power, similar to how Local Law 111 removed barriers to the use of natural gas generators for emergency power.⁵³ In addition to resiliency, cost savings are a priority across critical infrastructure. Unlike commercial buildings that generally require quick payback, public facilities may invest in solutions that offer long-term savings when upfront capital or third-party financing is available.

For commercial buildings on Con Edison’s SC 9 tariff, demand charges range from \$26 - \$31/kW, which is slightly lower than the demand charges for the NYPA customers modeled in this analysis (13% - 50% lower depending on the site and season). However, energy rates for SC 9 customers average around \$0.085/kWh while NYPA customers average around half that at \$0.044/kWh. If the sites used in this study were analyzed on Con Edison rates, it is expected that the resulting recommended systems would have smaller battery systems, and larger PV systems. The facilities that are space-constrained would likely see all available space used for solar, and smaller storage systems. Improved project economics for a Con Edison customer would be more likely at a location with ample roof space for solar.

⁵³ Building Resiliency Task Force, 2016. “Remove Barriers to Backup & Natural Gas Generators.” Urban Green Council. <http://urbangreencouncil.org/content/remove-barriers-backup-natural-gas-generators>.

Overall, results of this analysis show that pairing these systems with storage (and generators when resiliency is a priority) may be economical depending on payback requirements, site suitability, and other factors. As a next step, obtaining more granular cost assumption data on resilient PV projects would help fill in any gaps on integration, critical load isolation, and other additional costs. Improved cost assumptions would yield more accurate estimates to inform investment decisions, but these are difficult to obtain in a young market. However, as the solar and storage markets mature and prices decline, and as utilities adopt rates that are more advantageous to distributed generation⁵⁴, project economics will also improve for both NYPA and Con Edison customers. The question of how resiliency is valued for critical infrastructure also needs to be answered in order to truly understand the economics of emergency power investments.

In order to start a conversation about the value of resiliency, this analysis presents a potential resiliency value in order to compare results to systems that do not value resiliency. These values do not capture the full complexity of valuing resiliency. For example, power outages have real costs which are often borne by federal agencies that are less involved in local resiliency investments. The Federal Emergency Management Agency (FEMA) typically covers 75% or more of recovery costs when a local event is declared a national disaster. How to value resiliency will require local, state, and national conversations with the public, government agencies, and private companies that bear the brunt of outage costs.

⁵⁴ This is expected under New York State's [Reforming the Energy Vision](#).

Appendix A. Critical Load Calculations

Table A-1. NYCHA Cooling Center Daily Critical Load During the Summer

Equipment	Quantity	Power (W)	Total (W)	Day hours (7:00-5:00)	Evening (6:00-10:00)	Night (11:00-6:00)	Total (kWh/day)
Air conditioner	4	3000	12000	8			96
Desktop computer	1	230	230	2	1		0.69
Tube-Fluorescents (T-8)	10	32	320		4		1.28
CFL	3	16	48			8	0.38
Refrigerator	1	300	300	2	2	1	1.50
Total				97.11	2.11	0.68	99.85

Table A-2. NYC-DOE School Shelter Daily Critical Load During the Summer and Winter

Room Equipment	Total (W)	Summer				Winter			
		Hours used per day				Hours used per day			
		Day (7am-5pm)	Evening (6pm-10pm)	Night (10pm-6am)	Total kWh/day	Day (7am-5pm)	Evening (6pm-10pm)	Night (10pm-6am)	Total kWh/day
Window AC units	6000	9	3	0	72	0	0	0	0
Desktop computer	460	4	0	0	2	4	0	0	2
LED lamps	2016	10	4	0	28	10	4	0	28
Tube-Fluorescents (T-8)	4544	10	4	0	64	10	4	0	64
Electrical outlets	48	10	4	0	1	10	4	0	1
Boiler Room Equipment									
Fuel oil pump	1167	4	4		9	10	4	8	26
Vacuum pump	2691	4	4		22	10	4	8	59
Feed water pump	2725	4	4		22	10	4	8	60
Condensate pump	4248	4	4		34	10	4	8	93
Sewage ejector pump	2691	1			3	1			3
air compressors	4021	2			8	2			8
Sump pump	2043	3	2	3	16	3	2	3	16
Freezer (Walk-in)	3664	8	4	4	59	8	4	4	59
Refrigerator (Walk-in)	2774	2	1	2	14	2	1	2	14
Totals					352.57				432.20

Appendix B. Resiliency Calculations

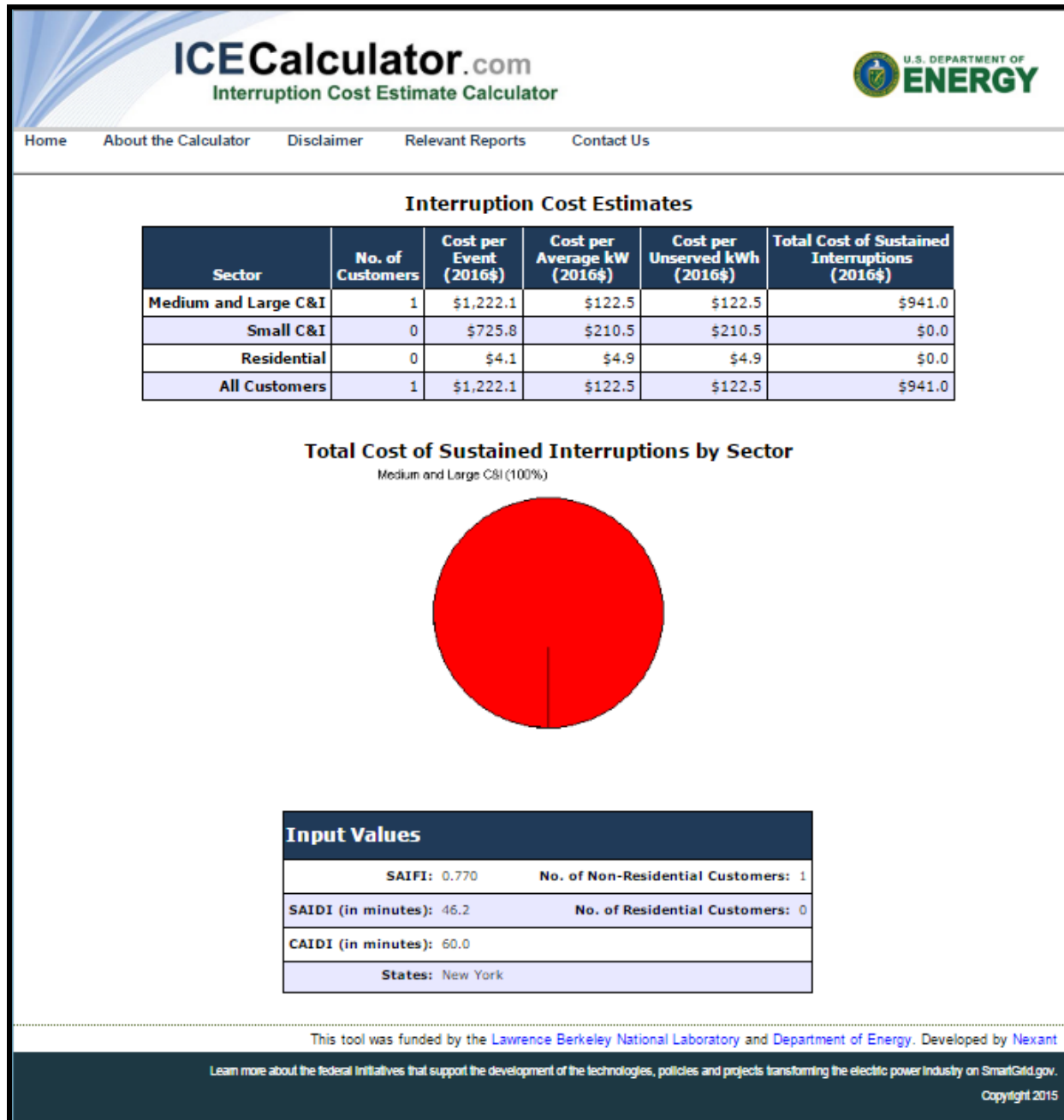


Figure B-1. Outputs from the ICE Calculator for the Fire Station

**Table B-1. Outputs from the ICE Calculator for 1-16 Hour Outages
(in 60-Minute Increments) for the Fire Station**

Fire Station Outage Cost Curve (radial customer)			
CAIDI		Cost	Unit Cost
Hours	Minutes	Interruption Cost	Cost of Interruption
1	60	\$ 941	\$ 941.00
2	120	\$ 1,447	\$ 723.70
3	180	\$ 2,110	\$ 703.30
4	240	\$ 2,935	\$ 733.70
5	300	\$ 3,918	\$ 783.64
6	360	\$ 5,044	\$ 840.70
7	420	\$ 6,287	\$ 898.09
8	480	\$ 7,608	\$ 951.04
9	540	\$ 8,963	\$ 995.89
10	600	\$ 10,298	\$ 1,029.77
11	660	\$ 11,554	\$ 1,050.38
12	720	\$ 12,674	\$ 1,056.17
13	780	\$ 13,601	\$ 1,046.24
14	840	\$ 14,287	\$ 1,020.52
15	900	\$ 14,695	\$ 979.67
16	960	\$ 14,801	\$ 925.06
Average			\$ 917.43

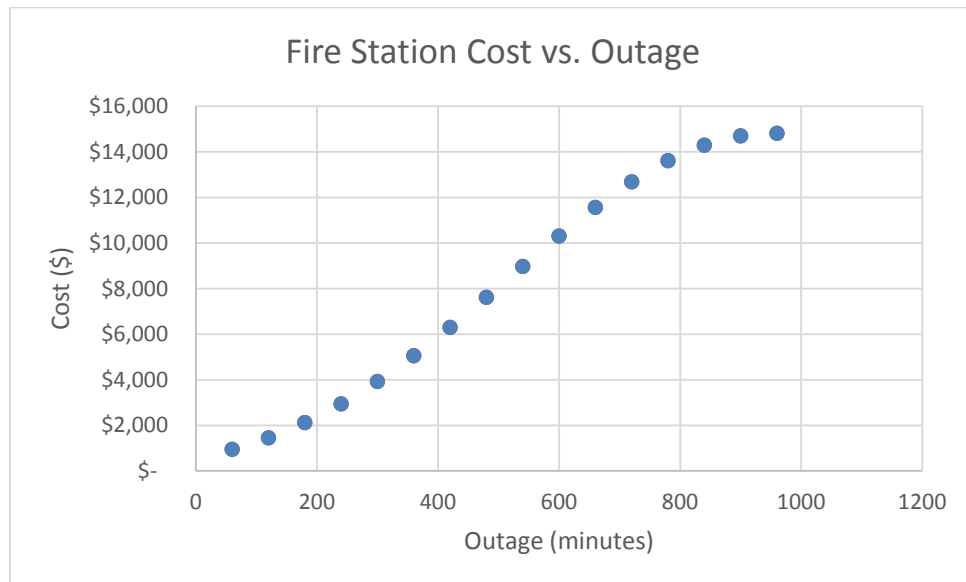


Figure B-2. Cost vs. Outage Length from the ICE Calculator for the Fire Station

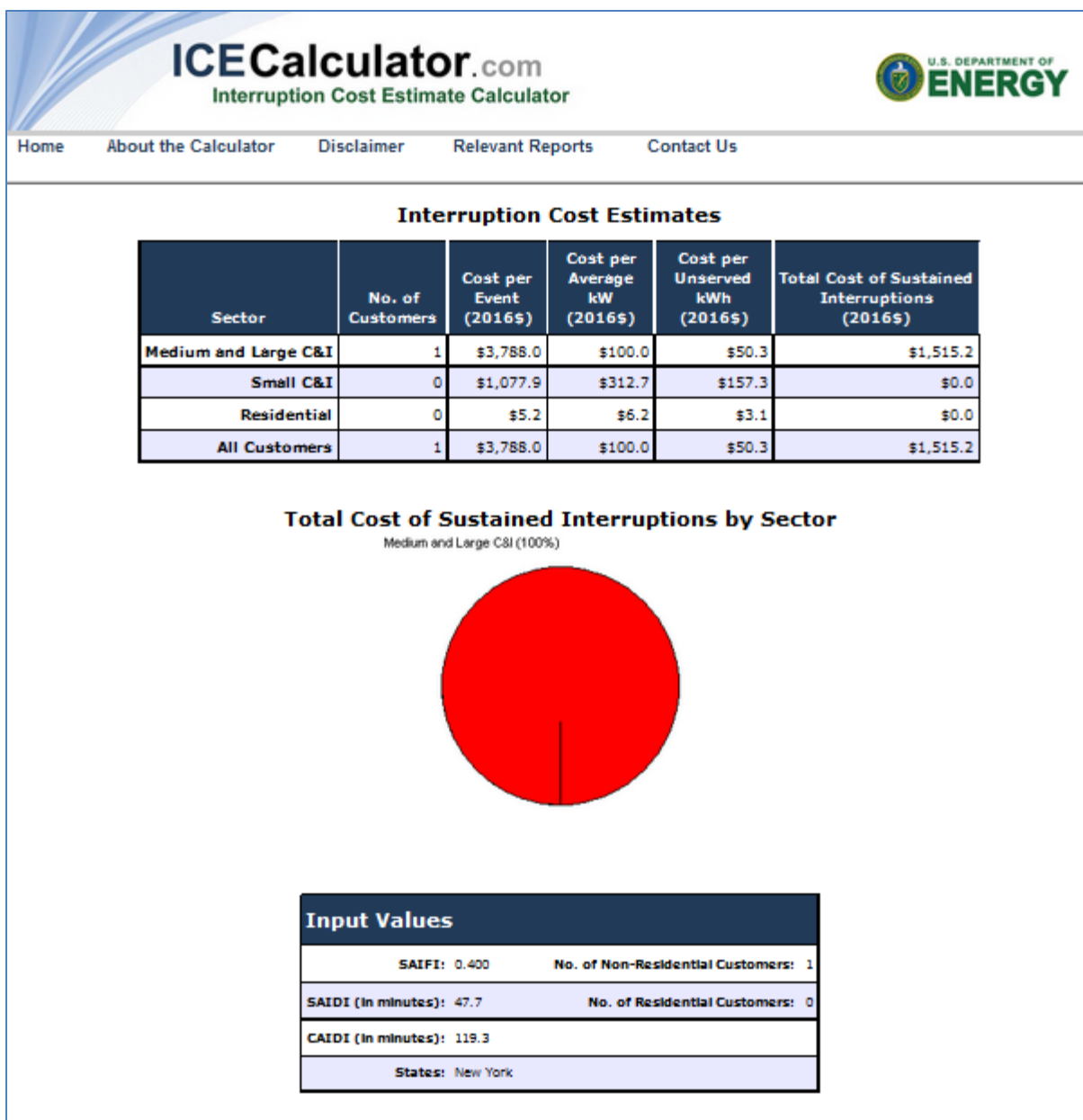


Figure B-3. Outputs from the ICE Calculator for the NYCHA Cooling Center

**Table B-2. Outputs from the ICE Calculator for 1-16 Hour Outages
(in 60-Minute Increments) for the Cooling Center**

NYCHA Cooling Center Outage Cost Curve (network customer)			
CAIDI		Cost	Unit Cost
Hours	Minutes	Interruption Cost	Cost of Interruption
1	60	\$30	\$ 29.70
2	120	\$47	\$ 23.60
3	180	\$71	\$ 23.53
4	240	\$100	\$ 25.03
5	300	\$136	\$ 27.12
6	360	\$177	\$ 29.43
7	420	\$222	\$ 31.69
8	480	\$270	\$ 33.75
9	540	\$319	\$ 35.48
10	600	\$368	\$ 36.76
11	660	\$413	\$ 37.53
12	720	\$453	\$ 37.73
13	780	\$485	\$ 37.32
14	840	\$508	\$ 36.31
15	900	\$521	\$ 34.74
16	960	\$523	\$ 32.67
Average			\$32.02

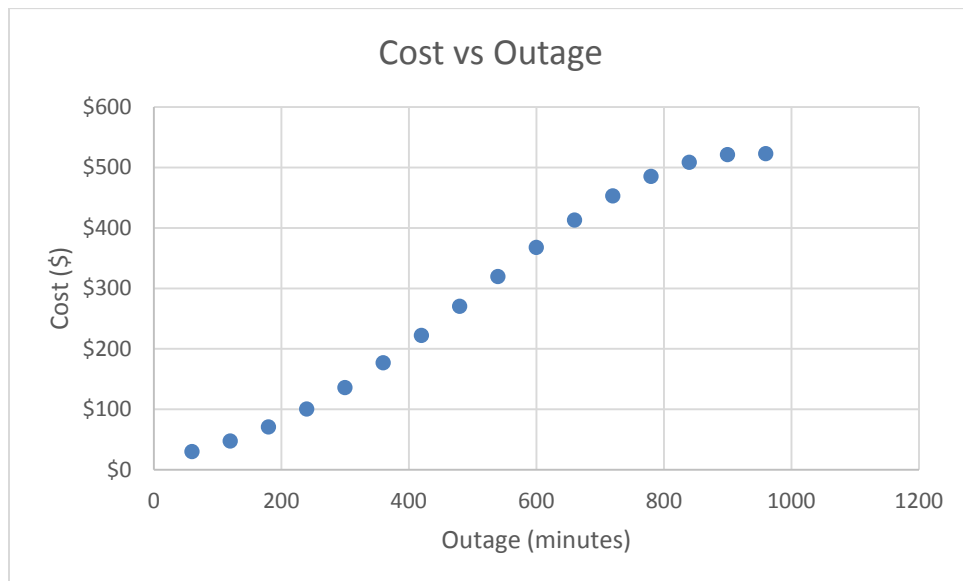


Figure B-4. Cost vs. Outage Length from the ICE Calculator for the Cooling Center

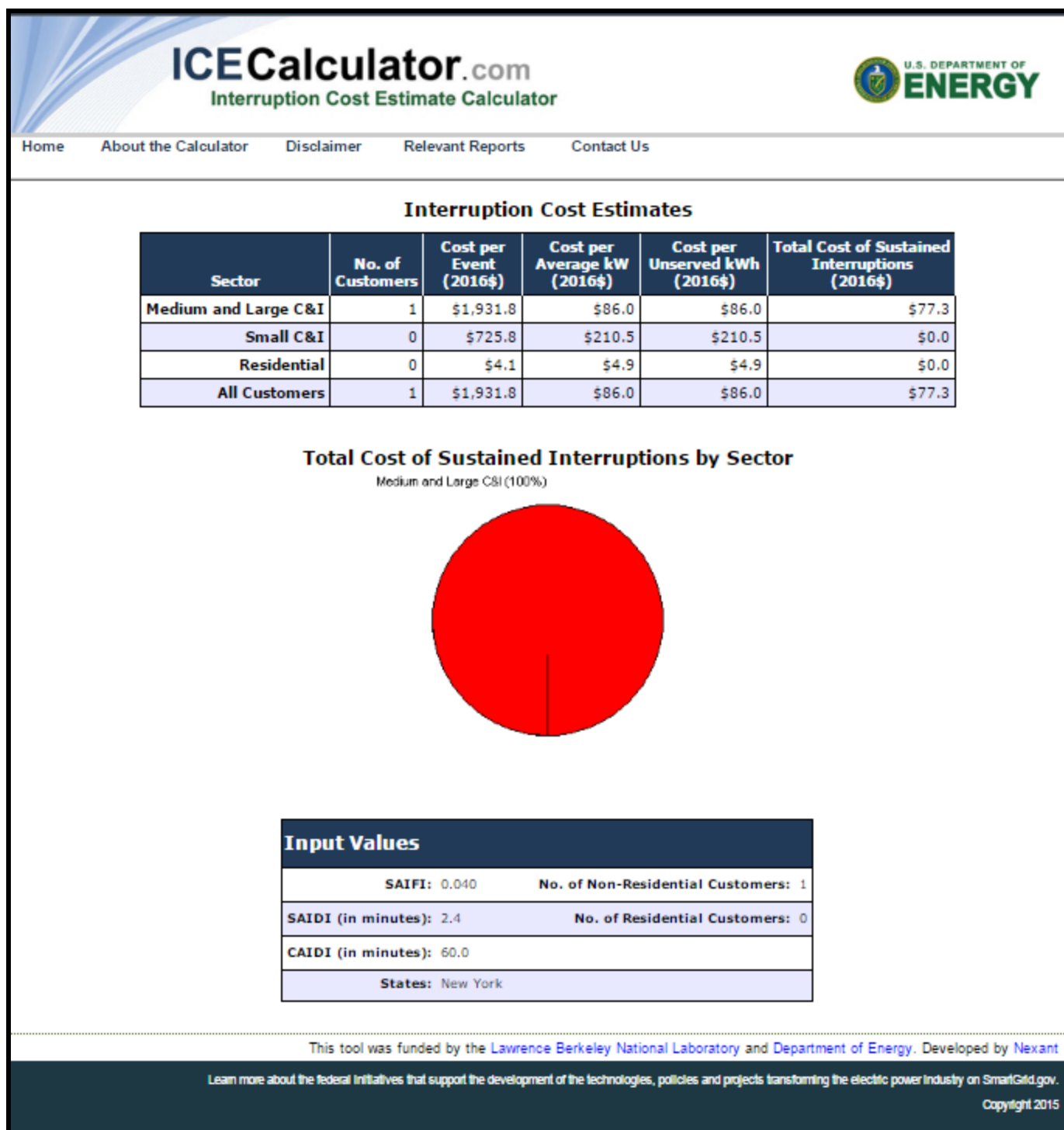


Figure B-5. Outputs from the ICE Calculator for the School Shelter

Table B-3. Outputs from the ICE Calculator for 1-16 Hour Outages (in 60-Minute Increments) for the School Shelter

School Shelter Outage Cost Curve (network customer)			
CAIDI		Cost	Unit Cost
Hours	Minutes	Interruption Cost	Cost of Interruption
1	60	\$ 77	\$ 77.30
2	120	\$ 116	\$ 57.75
3	180	\$ 165	\$ 54.90
4	240	\$ 225	\$ 56.30
5	300	\$ 297	\$ 59.34
6	360	\$ 378	\$ 63.02
7	420	\$ 468	\$ 66.83
8	480	\$ 563	\$ 70.39
9	540	\$ 661	\$ 73.44
10	600	\$ 758	\$ 75.78
11	660	\$ 850	\$ 77.23
12	720	\$ 932	\$ 77.68
13	780	\$ 1,002	\$ 77.04
14	840	\$ 1,054	\$ 75.31
15	900	\$ 1,088	\$ 72.52
16	960	\$ 1,100	\$ 68.74
Average			\$ 68.97

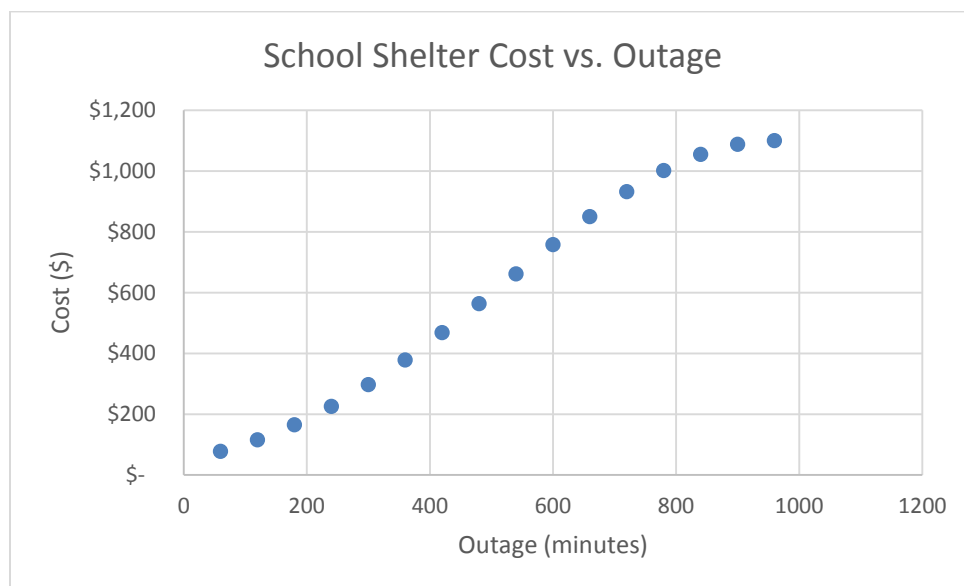


Figure B-6. Cost vs. Outage Length from the ICE Calculator for the School Shelter

Appendix C. Utility Rate Tariffs

New York Power Authority
First Revised Service Tariff No. 100

NYC
Eighth Revised Leaf No. 16
Superseding Seventh Revised Leaf No. 16

Service Classification No. 68
Multiple Dwellings - Redistribution

Applicability:

- To use of service for light, heat and power for multiple dwellings where the Account's requirements are in excess of 10 kW.

CONVENTIONAL

		PRODUCTION	DELIVERY	
Demand (\$/kW)		15.83	Low Tension 22.69	High Tension 20.43
Energy (¢/kWh)	Summer	4.589		
	Winter	4.081		
Reactive Power (\$/kVar)		Billable reactive power demand	1.41	
		Induction-generation exception	1.41	

TOD

		PRODUCTION		DELIVERY	
Demand (\$/kW)	Summer	17.29		Low Tension 44.70	High Tension 24.74
	Winter	17.29		16.87	10.56
Energy (¢/kWh)	Summer	On Peak 5.884	Off Peak 3.696		
	Winter	4.787	3.634		
Reactive Power (\$/kVar)		Billable reactive power demand		1.41	
		Induction-generation exception		1.41	

Time Period Conventional:

- All hours, all days

Time Period TOD:

- Demand Charge:

On-Peak: 8:00 a.m. to 6:00 p.m. weekdays (including holidays)

Off-Peak: All other times

- Energy Charge:

On-Peak: 8:00 a.m. to 10 p.m. weekdays (including holidays)

Off-Peak: All other times

(SC 68 – Continued on Leaf No. 17)

Date of Issue: March 26, 2015

Date Effective: March 2015 Bill Period

Modified to be consistent with Con Edison PSC No. 12, Case 13-E-0030

Issued by James F. Pasquale, Senior Vice President
Power Authority of the State of New York
30 South Pearl Street, Albany, NY 12207

Figure C-1. Service Classification No. 68

Service Classification No. 91

New York City Public Buildings

Applicability:

- To use of service for light, heat and power for the City of New York's public buildings, offices and structures, or parts thereof, used by the City of New York for public purposes.

CONVENTIONAL

PRODUCTION		DELIVERY	
Demand (\$/kW)		Low Tension	High Tension
	9.94	22.69	20.43
Energy (¢/kWh)			
Summer	4.844		
Winter	4.335		
Reactive Power (\$/kVar)			
Billable reactive power demand		1.41	
Induction-generation exception		1.41	

TOD

PRODUCTION		DELIVERY	
Demand (\$/kW)		Low Tension	High Tension
Summer	13.98	44.70	24.74
Winter	13.98	16.87	10.56
Energy (¢/kWh)			
Summer	On Peak: 5.940 Off Peak: 3.752		
Winter	4.843 3.690		
Reactive Power (\$/kVar)			
Billable reactive power demand		1.41	
Induction-generation exception		1.41	

UNMETERED FIRE ALARM AND SIGNAL SYSTEMS

- For the operation of interior fire alarm or signal systems not connected to the metered supply for the building and where separate service is supplied

For service connection	(\$ per month)	119.79
For each gong or signal circuit or combination of gong or signal circuits, in which there is a continuous flow of current of not over 125 milliamperes, the voltage of the supply being approximately 120 volts or the equivalent (taken as 15 volt-amperes) at other supply voltages	(\$ per month)	8.23
For each additional 125 milliamperes (or equivalent) of continuous flow, or traction thereof, an additional charge of	(\$ per month)	8.23

(SC 91 – Continued on Leaf No. 28)

Date of Issue: March 26, 2015

Date Effective: March 2015 Bill Period

Modified to be consistent with Con Edison PSC No. 12, Case 13-E-0030

Issued by James F. Pasquale, Senior Vice President
Power Authority of the State of New York
30 South Pearl Street, Albany, NY 12207

Figure C-2. Service Classification No. 91

Appendix D. Additional Results

NYC-DOE

Table D-1. School Shelter Baseline: No Resilient PV

Scenario Number	0.1	0.2	0.3
Description	Without cost of grid interruptions	With cost of 2 hours/year grid interruptions	With cost of 22 hours/year grid interruptions
Outage START (hour of year)	-	-	-
Outage STOP (hour of year)	-	-	-
Resiliency Value (\$/hour)	0	68.97, 7.25 hours	68.97, 50.96 hours
Outage Duration (hours)	0	0	0
PV Size (kW-DC)	0	0	0
Battery Size (kWh)	0	0	0
Battery Size (kW)	0	0	0
Diesel Generator Size (kW)	0	0	0
PV Cost (\$)	0	0	0
PV Cost Less NY Sun incentive (\$)	0	0	0
Battery Cost (\$)	0	0	0
Generator Cost (\$)	0	0	0
Total Capital Cost (\$)	0	0	0
Year 1 Electric Cost (\$)	69,920	69,920	69,920
Year 1 Demand Cost (\$)	191,751	191,751	191,751
Year 1 Electric Savings (\$)	0	0	0
Year 1 Demand Savings (\$)	0	0	0
Annual Resiliency Savings (\$)	0	0	0
LCC (\$)	5,385,190	5,393,890	5,446,340
NPV (\$)	0	0	0
SPP (years)	0	0	0
Diesel Fuel Used (gallons)	0	0	0
Incentive Required to get to NPV=0 (%)	0	0	0

Table D-2. School Shelter Scenario 1: Resilient PV Sized for Economic Savings

Scenario Number	1.1	1.2	1.3
Description	No resiliency value	2 hour resiliency value	22 hour resiliency value
Outage START (hour of year)	-	-	-
Outage STOP (hour of year)	-	-	-
Resiliency Value (\$/hour)	0	68.97, 7.25 hours	68.97, 7.25 hours
Outage Duration (hours)	0	0	0
PV Size (kW-DC)	50	50	50
Battery Size (kWh)	73.76	73.76	73.76
Battery Size (kW)	34.86	34.86	34.86
Diesel Generator Size (kW)	0	0	0
PV Cost (\$)	172,500	172,500	172,500
PV Cost Less NY Sun incentive (\$)	132,500	132,500	132,500
Battery Cost (\$)	73,216	73,216	73,216
Generator Cost (\$)	0	0	0
Total Capital Cost (\$)	205,716	205,716	205,716
Year 1 Electric Cost (\$)	69,652	69,652	69,652
Year 1 Demand Cost (\$)	177,620	177,620	177,620
Year 1 Electric Savings (\$)	268	268	268
Year 1 Demand Savings (\$)	14,131	14,131	14,131
Annual Resiliency Savings (\$)	-	413	413
LCC (\$)	5,333,630	5,335,240	5,335,240
NPV (\$)	51,560	58,650	58,650
SPP (years)	14.29	13.89	13.89
Diesel Fuel Used (gallons)	0	0	0
Incentive Required to get to NPV=0 (%)	0	0	0
Size of Critical Load that Can Be Supported for Full Length of Outage (%)			
7 Hour Outage- Worst	46%	46%	46%
7 Hour Outage- Best	285%	285%	285%
51 Hour Outage- Worst	12%	12%	12%
51 Hour Outage- Best	50%	50%	50%

Table D-3. School Shelter Scenario 2: Resilient PV Sized to Meet Resiliency Needs

Scenario Number	2.1.a	2.1.b	2.2.a	2.2.b
Description	2 hour outage, no resiliency value	2 hour outage, with resiliency value	22 hour outage, no resiliency value	22 hour outage, with resiliency value
Outage START (hour of year)	8584	8584	8394	8394
Outage STOP (hour of year)	8590	8590	8444	8444
Resiliency Value (\$/hour)	0	68.97	0	68.97
Outage Duration (hours)	7.25	7.25	50.96	50.96
PV Size (kW-DC)	50	50	200	200
Battery Size (kWh)	202.71	202.71	984.93	984.93
Battery Size (kW)	68.38	68.38	157.60	157.60
Diesel Generator Size (kW)	0	0	0	0
PV Cost (\$)	172,500	172,500	690,000	690,000
PV Cost Less NY Sun incentive (\$)	132,500	132,500	575,000	575,000
Battery Cost (\$)	173,782	173,782	669,758	669,758
Generator Cost (\$)	-	-	-	-
Total Capital Cost (\$)	306,282	306,282	1,244,758	1,244,758
Year 1 Electric Cost (\$)	67,235	67,235	64,644	64,644
Year 1 Demand Cost (\$)	168,837	168,837	129,225	129,225
Year 1 Electric Savings (\$)	2,685	2,685	5,276	5,276
Year 1 Demand Savings (\$)	22,914	22,914	62,526	62,526
Annual Resiliency Savings (\$)	0	500	0	3,515
LCC (\$)	5,363,320	5,363,320	5,908,670	5,908,670
NPV (\$)	21,870	30,570	(523,480)	(462,330)
SPP (years)	11.96	11.74	18.36	17.45
Diesel Fuel Used (gallons)	0	0	0	0
Incentive Required to get to NPV=0 (%)	0	0	42%	37%

**Table D-4. School Shelter Scenario 3: Resilient PV and Generator
(Hybrid System) Sized to Meet Resiliency Needs**

Scenario Number	3.1.a	3.1.b	3.2.a	3.2.b
Description	2 hour outage, no resiliency value	2 hour outage, with resiliency value	22 hour outage, no resiliency value	22 hour outage, with resiliency value
Outage START (hour of year)	8584	8584	8394	8394
Outage STOP (hour of year)	8590	8590	8444	8444
Resiliency Value (\$/hour)	0	68.97	0	68.97
Outage Duration (hours)	7.25	7.25	50.96	50.96
PV Size (kW-DC)	50	50	50	50
Battery Size (kWh)	117.93	117.93	87.03	87.03
Battery Size (kW)	47.62	47.62	39.38	39.38
Diesel Generator Size (kW)	9.69	9.69	18.13	18.13
PV Cost (\$)	172,500	172,500	172,500	172,500
PV Cost Less NY Sun incentive (\$)	132,500	132,500	132,500	132,500
Battery Cost (\$)	108,939	108,939	84,636	84,636
Generator Cost (\$)	14,535	14,535	27,195	27,195
Total Capital Cost (\$)	255,974	255,974	244,331	244,331
Year 1 Electric Cost (\$)	69,635	69,635	69,447	69,447
Year 1 Demand Cost (\$)	174,330	174,330	176,492	176,492
Year 1 Electric Savings (\$)	285	285	473	473
Year 1 Demand Savings (\$)	17,421	17,421	15,259	15,259
Annual Resiliency Savings (\$)	-	500	-	3,515
LCC (\$)	5,361,540	5,361,540	5,367,810	5,367,810
NPV (\$)	23,650	32,350	17,380	78,530
SPP (years)	14.46	14.06	15.53	12.69
Diesel Fuel Used (gallons)	7.94	7.94	88.42	88.42
Incentive Required to get to NPV=0 (%)	0	0	0	0

Table D-5. School Shelter Scenario 4: Generator Sized to Meet Resiliency Needs

Scenario Number	4.1.a	4.1.b	4.2.a	4.2.b
Description	2 hour outage, no resiliency value	2 hour outage, with resiliency value	22 hour outage, no resiliency value	22 hour outage, with resiliency value
Outage START (hour of year)	8584	8584	8394	8394
Outage STOP (hour of year)	8590	8590	8444	8444
Resiliency Value (\$/hour)	0	68.97	0	68.97
Outage Duration (hours)	7.25	7.25	50.96	50.96
PV Size (kW-DC)	0	0	0	0
Battery Size (kWh)	0	0	0	0
Battery Size (kW)	0	0	0	0
Diesel Generator Size (kW)	29.9	29.9	32.6	32.6
PV Cost (\$)	0	0	0	0
PV Cost Less NY Sun incentive (\$)	0	0	0	0
Battery Cost (\$)	0	0	0	0
Generator Cost (\$)	44,850	44,850	48,900	48,900
Total Capital Cost (\$)	44,850	44,850	48,900	48,900
Year 1 Electric Cost (\$)	69,920	69,920	70,158	70,158
Year 1 Demand Cost (\$)	191,751	191,751	191,751	191,751
Year 1 Electric Savings (\$)	(1)	(1)	(239)	(239)
Year 1 Demand Savings (\$)	0	0	0	0
Annual Resiliency Savings (\$)	0	500	0	3,515
LCC (\$)	5,446,660	5,446,660	5,448,740	5,448,740
NPV (\$)	(61,470)	(52,770)	(63,550)	(2,400)
SPP (years)	N/A	N/A	N/A	14.93
Diesel Fuel Used (gallons)	14.78	14.78	97.67	97.67
Incentive Required to get to NPV=0 (%)	N/A	N/A	N/A	N/A

Table D-6. Fire Station Baseline: No Resilient PV

Scenario Number	0.1	0.2	0.3
Description	Without cost of grid interruptions	With cost of 2 hours/year grid interruptions	With cost of 22 hours/year grid interruptions
Outage START (hour of year)	-	-	-
Outage STOP (hour of year)			
Resiliency Value (\$/hour)	0	\$917.43/hr, 2 hours	917.43/hr, 22 hours
Outage Duration (hours)	0	0	0
PV Size (kW-DC)	0	0	0
Battery Size (kWh)	0	0	0
Battery Size (kW)	0	0	0
Diesel Generator Size (kW)	0	0	0
PV Cost (\$)	0	0	0
PV Cost Less NY Sun incentive (\$)	0	0	0
Battery Cost (\$)	0	0	0
Generator Cost (\$)	0	0	0
Total Capital Cost (\$)	0	0	0
Year 1 Electric Cost (\$)	6,092	6,092	6,092
Year 1 Demand Cost (\$)	15,214	15,214	15,214
Year 1 Electric Savings (\$)	0	0	0
Year 1 Demand Savings (\$)	0	0	0
Annual Resiliency Savings (\$)	0	0	0
LCC (\$)	438,478	470,245	787,754
NPV (\$)	0	0	0
SPP (years)	0	0	0
Diesel Fuel Used (gallons)	0	0	0
Incentive Required to get to NPV=0 (%)	0	0	0

Table D-7. Fire Station Scenario 1: Resilient PV Sized for Economic Savings

Scenario Number	1.1	1.1 Solar	1.2	1.2 Solar	1.3	1.3 Solar
Description	No resiliency value	No resiliency value, require PV	2 hour resiliency value	2 hour resiliency value, require PV	22 hour resiliency value	22 hour resiliency value, require PV
Outage START (hour of year)	-	-	-	-	-	-
Outage STOP (hour of year)	-	-	-	-	-	-
Resiliency Value (\$/hour)	0	0	\$917.43/hr 2 hrs	\$917.43/hr 2 hrs	\$917.43/hr 22 hrs	\$917.43/hr 22 hrs
Outage Duration (hours)	0	0	0	0	0	0
PV Size (kW-DC)	0	10.0	0	10.0	0	10.0
Battery Size (kWh)	60.1	42.5	60.1	42.5	214.3	213.0
Battery Size (kW)	18.7	16.5	18.7	16.5	29.8	31.2
Diesel Generator Size (kW)	0	0	0	0	0	0
PV Cost (\$)	0	38,800	0	38,800	0	38,800
PV Cost Less NY Sun incentive (\$)	0	30,800	0	30,800	0	30,800
Battery Cost (\$)	49,945	38,613	49,945	38,613	141,226	141,941
Generator Cost (\$)	0	0	0	0	0	0
Total Capital Cost (\$)	49,945	69,413	49,945	69,413	141,226	172,741
Year 1 Electric Cost (\$)	6,095	5,987	6,095	5,576	6,122	5,590
Year 1 Demand Cost (\$)	10,888	10,943	10,888	10,943	8,240	7,263
Year 1 Electric Savings (\$)	(3)	105	(3)	516	(30)	502
Year 1 Demand Savings (\$)	4,327	4,271	4,327	4,271	6,974	7,951
Annual Resiliency Savings (\$)	0	0	1,826	1,826	20,073	20,073
LCC (\$)	404,498	416,113	404,498	416,113	452,415	463,504
NPV (\$)	33,980	22,365	65,747	54,132	335,339	324,250
SPP (years)	11.55	15.86	8.12	10.50	5.23	6.06
Diesel Fuel Used (gallons)	0	0	0	0	0	0
Incentive Required to get to NPV=0 (%)	0	0	0	0	0	0
Size of Critical Load that Can Be Supported for Full Length of Outage (%)						
2 Hour Outage- Worst		41%		41%		77%
2 Hour Outage- Best		732%		732%		1181%
22 Hour Outage- Worst		2.4%		2.4%		47%
22 Hour Outage- Best		73%		73%		264%

Table D-8. Fire Station Scenario 2: Resilient PV Sized to Meet Resiliency Needs

Scenario Number	2.1.a	2.1.b	2.1.b Solar	2.2.a	2.2.b
Description	2 hour outage, no resiliency value	2 hour outage, with resiliency value	2 hour outage, with resiliency value, require PV	22 hour outage, no resiliency value	22 hour outage, with resiliency value
Outage START (hour of year)	6015	6015	6015	6004	6004
Outage STOP (hour of year)	6016	6016	6016	6025	6025
Resiliency Value (\$/hour)	0	917.43	917.43	0	917.43
Outage Duration (hours)	1.99	1.99	1.99	21.88	21.88
PV Size (kW-DC)	0.0	0.0	10.0	10.0	10.0
Battery Size (kWh)	136.3	136.3	130.5	613.0	613.0
Battery Size (kW)	41.1	41.1	40.2	40.2	40.2
Diesel Generator Size (kW)	0	0	0	0	0
PV Cost (\$)	0	0	38,800	38,800	38,800
PV Cost Less NY Sun incentive (\$)	0	0	30,800	30,800	30,800
Battery Cost (\$)	111,930	111,930	108,028	358,906	358,906
Generator Cost (\$)	0	0	0	0	0
Total Capital Cost (\$)	111,930	111,930	138,828	389,706	389,706
Year 1 Electric Cost (\$)	6,099	6,099	5,575	5,584	5,584
Year 1 Demand Cost (\$)	9,802	9,802	9,356	7,038	7,038
Year 1 Electric Savings (\$)	(7)	(7)	517	508	508
Year 1 Demand Savings (\$)	5,412	5,412	5,858	8,176	8,176
Annual Resiliency Savings (\$)	0	1,826	1,826	0	20,073
LCC (\$)	450,548	450,548	460,096	694,636	694,636
NPV (\$)	(12,070)	19,697	10,149	(256,158)	93,118
SPP (years)	20.71	15.48	16.93	44.88	13.55
Diesel Fuel Used (gallons)	0.00	0.00	1.00	0.00	0.00
Incentive Required to get to NPV=0 (%)	11%	0	0	66%	0

Note: We did not run a separate “Solar” case requiring PV for Scenario 2.1.a because there are not positive NPV savings to subsidize the cost of PV. Solar is already part of the cost-optimal solution in Scenario 2.2.a and 2.2.b, so we did not run a separate “Solar” case requiring PV for these two scenarios.

Table D-9. Fire Station Scenario 3: Resilient PV and Generator (Hybrid System) Sized to Meet Resiliency Needs

Scenario Number	3.1.a	3.1.a SOLAR	3.1.b	3.1.b Solar	3.2.a	3.2.b
Description	2 hour outage, no resiliency value	2 hour outage, no resiliency value, require PV	2 hour outage, with resiliency value	2 hour outage, with resiliency value, require PV	22 hour outage, no resiliency value	22 hour outage, with resiliency value
Outage START (hour of year)	6015	6015	6015	6015	6004	6004
Outage STOP (hour of year)	6016	6016	6016	6016	6025	6025
Resiliency Value (\$/hour)	0	0	917.43	917.43	0	917.43
Outage Duration (hours)	1.99	1.99	1.99	1.99	21.88	21.88
PV Size (kW-DC)	0.0	4.0	0.0	10.0	0.6	0.6
Battery Size (kWh)	74.1	73.2	74.1	74.3	60.5	60.5
Battery Size (kW)	19.0	18.2	19.0	18.3	16.5	16.5
Diesel Generator Size (kW)	22.11	22.51	22.11	21.86	26.30	26.30
PV Cost (\$)	0	15,520	0	38,800	2,483	2,483
PV Cost Less NY Sun incentive (\$)	0	12,320	0	30,800	1,971	1,971
Battery Cost (\$)	57,466	56,243	57,466	56,915	47,960	47,960
Generator Cost (\$)	33,165	33,765	33,165	32,790	39,450	39,450
Total Capital Cost (\$)	90,631	102,328	90,631	120,505	89,381	89,381
Year 1 Electric Cost (\$)	6,118	5,908	6,118	5,594	6,122	6,122
Year 1 Demand Cost (\$)	10,392	10,085	10,392	9,729	10,673	10,673
Year 1 Electric Savings (\$)	(26)	184	(26)	498	(30)	(30)
Year 1 Demand Savings (\$)	4,822	5,129	4,822	5,485	4,541	4,541
Annual Resiliency Savings (\$)	0	0	1,826	1,826	0	20,073
LCC (\$)	436,052	438,478	436,052	444,861	440,157	440,157
NPV (\$)	2,426	0	34,193	25,384	(1,679)	347,597
SPP (years)	18.90	19.26	13.69	15.43	19.81	3.64
Diesel Fuel Used (gallons)	4.06	4.12	4.06	4.03	43.30	43.30
Incentive Required to get to NPV=0 (%)	0	0	0	0	0	0

Note: Solar is already part of the cost-optimal solution in Scenario 3.2.a and 3.2.b, so we did not run a separate “Solar” case requiring PV for these two scenarios.

Table D-10. Fire Station Scenario 4: Generator Sized to Meet Resiliency Needs

Scenario Number	4.1.a	4.1.b	4.2.a	4.2.b
Description	2 hour outage, no resiliency value	2 hour outage, with resiliency value	22 hour outage, no resiliency value	22 hour outage, with resiliency value
Outage START (hour of year)	6015	6015	6004	6004
Outage STOP (hour of year)	6016	6016	6025	6025
Resiliency Value (\$/hour)	-	917.43	-	917.43
Outage Duration (hours)	1.99	1.99	21.88	21.88
PV Size (kW-DC)	0.0	0.0	0.0	0.0
Battery Size (kWh)	0.0	0.0	0.0	0.0
Battery Size (kW)	0.0	0.0	0.0	0.0
Diesel Generator Size (kW)	41.08	41.08	41.08	41.08
PV Cost (\$)	0	0	0	0
PV Cost Less NY Sun incentive (\$)	0	0	0	0
Battery Cost (\$)	0	0	0	0
Generator Cost (\$)	61,620	61,620	61,620	61,620
Total Capital Cost (\$)	61,620	61,620	61,620	61,620
Year 1 Electric Cost (\$)	6,100	6,100	6,157	6,157
Year 1 Demand Cost (\$)	14,725	14,725	14,725	14,725
Year 1 Electric Savings (\$)	(8)	(8)	(65)	(65)
Year 1 Demand Savings (\$)	489	489	489	489
Annual Resiliency Savings (\$)	-	1,826	-	20,073
LCC (\$)	490,209	490,209	491,374	491,374
NPV (\$)	(51,731)	(19,964)	(52,896)	296,380
SPP (years)	128.15	26.72	145.38	3.01
Diesel Fuel Used (gallons)	6.50	6.50	47.20	47.20
Incentive Required to get to NPV=0 (%)	N/A	N/A	N/A	N/A

Table D-11. Cooling Center Baseline: No Resilient PV

Scenario Number	0.1	0.2	0.3
Description	Without cost of grid interruptions	With cost of 7 hours/year grid interruptions	With cost of 51 hours/year grid interruptions
Outage START (hour of year)	-	-	-
Outage STOP (hour of year)	-	-	-
Resiliency Value (\$/hour)	0	32.02, 7.25 hours	32.02, 50.96 hours
Outage Duration (hours)	0	0	0
PV Size (kW-DC)	0	0	0
Battery Size (kWh)	0	0	0
Battery Size (kW)	0	0	0
Diesel Generator Size (kW)	0	0	0
PV Cost (\$)	0	0	0
PV Cost Less NY Sun incentive (\$)	0	0	0
Battery Cost (\$)	0	0	0
Generator Cost (\$)	0	0	0
Total Capital Cost (\$)	0	0	0
Year 1 Electric Cost (\$)	14,047	14,047	14,047
Year 1 Demand Cost (\$)	31,736	31,736	31,736
Year 1 Electric Savings (\$)	0	0	0
Year 1 Demand Savings (\$)	0	0	0
Annual Resiliency Savings (\$)	0	0	0
LCC (\$)	942,194	946,233	970,586
NPV (\$)	0	0	0
SPP (years)	0	0	0
Diesel Fuel Used (gallons)	0	0	0
Incentive Required to get to NPV=0 (%)	0	0	0

Table D-12. Cooling Center Scenario 1: Resilient PV Sized for Economic Savings

Scenario Number	1.1	1.1 Solar	1.2	1.2 Solar	1.3	1.3 Solar
Description	No resiliency value	No resiliency value, require PV	7 hour resiliency value	7 hour resiliency value, require PV	51 hour resiliency value	51 hour resiliency value, require PV
Outage START (hour of year)	-	-	-	-	-	-
Outage STOP (hour of year)	-	-	-	-	-	-
Resiliency Value (\$/hour)	0	0	32.02, 7.25 hours	32.02, 7.25 hours	32.02, 50.96 hours	32.02, 50.96 hours
Outage Duration (hours)	0	0	0	0	0	0
PV Size (kW-DC)	0	7	0	9	0	9
Battery Size (kWh)	23.88	24.75	24.75	24.75	24.75	25.38
Battery Size (kW)	6.44	6.54	6.56	6.53	6.56	6.62
Diesel Generator Size (kW)	0	0	0	0	0	0
PV Cost (\$)	0	32,480	0	37,120	0	37,120
PV Cost Less NY Sun incentive (\$)	0	26,880	0	30,720	0	30,720
Battery Cost (\$)	18,857	19,406	19,430	19,400	19,430	19,818
Generator Cost (\$)	0	0	0	0	0	0
Total Capital Cost (\$)	18,857	46,286	19,430	50,120	19,430	50,538
Year 1 Electric Cost (\$)	14,039	14,034	14,039	13,627	14,039	13,628
Year 1 Demand Cost (\$)	28,877	28,771	28,818	28,767	28,818	28,727
Year 1 Electric Savings (\$)	8	13	8	420	8	419
Year 1 Demand Savings (\$)	2,859	2,965	2,918	2,969	2,918	3,009
Annual Resiliency Savings (\$)	-	-	187	174	187	1,142
LCC (\$)	922,673	941,781	923,456	944,550	947,809	968,724
NPV (\$)	19,521	413	22,777	1,683	22,777	1,862
SPP (years)	6.58	15.55	6.24	14.07	6.24	11.06
Diesel Fuel Used (gallons)	-	-	0	0	0	0
Incentive Required to get to NPV=0 (%)	0	0	0	0	0	0
Size of Critical Load that Can Be Supported for Full Length of Outage (%)						
2 Hour Outage- Worst		31%		32%		32%
2 Hour Outage- Best		2996%		3138%		3138%
22 Hour Outage- Worst		13%		13%		13%
22 Hour Outage- Best		20%		22%		22%

Table D-13. Cooling Center Scenario 2: Resilient PV Sized to Meet Resiliency Needs

Scenario Number	2.1.a	2.1.b	2.2.a	2.2.b
Description	7 hour outage, no resiliency value	7 hour outage, with resiliency value	51 hour outage, no resiliency value	51 hour outage, with resiliency value
Outage START (hour of year)	5220	5220	5172	5172
Outage STOP (hour of year)	5226	5226	5222	5222
Resiliency Value (\$/hour)	0	32.02	0	32.02
Outage Duration (hours)	7.25	7.25	50.96	50.96
PV Size (kW-DC)	2.27	2.27	9	9
Battery Size (kWh)	104.00	104.00	230.30	230.30
Battery Size (kW)	12.11	12.11	12.69	12.69
Diesel Generator Size (kW)	0	0	0	0
PV Cost (\$)	10,533	10,533	41,760	41,760
PV Cost Less NY Sun incentive (\$)	8,717	8,717	34,560	34,560
Battery Cost (\$)	66,190	66,190	132,446	132,446
Generator Cost (\$)	0	0	0	0
Total Capital Cost (\$)	74,907	74,907	167,006	167,006
Year 1 Electric Cost (\$)	13,893	13,893	13,399	13,399
Year 1 Demand Cost (\$)	26,874	26,874	25,834	25,834
Year 1 Electric Savings (\$)	154	154	648	648
Year 1 Demand Savings (\$)	4,862	4,862	5,902	5,902
Annual Resiliency Savings (\$)	0	232	0	1,632
LCC (\$)	987,749	987,749	1,123,830	1,123,830
NPV (\$)	(45,555)	(41,516)	(181,636)	(153,244)
SPP (years)	14.94	13.26	25.50	15.17
Diesel Fuel Used (gallons)	0	0	0	0
Incentive Required to get to NPV=0 (%)	61%	55%	109%	92%

Note: We did not run separate “Solar” cases because solar is already part of the cost-optimal solutions.

**Table D-14. Cooling Center Scenario 3: Resilient PV and Generator
(Hybrid System) Sized to Meet Resiliency Needs**

Scenario Number	3.1.a	3.1.b	3.1.b SOLAR	3.2.a	3.2.b	3.2.b SOLAR
Description	7 hour outage, no resiliency value	7 hour outage, with resiliency value	7 hour outage, with resiliency value, require PV	51 hour outage, no resiliency value	51 hour outage, with resiliency value	51 hour outage, with resiliency value
Outage START (hour of year)	5220	5220	5220	5172	5172	5172
Outage STOP (hour of year)	5226	5226	5226	5222	5222	5222
Resiliency Value (\$/hour)	0	32.02	32.02	0	32.02	32.02
Outage Duration (hours)	7.25	7.25	7.25	50.96	50.96	50.96
PV Size (kW-DC)	0	0	2	0	0	9
Battery Size (kWh)	25.38	25.38	27.80	25.38	25.38	35.13
Battery Size (kW)	6.65	6.65	7.00	6.65	6.65	7.85
Diesel Generator Size (kW)	9.30	9.30	8.75	9.69	9.69	6.81
PV Cost (\$)	0	0	9,280	0	0	41,760
PV Cost Less NY Sun incentive (\$)	0	0	7,680	0	0	34,560
Battery Cost (\$)	19,848	19,848	21,456	19,845	19,845	26,118
Generator Cost (\$)	13,950	13,950	13,125	14,531	14,531	10,215
Total Capital Cost (\$)	33,798	33,798	42,261	34,376	34,376	70,893
Year 1 Electric Cost (\$)	14,034	14,034	13,927	13,967	13,967	13,467
Year 1 Demand Cost (\$)	28,780	28,780	28,618	28,780	28,780	28,164
Year 1 Electric Savings (\$)	13	13	120	80	80	580
Year 1 Demand Savings (\$)	2,956	2,956	3,118	2,956	2,956	3,572
Annual Resiliency Savings (\$)	-	232	232	-	1,632	1,632
LCC (\$)	941,764	934,415	946,233	941,186	942,942	961,257
NPV (\$)	430	11,818	0.00	1,008	27,644	9,329
SPP (years)	11.39	9.38	12.18	11.32	7.37	12.26
Diesel Fuel Used (gallons)	7.75	7.75	7.47	41.28	18.11	30.22
Incentive Required to get to NPV=0 (%)	0%	0%	0%	0%	0%	0%

Table D-15. Cooling Center Scenario 4: Generator Sized to Meet Resiliency Needs

Scenario Number	4.1.a	4.1.b	4.2.a	4.2.b
Description	2 hour outage, no resiliency value	2 hour outage, with resiliency value	22 hour outage, no resiliency value	22 hour outage, with resiliency value
Outage START (hour of year)	5220	5220	5172	5172
Outage STOP (hour of year)	5226	5226	5222	5222
Resiliency Value (\$/hour)	0	32.02	0	32.02
Outage Duration (hours)	7.25	7.25	50.96	50.96
PV Size (kW-DC)	0	0	0	0
Battery Size (kWh)	0.00	0.00	0.00	0.00
Battery Size (kW)	0.00	0.00	0.00	0.00
Diesel Generator Size (kW)	12.40	12.40	12.40	12.40
PV Cost (\$)	0	0	0	0
PV Cost Less NY Sun incentive (\$)	0	0	0	0
Battery Cost (\$)	0	0	0	0
Generator Cost (\$)	18,600	18,600	18,600	18,600
Total Capital Cost (\$)	18,600	18,600	18,600	18,600
Year 1 Electric Cost (\$)	14,043	14,043	13,986	13,986
Year 1 Demand Cost (\$)	31,735	31,735	31,735	31,735
Year 1 Electric Savings (\$)	4	4	61	61
Year 1 Demand Savings (\$)	1	1	1	1
Annual Resiliency Savings (\$)	-	232	-	1,632
LCC (\$)	967,605	967,605	966,440	968,024
NPV (\$)	(25,411)	(21,372)	(24,246)	2,562
SPP (years)	4133.33	78.60	302.44	10.98
Diesel Fuel Used (gallons)	9.2	9.2	47.55	47.55
Incentive Required to get to NPV=0 (%)	N/A	N/A	N/A	N/A