System Impact Study of the Eastern Grid of Sumba Island, Indonesia

Steady-State and Dynamic System Modeling for the Integration of One and Two 850-kW Wind Turbine Generators

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¹ *Innovative Wind Energy, Inc.*

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List of Acronyms

Hz	hertz
Km	kilometer
kV	kilovolt
kW	kilowatt
Li-ion	lithium-ion
MVA	mega-volt-ampere
MW	megawatt
MWh	megawatt-hour
NREL	National Renewable Energy Laboratory
p.u.	per unit
PF	power factor
PLN	State Electricity Company of Indonesia
SCPR	short-circuit power ratio
WTG	wind turbine generator

Executive Summary

The goal of this project was to study the impact of integrating one and two 850-kW wind turbine generators (WTGs) into the eastern power system network of Sumba Island, Indonesia. A model was created for the 20-kV distribution network as it existed in the first quarter of 2015, with a peak load of 5.682 MW. Detailed data were collected for each element of the network. Load flow, short-circuit, and transient analyses were performed using DIgSILENT PowerFactory 15.2.1.

The load flow analysis suggests that in the baseline (no WTGs) and with both integration options there is no overloading of generators, no overloading of conductors, and all of the bus voltages are within range.

The short-circuit analysis suggests that the short-circuit power ratio is comfortably above the minimum requirement at the Haharu Bus—the point of common coupling of the WTG. In addition, because the short-circuit power contribution of the WTGs is minimal, the ratings of the devices in the substations should not be impacted.

The transient analysis suggests that with one 850-kW WTG, the system is unstable under the following fault scenarios: a 400-kW loss of generation at the Kambajawa Bus with no reconnection, a 400-kW loss of generation at the Waingapu Bus with no reconnection, and the loss of the 850-kW WTG with no reconnection. However, the system is stable with the addition of 500 kW/4.17 kWh of storage (stability support equipment) coupled with the auto-start capability of the backup generator within 10 s after the fault.

As a result of the analysis of integrating one 850-kW WTG at the Haharu Bus in the eastern grid of Sumba Island, the following options for changes to the grid are explored:

1. Add a 500-kW/4.17-kWh storage unit¹ to the Haharu Bus along with a hybrid control system to auto-start a designated backup generator (an existing CAT32 diesel unit with a capacity of 550 kW located in Waingapu). In the high-wind scenario (which occurs with a frequency of approximately 2% duration of the wind speeds) and under a variety of disturbances—such as the loss of a WTG or the loss of a generator at the Kambajawa Bus—the following sequence of events will need to happen to maintain system stability:
 - A. The storage unit provides maximum energy from the start of the disturbance for a duration of 10 s, thereby reducing the rate of the decrease in grid frequency and improving the frequency nadir of the frequency dip during the loss of generation.
 - B. The controller sends an auto-start signal to CAT32 when the fault occurs.
 - C. The CAT32 diesel unit starts within 10 s.
 - D. The storage unit continues to provide power for 30 s and then disconnects.
 - E. After 30 s, if there is a shortfall in power, other generators in the system increase production by tapping into headroom to deliver the additional power required.

¹ The requirement is for 500 kW/4.17 kWh. The exact sizing and specifications of the storage unit is not within the scope of this project; however, it must be noted that commercially available storage units of 500 kW will have energy content much larger than 4.17 kWh.

2. If no storage is used, then grid management becomes a challenge. The following strategy could address this challenge, but it would cause the diesel generator sets to run at lower efficiency:
 - A. Run the diesel generators with sufficient headroom to provide close to 850 kW of power in case of the loss of the WTG during high wind. This would be challenging during low demand, because it would require running the diesel generator sets at less than 90% of full rating; this could provide the headroom, but it would sacrifice efficiency. The current practice is to run the diesel generator sets at 100% full rating (no headroom).

Thus, adding one 850-kW WTG to the eastern power system network of Sumba along with a 500-kW storage unit, hybrid power plant controller, 550-kW backup diesel generator set with 10-s cold-start time, and high-speed communications is a solution that will improve the reliability of the energy supply, enhance the stability of the system, and reduce greenhouse gas emissions.

The transient analysis suggests that with two 850-kW WTGs located in the same area, the system is unstable under the following fault scenarios: a loss of generation at the Kambajawa Bus with no reconnection and the loss of two WTGs with no reconnection. With the addition of the following, the system is stable: (1) 1,500 kW/25 kWh of storage,² (2) one 550-kW backup diesel generator with 10-s cold-start time, (3) additional backup generators with 60-s cold-start times, (4) a hybrid controller to manage all of the generation units, and (5) a high-speed communications network. Most commercial lithium-ion storage systems and some flywheel storage systems contain energy for 60 s of discharge at rated power; therefore, the combination of adding (1)–(5) is appropriate to improve the reliability of the energy supply, enhance the stability of the system, and reduce greenhouse gas emissions.

The trip report for 2014, provided by the State Electricity Company of Indonesia (PLN), indicates that the number of blackouts and trips is high: approximately one per day. Preliminary analysis suggests that this is because of the following reasons: (1) the faults are not cleared within the specified setting time of the circuit breakers, (2) the generators are dispatched with low headroom (low spinning reserves), (3) the lack of vegetation management causes overhang on transmission lines, and (4) the diesel generators are old. Improvements to (1)–(4) and the introduction of storage will reduce the number of blackouts and trips and thereby improve the reliability of the system.

To reach the longer-term goal of 100% renewable energy in Sumba Island, this report analyzes one path: variable sources (wind/solar) + energy storage (with minimal energy content, in the range from 30 s to a few minutes) + diesel generators with short cold-start times (10–20 s) + a hybrid controller to manage all the generation assets. If implemented, the 850-kW wind project will be a pilot for this path. Note, however, that there are other paths that have not been explored, such as no diesel. As the wind project pilot is scaled up, distributing energy storage to be located near load centers should be considered so that the colocated wind and storage units do not become a single point of failure; locating them separately would increase the resiliency of the

² The requirement is for 1,500 kW/25 kWh. The exact sizing and specifications of the storage unit is not within the scope of this project; however, it must be noted that commercially available storage units of 1,500 kW will have energy content much larger than 25 kWh.

network. Similarly, to integrate two WTGs, the second WTG should be placed in a different location than the first, and one with high wind resources, also to avoid a single point of failure and thereby further increase the resiliency of the network.

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1 Background

The goal of this project was to study the impact of integrating one or two 850-kW Vestas Type 3 (doubly-fed induction generators) WTGs into the eastern power system network of Sumba Island, Indonesia. Sumba Island was chosen as the iconic island for a renewable energy initiative based on a study performed by Hivos International in collaboration with Winrock International, Inc. Sumba was chosen because of the following considerations:

- Residents have low access to electricity. (The electrification ratio was 24.5% in 2010.)
- Until now, Sumba has been heavily dependent on its diesel power plants. (Eighty-five percent of the electricity is from fuel oil/diesel.)
- Fuel oil is sent from other regions in Indonesia, which incurs high transportation costs.
- Sumba is rich in renewable energy resources, including water, bioenergy, wind, and solar/photovoltaic.
- Approximately 20% of Sumba's population is considered low income (poor).

The predicted growth of Sumba's energy consumption is illustrated in Figure 1, shown with different accelerations. At the minimum, it is predicted that the peak load will reach approximately 13 MW by 2025, a growth of approximately 300%. At the maximum, the peak load is predicted to reach approximately 20 MW by 2025, a growth of approximately 500%.

Figure 1. Projected peak load growth in Sumba Island. Image from Hivos International (2011)

A map of the wind resources is given in Figure 2. As shown, the wind resources are generally very good throughout Sumba Island, reaching up to 7.5 m/s in some places not far from the load centers.

Figure 2. Annual average wind resources in Sumba Island. Image from Hirsch et al. (2015)

This project is a collaboration among the National Renewable Energy Laboratory (NREL), Winrock International, Inc., and the State Electricity Company of Indonesia (PLN). The North American Electric Reliability Corporation's standard on Steady-State and Dynamic System Model Validation mandates that planning coordinators develop and implement a documented data validation process to validate their steady-state and dynamic system models. Toward that end, this group developed such a process, which is described herein, to study the eastern grid of Sumba Island. Note that the validation has not been performed.

2 Steady-State Analysis

The steady-state analysis was performed to analyze the steady-state conditions of the power system network, including the bus voltages and the power flows through the branches and transformers, by considering different scenarios when the power system operates under stresses.

2.1 The Process

The process used to analyze the steady-state system model was based on the North American Electric Reliability Corporation's Procedures for Validation of Powerflow and Dynamics Cases. Some changes were made to the procedures based on regional regulation (by PLN) and based on engineering judgment. The following data were obtained from PLN in eastern Sumba. The complete data are shown in Appendix A. The process was as follows:

1. Obtain data from PLN for the following:
 - A. Transmission lines
 - i. Status
 - B. Transformers
 - i. Status
 - ii. Load tap changer position
 - iii. Type (Transformers that had load tap changers were changed to Type 1 to deactivate the load tap changers.)
 - C. Loads
 - i. Real power
 - ii. Reactive power
 - D. Generators
 - i. Real power
 - ii. Reactive power
2. Model all diesel generator sets and wind generation that is connected via 20-kV feeders as generators at the appropriate buses.

2.2 Power Flow Analysis

The power system network, load data, and power plant data were needed to analyze the steady-state power system model. Appendix B contains the input data for each scenario, and Appendix C contains the detailed results of power flow analysis for each scenario.

Table 1. Bus/Substation Data for Sumba Island

No.	Substation Name	Voltage Level (kV)	Breaker Rating (kA)	Area/Zone	District Name
1	Haharu	20	16	Hambapraing	Haharu
2	Kambajawa	20	16	East Sumba	Kambajawa
3	Waingapu	20	16	Waingapu	Waingapu

Note: MHaharu is the bus between Haharu and Kambajawa. It was introduced because the conductor type changes—17 Km is one type, and 8 Km is another. In the diagrams in Figure 4, this bus is labeled “Single busbar(3)/K-H2,” and it is located right beneath the Haharu Bus.

Table 2. List of Generators at Haharu Bus #1

No.	Generator Name	Rated Voltage (kV)	MVA Rating
1	WTG1	0.69	0.85
2	WTG2	0.69	0.85

Note: The second generator is not used in the case of integrating one 850-kW WTG.

Table 3. List of Generators at Kambajawa Bus #2

SNo.	Generator Name	Rated Voltage (kV)	MVA Rating
1	Volvo	0.4	0.22
2	MTU1	0.4	0.65
3	MAN1	0.4	0.43
4	MTU2	0.4	0.43
5	MTU4	0.4	0.43
6	MAN2	0.4	0.32
7	DOOSAN1	0.4	0.42
8	DOOSAN2	0.4	0.42
9	DOOSAN3	0.4	0.42
10	DOOSAN4	0.4	0.42
11	DOOSAN5	0.4	0.42
Total:			4.58

Table 4. List of Generators at Waingapu Bus #3

SNo.	Generator Name	Rated Voltage (kV)	MVA Rating
1	CAT	0.4	0.55
2	YANMAR	6.3	0.22
3	DEUTZ1	0.4	0.18
4	DEUTZ2	0.4	0.18
5	SWD1	6.3	0.22
6	SWD2	6.3	0.22
7	SWD3	6.3	0.22
Total			1.79

2.2.1 Baseline Power Flow

The baseline power flow analyzes the power system during light load and heavy load conditions before a WTG is installed.

According to the information received, the total maximum load in the system is 5.682 MW around 6:00 p.m., and the total minimum load of the system is 2.751 MW during daytime. The actual loads on each bus during the maximum and minimum load conditions are given in Table 5. Information about the load power factor (PF) under both conditions is also shown.

Table 5. Power Demand and Power Factor of Loads at Three Substations

Bus No.	Name of Substation	Voltage Level (kV)	Max. Load (MW), Peak Load	Power Factor, Peak Load	Min. Load (MW), Off-Peak Load	PF, Off-Peak Load
1	Haharu	20	0.104	0.85	0.051	0.85
2	Kambajawa	20	3.494	0.9	1.691	0.95
3	Waingapu	20	2.084	0.9	1.0086	0.95
	Total		5.682		2.751	

According to the information collected from PLN in Sumba, during off-peak hours only the generators at the Kambajawa Bus operate. During peak load hours, specific generators at the Waingapu Bus are turned on depending on the extra generation needed. This decision is based on the fuel efficiency of the generators. The first priority is given to CAT C32, followed by Yanmar, DEUTZ, and SWD.

To model this type of dispatch, the slack bus definition shown in Table 6 is used for the different scenarios.

Table 6. Slack Buses for the Scenarios

Scenario	Slack Bus
No Wind High Load	MTU 1
No Wind Low Load	MAN 1
High Wind (1) ^a High Load	MTU 1
High Wind (1) Low Load	DOOSAN 5
High Wind (2) High Load	MAN 1
High Wind (2) Low Load	DOOSAN 3

^a The number in the parentheses indicates the number of WTGs.

Data collected from PLN in Sumba suggests that all the generators run at PF = 0.8. Modeling this power factor resulted in a large generation of reactive power compared to demand, thereby causing a large absorption of reactive power at the slack bus. To rectify this situation, a few generators are made to run at PF = 1 to ensure that there is minimal absorption of reactive power at the slack bus. Table 7 lists the generators that are turned on, off, and running at PF = 1 in the four scenarios. The results of the baseline model indicate that the Kambajawa generators are not overloaded, and all the voltages are within the specified band.

Table 7. Status of Each Generator and Its Power Factor for One and Two WTGs

Generator Name	Derated	No Wind High Load		No Wind Low Load		High Wind (1) High Load		High Wind (1) Low Load		High Wind (2) High Load		High Wind (2) Low Load	
		Status	PF	Status	PF	Status	PF	Status	PF	Status	PF	Status	PF
MTU2	430	ON	0.8	ON	0.8	ON	1	OFF	0	ON	0.8	OFF	0
DOOSAN1	420	ON	1	ON	1	ON	1	ON	1	ON	0.8	ON	1
DOOSAN2	420	ON	1	ON	1	ON	0.8	ON	0.8	ON	0.8	ON	0.8
DOOSAN3	420	ON	0.8	ON	1	ON	0.8	ON	0.8	ON	0.8	ON	0.8
DOOSAN4	420	ON	0.8	ON	0.8	ON	0.8	ON	0.8	ON	0.8	OFF	0
DOOSAN5	420	ON	1	ON	0.8	ON	0.8	ON	0.8	ON	0.8	OFF	0
VOLVO	220	ON	0.8	OFF	0	ON	0.8	OFF	0	ON	0.8	OFF	0
MAN1	430	ON	0.8	ON	0.8	ON	0.8	OFF	0	ON	0.8	OFF	0
MTU1	650	ON	0.8	OFF	0	ON	0.8	OFF	0	ON	0.8	OFF	0
MTU4	430	ON	0.8	OFF	0	ON	0.8	OFF	0	ON	0.8	OFF	0
CAT	550	ON	0.8	OFF	0	ON	0.8	OFF	0	OFF	0	OFF	0
YANMAR	220	ON	0.8	OFF	0	ON	1	OFF	0	ON	0.8	OFF	0
MAN2	320	ON	0.8	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
DEUTZ-1	180	ON	1	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
DEUTZ-2	180	ON	0.8	OFF	0	ON	1	OFF	0	OFF	0	OFF	0
SWD-1	220	ON	1	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
SWD-2	220	ON	0.8	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
SWD-3	220	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
WTG	850	OFF	0	OFF	0	ON	1	ON	1	ON	1	ON	1

Legends:

Nodes	Branches
Line-Line Voltage, Magnitude [kV]	Active Power [MW]
Voltage, Magnitude [p.u.]	Reactive Power [Mvar]
Voltage, Angle [deg]	Current, Magnitude [kA]

Figure 3. Power flow display: high load without WTG(s). MTU 1 = slack bus

2.2.2 Power Flow with Wind Turbine Generator Installed

The system was also analyzed under the same two baseline scenarios with the two options related to integrating one and two WTGs. The WTGs have capacities of 850 kW and output voltages of 0.69 kV. The load flow analysis was performed under the same load conditions as the baseline and for the same scenarios. The results are presented in Table 8.

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Figure 6. Power flow display: low load with WTG. DOOSAN 5 = slack bus

Figure 7. Power flow display: high load, with 2 WTGs. MAN 1 = slack bus

Figure 8. Power flow display: low load, with 2 WTGs. DOOSAN 3 = slack bus

Table 8. Comparison of Different Load Flow Scenarios

	High Load Scenario			Low Load Scenario		
	Without WTG(s)	With 1 WTG	With 2 WTGs	Without WTG(s)	With 1 WTG	With 2 WTGs
INPUT						
Load, PF at Kambajawa	3.494 MW, 0.9	3.494 MW, 0.9	3.494 MW, 0.9	1.691 MW, 0.95	1.691 MW, 0.95	1.691 MW, 0.95
Load, PF at Waingapu	2.084 MW, 0.9	2.084 MW, 0.9	2.084 MW, 0.9	1.009 MW, 0.95	1.009 MW, 0.95	1.009 MW, 0.95
Load, PF at Haharu	0.104 MW, 0.85	0.104 MW, 0.85	0.104 MW, 0.85	0.051 MW, 0.85	0.051 MW, 0.85	0.051 MW, 0.85
OUTPUT						
Real Power Generated by WTG(s)	0	0.85 MW	1.7 MW	0	0.85 MW	1.7 MW
Reactive Power Generated by WTG(s)	0	0 MVAR	0 MVAR	0	0.085 MVAR	0 MVAR
Real Power Generated by Kambajawa Generators	4.171 MW	3.988 MW	3.956 MW	2.779 MW	1.954 MW	1.198 MW
Reactive Power Generated by Kambajawa Generators	2.108 MVAR	2.64 MVAR	2.955 MVAR	1.022 MVAR	1.031 MVAR	1.095 MVAR
Real Power Generated by Waingapu Generators	1.567 MW	0.94 MW	0.22 MW	0	0	0

	High Load Scenario			Low Load Scenario		
	Without WTG(s)	With 1 WTG	With 2 WTGs	Without WTG(s)	With 1 WTG	With 2 WTGs
Reactive Power Generated by Waingapu Generators	0.876 MVAR	0.412 MVAR	0.165 MVAR	0	0	0
PU Voltage at Haharu (20 kV)	0.984	1.032	1.084	0.986	1.04	1.081
PU Voltage at MHaharu (20 kV)	0.99	1.003	1.025	0.989	1.008	1.018
PU Voltage at Kambajawa (20 kV)	0.992	0.996	1.009	0.99	0.999	1.001
PU Voltage at Waingapu (20 kV)	0.989	0.988	0.997	0.984	0.994	0.996
Real Power Consumed by Line between Kambajawa and MHaharu	0 MW	0.006 MW	0.025 MW	0 MW	0.007 MW	0.027 MW
Reactive Power Consumed by Line between Kambajawa and MHaharu	0.004 MVAR	0.001 MVAR	0.01 MVAR	0.004 MVAR	0.001 MVAR	0.011 MVAR
Real Power Consumed by Line between MHaharu and Haharu	0.001 MW	0.022 MW	0.092 MW	0 MW	0.025 MW	0.1 MW
Reactive Power Consumed by Line between MHaharu and Haharu	0.003 MVAR	0.005 MVAR	0.033 MVAR	0.004 MVAR	0.006 MVAR	0.036 MVAR

	High Load Scenario			Low Load Scenario		
	Without WTG(s)	With 1 WTG	With 2 WTGs	Without WTG(s)	With 1 WTG	With 2 WTGs
Real Power Consumed by Line between Kambajawa and Waingapu	0.001 MW	0.007 MW	0.016 MW	0.004 MW	0.004 MW	0.004 MW
Reactive Power Consumed by Line between Kambajawa and Waingapu	0.002 MVAR	0.005 MVAR	0.017 MVAR	0.001 MVAR	0.001 MVAR	0.001 MVAR
Haharu-Kambajawa Line Loading in kA (3.18 MVA)*	0.004	0.021	0.042	0.002	0.022	0.044
Kambajawa-Waingapu Line Loading in kA (7.4 MVA)*	0.016	0.05	0.059	0.031	0.031	0.031

2.2.3 Results of Power Flow with Wind Turbine Generator Installed

The results indicate the following:

- The voltages at all buses are within the limits of the grid code.
- The loads on the transmission lines are within the thermal limits of the conductor.

From a load flow perspective, installing one or two 850-kW WTGs will not have any detrimental impact on the grid.

2.3 Short-Circuit Analysis

Two types of short-circuit analyses were performed:

- Computation of the short-circuit power ratio to determine the strength of the grid at the point of common coupling. See Section 2.3.1.
- Computation of the short-circuit contribution of the WTG(s). See Section 2.3.2.

2.3.1 Short-Circuit Fault at the Point of Common Coupling of the Wind Power Plant (Before the Wind Turbine Generator Was Installed)

In the as-is scenario, the short-circuit power at the Haharu Bus (the point of common coupling of the WTG) was computed.

Table 9. Comparison of Different Short-Circuit Scenarios When Shorted at the Point of Common Coupling

	Without WTG(s)	
	Three-Phase Fault During High Load	Three-Phase Fault During Low Load
INPUT PARAMETERS		
Generation at Kambajawa	4.171 MW	2.779 MW
Generation at Waingapu	1.567 MW	0 MW
OUTPUT		
Short-Circuit Power at Haharu Bus	14.8 MVA	12.3 MVA
Short-Circuit Power Ratio at Haharu Bus (for 0.85-MW WTG)	17.41	14.47
Short-Circuit Power Ratio at Haharu Bus (for two 0.85-MW WTG)	8.71	7.24
Fault Contribution from Kambajawa Generators	11.3 MVA	12.3 MVA
Fault Contribution from Waingapu Generator Set	3.5 MVA	0 MVA

The terminology used in this section is explained as follows.

- The *short-circuit power* is actually the short-circuit apparent power output of the generator with the unit MVA. This is an indication that during a short circuit, very low “real power” is generated, and the “apparent power” is mostly consumed by the “reactive power” developed by the short-circuit current in the generator, transformer, and line reactances (Xs).
- The *short-circuit power ratio (SCPR)* is expressed per unit. The SCPR is 17.41 during high load and 14.47 during low load for one WTG and half those values for those WTGs. This is well above the SCPR requirement for connecting a wind turbine. In most grid codes, the SCPR requirement is 5 or higher to avoid large fluctuations in voltage at the point of common coupling when the wind power plant is off, connected during low wind speeds, and connected during high wind speeds.

Legends:

Short-Circuit Nodes	Nodes
Initial Short-Circuit Power [MVA]	Line-Line Voltage, Magn
Initial Short-Circuit Current [kA]	Voltage, Magnitude [p.u]
Peak Short-Circuit Current [kA]	Voltage, Angle [deg]

Figure 9. Short-circuit analysis of the three-phase fault at the point of common coupling (high load)

Figure 10. Short-circuit analysis of the three-phase fault at the point of common coupling (low load)

2.3.2 Short-Circuit Fault at the Point of Common Coupling of the Wind Power Plant (Before and After the Wind Turbine Generator Was Installed)

Table 10. Comparison of Short-Circuit Power Contribution by WTG(s)

	High Load		Low Load	
	Kambajawa Bus Shorted	Waingapu Bus Shorted	Kambajawa Bus Shorted	Waingapu Bus Shorted
One 850-kW WTG				
Short-Circuit Power at Shorted Bus	41.8 MVA	34.1 MVA	30.8 MVA	26.4 MVA
Fault Contribution from WTG Generator	1.8 MVA	1.5 MVA	1.9 MVA	1.6 MVA
Two 850-kW WTGs				
Short-Circuit Power at Shorted Bus	34 MVA	39.8 MVA	17.9 MVA	16.3 MVA
Fault Contribution from WTGs	2.8 MVA	3.4 MVA	3.6 MVA	3.2 MVA

As expected, the short-circuit power contribution from the WTG is minimal. The conclusion is that the MVA ratings of the existing protection systems and other existing equipment at the substations should be sufficient to accommodate the integration of one or two 850-kW WTGs.

2.4 Guidelines to Identify and Resolve Unacceptable Differences

The tables below were used to identify and resolve unacceptable differences in the steady-state model validation process.

Note that Table 11 contains the acceptable range of voltage, frequency, and power factor in a distribution network of 20 kV or lower voltage for renewable energy generation plants that have a nameplate capacity 10 MW or less.³

Table 11. Guidelines to Identify Acceptable Differences for 20kV network

Quantity	Acceptable Differences
Bus Voltage Magnitude	85% to 110%
Frequency	51 to 47.5 Hz
Power factor	0.9 leading to 0.85 lagging

³ “Guidelines for Connecting Renewable Energy Generation Plants (REGP) to PLN’s Distribution System,” Feb 2014, approved by PLN Board of Directors as DK. Dir. PLN No.0357/2014.

Table 12. Guidelines to Resolve Unacceptable Differences

Quantity	Resolution Guidelines
Bus Voltage Magnitude Real Power Flow Reactive Power Flow	<p>Verify that the generation should be modeled as gross instead of net values.</p> <p>Verify that shunt capacitors are sized correctly.</p> <p>Verify that all state estimator loads are accounted for.</p> <p>Verify that the network configuration is modeled appropriately based on the circuit breaker and switch status (e.g., does a bus need to be modeled as a split bus due to an open circuit?).</p> <p>Verify that the modeled line and transformer impedances are correct.</p> <p>Verify that no-load tap changers are modeled appropriately for all transformers.</p> <p>Verify that all other system elements are modeled appropriately.</p> <p>Consider whether PI data should be used when state estimator data are questionable.</p> <p>Consider whether differences are caused by measurement error.</p>

3 Dynamic System Analyses

3.1 The Process

The process used to analyze the dynamic system model was based on the North American Electric Reliability Corporation's Procedures for Validation of Powerflow and Dynamics Cases. Some changes were made based on engineering judgment.

In essence, we analyzed the dynamic system by using the system conditions recorded on a specific day and time as model inputs to see if the resultant model outputs (bus voltages and real and reactive power flows) matched the corresponding recorded system conditions. More importantly, we needed to analyze the pre-fault and post-fault conditions (voltage, frequency, and overloaded lines or transformers) at important buses.

Various contingencies should be considered in discussions with the utility companies. Consideration should be given to the highest probability based on historic data recorded by PLN. Some examples of contingencies for peak and light loads with and without WTGs should be included. For example:

- Disconnection of WTG (light/high wind scenarios)
- Disconnection of the partial loads at buses
- Disconnection of one or several diesel generator sets
- Faults at buses.

For this analysis, we used PowerFactory's electromechanical transient simulation method using root mean square values. In this method, the A-Stable algorithm with automatic step size adaptation was used.

3.2 Dynamic Data of Grid Elements

The data used for the dynamic simulation are in Appendix D. For the elements for which complete dynamic data were not provided by PLN or are not available for East Sumba, we used generic dynamic data.

3.2.1 Transient Faults and Power System Conditions

The following cases were examined:

- Pre-fault: Baseline, no WTG (peak load and off-peak load). This is labeled "No Wind High Load" and "No Wind Low Load"
- Pre-fault: Single WTG is installed (peak load and off-peak load). This is labeled "High Wind High Load" and "High Wind Low Load"
- The term *fault* is used to describe disturbances caused by short circuits or the disconnection of a load or generator.
- Fault analysis followed by:
 - Self-clearing (no load, no generator, no lines were disconnected). It is assumed that the fault self-clears before the circuit breaker is activated.

- No self-clearing. These cases are labeled “no self-clearing.” It is assumed that the fault/disturbance persisted with no attempt to clear the fault/disturbance. If a fault is not isolated, eventually the power system may lead to a blackout.

The duration of the fault was chosen to be 9 cycles, or 0.18 s, as commonly used in the United States.

The first set of faults analyzed were faults at each of the three buses: Haharu, Kambajawa, and Waingapu.

3.2.2 Loss of Partial Load

A disturbance that may cause a loss of load is generally caused by an overload or fault. It is usually a sequence of events that occurs because of the system protection. The most likely scenario is the removal of lines connected to a group of loads, and thus the impact is represented by the loss of loads. Because the size of the total generation is approximately 6 MW during peak load and 3.8 MW during off-peak load, the size chosen to represent the loss of load was 400 kW, which is about the size of a typical diesel generator set in East Sumba. Instead of an exact 400-kW load loss, DIGSILENT allows load loss to be specified only as a percent. The table below contains the load loss scenarios.

Table 13. Load Loss Scenarios

Bus	Scenario	High Load (MW)	Low Load (MW)
Haharu	Before Fault	0.104	0.069
	After Fault	0	0
	Loss (100%)	0.104	0.069
Kambajawa	Before Fault	3.494	2.085
	After Fault	2.981	1.776
	Loss (15%)	0.513	0.309
Waingapu	Before Fault	2.084	1.782
	After Fault	1.676	1.434
	Loss (20%)	0.408	0.348

3.2.3 Loss of Partial Generation

In this scenario, it was assumed that the loss of generation was equivalent to the loss of a single diesel generator, and the typical size of a diesel generator in East Sumba is 400 kW. Thus, the loss of a generator was chosen to be 400 kW. On the Kambajawa and Waingapu buses, one generator represented the group of generators that would stay connected during and after the disturbance, whereas the second generator (400 kW) represented the generator that was disconnected during the disturbance.

3.3 Voltage and Frequency Limits in Study

PLN in East Sumba provided some of the limits for acceptable voltage and frequency in the grid; engineering judgment was used for the rest. Following are the limits used for the study:

- The voltage operation limits are defined on $\pm 10\%$ of the nominal voltages.
- The limits of the frequency operation for all components of the grid are defined from 0.97–1.03 p.u.
- The limits of the low-voltage operation for the WTGs are defined on 0.9 p.u. for 60 s and 0.85 p.u. for 11 s.
- The limits of the high-voltage operation for the WTGs are defined on 1.1 p.u. for 60 s, 1.15 p.u. for 2 s, and 1.2 p.u. for 80 ms.
- The limits of the low and high frequency operation for the WTGs are defined as 47 Hz and 53 Hz for 200 ms.
- The limits of the voltage operation for the diesel generation are defined from 0.9–1.1 p.u.
- The limits of the frequency operation for the diesel generation are defined from 47–53 Hz for 200 ms.
- Higher priority is given to wind generation than diesel generation whenever the wind is available. For all of the scenarios considered, no unacceptable situations were identified.

3.4 Scenarios for the Integration of One 850-kW Wind Turbine Generator

A summary of the transient analysis of the scenarios and the observed performance of the network are presented in Table 14. These figures are contained in Appendix E. The highlighted case numbers (bold and underlined) correspond to instability; the type of instability is explained in the observations column.

Table 14. Scenarios and Observations for the Dynamic System Impact Analysis of the Integration of One WTG

Case #	Scenarios	Exhibit #	Observations
Three-phase-to-ground fault at Haharu Bus. The fault is created at 1 s, and it self-clears at 1.18 s.			
1	No Wind High Load	Figure E-1 and E-2	System is stable Line loadings are within limits Voltage drops to about 0.65 p.u. at the buses during the fault and recovers in 0.18 s Frequency drops to 0.97 p.u. and recovers in about 12 s
2	No Wind Low Load	Figure E-3, E-4	System is stable Line loadings are within limits Voltage drops to below 0.625 p.u. at the buses during the fault and recovers in 0.18 s

Case #	Scenarios	Exhibit #	Observations
3	High Wind High Load	Figure E-5, E-6 and E-7	System is stable Line loadings are within limits Frequency drops to 0.965 p.u. and recovers in about 2.5 s Bus voltages dip below 0.60 p.u. at the K and W buses Terminal voltage and power outputs of generators are stable
4	High Wind Low Load	Figure E-8, E-9 and E-10	System is stable Line loadings are within limits Frequency drops to 0.96 p.u. and recovers in about 2.0 s Bus voltages dip below 0.45 p.u. at the K and W buses Terminal voltage and power outputs of generators are stable
Three-phase-to-ground fault at Kambajawa Bus. The fault is created at 1 s, and it self-clears at 1.18 s.			
5	No Wind High Load	Figure E-11 and E-12	System is stable Line loadings are within limits Terminal voltage at generators drops to below 0.3 p.u. during fault Bus voltages at Haharu and Waingapu drop to below 0.1 p.u. during fault Voltage recovers soon after the fault clears
6	No Wind Low Load	Figure E-13	System is stable Line loadings are within limits Terminal voltage at generators drops to below 0.3 p.u. during fault Bus voltages at Haharu and Waingapu drop to below 0.1 p.u. during fault Voltage recovers soon after the fault clears
7	High Wind High Load	Figure E-14 and E-15	System is stable Line loadings are within limits Frequency drops to 0.99 p.u. and recovers in about 2.5 s Bus voltages dip below 0.10 p.u. at the K and W buses Terminal voltage and power outputs of generators are stable

Case #	Scenarios	Exhibit #	Observations
8	High Wind Low Load	Figure E-16 and E-17	System is stable Line loadings are within limits Frequency drops to 0.99 p.u. and recovers in about 8.0 s Bus voltages dip below 0.2 p.u. at the K and W buses Terminal voltage and power outputs of generators are stable
Three-phase-to-ground fault at Waingapu Bus. The fault is created at 1 s, and it self-clears at 1.18 s.			
9	No Wind High Load	Figure E-18 and E-19	Terminal voltage at generators drops to just above 0.1 p.u. during fault Bus voltages at Haharu and Kambajawa drop to below 0.2 p.u. during fault Voltage recovers soon after the fault clears
10	No Wind Low Load	Figure E-20	Terminal voltage at generators drops to just above 0.1 p.u. during fault Bus voltages at Haharu and Kambajawa drop to below 0.2 p.u. during fault Voltage recovers soon after the fault clears
11	High Wind High Load	Figure E-21 and E-22	Terminal voltage at generators drops to just above 0.3 p.u. during fault Bus voltages at Haharu and Kambajawa drop to below 0.2 p.u. during fault Voltage recovers soon after the fault clears
12	High Wind Low Load	Figure E-23 and E-24	Terminal voltage at generators drops to just above 0.3 p.u. during fault Bus voltages at Haharu and Kambajawa drop to below 0.2 p.u. during fault Voltage recovers soon after the fault clears
WTG outage. The fault is created at 1 s, and it self-clears at 1.18 s.			
13	High Wind High Load	Figure E-25, E-26 and E-27	System is stable Line loadings, voltages, and frequency are within limits Voltage transient at Haharu bus WTG power output transient after the fault clears

Case #	Scenarios	Exhibit #	Observations
14	High Wind Low Load	Figure E-28 and E-29	System is stable Line loadings, voltages, and frequency are within limits Voltage transient at Haharu bus WTG power output transient after the fault clears
WTG outage. The fault is created at 1 s, and it does not clear.			
15	High Wind High Load	Figure E-30, E-31 and E-32	Loss of synchronism is noticed for this case. This is expected because the loss of 850 kW of wind power with no self-clearing is a large loss of generation in the grid from which the grid cannot recover. Storage units with the WTGs will alleviate the situation by providing temporary power until additional diesel generators are dispatched to compensate for the large loss of generation.
16	High Wind Low Load	Figure E-33 and E-34	Loss of synchronism is noticed for this case. This is expected because the loss of 850 kW of wind power with no self-clearing is a large loss of generation in the grid from which the grid cannot recover. Storage units in parallel with the WTGs will alleviate the situation by providing temporary power until additional diesel generators are dispatched to compensate for the large loss of generation.
Partial generator outage at Kambajawa Bus. The fault is created at 1 s, and it self-clears at 1.18 s.			
17	No Wind High Load	Figure E-35 and E-36	System is stable Line loadings, voltages, and frequency are within limits
18	No Wind Low Load	Figure E-37	System is stable Line loadings and voltages are within limits After the fault, the frequency goes to 1.015 p.u. and 0.985 p.u., slightly outside the allowable range.
19	High Wind High Load	Figure E-38 and E-39	System is stable Line loadings and voltages are within limits After the fault, the frequency goes to 1.015 p.u. and 0.985 p.u., slightly outside the allowable range.

Case #	Scenarios	Exhibit #	Observations
20	High Wind Low Load	Figure E-40 and E-41	System is stable Line loadings and voltages are within limits After the fault, the frequency goes to 1.015 p.u. and 0.985 p.u., slightly outside the allowable range.
Partial generator outage at Kambajawa Bus. The fault is created at 1 s, and it does not clear.			
<u>21</u>	No Wind High Load	Figure E-42 and E-43	System is unstable After the fault, the frequency keeps dropping, and a frequency runaway is observed.
<u>22</u>	No Wind Low Load	Figure E-44	System is unstable After the fault, the frequency keeps dropping, and a frequency runaway is observed.
<u>23</u>	High Wind High Load	Figure E-45 and E-46	System is unstable After the fault, the frequency keeps dropping, and a frequency runaway is observed.
<u>24</u>	High Wind Low Load	Figure E-47 and E-48	System is unstable After the fault, the frequency keeps dropping, and a frequency runaway is observed. The bus and generator terminal voltage also keep dropping.
Partial generator outage at Waingapu Bus. The fault is created at 1 s, and it self-clears at 1.18 s.			
25	No Wind High Load	Figure E-49 and E-50	System is stable Line loadings, frequency, and bus voltages are within limits
26	High Wind High Load	Figure E-51 and E-52	System is stable Line loadings and bus voltages are within limits During the fault, the frequency goes outside the 1% band twice but damps out after 1 s of fault.
Partial generator outage at Waingapu Bus. The fault is created at 1 s, and it does not clear.			
<u>27</u>	No Wind High Load	Figure E-53 and E-54	System is unstable After the fault, the frequency keeps dropping, and a frequency runaway is observed. In this case, there is insufficient headroom in the dispatched generators.

Case #	Scenarios	Exhibit #	Observations
28	High Wind High Load	Figure E-55 and E-56	System is unstable After the fault, the frequency keeps dropping, and a frequency runaway is observed. In this case, there is insufficient headroom in the dispatched generators.
Load loss at Haharu Bus. The fault is created at 1 s, and it self-clears at 1.18 s.			
29	No Wind High Load	Figure E-57 and E-58	System is stable Line loadings, voltages, and frequency are well within limits
30	No Wind Low Load	Figure E-59	System is stable Line loadings, voltages, and frequency are well within limits
31	High Wind High Load	Figure E-60 and E-61	System is stable Line loadings, voltages, and frequency are well within limits
32	High Wind Low Load	Figure E-62 and E-63	System is stable Line loadings, voltages, and frequency are well within limits
Load loss at Haharu Bus. The fault is created at 1 s, and it does not clear.			
33	No Wind High Load	Figure E-64 and E-65	System is stable Line loadings, voltages, and frequency are well within limits
34	No Wind Low Load	Figure E-66	System is stable Line loadings, voltages, and frequency are well within limits
35	High Wind High Load	Figure E-67 and E-68	System is stable Line loadings, voltages, and frequency are well within limits
36	High Wind Low Load	Figure E-69 and E-70	System is stable Line loadings, voltages, and frequency are well within limits
Load loss at Kambajawa Bus. The fault is created at 1 s, and it self-clears at 1.18 s.			
37	No Wind High Load	Figure E-71 and E-72	System is stable Line loadings, voltages, and frequency are well within limits
38	No Wind Low Load	Figure E-73	System is stable Line loadings, voltages, and frequency are well within limits

Case #	Scenarios	Exhibit #	Observations
39	High Wind High Load	Figure E-74 and E-75	System is stable Line loadings, voltages, and frequency are well within limits
40	High Wind Low Load	Figure E-76 and E-77	System is stable Line loadings, voltages, and frequency are well within limits
Load loss at Kambajawa Bus. The fault is created at 1 s, and it does not clear.			
41	No Wind High Load	Figure E-78 and E-79	System is stable Line loadings, voltages, and frequency are well within limits
42	No Wind Low Load	Figure E-80	System is stable Line loadings, voltages, and frequency are well within limits
43	High Wind High Load	Figure E-81 and E-82	System is stable Line loadings, voltages, and frequency are well within limits
44	High Wind Low Load	Figure E-83 and E-84	System is stable Line loadings, voltages, and frequency are well within limits
Load loss at Waingapu Bus. The fault is created at 1 s, and it self-clears at 1.18 s.			
45	No Wind High Load	Figure E-85 and E-86	System is stable Line loadings, voltages, and frequency are well within limits
46	No Wind Low Load	Figure E-87	System is stable Line loadings, voltages, and frequency are well within limits
47	High Wind High Load	Figure E-88 and E-89	System is stable Line loadings, voltages, and frequency are well within limits
48	High Wind Low Load	Figure E-90 and E-91	System is stable Line loadings, voltages, and frequency are well within limits
Load loss at Waingapu Bus. The fault is created at 1 s, and it does not clear.			
49	No Wind High Load	Figure E-92 and E-93	System is stable Line loadings, voltages, and frequency are well within limits
50	No Wind Low Load	Figure E-94	System is stable Line loadings, voltages, and frequency are well within limits
51	High Wind High Load	Figure E-95 and E-96	System is stable Line loadings, voltages, and frequency are well within limits

Case #	Scenarios	Exhibit #	Observations
52	High Wind Low Load	Figure E-97 and E-98	System is stable Line loadings, voltages, and frequency are well within limits
Short-circuit at Kambajawa-Haharu Transmission Line. The fault is created at 1 s, and it clears in 180 ms.			
53	No Wind High Load	Figure E-99 and E-100	There is islanding of Haharu; the Haharu load will go offline for 180 ms. After the fault clears, the system is stable. The frequency drops to 0.97 p.u., which is outside the acceptable range, for less than 4 s and then returns to a normal level.
54	No Wind Low Load	Figure E-101	There is islanding of Haharu; the Haharu load will go offline for 180 ms. After the fault clears, the system is stable. The frequency drops to 0.97 p.u., which is outside the acceptable range, for less than 4 s and then returns to a normal level.
55	High Wind High Load	Figure E-102 and E-103	There is islanding of Haharu; the Haharu load will go offline for 180 ms. Frequency drops to 0.97 p.u., which is outside the acceptable range, for less than 4 s and then returns to a normal level WTG stays connected
56	High Wind Low Load	Figure E-104 and E-105	There is islanding of Haharu; the Haharu load will go offline for 180 ms. Frequency drops to 0.97 p.u., which is outside the acceptable range, for less than 4 s and then returns to a normal level WTG stays connected
Short-circuit at Kambajawa-Haharu Transmission Line. The fault is created at 1 s, and it does not clear.			
<u>57</u>	No Wind High Load	Figure E-106 and E-107	Relays are not modeled, therefore a sustained short-circuit fault on the transmission line causes a loss of synchronism.
58	No Wind Low Load	Figure E-108	Relays are not modeled, therefore a sustained short-circuit fault on the transmission line causes a loss of synchronism.

Case #	Scenarios	Exhibit #	Observations
59	High Wind High Load	Figure E-109 and E-110	Relays are not modeled, therefore a sustained short-circuit fault on the transmission line causes a loss of synchronism. WTG shuts down
60	High Wind Low Load	Figure E-111 and E-112	Relays are not modeled, therefore a sustained short-circuit fault on the transmission line causes a loss of synchronism. WTG shuts down
Short-circuit at Kambajawa-Waingapu Transmission Line. The fault is created at 1 s, and it self-clears in 180 ms.			
61	No Wind High Load	Figure E-113 and E-114	There is islanding of Waingapu After the fault clears, system is stable Line loadings, voltages, and frequency are within limits
62	No Wind Low Load	Figure E-115	There is islanding of Waingapu; the Waingapu load will go offline for 180 ms. After the fault clears, system is not stable Voltages at all the buses go to zero System loses synchronism
63	High Wind High Load	Figure E-116 and E-117	There is islanding of Waingapu After the fault clears, system is stable Line loadings, voltages, and frequency are within limits
64	High Wind Low Load	Figure E-118 and E-119	There is islanding of Waingapu After the fault clears, system is stable Line loadings, voltages, and frequency are within limits
Short-circuit at Kambajawa-Waingapu Transmission Line. The fault is created at 1 s, and it does not clear.			
65	No Wind High Load	Figure E-120 and E-121	Relays are not modeled, therefore a sustained short-circuit fault on the transmission line causes a loss of synchronism.
66	No Wind Low Load	Figure E-122	Relays are not modeled, therefore a sustained short-circuit fault on the transmission line causes a loss of synchronism.
67	High Wind High Load	Figure E-123 and E-124	Relays are not modeled, therefore a sustained short-circuit fault on the transmission line causes a loss of synchronism.

Case #	Scenarios	Exhibit #	Observations
68	High Wind Low Load	Figure E-125 and E-126	Relays are not modeled, therefore a sustained short-circuit fault on the transmission line causes a loss of synchronism.

3.5 Analysis of the System with the Addition of Storage

The scope of this study included an analysis of storage as a method to overcome the instability of the East Sumba system with the integration of one or two 850-kW WTGs. ABB's PowerStore energy storage (ES) system is used in the analysis. A control model provided by ABB for the ES system was used. It was modeled as a current source, and it independently and instantaneously controls active (I_R) and reactive (I_I) components of the current. The active power-frequency (P-f) controller and reactive power-voltage (Q-V) controller take as input grid frequency and terminal voltage and produce active and reactive current components. The active power-frequency controller provides inertial (rate of change of frequency) and droop (change of frequency) supports. Two types of ES units are available in the PowerStore: Flywheel and Li-ion battery.

Note that even without a WTG on the grid, most of the scenarios cause instability, as shown in the trip report for 2014 (provided by PLN), which indicates that the number of blackouts and trip is high (about one per day). Preliminary analysis of the trip report suggests that this is because of the following reasons: (1) the faults do not clear within the specified setting time of the circuit breakers, (2) generators are dispatched with low headroom (low spinning reserves), (3) a lack of vegetation management causes overhang on the transmission lines, and (4) the fleet of diesel generators is old. Independent of the introduction of 850-kW WTGs, improvements to (1)–(4) and the introduction of storage will reduce the number of blackouts and trips and thereby improve the reliability of the system.

For the dynamic analysis with storage, the following parameter were assumed:

- A 550-kW CAT C32 diesel generator at the Waingapu station is available as a backup generator with an auto-start switch. One or more such generators may be required.
- There is a basic supervisory control system that monitors disturbances and sends an auto-start signal to the backup generator above for a predefined list of disturbances (system parameters).
- The backup generator has a cold-start time of 10 s, which means that it is able to start, synchronize with the grid, and deliver full power within 10 s.

The primary utility of storage analyzed in the scenarios is the delivery of energy during the time gap between the occurrence of a disturbance and start of the reserve generator. The other well-known utility of short-duration storage is to smooth out the short-term variability of wind power and smooth out the load on the diesel generators during ramping up and down of wind power. For 850 kW of wind power in East Sumba, the current set of diesel generators (with assumed inertia, automatic voltage regulation, and governor models) is able to manage the variability and ramping needs (analysis results shown in Appendix E, Figures E-127 to E-136). However, note that the age of the generators strongly suggests that additional variability beyond that caused by

current load variations may lead to higher scheduled and unscheduled maintenance. Therefore, the addition of storage would add to the reliability and resiliency of the grid.

Table 15 contains results of the stability study of different scenarios after the addition of a storage unit. This analysis was conducted by the ABB consulting office in Madrid. The full report is attached as Appendix F.

To determine the optimal size of the storage unit, the following information was used: (1) the amount of power required to replace the loss of generation during a major fault in the system and the available rotating inertia in the system, and (2) the length of time the power should be supplied until the backup generation is online. The following illustration is for a single 850-kW WTG. The same process was conducted for two WTGs.

1. The critical fault considered in this study was the loss of a WTG (850 kW). The headroom available from the scheduled generators during the high and low load scenarios was 597.8 kW and 377.3 kW, respectively. That is, the dispatched generators were able to increase their power output by an amount equal to the headroom. Therefore, there was a gap of 252.1 kW and 472 kW in the high and low load scenarios, respectively, that must be supplied by the storage unit to stabilize the system. Hence, a storage unit with a power capacity of 500 kW was chosen.
2. To determine how long the unit would need to supply this power, the cold-start time of the backup generator needed to be considered. As indicated, a backup generator with a “rated” cold-start time of 10 s was used. Because this generator was 15 years old, the cold-start time was stretched to 30 s, which included the times for cold-start, synchronization, and ramping up to full capacity. The energy capacity of the storage unit was

$$500 \text{ kW} \times (30/3600) \text{ hours} = 4.17 \text{ kWh}$$

The size of the storage unit for integrating two 850-kW WTGs at the Haharu Bus in the eastern grid of Sumba is described below.

1. The critical fault considered in this study was the loss of both WTGs (1,700 kW). Based on the available headroom and the assumption that the storage units are sold in increments of 500 kW, a storage unit with a total power capacity of 1,500 kW was chosen.
2. To determine how long the storage unit would need to supply this power, the 10-s cold-start backup generator was supplemented with other backup generators with 60-s start-up times. Considering this situation, the storage supply’s energy content should be for 60 s:

$$1,500 \text{ kW} \times (60/3600) \text{ h} = 25 \text{ kWh}$$

Therefore, an energy storage unit with a power and energy capacity of 500 kW and 4.17 kWh, respectively, for the case of integrating a single WTG and 1,500 kW and 25 kWh, respectively, for the case of integrating two WTGs were chosen. The selection of the storage (flywheel, battery technology—lithium-ion [Li-ion], lead acid, or other chemistry) and detailed specification and sizing of the storage are not within the scope of this project. The above specified ratings are the requirement for storage; however, note that commercially available

storage units of 500 kW and 1,500 kW will have much larger energy content. For example, the Beacon Flywheel of 500 kW has an energy content of 50 kWh, a SAFT IM20P Li-ion 500-kW battery has an energy content of approximately 160 kWh, the Beacon Flywheel of 1,500 kW has an energy content of 150 kWh, and a SAFT IM20P Li-ion 1,500-kW battery has an energy content of approximately 500 kWh.

Figure 11. Power flow display: high load with WTG and PowerStore. MTU1 = slack bus

The figures mentioned in Table 15 for cases 1 to 6 are contained in Appendix F, the dynamic system impact study conducted by ABB. Figures for cases 7 to 10 are contained in Appendix E, the dynamic system impact study conducted by IWE.

Table 15. Scenarios and Observations for the Dynamic System Impact Analysis with Storage (ABB PowerStore)

Case #	Scenarios	Exhibit #	Observations
Loss of Diesel Generator (650 kW)			
1	High Wind High Load	Figure 4 (Appendix F)	<p>The stability support equipment supplies power (400 kW) for 10 s, until the designated generator CAT C32 comes into operation and stabilizes the system.</p> <p>The frequency and voltage fall but are stabilized to an acceptable value.</p> <p>The system is stable.</p>
2	High Wind Low Load	Figure 7 (Appendix F)	<p>The stability support equipment supplies power (400 kW) for 10 s, until the designated generator CAT C32 comes into operation and stabilizes the system.</p> <p>The frequency and voltage fall but are stabilized to an acceptable value.</p> <p>Without the use of the stability support equipment, the system does not withstand the fault because the frequency drops so sharply that the WTG is also lost, and there is not enough time to put the backup generator into service.</p>
Load Loss			
3	High Wind High Load	Figure 5 (Appendix F)	<p>The loss of the largest load (3,494 kW) is simulated, then the stability support equipment absorbs power (200 kW) for 10 s and stabilizes the system, so the system is stable for this case.</p> <p>The use of the stability support equipment is not decisive for the system stability of this case because the generators quickly change their operating point.</p>

Case #	Scenarios	Exhibit #	Observations
4	High Wind Low Load	Figure 8 (Appendix F)	<p>The loss of the largest load (1,691 kW) is simulated, then the stability support equipment absorbs power (330 kW) for 10 s and stabilizes the system, so the system is stable for this case.</p> <p>The use of the stability support equipment is not decisive for the system stability of this case because the generators quickly change their operating point.</p>
Loss of Wind Generator (850 kW)			
5	High Wind High Load	Figure 6 (Appendix F)	<p>The stability support equipment supplies power (400 kW) for 10 s, until the backup generators start and stabilize the system.</p> <p>Without the use of the stability support equipment, the system is not stable because the frequency drops so sharply that the backup generator does not have enough power to compensate for the loss of generation and stabilize the system frequency.</p>
6	High Wind Low Load	Figure 9 (Appendix F)	<p>The stability support equipment supplies power (500 kW) for 10 s, until the backup generator starts and stabilizes the system.</p> <p>Without the use of the stability support equipment, the system is not stable because the frequency drops so sharply that the backup generator does not have enough power to compensate for the loss generation and stabilize the system frequency.</p>
Random output of WTG			
7	High Wind High Load	Figure E-127, E-128 and E-129	<p>Randomness in the output of the WTG causes the output of the diesel generators to vary by 5% for the generator sets that have no headroom and close to 10% for generator set that has headroom. The difference is provided by PowerStore. The frequency and voltage variations are within range.</p>
8	High Wind Low Load	Figure E-130 and E-131	<p>Randomness in the output of the WTG causes the output of the two diesel generators to vary by 2.5%. (The generator sets have no headroom.) The difference is provided by PowerStore. The frequency and voltage variations are within range.</p>

Case #	Scenarios	Exhibit #	Observations
Ramping down of WTG output			
9	High Wind High Load	Figure E-132, E-133 and E-134	During the ramping down of the WTG output, the diesel generator set that has headroom and PowerStore share in ramping up the power output.
10	High Wind Low Load	Figure E-135 and E-136	During the ramping down of the WTG output, the diesel generator set that has headroom and PowerStore share in ramping up the power output. After 18 s, the diesel generator set reaches its peak output, after which PowerStore provides the full ramp-up.

The system was found unstable under the following fault scenarios as well: a short circuit at the Kambajawa-Haharu Transmission Line with no clearing and a short circuit at the Kambajawa-Waingapu Transmission Line with no clearing. If the fault does not clear in 180 ms, the system loses its synchronism. To resolve this issue, the protection relays need to be programmed to isolate the fault.

3.6 Scenarios for the Integration of Two 850-kW Wind Turbine Generators

The figures mentioned in Table 16 are contained in Appendix G. The values contained in the graphs are summarized below.

Table 16. Scenarios and Observations for Dynamic System Impact Analysis for the Integration of Two WTGs

Case #	Scenarios	Exhibit #	Observations
Three-phase-to-ground fault at Kambajawa Bus. The fault was created at 1 s, and it self-clears at 1.18 s.			
1	High Wind High Load	Figure G-1, G-2 and G-3	System is stable Line loadings are within limits Low-voltage ride-through capability of the WTG prevents it from going offline WTG recovers to normal operation quickly after the fault clears
2	High Wind Low Load	Figure G-4 and G-5	System is stable Line loadings are within limits Low-voltage ride-through capability of the WTG prevents it from going offline WTG recovers to normal operation quickly after the fault clears

Case #	Scenarios	Exhibit #	Observations
3	High Wind High Load With PowerStore	Figure G-6 and G-7	System is stable Line loadings are within limits. Terminal voltage and power outputs of generators are stable PowerStore supplies power during the fault
4	High Wind Low Load With PowerStore	Figure G-8 and G-9	System is stable Line loadings are within limits Bus voltages dip below 0.50 p.u. at the H and W buses PowerStore supplies power during the fault, when the WTGs are down
Three-phase-to-ground fault at Waingapu Bus. The fault was created at 1 s, and it self-clears at 1.18 s.			
5	High Wind High Load	Figure G-10, G-11 and G- 12	System is stable Line loadings are within limits Low-voltage ride-through capability of the WTG prevents it from going offline WTG recovers to normal operation quickly after the fault clears
6	High Wind Low Load	Figure G-13 and G-14	System is stable Line loadings are within limits Low-voltage ride-through capability of the WTG prevents it from going offline WTG recovers to normal operation quickly after the fault clears
7	High Wind High Load With PowerStore	Figure G-15 and G-16	System is stable Line loadings are within limits. Terminal voltage and power outputs of generators are stable PowerStore supplies power during the fault
8	High Wind Low Load With PowerStore	Figure G-17 and G-18	System is stable Line loadings are within limits Bus voltages dip below 0.50 p.u. at the H and W buses PowerStore supplies power during the fault, when the WTGs are down
Outage of two WTGs. The fault is created at 1 s, and it does not clear.			
<u>9</u>	High Wind High Load	Figure G-19, G-20 and G- 21	The frequency keeps falling after the fault, and there is a loss of synchronism in the system. This is expected, because the loss of two 850-kW WTGs with no self-clearing is a large loss of generation from which the grid cannot recover.

Case #	Scenarios	Exhibit #	Observations
10	High Wind Low Load	Figure G-22 and G-23	The frequency keeps falling after the fault, and there is a loss of synchronism in the system. This is expected, because the loss of two 850-kW WTGs with no self-clearing is a large loss of generation from which the grid cannot recover.
11	High Wind High Load With PowerStore	Figure G-24 and G-25	<p>PowerStore supplies power when the two 0.85-MW WTGs go down. It supplies approximately 1.5 MW of active power until the designated generator, CAT C32, starts supplying 0.55 MW of power at 10 s. This reduces the contribution of PowerStore to 0.95 MW.</p> <p>After 30 s, when the PowerStore is depleted, there is a frequency runaway because there is a large loss of power.</p> <p>To prevent a frequency runaway, two additional CAT C32 generators of 0.55-kW capacity with 10-s cold-start times are required in reserve, or a plan to implement load shedding in such cases is required.</p>
12	High Wind Low Load With PowerStore	Figure G-26 and G-27	<p>PowerStore supplies power when the two 0.85-MW WTGs go down. It supplies approximately 1.8 MW of active power until the designated generator, CAT C32, starts supplying 0.55 MW of power at 10 s. This reduces the contribution of PowerStore to 1.2 MW.</p> <p>After 30 s, when the PowerStore is depleted, there is a frequency runaway because there is a large loss of power.</p> <p>To prevent a frequency runaway, two additional CAT C32 generators with capacities of 0.55 kW and 10-s cold-start times are required in reserve, or a plan to implement load shedding in such cases is required.</p>
Generator outage at Kambajawa Bus. The fault was created at 1 s, and it does not clear.			
13	High Wind High Load	Figure G-28, G-29 and G-30	<p>A frequency runaway is observed because the system loses 650 kW of generation.</p> <p>Not enough headroom is available to compensate for this loss.</p> <p>Because of this, the frequency falls for 10 s by an amount large enough to cause the WTGs to disconnect. This results in a loss of power of 2.35 MW in the system.</p> <p>So when the CAT C32 generator starts supplying power at 10 s, the generator is not able to synchronize, and the system as a whole loses synchronism.</p>

Case #	Scenarios	Exhibit #	Observations
14	High Wind Low Load	Figure G-31 and G-32	<p>A frequency runaway is observed because the system loses 420 kW of generation.</p> <p>There is not enough headroom available to compensate for this loss.</p> <p>Because of this, the frequency falls for 10 s by an amount large enough to cause the WTGs to disconnect. This results in a loss of power of 2.35 MW in the system.</p> <p>So when the CAT C32 generator starts supplying power at 10 s, the generator is not able to synchronize, and the system as a whole loses synchronism.</p>
15	High Wind High Load With PowerStore	Figure G-33 and G-34	<p>At the fault, the PowerStore starts supplying approximately 600 kW.</p> <p>This stabilizes the system until the reserve generator, CAT C32, starts supplying power at 10 s.</p> <p>At 30 s, when the PowerStore shut down, the system is still stable.</p>
16	High Wind Low Load With PowerStore	Figure G-35 and G-36	<p>At the fault, the PowerStore starts supplying approximately 500 kW.</p> <p>This stabilizes the system until the reserve generator, CAT C32, starts supplying power at 10 s.</p> <p>There is enough power generation available in the system to compensate for this loss.</p>
Load loss at Kambajawa Bus. The fault was created at 1 s, and it does not clear.			
17	High Wind High Load	Figure G-37, G-38 and G-39	<p>A load of 3.494 MW is lost at 1 s at the Kambajawa Bus.</p> <p>The bus frequency increases to 1.04 p.u. and bus voltages by 0.02 p.u., but overall the system stable.</p> <p>As shown, the generators reduce their generation by 60%–70% of their initial value. In reality, the diesel generator sets would be disconnected to attain stability.</p>
18	High Wind Low Load	Figure G-40 and G-41	<p>A load of 1.691 MW is lost at 1 s at Kambajawa Bus.</p> <p>The bus frequency and bus voltages increase by a very small value, but overall the system is stable.</p> <p>As shown, the generators reduce their generation and reach a negative value. In reality, the diesel generator sets would be disconnected to attain stability.</p>

Case #	Scenarios	Exhibit #	Observations
19	High Wind High Load With PowerStore	Figure G-42 and G-43	<p>A load of 3.494 MW is lost at 1 s at Kambajawa Bus.</p> <p>The bus frequency increases to 1.04 p.u., but overall the system is stable. Because there is PowerStore in the system, it starts absorbing at 1 s.</p> <p>As shown, the generators reduce their generation by 60%–70% of their initial value when the PowerStore shuts down at 30 s.</p> <p>In reality, the diesel generator sets would be disconnected to attain stability.</p>
20	High Wind Low Load With PowerStore	Figure G-44 and G-45	<p>A load of 1.691 MW is lost at 1 s at Kambajawa Bus.</p> <p>The bus frequency and bus voltages increase by a very small value, but overall the system is stable.</p> <p>PowerStore in the system starts absorbing at 1 s.</p> <p>In reality, the diesel generator sets would be disconnected to attain stability.</p>
Kambajawa-Haharu Transmission Line fault. The fault was created at 1 s, and it self-clears at 1.18 s.			
21	High Wind High Load	Figure G-46, G-47 and G-48	<p>Islanding of Haharu is occurring, and the Haharu load goes offline for 180 ms.</p> <p>After clearing the fault, the system is stable—line loadings, voltages, and frequency are within limits.</p>
22	High Wind Low Load	Figure G-49 and G-50	<p>Islanding of Haharu is occurring, and the Haharu load goes offline for 180 ms.</p> <p>After clearing the fault, the system is stable—line loadings, voltages, and frequency are within limits.</p>
23	High Wind High Load With PowerStore	Figure G-51 and G-52	<p>Islanding of Haharu is occurred, and the Haharu load goes offline for 180 ms.</p> <p>After clearing the fault, the system is stable—line loadings, voltages, and frequency are within limits.</p> <p>PowerStore supplies power as the WTGs recover from the low-voltage ride-through.</p>
24	High Wind Low Load With PowerStore	Figure G-53 and G-54	<p>Islanding of Haharu is occurring, and the Haharu load goes offline for 180 ms.</p> <p>After clearing the fault, the system is stable—line loadings, voltages, and frequency are within limits.</p> <p>PowerStore supplies power as the WTGs recover from the low-voltage ride-through.</p>

4 Conclusions

The East Sumba grid was modeled for load flow, short-circuit, and transient analyses.

The load flow analysis suggests that in the baseline and in the case with one WTG, there is no overloading of generators, no overloading of conductors, and all of the bus voltages are within range.

The short-circuit analysis suggests that the short-circuit power ratio is comfortably above the minimum requirement at the Haharu Bus—the point of common coupling of the WTG. In addition, because the short-circuit power contribution of the WTG is small, the ratings of the devices in the substations are not impacted.

The transient stability study conducted to analyze the impact of integrating one 850-kW WTG onto the grid identified transient scenarios with stability issues. Adding storage to the grid along with a backup generator, a hybrid controller, and high-speed communications within the network would ensure stability of the system. Storage equipment with at least 500 kW of capacity and 4.17 kWh of energy would be adequate to ensure stability. In addition to storage, a diesel generator, CAT C32, of 550 kW with a cold-start time of 10 s should be designated as a backup generator. It should be controlled by a hybrid plant controller that manages all the diesel generators, the WTG, and the storage unit based on network parameters, wind production, the state of charge of the storage unit, and other factors. This would also require high-speed communications between the hybrid plant controller and all controllable units on the network.

In conclusion, installing one 850-kW WTG in East Sumba with a 500-kW (with at least 4.17-kWh) storage unit, 550-kW backup diesel generator set with 10-s cold-start time, hybrid power plant controller, and high-speed communications in the network is a solution that will improve the reliability of the energy supply, enhance the stability of the system, and reduce greenhouse gas emissions.

Introducing two 850-kW WTGs would require adding storage equipment of 1,500 kW, which is slightly below the power rating of the two turbines. The energy content was designed to be 60 s, which is sufficient time to start the backup diesel generators. In addition to storage, one CAT C32 diesel generator with a capacity of 550 kW and cold-start time of 10 s and other generators with a total of 950 kW of power with 60-s cold-start times should be designated as backup generators. Note that increasing wind power from 850 kW to 1,700 kW leads to a substantial increase in storage and backup generation, which would incur significantly higher costs to grid upgrades (storage, backup generators, and hybrid controller). It is recommended that as a first step only one 850-kW should be integrated onto the grid. After all the setup issues are resolved, an updated set of data should be collected, and the technical grid integration analysis for the two-turbine scenario should be run again. Options such as colocating the second turbine in the same region as the first or choosing a different location should be evaluated. The new data set and experience gained from the first integration will allow higher fidelity modeling of the grid with more than one WTG.

5 References

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Appendix A: Load Flow, Short-Circuit, and Dynamic Model Data

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Table A-1. Input Data of Generators

Particulars	kVA Rating	Rated Voltage (kV)	PF	Connection	Xn	X0	Xd	Xd''	Xd'	Xq	Xq'	Xq''
Volvo	220	0.4	0.8	YN	0.16	0.009	3.36	0.135	0.193	2.01	2.01	0.184
MTU1	650	0.4	0.8	YN	0.175	0.037	3.81	0.155	0.282	2.290	2.290	0.195
MAN1	430	0.4	0.8	YN	0.152	0.009	3.43	0.14	0.175	2.05	2.05	0.163
MTU2	430	0.4	0.8	YN	0.152	0.009	3.43	0.14	0.175	2.05	2.05	0.163
MTU4	430	0.4	0.8	YN	0.152	0.009	3.43	0.14	0.175	2.05	2.05	0.163
MAN2	320	0.4	0.8	YN	0.152	0.026	3.12	0.106	0.194	1.65	1.65	0.171
DOOSAN1	420	0.4	0.8	YN	0.12	0.006	2.839	0.101	0.129	1.267	1.267	0.14
DOOSAN2	420	0.4	0.8	YN	0.12	0.006	2.839	0.101	0.129	1.267	1.267	0.14
DOOSAN3	420	0.4	0.8	YN	0.12	0.006	2.839	0.101	0.129	1.267	1.267	0.14
DOOSAN4	420	0.4	0.8	YN	0.12	0.006	2.839	0.101	0.129	1.267	1.267	0.14
DOOSAN5	420	0.4	0.8	YN	0.12	0.006	2.839	0.101	0.129	1.267	1.267	0.14
CAT	550	0.4	0.8	YN	0.175	0.037	3.81	0.1475	0.2188	2.290	2.290	0.195
YANMAR	220	6.3	0.8	YN	0.16	0.009	3.36	0.135	0.193	2.01	2.01	0.184
DEUTZ1	180	0.4	0.8	YN	0.19	0.11	3.27	0.13	0.18	2.66	2.66	0.26
DEUTZ2	180	0.4	0.8	YN	0.19	0.11	3.27	0.13	0.18	2.66	2.66	0.26
SWD3	220	6.3	0.8	YN	0.16	0.009	3.36	0.135	0.193	2.01	2.01	0.184
SWD2	220	6.3	0.8	YN	0.16	0.009	3.36	0.135	0.193	2.01	2.01	0.184
SWD1	220	6.3	0.8	YN	0.16	0.009	3.36	0.135	0.193	2.01	2.01	0.184

Table A-2. Input Data of Transformers

Sl. No.	kVA Capacity	Primary/Secondary Voltage in kV	Tap Changer, Voltage per Tap	% Positive-Sequence Impedance (z1)	% Zero-Sequence Impedance (z0)	X/R Ratio	Winding Configuration
T1	750	0.4/20	2.50%	4.5	10.2 p.u.	3.5	YN5d, star grounded
T2	750	0.4/20	2.50%	4.5	10.2 p.u.	3.5	YN5d, star grounded
T3	630	0.4/20	2.50%	4	10 p.u.	3.7	YN5d, star grounded
T4	1600	0.4/20	2.50%	6	6	4.95	YN5d, star grounded
T5	1600	0.4/20	2.50%	6	6	4.95	YN5d, star grounded
T6	1000	0.4/20	2.50%	5	11 p.u.	4	YN5d, star grounded
T7	630	0.4/20	2.50%	4	10 p.u.	3.7	YN5d, star grounded
T8	315	0.4/20	2.50%	4	10 p.u.	3.3	YN5d, star grounded
T11	400	0.4/20	2.50%	4	10 p.u.	3.3	YN5d, star grounded
T12	1250	6.3/20	2.50%	5.5	12 p.u.	4.5	YN5d, star grounded
T13	315	0.4/20	2.50%	4	10	3.3	YN5d, star grounded
T14	1000	0.4/20	2.50%	5	11 p.u.	4	YN5d, star grounded
T16	900	0.69/20	2.50%	6.14	6.14	4.5	d11YN, star grounded

Table A-3. Input Data of Transmission Lines

Transmission Line	K-H2 TLine: Haharu–MHaharu	K-H1 TLine: MHaharu–Kambajawa	K-W Tline: Kambajawa–Waingapu
Voltage (kV)	20	20	20
Length (Km)	18	7	7
Rated current (kA)	0.129	0.210	0.323
Zero-sequence resistance (Ohms/Km)	1.106	0.813	0.373
Zero-sequence reactance (Ohms/Km)	1.884	1.87	1.835
Positive-sequence resistance (Ohms/Km)	0.958	0.665	0.225
Positive-sequence reactance (Ohms/Km)	0.39	0.37	0.30
Negative-sequence resistance (Ohms/Km)	0.958	0.665	0.225
Negative-sequence reactance (Ohms/Km)	0.39	0.37	0.30
Positive-sequence susceptance ($\mu\text{S}/\text{Km}$)	0.56	1.4	1.66
Zero-sequence susceptance ($\mu\text{S}/\text{Km}$)	0.56	1.43	1.71

Appendix B: Steady-State and Short-Circuit Model in Power Factory—Input Data

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Generators

- 180-kW generator = DEUT Z-1, DEUT Z-2
- 220 kW–0.4 kV = Volvo
- 220-kW generator = SWD1, SWD2, SWD3, YANMAR
- 320-kW generator = MAN2
- 420-kW generator = DOOSAN1, DOOSAN2, DOOSAN3, DOOSAN4, DOOSAN5
- 430-kW generator = MAN1, MAN2, MTU2, MTU4
- 550-kW generator = CAT C32
- 650-kW generator = MTU1
- WTG01 = Wind turbine generator

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 402
180kWGen	Synchronous Machine Type	1	/8
Stator Resistance		0.0065	p.u.
rstr			
rs(f)			
Subtransient Reactances		0.1300	p.u.
xd''		0.2000	p.u.
xq''			
l''(f)			
Zero Sequence Data		0.1100	p.u.
Reactance x0			
l0(f)			
Resistance r0		0.0000	p.u.
r0(f)			
Consider Transient Parameter	No		
Negative Sequence Data		0.1900	p.u.
Reactance x2			
l2(f)			
Resistance r2		0.0000	p.u.
r2(f)			
Subtransient Reactances			
Use saturated value	No		
Inrush Peak Current		10.0000	p.u.
Ratio Ip/In		0.0200	s
Max. Time			
Stall Time		20.0000	s
Cold		10.0000	s
Hot			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/12/2015 4:09:05 PM	
Modified by	pramod		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 403
220kw-0.4kv	Synchronous Machine Type	2	/8
Stator Resistance		0.0000	p.u.
rstr			
rs(f)			

Subtransient Reactances			
xd''		0.1350	p.u.
xq''		0.2000	p.u.
l''(f)			
Zero Sequence Data			
Reactance x0		0.0090	p.u.
l0(f)			
Resistance r0		0.0000	p.u.
r0(f)			
Consider Transient Parameter	No		
Negative Sequence Data			
Reactance x2		0.1600	p.u.
l2(f)			
Resistance r2		0.0000	p.u.
r2(f)			
Subtransient Reactances			
Use saturated value	No		
Inrush Peak Current			
Ratio Ip/In		10.0000	p.u.
Max. Time		0.0200	s
Stall Time			
Cold		20.0000	s
Hot		10.0000	s
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/12/2015 6:30:48 PM	
Modified by	pramod		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 404
220kWGen	Synchronous Machine Type	3	/8
Stator Resistance			
rstr		0.0000	p.u.
rs(f)			
Subtransient Reactances			
xd''		0.1350	p.u.
xq''		0.2000	p.u.
l''(f)			
Zero Sequence Data			
Reactance x0		0.0090	p.u.
l0(f)			
Resistance r0		0.0000	p.u.
r0(f)			
Consider Transient Parameter	No		
Negative Sequence Data			
Reactance x2		0.1600	p.u.
l2(f)			
Resistance r2		0.0000	p.u.
r2(f)			
Subtransient Reactances			
Use saturated value	No		
Inrush Peak Current			
Ratio Ip/In		10.0000	p.u.
Max. Time		0.0200	s
Stall Time			
Cold		20.0000	s
Hot		10.0000	s
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015 2:28:52 PM	
Modified by	pramod		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 405
320kWGen	Synchronous Machine Type	4	/8
Stator Resistance		0.0130	p.u.
rstr			
rs(f)			
Subtransient Reactances		0.1060	p.u.
xd''			
xq''		0.2000	p.u.
l''(f)			
Zero Sequence Data			
Reactance x0		0.0260	p.u.
l0(f)			
Resistance r0		0.0000	p.u.
r0(f)			
Consider Transient Parameter	No		
Negative Sequence Data			
Reactance x2		0.1520	p.u.
l2(f)			
Resistance r2		0.0000	p.u.
r2(f)			
Subtransient Reactances			
Use saturated value	No		
Inrush Peak Current			
Ratio Ip/In		10.0000	p.u.
Max. Time		0.0200	s
Stall Time			
Cold		20.0000	s
Hot		10.0000	s
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		4/12/2015 3:45:57 PM	
Modified by	pramod		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 406
420kWGen	Synchronous Machine Type	5	/8
Stator Resistance		0.0000	p.u.
rstr			
rs(f)			
Subtransient Reactances		0.1010	p.u.
xd''			
xq''		0.2000	p.u.
l''(f)			
Zero Sequence Data			
Reactance x0		0.0060	p.u.
l0(f)			
Resistance r0		0.0000	p.u.
r0(f)			
Consider Transient Parameter	No		
Negative Sequence Data			
Reactance x2		0.1200	p.u.
l2(f)			
Resistance r2		0.0000	p.u.
r2(f)			
Subtransient Reactances			
Use saturated value	No		
Inrush Peak Current			
Ratio Ip/In		10.0000	p.u.
Max. Time		0.0200	s
Stall Time			
Cold		20.0000	s
Hot		10.0000	s
Manufacturer			
Characteristic Name			

Data source	MAN	
Foreign Key		
Additional Data		
Description		
Approval Information		
Status	Not Approved	
Modified		3/11/2015 3:49:05 PM
Modified by	pramod	

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 407
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430kWGen	Synchronous Machine Type	6	/8
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Stator Resistance		
rstr	0.0000	p.u.
rs(f)		
Subtransient Reactances		
xd''	0.1400	p.u.
xq''	0.2000	p.u.
l''(f)		
Zero Sequence Data		
Reactance x0	0.0090	p.u.
l0(f)		
Resistance r0	0.0000	p.u.
r0(f)		
Consider Transient Parameter	No	
Negative Sequence Data		
Reactance x2	0.1520	p.u.
l2(f)		
Resistance r2	0.0000	p.u.
r2(f)		
Subtransient Reactances		
Use saturated value	No	
Inrush Peak Current		
Ratio Ip/In	10.0000	p.u.
Max. Time	0.0200	s
Stall Time		
Cold	20.0000	s
Hot	10.0000	s
Manufacturer		
Characteristic Name		
Data source	MAN	
Foreign Key		
Additional Data		
Description		
Approval Information		
Status	Not Approved	
Modified		3/11/2015 2:58:06 PM
Modified by	pramod	

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 408
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550kWGen	Synchronous Machine Type	7	/8
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Stator Resistance		
rstr	0.0000	p.u.
rs(f)		
Subtransient Reactances		
xd''	0.1475	p.u.
xq''	0.2000	p.u.
l''(f)		
Zero Sequence Data		
Reactance x0	0.0370	p.u.
l0(f)		
Resistance r0	0.0000	p.u.
r0(f)		
Consider Transient Parameter	No	
Negative Sequence Data		
Reactance x2	0.1750	p.u.
l2(f)		
Resistance r2	0.0000	p.u.
r2(f)		
Subtransient Reactances		
Use saturated value	No	

Inrush Peak Current			
Ratio Ip/In	10.0000	p.u.	
Max. Time	0.0200	s	
Stall Time			
Cold	20.0000	s	
Hot	10.0000	s	
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified			3/12/2015 4:31:31 PM
Modified by	pramod		
<hr/>			
Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 409
650kw	Synchronous Machine Type	8	/8
Stator Resistance			
rstr	0.0000	p.u.	
rs(f)			
Subtransient Reactances			
xd''	0.1550	p.u.	
xq''	0.2000	p.u.	
l''(f)			
Zero Sequence Data			
Reactance x0	0.0370	p.u.	
l0(f)			
Resistance r0	0.0000	p.u.	
r0(f)			
Consider Transient Parameter	No		
Negative Sequence Data			
Reactance x2	0.1750	p.u.	
l2(f)			
Resistance r2	0.0000	p.u.	
r2(f)			
Subtransient Reactances			
Use saturated value	No		
Inrush Peak Current			
Ratio Ip/In	10.0000	p.u.	
Max. Time	0.0200	s	
Stall Time			
Cold	20.0000	s	
Hot	10.0000	s	
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified			3/11/2015 3:18:37 PM
Modified by	pramod		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 336
WTG01	Static Generator	1	/1
Harmonic Source			
Harmonic Currents	Fundamental Current		
Harmonic currents referred to			
Norton Equivalent			
Resistance, r1h		99999.0000	p.u.
Reactance, x1h		99999.0000	p.u.
Frequency-Dependence, r1h(f)			
Frequency-Dependence, x1h(f)			
Resistance, r2h		99999.0000	p.u.
Reactance, x2h		99999.0000	p.u.
Frequency-Dependence, r2h(f)			
Frequency-Dependence, x2h(f)			
Resistance, r0h		99999.0000	p.u.
Reactance, x0h		99999.0000	p.u.
Frequency-Dependence, r0h(f)			
Frequency-Dependence, x0h(f)			
Flicker Coefficients			
Controls			
Reactive Power	No		
Reactive Power Limits			
Min.	Yes		
Max.	Yes		
Scaling Factor (min.)		100.0000	%
Scaling Factor (max.)		100.0000	%
Capability Curve	...rary\0.85MW VCS 50Hz Capability Curve		
Stochastic Model			
Serial Number			
Year of Construction		0	
Commissioning Date		12/31/1969	7:00:00 PM
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Owner			
Operator			
Description			
Approval Information			
Status	Not Approved		
Modified		1/18/2012	3:01:42 AM
Modified by	PACAL VESTAS		
Operator Comment			
State Estimation			
Estimate Active Power	No		
Estimate Reactive Power	No		
Wind Model	No		

Transformers

- 1,000 KVA = T6, T14
- 1,600 KVA = T4, T5
- 315 KVA = T8
- 400 KVA = T11, T13
- 630 KVA = T2, T7
- 750 KVA = T1, T3
- 6.3 KV–20 KV = T12
- WTG TF_0.85-MW VCS = Transformer from WTG to Haharu Bus

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 410
1000KVA	2-winding Transformer Type	1	/9
Magnetising Impedance			
No Load Current		0.0000	%
No Load Losses		0.0000	kw
Distribution of Leakage Reactances (p.u.)			
x,Pos.Seq. HV-Side		0.5000	
x,Pos.Seq. LV-Side		0.5000	
Distribution of Leakage Resistances (p.u.)			
r,Pos.Seq. HV-Side		0.5000	
r,Pos.Seq. LV-Side		0.5000	
Tap Changer 1	Yes		
Type	Ratio/Asym. Phase Shifter		
at Side	HV		
Additional Voltage per Tap		0.0000	%
Phase of du		0.0000	deg
Neutral Position		3	
Minimum Position		1	
Maximum Position		5	
Tap Changer 2	No		
Tap dependent impedance	No		
Data for K-factor, Factor-K and FHL			
Ratio		0.1000	
Frequency Dependencies of Pos.-Sequence Impedance			
r1(f)			
l1(f)			
Frequency Dependencies of Zero-Sequence Impedance			
r0(f)			
l0(f)			
Inrush Peak Current			
Ratio Ip/In (1)		25.0000	p.u.
Max. Time (1)		0.0100	s
Ratio Ip/In (2)		0.0000	p.u.
Max. Time (2)		0.0000	s
Transformer Type	0		
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/12/2015 4:29:15 PM	
Modified by	pramod		
Rated Power (forced cooling)		0.0000	MVA
On-load Tap Changer	No		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 411
1000kVA	2-Winding Transformer Type	2	/9
Magnetising Impedance			
No Load Current		0.0000	%
No Load Losses		0.0000	kw
Distribution of Leakage Reactances (p.u.)			
x,Pos.Seq. HV-Side		0.5000	
x,Pos.Seq. LV-Side		0.5000	
Distribution of Leakage Resistances (p.u.)			
r,Pos.Seq. HV-Side		0.5000	
r,Pos.Seq. LV-Side		0.5000	
Tap Changer 1	Yes		
Type	Ratio/Asym. Phase Shifter		
at Side	HV		
Additional voltage per Tap		2.2200	%
Phase of du		0.0000	deg
Neutral Position		3	
Minimum Position		1	
Maximum Position		5	
Tap Changer 2	No		
Tap dependent impedance	No		
Data for K-factor, Factor-K and FHL			
Ratio		0.1000	
Frequency Dependencies of Pos.-Sequence Impedance			
r1(f)			
l1(f)			
Frequency Dependencies of Zero-Sequence Impedance			
r0(f)			
l0(f)			
Inrush Peak Current			
Ratio Ip/In (1)		25.0000	p.u.
Max. Time (1)		0.0100	s
Ratio Ip/In (2)		0.0000	p.u.
Max. Time (2)		0.0000	s
Transformer Type	0		
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015 3:29:44 PM	
Modified by	pramod		
Rated Power (forced cooling)		0.0000	MVA
On-load Tap Changer	No		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 412
1600kVA	2-Winding Transformer Type	3	/9
Magnetising Impedance			
No Load Current		0.0000	%
No Load Losses		0.0000	kw
Distribution of Leakage Reactances (p.u.)			
x,Pos.Seq. HV-Side		0.5000	
x,Pos.Seq. LV-Side		0.5000	
Distribution of Leakage Resistances (p.u.)			
r,Pos.Seq. HV-Side		0.5000	
r,Pos.Seq. LV-Side		0.5000	
Tap Changer 1	Yes		
Type	Ratio/Asym. Phase Shifter		
at Side	HV		
Additional voltage per Tap		2.2200	%
Phase of du		0.0000	deg
Neutral Position		3	
Minimum Position		1	
Maximum Position		5	
Tap Changer 2	No		
Tap dependent impedance	No		
Data for K-factor, Factor-K and FHL			

Ratio		0.1000	
Frequency Dependencies of Pos.-Sequence Impedance			
r1(f)			
l1(f)			
Frequency Dependencies of Zero-Sequence Impedance			
r0(f)			
l0(f)			
Inrush Peak Current			
Ratio Ip/In (1)		25.0000	p.u.
Max. Time (1)		0.0100	s
Ratio Ip/In (2)		0.0000	p.u.
Max. Time (2)		0.0000	s
Transformer Type	0		
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015 3:37:18 PM	
Modified by	pramod		
Rated Power (forced cooling)		0.0000	MVA
On-load Tap Changer	No		

Grid:Sumba Syst.Stage:Sumba | Annex: / 413|

315kVA 2-Winding Transformer Type 4 /9

Magnetising Impedance			
No Load Current		0.0000	%
No Load Losses		0.0000	kw
Distribution of Leakage Reactances (p.u.)			
x,Pos.Seq. HV-Side		0.5000	
x,Pos.Seq. LV-Side		0.5000	
Distribution of Leakage Resistances (p.u.)			
r,Pos.Seq. HV-Side		0.5000	
r,Pos.Seq. LV-Side		0.5000	
Tap Changer 1	Yes		
Type	Ratio/Asym. Phase Shifter		
at Side	HV		
Additional voltage per Tap		2.2200	%
Phase of du		0.0000	deg
Neutral Position		3	
Minimum Position		1	
Maximum Position		5	
Tap Changer 2	No		
Tap dependent impedance	No		
Data for K-factor, Factor-K and FHL			
Ratio		0.1000	
Frequency Dependencies of Pos.-Sequence Impedance			
r1(f)			
l1(f)			
Frequency Dependencies of Zero-Sequence Impedance			
r0(f)			
l0(f)			
Inrush Peak Current			
Ratio Ip/In (1)		25.0000	p.u.
Max. Time (1)		0.0100	s
Ratio Ip/In (2)		0.0000	p.u.
Max. Time (2)		0.0000	s
Transformer Type	0		
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		

Modified		3/11/2015 3:09:54 PM
Modified by	pramod	
Rated Power (forced cooling)		0.0000 MVA
On-load Tap Changer	No	
<hr/>		
Grid:Sumba	Syst.Stage:Sumba	Annex: / 414
<hr/>		
400KVA	2-Winding Transformer Type	5 /9
<hr/>		
Magnetising Impedance		
No Load Current	0.0000	%
No Load Losses	0.0000	kw
Distribution of Leakage Reactances (p.u.)		
x,Pos.Seq. HV-Side	0.5000	
x,Pos.Seq. LV-Side	0.5000	
Distribution of Leakage Resistances (p.u.)		
r,Pos.Seq. HV-Side	0.5000	
r,Pos.Seq. LV-Side	0.5000	
Tap Changer 1	Yes	
Type	Ratio/Asym. Phase Shifter	
at Side	HV	
Additional voltage per Tap	0.0000	%
Phase of du	0.0000	deg
Neutral Position	3	
Minimum Position	1	
Maximum Position	5	
Tap Changer 2	No	
Tap dependent impedance	No	
Data for K-factor, Factor-K and FHL		
Ratio	0.1000	
Frequency Dependencies of Pos.-Sequence Impedance		
r1(f)		
l1(f)		
Frequency Dependencies of Zero-Sequence Impedance		
r0(f)		
l0(f)		
Inrush Peak Current		
Ratio Ip/In (1)	25.0000	p.u.
Max. Time (1)	0.0100	s
Ratio Ip/In (2)	0.0000	p.u.
Max. Time (2)	0.0000	s
Transformer Type	0	
Stochastic model		
Manufacturer		
Characteristic Name		
Data source	MAN	
Foreign Key		
Additional Data		
Description		
Approval Information		
Status	Not Approved	
Modified		3/12/2015 4:19:01 PM
Modified by	pramod	
Rated Power (forced cooling)		0.0000 MVA
On-load Tap Changer	No	
<hr/>		
Grid:Sumba	Syst.Stage:Sumba	Annex: / 415
<hr/>		
6.3kv-20kv	2-Winding Transformer Type	6 /9
<hr/>		
Magnetising Impedance		
No Load Current	0.0000	%
No Load Losses	0.0000	kw
Distribution of Leakage Reactances (p.u.)		
x,Pos.Seq. HV-Side	0.5000	
x,Pos.Seq. LV-Side	0.5000	
Distribution of Leakage Resistances (p.u.)		
r,Pos.Seq. HV-Side	0.5000	
r,Pos.Seq. LV-Side	0.5000	
Tap Changer 1	Yes	
Type	Ratio/Asym. Phase Shifter	
at Side	HV	
Additional voltage per Tap	0.0000	%
Phase of du	0.0000	deg

Neutral Position		3	
Minimum Position		1	
Maximum Position		5	
Tap Changer 2	No		
Tap dependent impedance	No		
Data for K-factor, Factor-K and FHL			
Ratio		0.1000	
Frequency Dependencies of Pos.-Sequence Impedance			
r1(f)			
l1(f)			
Frequency Dependencies of Zero-Sequence Impedance			
r0(f)			
l0(f)			
Inrush Peak Current			
Ratio Ip/In (1)		25.0000	p.u.
Max. Time (1)		0.0100	s
Ratio Ip/In (2)		0.0000	p.u.
Max. Time (2)		0.0000	s
Transformer Type	0		
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015 6:00:21 PM	
Modified by	pramod		
Rated Power (forced cooling)		0.0000	MVA
On-load Tap Changer	No		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 416
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630kVA	2-Winding Transformer Type	7	/9
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Magnetising Impedance			
No Load Current		0.0000	%
No Load Losses		0.0000	kw
Distribution of Leakage Reactances (p.u.)			
x,Pos.Seq. HV-Side		0.5000	
x,Pos.Seq. LV-Side		0.5000	
Distribution of Leakage Resistances (p.u.)			
r,Pos.Seq. HV-Side		0.5000	
r,Pos.Seq. LV-Side		0.5000	
Tap Changer 1	Yes		
Type	Ratio/Asym. Phase Shifter		
at Side	HV		
Additional voltage per Tap		2.2200	%
Phase of du		0.0000	deg
Neutral Position		3	
Minimum Position		1	
Maximum Position		5	
Tap Changer 2	No		
Tap dependent impedance	No		
Data for K-factor, Factor-K and FHL			
Ratio		0.1000	
Frequency Dependencies of Pos.-Sequence Impedance			
r1(f)			
l1(f)			
Frequency Dependencies of Zero-Sequence Impedance			
r0(f)			
l0(f)			
Inrush Peak Current			
Ratio Ip/In (1)		25.0000	p.u.
Max. Time (1)		0.0100	s
Ratio Ip/In (2)		0.0000	p.u.
Max. Time (2)		0.0000	s
Transformer Type	0		
Stochastic model			
Manufacturer			
Characteristic Name			

Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015 2:46:45 PM	
Modified by	pramod		
Rated Power (forced cooling)		0.0000	MVA
On-load Tap Changer	No		
<hr/>			
Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 417
750KVA	2-Winding Transformer Type	8	/9
Magnetising Impedance			
No Load Current		0.0000	%
No Load Losses		0.0000	kw
Distribution of Leakage Reactances (p.u.)			
x,Pos.Seq. HV-Side		0.5000	
x,Pos.Seq. LV-Side		0.5000	
Distribution of Leakage Resistances (p.u.)			
r,Pos.Seq. HV-Side		0.5000	
r,Pos.Seq. LV-Side		0.5000	
Tap Changer 1	Yes		
Type	Ratio/Asym. Phase Shifter		
at Side	HV		
Additional voltage per Tap		0.0000	%
Phase of du		0.0000	deg
Neutral Position		3	
Minimum Position		1	
Maximum Position		5	
Tap Changer 2	No		
Tap dependent impedance	No		
Data for K-factor, Factor-K and FHL			
Ratio		0.1000	
Frequency Dependencies of Pos.-Sequence Impedance			
r1(f)			
l1(f)			
Frequency Dependencies of Zero-Sequence Impedance			
r0(f)			
l0(f)			
Inrush Peak Current			
Ratio Ip/In (1)		25.0000	p.u.
Max. Time (1)		0.0100	s
Ratio Ip/In (2)		0.0000	p.u.
Max. Time (2)		0.0000	s
Transformer Type	0		
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/12/2015 10:11:37 PM	
Modified by	pramod		
Rated Power (forced cooling)		0.0000	MVA
On-load Tap Changer	No		
<hr/>			
Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 188
WTG TF_0.85MW VCS 50Hz	2-Winding Transformer Type	5	/5
Technology	Three Phase Transformer		
Rated Power		0.8500	MVA
Nominal Frequency		50.0000	Hz
Rated voltage			
HV-Side		20.0000	kV
LV-Side		0.6900	kV
Positive Sequence Impedance			
Short-Circuit Voltage uk		6.0000	%

Ratio X/R		5.0010	
Vector Group			
HV-Side	D		
LV-Side	YN		
Phase Shift		11.0000	*30deg
Zero Sequence Impedance			
Short-Circuit Voltage uk0		5.4000	%
SHC-voltage (Re(uk0)) uk0r		0.0000	%
Magnetising Impedance			
No Load Current		1.2000	%
No Load Losses		0.5000	kw
Distribution of Leakage Reactances (p.u.)			
x,Pos.Seq. HV-Side		0.5000	
x,Pos.Seq. LV-Side		0.5000	
Distribution of Leakage Resistances (p.u.)			
r,Pos.Seq. HV-Side		0.5000	
r,Pos.Seq. LV-Side		0.5000	
Tap Changer 1	Yes		
Type	Ratio/Asym. Phase Shifter		
at Side	HV		
Additional voltage per Tap		2.5000	%
Phase of du		0.0000	deg
Neutral Position		0	
Minimum Position		-2	
Maximum Position		2	
Tap Changer 2	No		
Tap dependent impedance	No		
Magnetising Reactance			
Type	Linear		
Transformer Ratio Adaptation	Yes		
On-load Tap Changer	No		
Class	FOA		

Transmission Lines

- AAAC-50 mm = Transmission lines from Kambajawa to Mid-Haharu Bus
- AAAC-150 mm = Transmission lines from Kambajawa to Waingapu Bus
- TLine35 mm = Transmission lines from Mid-Haharu to Haharu Bus

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 398
AAAC-150mm	Line Type	1	/3
Parameters per Length 1,2-Sequence			
Susceptance B'		1.6600	uS/km
Ins. Factor		0.0000	
Parameters per Length Zero Sequence			
Susceptance B0'		0.0000	uS/km
Ins. Factor		0.0000	
Frequency Dependency of Pos.-Sequence Capacitance			
Capacitance C'		0.0053	uF/km
C1'(f)			
Frequency Dependency of Zero-Sequence Capacitance			
Capacitance C0'		0.0000	uF/km
C0'(f)			
Frequency Dependencies of Pos.-Sequence Impedance			
AC-Resistance R'(20°C)		0.2250	Ohm/km
R1'(AC)(f)			
Inductance L'		0.9549	mH/km
L1'(f)			
Frequency Dependencies of Zero-Sequence Impedance			
AC-Resistance R0'		0.0000	Ohm/km
R0'(AC)(f)			
Inductance L0'		0.0000	mH/km
L0'(f)			
Inrush Peak Current			
Ratio Ip/In		0.0000	p.u.
Maximum Time		0.0000	s
Rated Short-Time (1s) Current (Conductor)		0.0000	kA
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015 6:20:22 PM	
Modified by	pramod		
System Type			
Phases	AC		
Number of Neutrals		3	
Cable Design Parameter		0	
Conductor Material	Copper		
Insulation Material	0		
Cable Cores	Multi-Core		
Rated Voltage		20.0000	kV
Rated Current		1.0000	kA
Nominal Cross Section		0.0000	mm^2
with Sheath	No		
Sheath Type	0		
Sheath Insulation Material	PVC		
Armoured Cable	No		
Radial Cable Screen	No		
Line Cost		0.0000	\$/km
Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 399
AAAC50mm	Line Type	2	/3

Parameters per Length 1,2-Sequence			
Susceptance B'	1.4920	uS/km	
Ins. Factor	0.0000		
Parameters per Length Zero Sequence			
Susceptance B0'	0.0000	uS/km	
Ins. Factor	0.0000		
Frequency Dependency of Pos.-Sequence Capacitance			
Capacitance C'	0.0047	uF/km	
C1'(f)			
Frequency Dependency of Zero-Sequence Capacitance			
Capacitance C0'	0.0000	uF/km	
C0'(f)			
Frequency Dependencies of Pos.-Sequence Impedance			
AC-Resistance R'(20°C)	0.6650	Ohm/km	
R1'(AC)(f)			
Inductance L'	1.1777	mH/km	
L1'(f)			
Frequency Dependencies of Zero-Sequence Impedance			
AC-Resistance R0'	0.0000	Ohm/km	
R0'(AC)(f)			
Inductance L0'	0.0000	mH/km	
L0'(f)			
Inrush Peak Current			
Ratio Ip/In	0.0000	p.u.	
Maximum Time	0.0000	s	
Rated Short-Time (1s) Current (Conductor)	0.0000	kA	
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015 6:28:58 PM	
Modified by	pramod		
System Type	AC		
Phases		3	
Number of Neutrals		0	
Cable Design Parameter			
Conductor Material	Copper		
Insulation Material	0		
Cable Cores	Multi-Core		
Rated Voltage		20.0000	kV
Rated Current		1.0000	kA
Nominal Cross Section		0.0000	mm^2
with Sheath	No		
Sheath Type	0		
Sheath Insulation Material	PVC		
Armoured Cable	No		
Radial Cable Screen	No		
Line Cost		0.0000	\$/km

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 400
Tline35mm	Line Type	3	/3
Parameters per Length 1,2-Sequence			
Susceptance B'	0.5630	uS/km	
Ins. Factor	0.0000		
Parameters per Length Zero Sequence			
Susceptance B0'	0.0000	uS/km	
Ins. Factor	0.0000		
Frequency Dependency of Pos.-Sequence Capacitance			
Capacitance C'	0.0018	uF/km	
C1'(f)			
Frequency Dependency of Zero-Sequence Capacitance			
Capacitance C0'	0.0000	uF/km	
C0'(f)			
Frequency Dependencies of Pos.-Sequence Impedance			
AC-Resistance R'(20°C)	0.9580	Ohm/km	
R1'(AC)(f)			
Inductance L'	1.2414	mH/km	
L1'(f)			

Frequency Dependencies of Zero-Sequence Impedance			
AC-Resistance R0'	0.0000	Ohm/km	
R0'(AC)(f)			
Inductance L0'	0.0000	mH/km	
L0'(f)			
Inrush Peak Current			
Ratio Ip/In	0.0000	p.u.	
Maximum Time	0.0000	s	
Rated Short-Time (1s) Current (Conductor)	0.0000	kA	
Stochastic model			
Manufacturer			
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015 6:38:25 PM	
Modified by	pramod		
System Type			
Phases	AC		
Number of Neutrals		3	
Cable Design Parameter		0	
Conductor Material	Copper		
Insulation Material	0		
Cable Cores	Multi-Core		
Rated Voltage		20.0000	kV
Rated Current		1.0000	kA
Nominal Cross Section		0.0000	mm^2
with Sheath	No		
Sheath Type	0		
Sheath Insulation Material	PVC		
Armoured Cable	No		
Radial Cable Screen	No		
Line Cost		0.0000	\$/km

Loads

- Haharu Load = Load at Haharu Bus
- Kambajawa Load = Load at Kambajawa Bus
- Waingapu Load = Load at Waingapu Bus

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 340
Haharu Load	General Load	1	/3
Harmonic Current Injections			
Harmonic Currents			
Harmonic currents referred to	Fundamental Current		
Fault Contribution			
Scalable Fault Contribution			
Subtransient Short-Circuit Level	0.0000	MVA/MW	
Transient Short-Circuit Level	0.0000	MVA/MW	
Fixed Fault Contribution			
Subtransient Short-Circuit Level	0.0000	MVA	
Transient Short-Circuit Level	0.0000	MVA	
R to X'' ratio	0.1000		
Additional LV Capacitance	0.0000	Mvar	
Controls			
Allow load shedding	No		
Costs			
Costs for load shedding	1.0000	\$/MVA	
Constraints			
Min. load shedding	0.0000	%	
Max. load shedding	100.0000	%	
Number of connected customers	1		
Priority	0		
Contracted Active Power	0.0000	MW	
Load shedding/transfer (Transmission option)			
Shedding steps	0		
Transferable	0.0000	%	
Alternative Supply (Load)			
Interruption costs			
Tariff			
Scaling factor	1.0000		
Load Classification			
Serial Number			
Year of Construction	0		
Commissioning Date	12/31/1969	7:00:00 PM	
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Owner			
Operator			
Description			
Approval Information			
Status	Not Approved		
Modified	3/11/2015	6:26:45 PM	
Modified by	pramod		
State Estimation			
Active/Reactive Power			
Estimate Active Power	No		
Estimate Reactive Power	No		
Scaling Factor			
Estimate Scaling Factor	No		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 341
Kambajawa Load	General Load	2	/3
Harmonic Current Injections			
Harmonic Currents			
Harmonic currents referred to	Fundamental Current		
Fault Contribution			
Scalable Fault Contribution			
Subtransient Short-Circuit Level		0.0000	MVA/MW
Transient Short-Circuit Level		0.0000	MVA/MW
Fixed Fault Contribution			
Subtransient Short-Circuit Level		0.0000	MVA
Transient Short-Circuit Level		0.0000	MVA
R to X'' ratio		0.1000	
Additional LV Capacitance		0.0000	Mvar
Controls			
Allow load shedding	No		
Costs			
Costs for load shedding		1.0000	\$/MVA
Constraints			
Min. load shedding		0.0000	%
Max. load shedding		100.0000	%
Number of connected customers		1	
Priority		0	
Contracted Active Power		0.0000	MW
Load shedding/transfer (Transmission Option)			
Shedding steps	0		
Transferable		0.0000	%
Alternative Supply (Load)			
Interruption costs			
Tariff			
Scaling factor		1.0000	
Load Classification			
Serial Number			
Year of Construction		0	
Commissioning Date		12/31/1969	7:00:00 PM
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Owner			
Operator			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015	4:23:33 PM
Modified by	pramod		
State Estimation			
Active/Reactive Power			
Estimate Active Power	No		
Estimate Reactive Power	No		
Scaling Factor			
Estimate Scaling Factor	No		

Grid:Sumba	Syst.Stage:Sumba	Annex:	/ 342
Waingapu Load	General Load	3	/3
Harmonic Current Injections			
Harmonic Currents			
Harmonic currents referred to	Fundamental Current		
Fault Contribution			
Scalable Fault Contribution			
Subtransient Short-Circuit Level		0.0000	MVA/MW
Transient Short-Circuit Level		0.0000	MVA/MW
Fixed Fault Contribution			
Subtransient Short-Circuit Level		0.0000	MVA
Transient Short-Circuit Level		0.0000	MVA
R to X'' ratio		0.1000	
Additional LV Capacitance		0.0000	Mvar
Controls			
Allow load shedding	No		
Costs			
Costs for load shedding		1.0000	\$/MVA
Constraints			
Min. load shedding		0.0000	%
Max. load shedding		100.0000	%
Number of connected customers		1	
Priority		0	
Contracted Active Power		0.0000	MW
Load shedding/transfer (Transmission Option)			
Shedding steps	0		
Transferable		0.0000	%
Alternative Supply (Load)			
Interruption costs			
Tariff			
Scaling factor		1.0000	
Load Classification			
Serial Number			
Year of Construction		0	
Commissioning Date		12/31/1969	7:00:00 PM
Characteristic Name			
Data source	MAN		
Foreign Key			
Additional Data			
Owner			
Operator			
Description			
Approval Information			
Status	Not Approved		
Modified		3/11/2015	6:13:21 PM
Modified by	pramod		
State Estimation			
Active/Reactive Power			
Estimate Active Power	No		
Estimate Reactive Power	No		
Scaling Factor			
Estimate Scaling Factor	No		

Appendix C: Load Profile Results

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High Wind High Load (For One WTG)	93
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No Wind High Load

										DigSILENT PowerFactory 15.2.1		Project: ----- Date: 4/22/2015				
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange																
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits								Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %		
Grid: Sumba				System Stage: Sumba				Study Case: KHTL				Annex: / 1				
rated voltage [kV]		Bus-voltage [p.u.]		Bus-voltage [kV]		[deg]		Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data			
HB(1)																
Haharu 20.00		0.98		19.69		149.44		0.10	0.06	0.85	0.00		P10: 0.10 MW			
Cub_1 /Lod		Haharu Load						-0.10	-0.06	-0.85	0.00	0.36	Pv: 0.65 kW			
Cub_1 /Lne		K-H2 Tline						0.00	0.00	1.00	0.00	0.00	Q10: 0.06 Mvar			
Cub_1 /Tr2		WTG01 Trafo											cLod: 0.00 Mvar L: 18.00 km			
													Tap: 0.00 Min: -2 Max: 2			
K-BB(1)																
K1 400V Bu.40		1.02		0.41		0.56		0.22	0.17	0.80	0.39	100.00	Typ: PQ			
Cub_1 /Sym		Volvo						0.22	0.17	0.80	0.39	85.66	Tap: 3.00			
Cub_1 /Tr2		T8											Min: 1 Max: 5			
K-BB(2)																
K3 400V Bu.40		1.00		0.40		0.00		0.25	0.11	0.91	0.39	33.32	Typ: SL			
Cub_1 /Sym		MTU1						0.25	0.11	0.91	0.39	27.07	Tap: 3.00			
Cub_1 /Tr2		T6											Min: 1 Max: 5			
K-BB(3)																
K4 400V Bu.40		1.02		0.41		1.74		0.42	0.31	0.80	0.74	100.00	Typ: PQ			
Cub_1 /Sym		DOOSAN3						0.42	0.31	0.80	0.74	100.00	Typ: PQ			
Cub_1 /Sym		DOOSAN4						0.42	0.00	1.00	0.59	80.00	Typ: PQ			
Cub_1 /Sym		DOOSAN5						1.26	0.63	0.89	1.99	86.09	Tap: 3.00			
Cub_1 /Tr2		T4											Min: 1 Max: 5			
		Total						-----	-----							
		Generation:						1.26	0.63							
Grid: Sumba System Stage: Sumba Study Case: KHTL Annex: / 2																
rated voltage [kV]		Bus-voltage [p.u.]		Bus-voltage [kV]		[deg]		Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data			
K-BB(4)																
Kambajawa0.00		0.99		19.83		149.38		3.49	1.69	0.90	0.11		P10: 3.49 MW			
Cub_1 /Lod		Kambajawa Load											Q10: 1.69 Mvar			

Cub_1 /Lne	K-H1	0.10	0.06	0.88	0.00	0.35	Pv:	0.17 kw	cLod:	0.00	Mvar	L:	7.00 km
Cub_1 /Lne	K-W Tline	0.53	0.18	0.95	0.02	1.64	Pv:	1.27 kw	cLod:	0.00	Mvar	L:	7.00 km
Cub_1 /Tr2	T1	-0.43	-0.31	-0.81	0.02	70.48	Tap:	3.00	Min:	1	Max:	5	
Cub_1 /Tr2	T2	-0.31	-0.22	-0.81	0.01	63.96	Tap:	5.00	Min:	1	Max:	5	
Cub_1 /Tr2	T3	-0.43	-0.31	-0.81	0.02	70.48	Tap:	3.00	Min:	1	Max:	5	
Cub_1 /Tr2	T4	-1.25	-0.56	-0.91	0.04	86.09	Tap:	3.00	Min:	1	Max:	5	
Cub_1 /Tr2	T5	-0.83	0.03	-1.00	0.02	52.63	Tap:	3.00	Min:	1	Max:	5	
Cub_1 /Tr2	T6	-0.25	-0.11	-0.92	0.01	27.07	Tap:	3.00	Min:	1	Max:	5	
Cub_1 /Tr2	T7	-0.42	-0.30	-0.82	0.02	86.81	Tap:	5.00	Min:	1	Max:	5	
Cub_1 /Tr2	T8	-0.22	-0.16	-0.81	0.01	85.66	Tap:	3.00	Min:	1	Max:	5	
K-BB(5)													
K4 400v Bu.40	1.00	0.40	1.17										
Cub_1 /Sym	DOOSAN1	0.42	0.00	1.00	0.61	80.00	Typ:	PQ					
Cub_1 /Sym	DOOSAN2	0.42	0.00	1.00	0.61	80.00	Typ:	PQ					
Cub_1 /Tr2	T5	0.84	0.00	1.00	1.22	52.63	Tap:	3.00	Min:	1	Max:	5	
Total Generation:		0.84	0.00										
K-BB													
K2 400v Bu.40	0.98	0.39	1.04										
Cub_1 /Sym	MAN1	0.43	0.32	0.80	0.79	100.00	Typ:	PQ					
Cub_1 /Tr2	T7	0.43	0.32	0.80	0.79	86.81	Tap:	5.00	Min:	1	Max:	5	
KBB10													
K5 400v 0.40	1.02	0.41	0.49										
Cub_1 /Sym	MTU2	0.43	0.32	0.80	0.76	100.00	Typ:	PQ					
Cub_1 /Tr2	T1	0.43	0.32	0.80	0.76	70.48	Tap:	3.00	Min:	1	Max:	5	
KBB11													
K6 400v 0.40	0.97	0.39	0.60										
Cub_1 /Sym	MAN2	0.31	0.24	0.80	0.58	98.13	Typ:	PQ					
Cub_1 /Tr2	T2	0.31	0.24	0.80	0.58	63.96	Tap:	5.00	Min:	1	Max:	5	
KBB12													
K7 400v 0.40	1.02	0.41	0.49										
Cub_1 /Sym	MTU4	0.43	0.32	0.80	0.76	100.00	Typ:	PQ					
Cub_1 /Tr2	T3	0.43	0.32	0.80	0.76	70.48	Tap:	3.00	Min:	1	Max:	5	

Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex: / 3			
rated voltage [kv]		Bus-voltage [p.u.]	Bus-voltage [kv]	[deg]	Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data			
Single Busbar(3)													
K-H2	20.00	0.99	19.80	149.39									
Cub_1 /Lne	K-H1	-0.10	-0.06	-0.86	0.00	0.35	Pv:	0.17 kw	cLod:	0.00	Mvar	L:	7.00 km
Cub_1 /Lne	K-H2 Tline	0.10	0.06	0.86	0.00	0.36	Pv:	0.65 kw	cLod:	0.00	Mvar	L:	18.00 km
WBB(1)													
w6.3kv	6.30	1.01	6.35	0.71									
Cub_1 /Sym	SWD1	0.22	0.00	1.00	0.02	80.00	Typ:	PQ					
Cub_1 /Sym	SWD2	0.22	0.17	0.80	0.02	100.00	Typ:	PQ					
Cub_1 /Sym	SWD3						Typ:	PQ					
Cub_1 /Sym	YANMAR	0.22	0.17	0.80	0.02	100.00	Typ:	PQ					

Cub_1 /Tr2	T12	0.66	0.33	0.89	0.07	58.53	Tap:	3.00	Min:	1	Max:	5
	Total Generation:	0.66	0.33									
WBB(2)												
w3 400v 0.40	1.01 0.41 0.50											
Cub_1 /Sym	CAT C32	0.55	0.41	0.80	0.98	100.00	Typ:	PQ				
Cub_1 /Tr2	T14	0.55	0.41	0.80	0.98	67.76	Tap:	3.00	Min:	1	Max:	5
WBB(3)												
waingapu20.00	0.99 19.77 149.26											
Cub_1 /Lod	waingapu Load	2.08	1.01	0.90	0.07		P10:	2.08 MW	Q10:	1.01 Mvar		
Cub_1 /Lne	K-W Tline	-0.53	-0.19	-0.94	0.02	1.64	Pv:	1.27 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1 /Tr2	T11	-0.18	0.00	-1.00	0.01	45.03	Tap:	3.00	Min:	1	Max:	5
Cub_1 /Tr2	T12	-0.65	-0.31	-0.91	0.02	58.53	Tap:	3.00	Min:	1	Max:	5
Cub_1 /Tr2	T13	-0.18	-0.13	-0.81	0.01	55.27	Tap:	3.00	Min:	1	Max:	5
Cub_1 /Tr2	T14	-0.54	-0.39	-0.81	0.02	67.76	Tap:	3.00	Min:	1	Max:	5
WBB(4)												
w2 400v 0.40	1.01 0.40 0.02											
Cub_1 /Sym	DEUT Z-2	0.18	0.13	0.80	0.32	98.89	Typ:	PQ				
Cub_1 /Tr2	T13	0.18	0.13	0.80	0.32	55.27	Tap:	3.00	Min:	1	Max:	5
WBB												
w1 400v 0.40	0.99 0.40 0.26											
Cub_1 /Sym	DEUT Z-1	0.18	0.00	1.00	0.26	79.56	Typ:	PQ				
Cub_1 /Tr2	T11	0.18	0.00	1.00	0.26	45.03	Tap:	3.00	Min:	1	Max:	5
WTG01LV												
Cub_4 /Genstat	WTG01	0.00	0.00	1.00	0.00	0.00						
Cub_3 /Tr2	WTG01 Trafo	0.00	0.00	1.00	0.00	0.00	Tap:	0.00	Min:	-2	Max:	2

		DigSILENT	Project:
		PowerFactory	
		15.2.1	Date: 4/22/2015

Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange

AC Load Flow, balanced, positive sequence	Automatic Model Adaptation for Convergence	No
Automatic Tap Adjust of Transformers	Max. Acceptable Load Flow Error for	
Consider Reactive Power Limits	Nodes	0.01 kVA
	Model Equations	0.01 %

Grid: Sumba System Stage: Sumba Study Case: KHTL Annex: / 4

rtd.V	Bus - voltage								
[kV]	[p.u.]	[kV]	[deg]	-10	-5	0	+5	+10	
HB(1)									
Haharu	20.00	0.984	19.69 149.44						<<<<
K-BB(1)									
K1 400v Bus	0.40	1.019	0.41 0.56						>>>>
K-BB(2)									

K3 400V Bus	0.40	1.000	0.40	0.00	
K-BB(3)					
K4 400V Bus	0.40	1.023	0.41	1.74	>>>>
K-BB(4)					
Kambajawa	20.00	0.992	19.83	149.38	<<
K-BB(5)					
K4 400V Bus	0.40	0.997	0.40	1.17	<
K-BB					
K2 400V Bus	0.40	0.983	0.39	1.04	<<<<
KBB10					
K5 400V	0.40	1.017	0.41	0.49	>>>>
KBB11					
K6 400V	0.40	0.974	0.39	0.60	<<<<<<
KBB12					
K7 400V	0.40	1.017	0.41	0.49	>>>>
Single Busbar(3)					
K-H2	20.00	0.990	19.80	149.39	<<
WBB(1)					
w6.3kv	6.30	1.009	6.35	0.71	>>
WBB(2)					
w3 400v	0.40	1.015	0.41	0.50	>>>>
WBB(3)					
waingapu	20.00	0.989	19.77	149.26	<<<
WBB(4)					
w2 400v	0.40	1.006	0.40	0.02	>>
WBB					
w1 400v	0.40	0.994	0.40	0.26	<
WTG01LV					

Grid: Sumba	System Stage: Sumba			Study Case: KHTL			Annex:	/ 5
	rtd.V	Bus - voltage		Voltage - Deviation [%]				
	[kV]	[p.u.]	[kV]	[deg]	-10	-5	0	+5
	0.69	0.000	0.00	0.00	<			

						DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015			
Load Flow Calculation						Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange					
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits				Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %	
Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex: / 6	
Volt. Level [kV]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]	
0.40	5.08 2.65	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv		0.00	0.00	0.00	
								0.00	0.00	0.00	
								0.05 0.21	0.05 0.21	0.00 0.00	
0.69	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00	0.00	0.00	
								0.00	0.00	0.00	
6.30	0.66 0.33	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv		0.00	0.00	0.00	
								0.00	0.00	0.00	
								0.01 0.02	0.01 0.02	0.00 0.00	
20.00	0.00 0.00	0.00 0.00	5.68 2.77	0.00 0.00	0.00 0.00	0.40 kv 6.30 kv		-0.01	0.00	-0.01	
								0.05	0.05	0.00	
								0.21	0.21	0.00	
								0.01 0.02	0.01 0.02	0.00 0.00	
Total:	5.74 2.98	0.00 0.00	5.68 2.77	0.00 0.00	0.00 0.00			0.06	0.06	0.00	
								0.22	0.23	-0.01	
						DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015			
Load Flow Calculation						Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange					
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits				Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %	

Total System Summary						Study Case: KHTL		Annex:		/ 7
Generation	Motor Load	Load	Compensation	External Infeed	Inter Area Flow	Total Losses	Load Losses	No load Losses		
[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	
\pramod\Sumba-V3_NWHL\Network Model\Network Data\Sumba										
5.74	0.00	5.68	0.00	0.00	0.00	0.06	0.06	0.00		
2.98	0.00	2.77	0.00	0.00	0.00	0.22	0.23	-0.01		
Total:										
5.74	0.00	5.68	0.00	0.00		0.06	0.06	0.00		
2.98	0.00	2.77	0.00	0.00		0.22	0.23	-0.01		
						DIGSILENT PowerFactory 15.2.1	Project:			
							Date: 4/22/2015			
Load Flow Calculation						Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange				
AC Load Flow, balanced, positive sequence				Yes No	Automatic Model Adaptation for Convergence				No	
Automatic Tap Adjust of Transformers					Max. Acceptable Load Flow Error for					
Consider Reactive Power Limits					Nodes Model Equations				0.01 kVA 0.01 %	
Area: Kambajawa						Study Case: KHTL		Annex:		/ 8
Volt. Level	Generation	Motor Load	Load	Compensation	External Infeed	Interchange to	Power Interchange	Total Losses	Load Losses	No load Losses
[kv]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]		[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]
0.40	4.17	0.00	0.00	0.00	0.00	20.00 kv		0.00	0.00	0.00
	2.11	0.00	0.00	0.00	0.00			0.00	0.00	0.00
							4.17	0.04	0.04	0.00
						2.11	0.18	0.18	0.00	
20.00	0.00	0.00	3.49	0.00	0.00	0.40 kv waingapu		0.00	0.00	0.00
	0.00	0.00	1.69	0.00	0.00			0.00	0.00	0.00
							-4.13	0.04	0.04	0.00
							-1.93	0.18	0.18	0.00
							0.53	0.00	0.00	0.00
							0.18	-0.00	0.00	-0.00
Total:	4.17	0.00	3.49	0.00	0.00	waingapu	0.64	0.04	0.04	0.00
	2.11	0.00	1.69	0.00	0.00		0.24	0.18	0.18	0.00
							0.53	0.00	0.00	0.00
							0.18	-0.00	0.00	-0.00
						DIGSILENT PowerFactory 15.2.1	Project:			
							Date: 4/22/2015			

Load Flow Calculation			Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange		
AC Load Flow, balanced, positive sequence	Yes No	Automatic Model Adaptation for Convergence	No		
Automatic Tap Adjust of Transformers			Max. Acceptable Load Flow Error for		
Consider Reactive Power Limits			Nodes	0.01 kVA	
			Model Equations	0.01 %	

Area: Waingapu	Study Case: KHTL	Annex:	/ 9
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Volt. Level [kV]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No-load Losses [MW]/ [Mvar]
0.40	0.91 0.55	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	0.91 0.55	0.00 0.00 0.01 0.03	0.00 0.00 0.01 0.03	0.00 0.00 0.00 0.00
6.30	0.66 0.33	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	0.66 0.33	0.00 0.00 0.01 0.02	0.00 0.00 0.01 0.02	0.00 0.00 0.00 0.00
20.00	0.00 0.00	0.00 0.00	2.08 1.01	0.00 0.00	0.00 0.00	0.40 kv 6.30 kv Kambajawa	-0.90 -0.52 -0.65 -0.31 -0.53 -0.18	0.00 0.00 0.01 0.03 0.01 0.02 0.00 -0.00	0.00 0.00 0.01 0.03 0.01 0.02 0.00 0.00	0.00 0.00 0.00 0.00 0.00 -0.00
Total:	1.57 0.88	0.00 0.00	2.08 1.01	0.00 0.00	0.00 0.00	Kambajawa	-0.53 -0.18 -0.53 -0.18	0.01 0.05 0.00 -0.00	0.01 0.05 0.00 0.00	0.00 -0.00 0.00 -0.00

		DigSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015
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Load Flow Calculation			Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange		
AC Load Flow, balanced, positive sequence	Yes No	Automatic Model Adaptation for Convergence	No		
Automatic Tap Adjust of Transformers			Max. Acceptable Load Flow Error for		
Consider Reactive Power Limits			Nodes	0.01 kVA	
			Model Equations	0.01 %	

Area: Haharu	Study Case: KHTL	Annex:	/ 10
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Volt. Level	Generation	Motor	Load	Compensation	External Infeed	Power Interchange	Total Losses	Load Losses	No-load Losses
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Level [kv]	[MW]/ [Mvar]	Load [MW]/ [Mvar]	[MW]/ [Mvar]	station [MW]/ [Mvar]	Infeed [MW]/ [Mvar]	Interchange to	Interchange [MW]/ [Mvar]	Losses [MW]/ [Mvar]	Losses [MW]/ [Mvar]	Losses [MW]/ [Mvar]
20.00	0.00 0.00	0.00 0.00	0.10 0.06	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
Total:	0.00 0.00	0.00 0.00	0.10 0.06	0.00 0.00	0.00 0.00		-0.10 -0.06	0.00 0.00	0.00 0.00	0.00 0.00
							DigSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015		
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits					Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %
Area Summaries						Study Case: KHTL			Annex: / 11	
Generation [MW]/ [Mvar]		Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Inter Area Flow [MW]/ [Mvar]		Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	NoLoad Losses [MW]/ [Mvar]
\pramod\Sumba-V3_NWHL\Network Model\Network Data\Areas\Kambajawa										
4.171		0.000	3.494	0.000	0.000	0.64		0.04	0.04	0.00
2.108		0.000	1.692	0.000	0.000	0.24		0.18	0.18	0.00
\pramod\Sumba-V3_NWHL\Network Model\Network Data\Areas\waingapu										
1.567		0.000	2.084	0.000	0.000	-0.53		0.01	0.01	0.00
0.876		0.000	1.009	0.000	0.000	-0.18		0.05	0.05	-0.00
\pramod\Sumba-V3_NWHL\Network Model\Network Data\Areas\Haharu										
0.000		0.000	0.104	0.000	0.000	-0.10		0.00	0.00	0.00
0.000		0.000	0.064	0.000	0.000	-0.06		0.00	0.00	0.00

No Wind Low Load

										DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015				
Load Flow Calculation														Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange		
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits							Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %			
Grid: Sumba				System Stage: Sumba				Study Case: KHTL				Annex: / 1				
rated Voltage [kV]		Bus-voltage [p.u.]		[kV] [deg]		Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data					
HB(1) Haharu 20.00 0.99 19.73 148.99 Cub_1 /Lod Haharu Load 0.05 0.03 -0.85 0.00 Cub_1 /Lne K-H2 Tline -0.05 -0.03 -0.85 0.00 0.18 Cub_1 /Tr2 WTG01 Trafo 0.00 0.00 1.00 0.00 0.00											P10: 0.05 MW Pv: 0.15 kW Tap: 0.00			Q10: 0.03 Mvar cLod: 0.00 Mvar L: 18.00 km Min: -2 Max: 2		
K-BB(1) K1 400V Bu.40 1.00 0.40 0.00 Cub_1 /Sym Volvo 0.00 0.00 1.00 0.00 0.00 Cub_1 /Tr2 T8 0.00 0.00 1.00 0.00 0.00											Typ: PQ Tap: 3.00		Min: 1		Max: 5	
K-BB(2) K3 400V Bu.40 1.00 0.40 0.00 Cub_1 /Sym MTU1 0.00 0.00 1.00 0.00 0.00 Cub_1 /Tr2 T6 0.00 0.00 1.00 0.00 0.00											Typ: SL Tap: 3.00		Min: 1		Max: 5	
K-BB(3) K4 400V Bu.40 1.07 0.43 1.13 Cub_1 /Sym DOOSAN3 0.42 0.00 1.00 0.57 80.00 Cub_1 /Sym DOOSAN4 0.42 0.31 0.80 0.71 100.00 Cub_1 /Sym DOOSAN5 0.42 0.31 0.80 0.71 100.00 Cub_1 /Tr2 T4 1.26 0.63 0.89 1.91 86.45											Typ: PQ Typ: PQ Typ: PQ Tap: 1.00		Min: 1		Max: 5	
Total Generation:						----- 1.26		----- 0.63								

Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex:		/ 2			
rated Voltage [kv]		Bus-voltage [p.u.]	[kv]	[deg]	Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data					
K-BB(4)															
Kambajawa		0.00	0.99	19.80	148.97										
Cub_1	/Lod	Kambajawa Load			1.69	0.56	0.95	0.05		P10:	1.69 MW	Q10:	0.56 Mvar		
Cub_1	/Lne	K-H1			0.05	0.02	0.91	0.00	0.17	Pv:	0.04 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Lne	K-W Tline			1.01	0.33	0.95	0.03	3.11	Pv:	4.58 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Tr2	T1			-0.43	-0.31	-0.81	0.02	70.60	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T2			-0.00	0.00	-1.00	0.00	0.00	Tap:	5.00	Min:	1	Max:	5
Cub_1	/Tr2	T3			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T4			-1.25	-0.57	-0.91	0.04	86.45	Tap:	1.00	Min:	1	Max:	5
Cub_1	/Tr2	T5			-0.84	0.02	-1.00	0.02	52.75	Tap:	1.00	Min:	1	Max:	5
Cub_1	/Tr2	T6			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T7			-0.25	-0.06	-0.97	0.01	41.05	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T8			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
K-BB(5)															
K4 400V Bu.40		1.04	0.42	0.61											
Cub_1	/Sym	DOOSAN1			0.42	0.00	1.00	0.58	80.00	Typ:	PQ				
Cub_1	/Sym	DOOSAN2			0.42	0.00	1.00	0.58	80.00	Typ:	PQ				
Cub_1	/Tr2	T5			0.84	0.00	1.00	1.16	52.75	Tap:	1.00	Min:	1	Max:	5
Total Generation:					0.84	0.00									
K-BB															
K2 400V Bu.40		1.00	0.40	0.00											
Cub_1	/Sym	MAN1			0.25	0.07	0.96	0.37	48.11	Typ:	SL				
Cub_1	/Tr2	T7			0.25	0.07	0.96	0.37	41.05	Tap:	3.00	Min:	1	Max:	5
KBB10															
K5 400V 0.40		1.02	0.41	0.08											
Cub_1	/Sym	MTU2			0.43	0.32	0.80	0.76	100.00	Typ:	PQ				
Cub_1	/Tr2	T1			0.43	0.32	0.80	0.76	70.60	Tap:	3.00	Min:	1	Max:	5
KBB11															
K6 400V 0.40		1.00	0.40	0.00											
Cub_1	/Sym	MAN2			0.00	-0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T2			0.00	-0.00	1.00	0.00	0.00	Tap:	5.00	Min:	1	Max:	5
KBB12															
K7 400V 0.40		1.00	0.40	0.00											
Cub_1	/Sym	MTU4			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T3			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5

Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex:				/ 3	
rated Voltage [kv]		Bus-voltage [p.u.]	Bus-voltage [kv]	[deg]	Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data					
Single Busbar(3)															
K-H2	20.00	0.99	19.78	148.97											
Cub_1	/Lne	K-H1			-0.05	-0.03	-0.88	0.00	0.17	Pv:	0.04 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Lne	K-H2 Tline			0.05	0.03	0.88	0.00	0.18	Pv:	0.15 kw	cLod:	0.00 Mvar	L:	18.00 km
WBB(1)															
w6.3kv	6.30	0.00	0.00	0.00											
Cub_1	/Sym	SWD1			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Sym	SWD2			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Sym	SWD3								Typ:	PQ				
Cub_1	/Sym	YANMAR			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T12			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Total Generation:					0.00	0.00									
WBB(2)															
w3 400v	0.40	1.00	0.40	0.00											
Cub_1	/Sym	CAT C32			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T14			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
WBB(3)															
Waingapu	20.00	0.98	19.68	148.73											
Cub_1	/Lod	Waingapu Load			1.01	0.33	0.95	0.03		P10:	1.01 MW	Q10:	0.33 Mvar		
Cub_1	/Lne	K-W Tline			-1.01	-0.33	-0.95	0.03	3.11	Pv:	4.58 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Tr2	T11			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T12			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T13			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T14			-0.00	-0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
WBB(4)															
w2 400v	0.40	1.00	0.40	0.00											
Cub_1	/Sym	DEUT Z-2			0.00	-0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T13			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
WBB															
w1 400v	0.40	1.00	0.40	0.00											
Cub_1	/Sym	DEUT Z-1			0.00	-0.00	1.00	0.00	0.00	Typ:	SL				
Cub_1	/Tr2	T11			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
WTG01LV															
	0.69	0.00	0.00	0.00											
Cub_4	/Genstat	WTG01			0.00	0.00	1.00	0.00	0.00						
Cub_3	/Tr2	WTG01 Trafo			0.00	0.00	1.00	0.00	0.00	Tap:	0.00	Min:	-2	Max:	2
										DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015			

15.2.1 Date: 4/22/2015										
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits						Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations			No 0.01 kVA 0.01 %
Grid: Sumba System Stage: Sumba Study Case: KHTL Annex: / 6										
Volt. Level [kV]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compen- sation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
0.40	2.78 1.02	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv		0.00 0.00	0.00 0.00	0.00 0.00
							2.78 1.02	0.02 0.11	0.02 0.11	0.00 0.00
0.69	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
6.30	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
20.00	0.00 0.00	0.00 0.00	2.75 0.92	0.00 0.00	0.00 0.00	0.40 kv		0.00 -0.01	0.00 0.01	0.00 -0.01
							-2.76 -0.91	0.02 0.11	0.02 0.11	0.00 0.00
Total:	2.78 1.02	0.00 0.00	2.75 0.92	0.00 0.00	0.00 0.00		0.00 0.00	0.03 0.10	0.03 0.12	0.00 -0.01
							DIGSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015		
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits						Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations			No 0.01 kVA 0.01 %
Total System Summary Study Case: KHTL Annex: / 7										
	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compen- sation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]		Inter Area Flow [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]

\pramod\Sumba-V3_NWLL\Network Model\Network Data\Sumba									
	2.78	0.00	2.75	0.00	0.00	0.00	0.03	0.03	0.00
	1.02	0.00	0.92	0.00	0.00	0.00	0.10	0.12	-0.01
Total:									
	2.78	0.00	2.75	0.00	0.00		0.03	0.03	0.00
	1.02	0.00	0.92	0.00	0.00		0.10	0.12	-0.01
							DigSILENT PowerFactory 15.2.1	Project:	
								Date: 4/22/2015	

Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange									
AC Load Flow, balanced, positive sequence					Automatic Model Adaptation for Convergence				No
Automatic Tap Adjust of Transformers					Max. Acceptable Load Flow Error for				
Consider Reactive Power Limits					Nodes				0.01 kVA
					Model Equations				0.01 %

Area: Kambajawa						Study Case: KHTL			Annex: / 8	
Volt. Level [kV]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
0.40	2.78 1.02	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv		0.00 0.00	0.00 0.00	0.00 0.00
							2.78 1.02	0.02 0.11	0.02 0.11	0.00 0.00
20.00	0.00 0.00	0.00 0.00	1.69 0.56	0.00 0.00	0.00 0.00	0.40 kv	-2.76 -0.91	0.02 0.11	0.02 0.11	0.00 0.00
						waingapu	1.01 0.33	0.00 0.00	0.00 0.01	-0.00 -0.00
Total:	2.78 1.02	0.00 0.00	1.69 0.56	0.00 0.00	0.00 0.00	waingapu	1.06 0.36 1.01 0.33	0.02 0.11 0.00 0.00	0.02 0.11 0.00 0.01	0.00 0.00 -0.00 -0.00

							DigSILENT PowerFactory 15.2.1	Project:	
								Date: 4/22/2015	

Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange									
AC Load Flow, balanced, positive sequence					Automatic Model Adaptation for Convergence				No
Automatic Tap Adjust of Transformers					Max. Acceptable Load Flow Error for				
Consider Reactive Power Limits					Nodes				0.01 kVA
					Model Equations				0.01 %

Area: Waingapu						Study Case: KHTL			Annex: / 9		
Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]	
0.40	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00	
6.30	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00	
20.00	0.00 0.00	0.00 0.00	1.01 0.33	0.00 0.00	0.00 0.00	Kambajawa	-1.01 -0.33	0.00 0.00 0.00	0.00 0.00 0.01	0.00 0.00 -0.00	
Total:	0.00 0.00	0.00 0.00	1.01 0.33	0.00 0.00	0.00 0.00	Kambajawa	-1.01 -0.33 -1.01 -0.33	0.00 0.00 0.00 0.00	0.00 0.01 0.00 0.01	-0.00 -0.00 -0.00 -0.00	
							DIGSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015			
Load Flow Calculation						Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange					
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits					Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %	
Area: Haharu						Study Case: KHTL			Annex: / 10		
Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]	
20.00	0.00 0.00	0.00 0.00	0.05 0.03	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00	
Total:	0.00 0.00	0.00 0.00	0.05 0.03	0.00 0.00	0.00 0.00		-0.05 -0.03	0.00 0.00	0.00 0.00	0.00 0.00	
							DIGSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015			

Load Flow Calculation					Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange				
AC Load Flow, balanced, positive sequence					Automatic Model Adaptation for Convergence		No		
Automatic Tap Adjust of Transformers					Yes		Max. Acceptable Load Flow Error for		
Consider Reactive Power Limits					No		Nodes		0.01 kVA
							Model Equations		0.01 %
Area Summaries					Study Case: KHTL			Annex:	
								/ 11	
Generation	Motor Load	Load	Compensation	External Infeed	Inter Area Flow	Total Losses	Load Losses	No load Losses	
[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	
\pramod\Sumba-V3_NWLL\Network Model\Network Data\Areas\Kambajawa					1.06	0.02	0.02	0.00	
2.779	0.000	1.691	0.000	0.000	0.36	0.11	0.11	0.00	
1.022	0.000	0.556	0.000	0.000					
\pramod\Sumba-V3_NWLL\Network Model\Network Data\Areas\Waingapu					-1.01	0.00	0.00	-0.00	
0.000	0.000	1.009	0.000	0.000	-0.33	0.00	0.01	-0.00	
0.000	0.000	0.332	0.000	0.000					
\pramod\Sumba-V3_NWLL\Network Model\Network Data\Areas\Haharu					-0.05	0.00	0.00	0.00	
0.000	0.000	0.051	0.000	0.000	-0.03	0.00	0.00	0.00	
0.000	0.000	0.032	0.000	0.000					

High Wind High Load (For One WTG)

										DigSILENT PowerFactory 15.2.1		Project: ----- Date: 4/22/2015												
Load Flow Calculation										Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange														
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits								Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations						No 0.01 kVA 0.01 %								
Grid: Sumba										System Stage: Sumba					Study Case: KHTL					Annex: / 1				
		rated voltage [kV]	Bus-voltage [p.u.]		[kV]	[deg]	Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data												
HB(1) Haharu 20.00 1.03 20.63 149.98 Cub_1 /Lod Haharu Load 0.10 0.06 0.85 0.00 Cub_1 /Lne K-H2 Tline 0.74 -0.12 0.99 0.02 2.09 Cub_1 /Tr2 WTG01 Trafo -0.84 0.06 -1.00 0.02 96.09												P10:	0.10 MW	Q10:	0.06 Mvar									
												Pv:	22.53 kW	clod:	0.00 Mvar	L:	18.00 km							
												Tap:	0.00	Min:	-2	Max:	2							
K-BB(1) K1 400V Bu.40 1.00 0.40 -0.15 Cub_1 /Sym Volvo 0.22 0.17 0.80 0.40 100.00 Cub_1 /Tr2 T8 0.22 0.17 0.80 0.40 87.14												Typ:	PQ											
												Tap:	4.00	Min:	1	Max:	5							
K-BB(2) K3 400V Bu.40 1.00 0.40 0.00 Cub_1 /Sym MTU1 0.58 0.40 0.82 1.01 86.33 Cub_1 /Tr2 T6 0.58 0.40 0.82 1.01 70.14												Typ:	SL											
												Tap:	4.00	Min:	1	Max:	5							
K-BB(3) K4 400V Bu.40 1.02 0.41 0.91 Cub_1 /Sym DOOSAN3 0.42 0.31 0.80 0.75 100.00 Cub_1 /Sym DOOSAN4 0.42 0.31 0.80 0.75 100.00 Cub_1 /Sym DOOSAN5 0.42 0.31 0.80 0.75 100.00 Cub_1 /Tr2 T4 1.26 0.94 0.80 2.24 96.83												Typ:	PQ											
												Typ:	PQ											
												Typ:	PQ											
												Tap:	4.00	Min:	1	Max:	5							
							-----	-----																
Total Generation:							1.26	0.94																

Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex:				/ 2			
rated Voltage [kv]		Bus-voltage [p.u.] [kv]		Active Power [MW]		Reactive Power [Mvar]		Power Factor [-]		Current [kA]		Loading [%]		Additional Data			
K-BB(4)																	
Kambajawa0.00		1.00 19.91 148.63															
Cub_1	/Lod	Kambajawa Load		3.49	1.69	0.90	0.11						P10:	3.49 MW	Q10:	1.69 Mvar	
Cub_1	/Lne	K-H1		-0.71	0.13	-0.98	0.02	2.09					Pv:	6.07 kw	cLod:	0.00 Mvar	
Cub_1	/Lne	K-W Tline		1.16	0.63	0.88	0.04	3.83					Pv:	6.91 kw	cLod:	0.00 Mvar	
Cub_1	/Tr2	T1		-0.33	-0.24	-0.81	0.01	54.19					Tap:	3.00	Min:	1	
Cub_1	/Tr2	T2		0.00	-0.00	1.00	0.00	0.00					Tap:	5.00	Min:	1	
Cub_1	/Tr2	T3		-0.33	-0.24	-0.81	0.01	54.19					Tap:	3.00	Min:	1	
Cub_1	/Tr2	T4		-1.24	-0.86	-0.82	0.04	96.83					Tap:	4.00	Min:	1	
Cub_1	/Tr2	T5		-0.83	-0.28	-0.95	0.03	56.55					Tap:	4.00	Min:	1	
Cub_1	/Tr2	T6		-0.57	-0.37	-0.84	0.02	70.14					Tap:	4.00	Min:	1	
Cub_1	/Tr2	T7		-0.42	-0.30	-0.82	0.02	86.49					Tap:	5.00	Min:	1	
Cub_1	/Tr2	T8		-0.22	-0.16	-0.81	0.01	87.14					Tap:	4.00	Min:	1	
K-BB(5)																	
K4 400V Bu.40		0.99 0.40 0.33															
Cub_1	/Sym	DOOSAN1		0.42	-0.00	1.00	0.61	80.00					Typ:	PQ			
Cub_1	/Sym	DOOSAN2		0.42	0.31	0.80	0.76	100.00					Typ:	PQ			
Cub_1	/Tr2	T5		0.84	0.31	0.94	1.31	56.55					Tap:	4.00	Min:	1	
Total Generation:				0.84	0.31												
K-BB																	
K2 400V Bu.40		0.99 0.39 0.27															
Cub_1	/Sym	MAN1		0.43	0.32	0.80	0.79	100.00					Typ:	PQ			
Cub_1	/Tr2	T7		0.43	0.32	0.80	0.79	86.49					Tap:	5.00	Min:	1	
KBB10																	
K5 400V 0.40		1.01 0.41 -0.52															
Cub_1	/Sym	MTU2		0.33	0.25	0.80	0.59	76.74					Typ:	PQ			
Cub_1	/Tr2	T1		0.33	0.25	0.80	0.59	54.19					Tap:	3.00	Min:	1	
KBB11																	
K6 400V 0.40		0.95 0.38 -1.37															
Cub_1	/Sym	MAN2		0.00	0.00	1.00	0.00	0.00					Typ:	PQ			
Cub_1	/Tr2	T2		-0.00	0.00	-1.00	0.00	0.00					Tap:	5.00	Min:	1	
KBB12																	
K7 400V 0.40		1.01 0.41 -0.52															
Cub_1	/Sym	MTU4		0.33	0.25	0.80	0.59	76.74					Typ:	PQ			
Cub_1	/Tr2	T3		0.33	0.25	0.80	0.59	54.19					Tap:	3.00	Min:	1	

Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex:		/ 3			
rated Voltage [kV]		Bus-voltage [p.u.]	Bus-voltage [kV]	[deg]	Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data					
Single Busbar(3)															
K-H2	20.00	1.00	20.06	148.98						Pv:	6.07 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Lne	K-H1			0.71	-0.13	0.98	0.02	2.09	Pv:	22.53 kw	cLod:	0.00 Mvar	L:	18.00 km
Cub_1	/Lne	K-H2 Tline			-0.71	0.13	-0.98	0.02	2.09						
WBB(1)															
w6.3kv	6.30	0.99	6.24	-1.02						Typ:	SL				
Cub_1	/Sym	SWD1			0.00	0.00	1.00	0.00	0.00	Typ:	SL				
Cub_1	/Sym	SWD2			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Sym	SWD3								Typ:	PQ				
Cub_1	/Sym	YANMAR			0.22	0.00	1.00	0.02	80.00	Tap:	PQ				
Cub_1	/Tr2	T12			0.22	0.00	1.00	0.02	17.78	Tap:	3.00	Min:	1	Max:	5
		Total Generation:			0.22	0.00									
WBB(2)															
w3 400v	0.40	1.01	0.41	-0.33						Typ:	PQ				
Cub_1	/Sym	CAT C32			0.55	0.41	0.80	0.98	100.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T14			0.55	0.41	0.80	0.98	67.81						
WBB(3)															
Waingapu	20.00	0.99	19.75	148.42						P10:	2.08 MW	Q10:	1.01 Mvar		
Cub_1	/Lod	Waingapu Load			2.08	1.01	0.90	0.07		Pv:	6.91 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Lne	K-W Tline			-1.15	-0.62	-0.88	0.04	3.83	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T11			0.00	-0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T12			-0.22	0.00	-1.00	0.01	17.78	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T13			-0.17	0.00	-1.00	0.00	42.82	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T14			-0.54	-0.39	-0.81	0.02	67.81	Tap:	3.00	Min:	1	Max:	5
WBB(4)															
w2 400v	0.40	0.99	0.40	-0.62						Typ:	PQ				
Cub_1	/Sym	DEUT Z-2			0.17	0.00	1.00	0.25	75.56	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T13			0.17	0.00	1.00	0.25	42.82						
WBB															
w1 400v	0.40	0.99	0.40	-1.58						Typ:	SL				
Cub_1	/Sym	DEUT Z-1			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T11			-0.00	-0.00	-1.00	0.00	0.00						
WTG01LV															
	0.69	1.04	0.72	-176.87											
Cub_4	/Genstat	WTG01			0.85	0.00	1.00	0.68	100.00	Tap:	0.00	Min:	-2	Max:	2
Cub_3	/Tr2	WTG01 Trafo			0.85	0.00	1.00	0.68	96.09						
										DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015			

						15.2.1		Date: 4/22/2015				
Load Flow Calculation						Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange						
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits						Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations			No 0.01 kVA 0.01 %	
Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex: / 6		
Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]		
0.40	4.71 3.05	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	4.71 3.05	0.00 0.00 0.05 0.22	0.00 0.00 0.05 0.22	0.00 0.00 0.00 0.00		
0.69	0.85 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	0.85 0.00	0.00 0.00 0.01 0.06	0.00 0.00 0.01 0.05	0.00 0.00 0.00 0.01		
6.30	0.22 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	0.22 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00		
20.00	0.00 0.00	0.00 0.00	5.68 2.77	0.00 0.00	0.00 0.00	0.40 kv 0.69 kv 6.30 kv	-4.66 -2.83 -0.84 0.06 -0.22 0.00	0.04 0.01 0.05 0.22 0.01 0.06 0.00	0.04 0.02 0.05 0.22 0.01 0.05 0.00	0.00 -0.01 0.00 0.00 0.01 0.00 0.00		
Total:	5.78 3.05	0.00 0.00	5.68 2.77	0.00 0.00	0.00 0.00		0.00 0.00	0.10 0.29	0.10 0.29	0.00 -0.00		
						DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015				
Load Flow Calculation						Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange						
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits						Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations			No 0.01 kVA 0.01 %	

Total System Summary					Study Case: KHTL			Annex:		/ 7
Generation	Motor Load	Load	Compensation	External Infeed	Inter Area Flow	Total Losses	Load Losses	No load Losses		
[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]		
\pramod\Sumba-V3_HWHL\Network Model\Network Data\Sumba										
5.78	0.00	5.68	0.00	0.00	0.00	0.10	0.10	0.00		
3.05	0.00	2.77	0.00	0.00	0.00	0.29	0.29	-0.00		
Total:										
5.78	0.00	5.68	0.00	0.00		0.10	0.10	0.00		
3.05	0.00	2.77	0.00	0.00		0.29	0.29	-0.00		
					DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015			
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence				Automatic Model Adaptation for Convergence		No				
Automatic Tap Adjust of Transformers				Max. Acceptable Load Flow Error for Nodes		0.01 kVA				
Consider Reactive Power Limits				Model Equations		0.01 %				
Area: Kambajawa					Study Case: KHTL			Annex:		/ 8
Volt. Level	Generation	Motor Load	Load	Compensation	External Infeed	Interchange to	Power Interchange	Total Losses	Load Losses	No load Losses
[kv]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]		[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]
0.40	3.99	0.00	0.00	0.00	0.00	20.00 kv		0.00	0.00	0.00
	2.64	0.00	0.00	0.00	0.00			0.00	0.00	0.00
							3.99	0.04	0.04	0.00
							2.64	0.19	0.19	0.00
20.00	0.00	0.00	3.49	0.00	0.00	0.40 kv		0.00	0.00	0.00
	0.00	0.00	1.69	0.00	0.00			0.00	0.00	0.00
							-3.94	0.04	0.04	0.00
							-2.45	0.19	0.19	0.00
						waingapu	1.16	0.01	0.01	0.00
							0.63	0.00	0.01	-0.00
Total:										
	3.99	0.00	3.49	0.00	0.00		0.45	0.04	0.04	0.00
	2.64	0.00	1.69	0.00	0.00		0.75	0.19	0.19	0.00
						waingapu	1.16	0.01	0.01	0.00
							0.63	0.00	0.01	-0.00
					DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015			

Load Flow Calculation		Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange			
AC Load Flow, balanced, positive sequence		Yes No	Automatic Model Adaptation for Convergence		No
Automatic Tap Adjust of Transformers			Max. Acceptable Load Flow Error for		
Consider Reactive Power Limits			Nodes Model Equations		0.01 kVA 0.01 %

Area: waingapu		Study Case: KHTL		Annex: / 9	
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Volt. Level [kV]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
0.40	0.72 0.41	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	0.72 0.41	0.00 0.00 0.01 0.03	0.00 0.00 0.01 0.03	0.00 0.00 0.00 0.00
6.30	0.22 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	0.22 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
20.00	0.00 0.00	0.00 0.00	2.08 1.01	0.00 0.00	0.00 0.00	0.40 kv 6.30 kv Kambajawa	-0.71 -0.39 -0.22 0.00 -1.16 -0.63	0.00 0.00 0.01 0.03 0.00 0.01 0.00	0.00 0.00 0.01 0.03 0.00 0.01 0.01	0.00 0.00 0.00 0.00 0.00 0.00 -0.00
Total:	0.94 0.41	0.00 0.00	2.08 1.01	0.00 0.00	0.00 0.00	Kambajawa	-1.16 -0.63 -1.16 -0.63	0.01 0.03 0.01 0.00	0.01 0.04 0.01 0.01	0.00 -0.00 0.00 -0.00

		DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015	
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Load Flow Calculation		Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange			
AC Load Flow, balanced, positive sequence		Yes No	Automatic Model Adaptation for Convergence		No
Automatic Tap Adjust of Transformers			Max. Acceptable Load Flow Error for		
Consider Reactive Power Limits			Nodes Model Equations		0.01 kVA 0.01 %

Area: Haharu		Study Case: KHTL		Annex: / 10	
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Volt.	Generation	Motor	Load	Compen-	External	Power	Total	Load	No load
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Level [kv]	[MW]/ [Mvar]	Load [MW]/ [Mvar]	[MW]/ [Mvar]	station [MW]/ [Mvar]	Infeed [MW]/ [Mvar]	Interchange to	Interchange [MW]/ [Mvar]	Losses [MW]/ [Mvar]	Losses [MW]/ [Mvar]	Losses [MW]/ [Mvar]	
20.00	0.00 0.00	0.00 0.00	0.10 0.06	0.00 0.00	0.00 0.00	0.69 kv		0.00 0.00 0.01 0.06	0.00 0.00 0.01 0.05	0.00 0.00 0.00 0.01	
Total:	0.00 0.00	0.00 0.00	0.10 0.06	0.00 0.00	0.00 0.00			-0.11 -0.12	0.01 0.06	0.01 0.05	0.00 0.01
							DIGSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015			
Load Flow Calculation Complete System Report: Substations, voltage Profiles, Grid Interchange, Area Interchange											
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits					Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %	
Area Summaries						Study Case: KHTL			Annex: / 11		
Generation [MW]/ [Mvar]		Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compen- sation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Inter Area Flow [MW]/ [Mvar]		Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]	
\pramod\Sumba-V3_HWHL\Network			Model\Network	Data\Areas\Kambajawa							
3.988		0.000	3.494	0.000	0.000	0.45		0.04	0.04	0.00	
2.640		0.000	1.692	0.000	0.000	0.75		0.19	0.19	0.00	
\pramod\Sumba-V3_HWHL\Network			Model\Network	Data\Areas\waingapu							
0.940		0.000	2.084	0.000	0.000	-1.16		0.01	0.01	0.00	
0.412		0.000	1.009	0.000	0.000	-0.63		0.03	0.04	-0.00	
\pramod\Sumba-V3_HWHL\Network			Model\Network	Data\Areas\Haharu							
0.000		0.000	0.104	0.000	0.000	-0.11		0.01	0.01	0.00	
0.000		0.000	0.064	0.000	0.000	-0.12		0.06	0.05	0.01	

										DigSILENT PowerFactory 15.2.1		Project: ----- Date: 4/22/2015					
Load Flow Calculation										Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange							
AC Load Flow, balanced, positive sequence							Automatic Model Adaptation for Convergence					No					
Automatic Tap Adjust of Transformers					Yes		Max. Acceptable Load Flow Error for					0.01 kVA					
Consider Reactive Power Limits					No		Nodes Model Equations					0.01 %					
Grid: Sumba										System Stage: Sumba		Study Case: KHTL				Annex: / 1	
rated Voltage [kV]		Bus-voltage [p.u.]		[kV] [deg]		Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data						
HB(1) Haharu 20.00 1.04 20.79 150.00																	
Cub_1 /Lod		Haharu Load				0.05	0.03	0.85	0.00		P10:	0.05 MW	Q10:	0.03 Mvar			
Cub_1 /Lne		K-H2 Tline				0.79	-0.08	1.00	0.02	2.22	Pv:	25.40 kw	cLod:	0.00 Mvar	L:	18.00 km	
Cub_1 /Tr2		WTG01 Trafo				-0.85	0.05	-1.00	0.02	44.03	Tap:	0.00	Min:	-2	Max:	2	
K-BB(1) K1 400V Bu.40 1.00 0.40 0.00																	
Cub_1 /Sym		Volvo				0.00	0.00	1.00	0.00	0.00	Typ:	PQ					
Cub_1 /Tr2		T8				0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5	
K-BB(2) K3 400V Bu.40 1.00 0.40 0.00																	
Cub_1 /Sym		MTU1				0.00	0.00	1.00	0.00	0.00	Typ:	PQ					
Cub_1 /Tr2		T6				0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5	
K-BB(3) K4 400V Bu.40 1.00 0.40 0.00																	
Cub_1 /Sym		DOOSAN3				0.42	0.26	0.85	0.71	94.12	Typ:	PQ					
Cub_1 /Sym		DOOSAN4				0.42	0.26	0.85	0.71	94.12	Typ:	PQ					
Cub_1 /Sym		DOOSAN5				0.27	0.25	0.74	0.54	70.63	Typ:	SL					
Cub_1 /Tr2		T4				1.11	0.77	0.82	1.95	52.09	Tap:	4.00	Min:	1	Max:	5	
		Total				-----	-----										
		Generation:				1.11	0.77										

Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex:		/ 2			
rated Voltage [kV]		Bus-voltage [p.u.]	[kV]	[deg]	Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data					
K-BB(4)															
Kambajawa0.00		1.00	19.99	148.73											
Cub_1	/Lod	Kambajawa Load			1.69	0.56	0.95	0.05		P10:	1.69 MW	Q10:	0.56 Mvar		
Cub_1	/Lne	K-H1			-0.76	0.08	-0.99	0.02	2.22	Pv:	6.85 kW	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Lne	K-W Tline			1.01	0.33	0.95	0.03	3.08	Pv:	4.49 kW	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Tr2	T1			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T2			-0.00	-0.00	-1.00	0.00	0.00	Tap:	5.00	Min:	1	Max:	5
Cub_1	/Tr2	T3			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T4			-1.11	-0.73	-0.83	0.04	52.09	Tap:	4.00	Min:	1	Max:	5
Cub_1	/Tr2	T5			-0.84	-0.24	-0.96	0.03	34.25	Tap:	4.00	Min:	1	Max:	5
Cub_1	/Tr2	T6			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T7			-0.00	-0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T8			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
K-BB(5)															
K4 400V Bu.40		0.99	0.39	-0.21											
Cub_1	/Sym	DOOSAN1			0.42	-0.00	1.00	0.61	80.00	Typ:	PQ				
Cub_1	/Sym	DOOSAN2			0.42	0.26	0.85	0.72	94.12	Typ:	PQ				
Cub_1	/Tr2	T5			0.84	0.26	0.96	1.29	34.25	Tap:	4.00	Min:	1	Max:	5
					Total Generation:	0.84	0.26								
K-BB															
K2 400V Bu.40		1.00	0.40	0.00											
Cub_1	/Sym	MAN1			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T7			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
KBB10															
K5 400V 0.40		1.00	0.40	0.00											
Cub_1	/Sym	MTU2			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T1			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
KBB11															
K6 400V 0.40		1.00	0.40	0.00											
Cub_1	/Sym	MAN2			0.00	-0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T2			0.00	0.00	1.00	0.00	0.00	Tap:	5.00	Min:	1	Max:	5
KBB12															
K7 400V 0.40		1.00	0.40	0.00											
Cub_1	/Sym	MTU4			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T3			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5

Grid: Sumba		System Stage: Sumba				Study Case: KHTL				Annex:				/ 3	
rated Voltage [kV]		Bus-voltage [p.u.]	Bus-voltage [kV]	[deg]	Active Power [MW]	Reactive Power [Mvar]	Power Factor [-]	Current [kA]	Loading [%]	Additional Data					
Single Busbar(3)															
K-H2	20.00	1.01	20.16	149.07											
Cub_1	/Lne	K-H1			0.77	-0.08	0.99	0.02	2.22	Pv:	6.85 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Lne	K-H2 Tline			-0.77	0.08	-0.99	0.02	2.22	Pv:	25.40 kw	cLod:	0.00 Mvar	L:	18.00 km
WBB(1)															
w6.3kv	6.30	0.00	0.00	0.00											
Cub_1	/Sym	SWD1			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Sym	SWD2			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Sym	SWD3								Typ:	PQ				
Cub_1	/Sym	YANMAR			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T12			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Total Generation:					0.00	0.00									
WBB(2)															
w3 400v	0.40	1.00	0.40	0.00											
Cub_1	/Sym	CAT C32			0.00	0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T14			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
WBB(3)															
Waingapu	20.00	0.99	19.87	148.50											
Cub_1	/Lod	Waingapu Load			1.01	0.33	0.95	0.03		P10:	1.01 MW	Q10:	0.33 Mvar		
Cub_1	/Lne	K-W Tline			-1.01	-0.33	-0.95	0.03	3.08	Pv:	4.49 kw	cLod:	0.00 Mvar	L:	7.00 km
Cub_1	/Tr2	T11			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T12			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T13			-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
Cub_1	/Tr2	T14			-0.00	-0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
WBB(4)															
w2 400v	0.40	1.00	0.40	0.00											
Cub_1	/Sym	DEUT Z-2			0.00	-0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T13			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
WBB															
w1 400v	0.40	1.00	0.40	0.00											
Cub_1	/Sym	DEUT Z-1			0.00	-0.00	1.00	0.00	0.00	Typ:	PQ				
Cub_1	/Tr2	T11			0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5
WTG01LV															
	0.69	1.04	0.72	-178.56											
Cub_4	/Genstat	WTG01			0.85	0.00	1.00	0.68	100.00						
Cub_3	/Tr2	WTG01 Trafo			0.85	0.00	1.00	0.68	44.03	Tap:	0.00	Min:	-2	Max:	2
										DigSILENT PowerFactory 15.2.1		Project: Date: 4/22/2015			

Load Flow Calculation		Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange					
AC Load Flow, balanced, positive sequence		Automatic Tap Adjust of Transformers		Automatic Model Adaptation for Convergence		No	
Consider Reactive Power Limits		Yes No		Max. Acceptable Load Flow Error for Nodes Model Equations		0.01 kVA 0.01 %	
Grid: Sumba		System Stage: Sumba		Study Case: KHTL		Annex: / 4	
	rtd.V [kv]	Bus - [p.u.]	voltage [kv] [deg]	-10	-5	Voltage - Deviation [%] 0 +5 +10	
HB(1)							
Haharu	20.00	1.039	20.79 150.00			>>>>>>>>	
K-BB(1)							
K1 400V Bus	0.40	1.000	0.40 0.00				
K-BB(2)							
K3 400V Bus	0.40	1.000	0.40 0.00				
K-BB(3)							
K4 400V Bus	0.40	1.000	0.40 0.00				
K-BB(4)							
Kambajawa	20.00	0.999	19.99 148.73				
K-BB(5)						<<<	
K4 400V Bus	0.40	0.987	0.39 -0.21				
K-BB							
K2 400V Bus	0.40	1.000	0.40 0.00				
KBB10							
K5 400V	0.40	1.000	0.40 0.00				
KBB11							
K6 400V	0.40	1.000	0.40 0.00				
KBB12							
K7 400V	0.40	1.000	0.40 0.00				
Single Busbar(3)						>>	
K-H2	20.00	1.008	20.16 149.07				
WBB(1)						<\\	
w6.3kv	6.30	0.000	0.00 0.00				
WBB(2)							
w3 400V	0.40	1.000	0.40 0.00				
WBB(3)							
waingapu	20.00	0.994	19.87 148.50			<	
WBB(4)							
w2 400V	0.40	1.000	0.40 0.00				
WBB							
w1 400V	0.40	1.000	0.40 0.00				
WTG01LV							
Grid: Sumba		System Stage: Sumba		Study Case: KHTL		Annex: / 5	
	rtd.V [kv]	Bus - [p.u.]	voltage [kv] [deg]	-10	-5	Voltage - Deviation [%] 0 +5 +10	
	0.69	1.043	0.72-178.56			>>>>>>>>	
				DigSILENT PowerFactory		Project:	

Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange

AC Load Flow, balanced, positive sequence	Yes	Automatic Model Adaptation for Convergence	No
Automatic Tap Adjust of Transformers	No	Max. Acceptable Load Flow Error for	0.01 kVA
Consider Reactive Power Limits		Nodes	0.01 %
		Model Equations	

Grid: Sumba System Stage: Sumba Study Case: KHTL Annex: / 6

Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
0.40	1.95 1.03	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	1.95 1.03	0.00 0.00 0.01 0.06	0.00 0.00 0.01 0.06	0.00 0.00 0.00 0.00
0.69	0.85 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	0.85 0.00	0.00 0.00 0.00 0.05	0.00 0.00 0.00 0.02	0.00 0.00 0.00 0.02
6.30	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
20.00	0.00 0.00	0.00 0.00	2.75 0.92	0.00 0.00	0.00 0.00	0.40 kv 0.69 kv	-1.94 -0.97 -0.85 0.05	0.04 0.01 0.01 0.06 0.00 0.05	0.04 0.02 0.01 0.06 0.00 0.02	-0.00 -0.01 0.00 0.00 0.00 0.02
Total:	2.80 1.03	0.00 0.00	2.75 0.92	0.00 0.00	0.00 0.00		0.00 0.00	0.05 0.11	0.05 0.10	0.00 0.01

DigSILENT PowerFactory 15.2.1	Project:
	Date: 4/22/2015

Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange

AC Load Flow, balanced, positive sequence	Yes	Automatic Model Adaptation for Convergence	No
Automatic Tap Adjust of Transformers	No	Max. Acceptable Load Flow Error for	0.01 kVA
Consider Reactive Power Limits		Nodes	0.01 %
		Model Equations	

Total System Summary Study Case: KHTL Annex: / 7

Generation	Motor	Load	Compensation	External Infeed	Inter Area	Total	Load	No load
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	[MW]/ [Mvar]	Load [MW]/ [Mvar]	[MW]/ [Mvar]	sation [MW]/ [Mvar]	Infeed [MW]/ [Mvar]		Flow [MW]/ [Mvar]	Losses [MW]/ [Mvar]	Losses [MW]/ [Mvar]	Losses [MW]/ [Mvar]
\pramod\Sumba-V3_HWLL\Network Model\Network Data\Sumba										
	2.80	0.00	2.75	0.00	0.00		0.00	0.05	0.05	0.00
	1.03	0.00	0.92	0.00	0.00		0.00	0.11	0.10	0.01
Total:										
	2.80	0.00	2.75	0.00	0.00			0.05	0.05	0.00
	1.03	0.00	0.92	0.00	0.00			0.11	0.10	0.01
							DigSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015		
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence					Yes No	Automatic Model Adaptation for Convergence				No
Automatic Tap Adjust of Transformers						Max. Acceptable Load Flow Error for				0.01 kVA
Consider Reactive Power Limits						Nodes Model Equations				0.01 %
Area: Kambajawa						Study Case: KHTL			Annex: / 8	
Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compen- sation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
0.40	1.95	0.00	0.00	0.00	0.00	20.00 kv		0.00	0.00	0.00
	1.03	0.00	0.00	0.00	0.00		1.95	0.01	0.01	0.00
							1.03	0.06	0.06	0.00
20.00	0.00	0.00	1.69	0.00	0.00	0.40 kv waingapu		0.00	0.00	0.00
	0.00	0.00	0.56	0.00	0.00			0.00	0.00	0.00
							-1.94	0.01	0.01	0.00
							-0.97	0.06	0.06	0.00
							1.01	0.00	0.00	0.00
						0.33	0.00	0.01	-0.00	
Total:	1.95	0.00	1.69	0.00	0.00	waingapu	0.25	0.01	0.01	0.00
	1.03	0.00	0.56	0.00	0.00		0.42	0.06	0.06	0.00
							1.01	0.00	0.00	0.00
							0.33	0.00	0.01	-0.00
							DigSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015		
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										

AC Load Flow, balanced, positive sequence	Yes	Automatic Model Adaptation for Convergence	No
Automatic Tap Adjust of Transformers	No	Max. Acceptable Load Flow Error for	0.01 kVA
Consider Reactive Power Limits		Nodes	0.01 %
		Model Equations	

Area: waingapu	Study Case: KHTL	Annex:	/ 9
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Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
0.40	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
6.30	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
20.00	0.00 0.00	0.00 0.00	1.01 0.33	0.00 0.00	0.00 0.00	Kambajawa	-1.01 -0.33	0.00 0.00 0.00	0.00 0.00 0.01	0.00 0.00 -0.00
Total:	0.00 0.00	0.00 0.00	1.01 0.33	0.00 0.00	0.00 0.00	Kambajawa	-1.01 -0.33 -1.01 -0.33	0.00 0.00 0.00 0.00	0.00 0.01 0.00 0.01	0.00 -0.00 0.00 -0.00

		DigSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015
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Load Flow Calculation	Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange
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AC Load Flow, balanced, positive sequence	Yes	Automatic Model Adaptation for Convergence	No
Automatic Tap Adjust of Transformers	No	Max. Acceptable Load Flow Error for	0.01 kVA
Consider Reactive Power Limits		Nodes	0.01 %
		Model Equations	

Area: Haharu	Study Case: KHTL	Annex:	/ 10
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Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
20.00	0.00 0.00	0.00 0.00	0.05 0.03	0.00 0.00	0.00 0.00	0.69 kv	-0.85 0.05	0.00 0.00 0.00 0.05	0.00 0.00 0.00 0.02	0.00 0.00 0.00 0.02
Total:	0.00 0.00	0.00 0.00	0.05 0.03	0.00 0.00	0.00 0.00		-0.06 -0.08	0.00 0.05	0.00 0.02	0.00 0.02

					DigSILENT PowerFactory 15.2.1	Project: Date: 4/22/2015
Load Flow Calculation					Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange	
AC Load Flow, balanced, positive sequence					Automatic Model Adaptation for Convergence	
Automatic Tap Adjust of Transformers					Max. Acceptable Load Flow Error for	
Consider Reactive Power Limits					Nodes	
					Model Equations	
Area Summaries					Study Case: KHTL	Annex: / 11
Generation	Motor Load	Load	Compensation	External Infeed	Inter Area Flow	Total Losses
[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]
\pramod\Sumba-V3_HWLL\Network Model\Network Data\Areas\Kambajawa					0.25	0.01
					0.42	0.06
\pramod\Sumba-V3_HWLL\Network Model\Network Data\Areas\Waingapu					-1.01	0.00
					-0.33	0.00
\pramod\Sumba-V3_HWLL\Network Model\Network Data\Areas\Haharu					-0.06	0.00
					-0.08	0.05

High Wind High Load (For Two WTGs)

										DigSILENT PowerFactory 15.2.1		Project: Date: 9/28/2015									
Load Flow Calculation										Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange											
AC Load Flow, balanced, positive sequence					Automatic Tap Adjust of Transformers					Yes		Automatic Model Adaptation for Convergence					No				
Consider Reactive Power Limits					No							Max. Acceptable Load Flow Error for					0.01 kVA				
												Nodes					0.01 %				
												Model Equations									
Grid: Sumba										System Stage: Sumba					Study Case: KGL-noclear					Annex: / 1	
rated voltage [kV]		Bus-voltage [p.u.]		[kV]		[deg]		Active Power [MW]		Reactive Power [Mvar]		Power Factor [-]		Current [kA]		Loading [%]		Additional Data			
HB(1)																					
Haharu		20.00		1.08		21.69		151.82										P10: 0.10 MW		Q10: 0.06 Mvar	
Cub_1 /Lod		Haharu Load						0.10		0.06		0.85		0.00				Pv: 92.37 kW		cLod: 0.00 Mvar	
Cub_1 /Lne		K-H2 Tline						1.58		-0.17		0.99		0.04		4.23		L: 18.00 km		L: 0.00 km	
Cub_1 /Lne		Line						-0.00		0.00		-1.00		0.00		0.00		cLod: -0.00 Mvar		L: 0.00 km	
Cub_1 /Tr2		WTG01 Trafo						-0.84		0.05		-1.00		0.02		91.49		Tap: 0.00		Min: -2	
Cub_1 /Tr2		WTG01 Trafo(1)						-0.84		0.05		-1.00		0.02		91.49		Tap: 0.00		Max: 2	
K-BB(1)																					
K1 400V Bu.40		1.06		0.42		0.43												Typ: PQ			
Cub_1 /Sym		Volvo						0.22		0.17		0.80		0.37		100.00		Tap: 2.00		Min: 1	
Cub_1 /Tr2		T8						0.22		0.17		0.80		0.37		84.34				Max: 5	
K-BB(2)																					
K3 400V Bu.40		1.06		0.42		0.69												Typ: PQ			
Cub_1 /Sym		MTU1						0.65		0.49		0.80		1.10		100.00		Tap: 2.00		Min: 1	
Cub_1 /Tr2		T6						0.65		0.49		0.80		1.10		78.27				Max: 5	
K-BB(3)																					
K4 400V Bu.40		1.07		0.43		1.38												Typ: PQ			
Cub_1 /Sym		DOOSAN3						0.42		0.31		0.80		0.71		100.00		Typ: PQ			
Cub_1 /Sym		DOOSAN4						0.42		0.31		0.80		0.71		100.00		Typ: PQ			
Cub_1 /Sym		DOOSAN5						0.42		0.31		0.80		0.71		100.00		Typ: PQ			
Cub_1 /Tr2		T4						1.26		0.94		0.80		2.12		93.85		Tap: 2.00		Min: 1	
Total Generation:								1.26		0.94										Max: 5	
Grid: Sumba										System Stage: Sumba					Study Case: KGL-noclear					Annex: / 2	
rated voltage [kV]		Bus-voltage [p.u.]		[kV]		[deg]		Active Power [MW]		Reactive Power [Mvar]		Power Factor [-]		Current [kA]		Loading [%]		Additional Data			
K-BB(4)																					

Kambajava0.00 1.01 20.19 149.35																
Cub_1 /Lod	Kambajava Load				3.49	1.69	0.90	0.11		P10:	3.49 MW	Q10:	1.69 Mvar	L:	7.00 km	
Cub_1 /Lne	K-H1				-1.46	0.21	-0.99	0.04	4.22	Pv:	24.91 kW	cLod:	0.00 Mvar	L:	7.00 km	
Cub_1 /Lne	K-W Tline				1.88	0.86	0.91	0.06	5.93	Pv:	16.59 kW	cLod:	0.00 Mvar	L:	7.00 km	
Cub_1 /Tr2	T1				-0.43	-0.31	-0.81	0.02	69.31	Tap:	3.00	Min:	1	Max:	5	
Cub_1 /Tr2	T2				-0.00	-0.00	-1.00	0.00	0.00	Tap:	5.00	Min:	1	Max:	5	
Cub_1 /Tr2	T3				-0.38	-0.27	-0.81	0.01	61.42	Tap:	3.00	Min:	1	Max:	5	
Cub_1 /Tr2	T4				-1.24	-0.87	-0.82	0.04	93.85	Tap:	2.00	Min:	1	Max:	5	
Cub_1 /Tr2	T5				-0.83	-0.59	-0.81	0.03	63.33	Tap:	2.00	Min:	1	Max:	5	
Cub_1 /Tr2	T6				-0.64	-0.46	-0.81	0.02	78.27	Tap:	2.00	Min:	1	Max:	5	
Cub_1 /Tr2	T7				-0.18	-0.12	-0.83	0.01	33.87	Tap:	4.00	Min:	1	Max:	5	
Cub_1 /Tr2	T8				-0.22	-0.16	-0.81	0.01	84.34	Tap:	2.00	Min:	1	Max:	5	
K-BB(5)																
K4 400v Bu.40	1.06 0.42 0.72															
Cub_1 /Sym	DOOSAN1				0.42	0.31	0.80	0.72	100.00	Typ:	PQ					
Cub_1 /Sym	DOOSAN2				0.42	0.31	0.80	0.72	100.00	Typ:	PQ					
Cub_1 /Tr2	T5				0.84	0.63	0.80			Tap:	2.00	Min:	1	Max:	5	
Total Generation:					0.84	0.63										
K-BB																
K2 400v Bu.40	1.00 0.40 0.00															
Cub_1 /Sym	MAN1				0.18	0.12	0.83	0.31	39.70	Typ:	SL					
Cub_1 /Tr2	T7				0.18	0.12	0.83	0.31	33.87	Tap:	4.00	Min:	1	Max:	5	
KBB10																
K5 400v 0.40	1.03 0.41 0.42															
Cub_1 /Sym	MTU2				0.43	0.32	0.80	0.75	100.00	Typ:	PQ					
Cub_1 /Tr2	T1				0.43	0.32	0.80	0.75	69.31	Tap:	3.00	Min:	1	Max:	5	
KBB11																
K6 400v 0.40	1.00 0.40 0.00															
Cub_1 /Sym	MAN2				0.00	0.00	1.00	0.00	0.00	Typ:	PQ					
Cub_1 /Tr2	T2				0.00	0.00	1.00	0.00	0.00	Tap:	5.00	Min:	1	Max:	5	
KBB12																
K7 400v 0.40	1.03 0.41 0.30															
Cub_1 /Sym	MTU4				0.38	0.28	0.80	0.66	88.37	Typ:	PQ					
Cub_1 /Tr2	T3				0.38	0.28	0.80	0.66	61.42	Tap:	3.00	Min:	1	Max:	5	
Grid: Sumba System Stage: Sumba Study Case: KGL-noclear Annex: / 3																
rated voltage [kv] Bus-voltage [p.u.] [kv] [deg] Active Power [MW] Reactive Power [Mvar] Power Factor [-] Current [kA] Loading [%]										Additional Data						
Single Busbar(3)																
K-H2 20.00	1.02 20.50 150.01															
Cub_1 /Lne	K-H1				1.49	-0.21	0.99	0.04	4.22	Pv:	24.91 kW	cLod:	0.00 Mvar	L:	7.00 km	
Cub_1 /Lne	K-H2 Tline				-1.49	0.21	-0.99	0.04	4.23	Pv:	92.37 kW	cLod:	0.00 Mvar	L:	18.00 km	
WBB(1)																
w6.3kv 6.30	1.01 6.34 -0.57															
Cub_1 /Sym	SWD1				0.00	0.00	1.00	0.00	0.00	Typ:	SL					
Cub_1 /Sym	SWD2				0.00	0.00	1.00	0.00	0.00	Typ:	SL					

		DigSILENT PowerFactory 15.2.1	Project: Date: 9/28/2015
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Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange			
Load Flow Calculation			
AC Load Flow, balanced, positive sequence		Automatic Model Adaptation for Convergence	No
Automatic Tap Adjust of Transformers	Yes	Max. Acceptable Load Flow Error for	
Consider Reactive Power Limits	No	Nodes	0.01 kVA
		Model Equations	0.01 %

Grid: Sumba System Stage: Sumba Study Case: KGL-nuclear Annex: / 5

	rtd.V [kV]	Bus - [p.u.]	voltage [kV]	[deg]	-10	-5	voltage - Deviation [%] 0 +5 +10
HB(1)							
Haharu	20.00	1.084	21.69	151.82			>>>>>>>>>>>>
K-BB(1)							
k1 400v Bus	0.40	1.059	0.42	0.43			>>>>>>>>>>
K-BB(2)							
k3 400v Bus	0.40	1.062	0.42	0.69			>>>>>>>>>>
K-BB(3)							
k4 400v Bus	0.40	1.073	0.43	1.38			>>>>>>>>>>
K-BB(4)							
Kambajava	20.00	1.009	20.19	149.35			>>
K-BB(5)							
k4 400v Bus	0.40	1.060	0.42	0.72			>>>>>>>>>>
K-BB							
k2 400v Bus	0.40	1.000	0.40	0.00			
KBB10							
k5 400v	0.40	1.034	0.41	0.42			>>>>>>>
KBB11							
k6 400v	0.40	1.000	0.40	0.00			
KBB12							
k7 400v	0.40	1.031	0.41	0.30			>>>>>>>
Single Busbar(3)							
K-H2	20.00	1.025	20.50	150.01			>>>>>>>
WBB(1)							
w6.3kv	6.30	1.007	6.34	-0.57			>>
WBB(2)							
w3 400v	0.40	1.000	0.40	0.00			
WBB(3)							
Waingapu	20.00	0.997	19.95	148.98			<
WBB(4)							
w2 400v	0.40	1.000	0.40	0.00			
WBB							
w1 400v	0.40	0.997	0.40	-1.02			<
WTG01LV							

Grid: Sumba System Stage: Sumba Study Case: KGL-nuclear Annex: / 6

rtd.v [kv]	Bus - voltage		voltage - Deviation [%]				
	[p.u.]	[kv]	[deg]	-10	-5	0	+5

[kv]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	to	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]
20.00	0.00 0.00	0.00 0.00	5.68 2.77	0.00 0.00	0.00 0.00			0.13 0.06	0.13 0.07	0.00 -0.01
						0.40 kv	-3.91 -2.77	0.04 0.18	0.04 0.18	0.00 0.00
						0.69 kv	-1.68 0.11	0.02 0.11	0.02 0.08	0.00 0.02
						6.30 kv	-0.22 -0.16	0.00 0.00	0.00 0.00	0.00 0.00
Total:	5.88 3.12	0.00 0.00	5.68 2.77	0.00 0.00	0.01 0.00		0.00 0.00	0.21 0.35	0.19 0.32	0.01 0.04
							DigSILENT PowerFactory 15.2.1	Project: Date: 9/28/2015		
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits					Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %
Total System Summary					Study Case: KGL-nuclear				Annex: / 9	
Generation	Motor Load	Load	Compen- sation	External Infeed		Inter Area Flow	Total Losses	Load Losses	NoLoad Losses	
[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]		[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	
\pramod\Sumba-V3_HWHL_twowTG_powerstore\Network Model\Network Data\Sumba						0.00 0.00	0.21 0.35	0.19 0.32	0.01 0.04	
Total:	5.88 3.12	0.00 0.00	5.68 2.77	0.00 0.00	0.01 0.00		0.21 0.35	0.19 0.32	0.01 0.04	
							DigSILENT PowerFactory 15.2.1	Project: Date: 9/28/2015		
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits					Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %

| Area: Kambajava | Study Case: KGL-noclear | Annex: / 10 |

Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
0.40	3.96 2.96	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
						20.00 kv	3.96 2.96	0.04 0.18	0.04 0.18	0.00 0.00
20.00	0.00 0.00	0.00 0.00	3.49 1.69	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
						0.40 kv	-3.91 -2.77	0.04 0.18	0.04 0.18	0.00 0.00
						waingapu	1.88 0.86	0.02 0.02	0.02 0.02	0.00 -0.00
Total:	3.96 2.96	0.00 0.00	3.49 1.69	0.00 0.00	0.00 0.00		0.42 1.08	0.04 0.18	0.04 0.18	0.00 0.00
						waingapu	1.88 0.86	0.02 0.02	0.02 0.02	0.00 -0.00

							DigSILENT PowerFactory 15.2.1	Project: Date: 9/28/2015
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| Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange |

AC Load Flow, balanced, positive sequence	Yes	Automatic Model Adaptation for Convergence	No
Automatic Tap Adjust of Transformers	No	Max. Acceptable Load Flow Error for	0.01 kVA
Consider Reactive Power Limits		Nodes Model Equations	0.01 %

| Area: Waingapu | Study Case: KGL-noclear | Annex: / 11 |

Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]
0.40	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
6.30	0.22 0.16	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
						20.00 kv	0.22 0.16	0.00 0.00	0.00 0.00	0.00 0.00
20.00	0.00 0.00	0.00 0.00	2.08 1.01	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00
						6.30 kv	-0.22 -0.16	0.00 0.00	0.00 0.00	0.00 0.00
						kambajava	-1.88	0.02	0.02	0.00

						-0.86	0.02	0.02	-0.00	
Total:	0.22	0.00	2.08	0.00	0.00	-1.88	0.02	0.02	0.00	
	0.16	0.00	1.01	0.00	0.00	-0.86	0.02	0.03	-0.00	
kambajava						-1.88	0.02	0.02	0.00	
						-0.86	0.02	0.02	-0.00	
						DigSILENT PowerFactory 15.2.1		Project: Date: 9/28/2015		
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence					Yes	Automatic Model Adaptation for Convergence			No	
Automatic Tap Adjust of Transformers					No	Max. Acceptable Load Flow Error for			0.01 kVA	
Consider Reactive Power Limits						Nodes Model Equations			0.01 %	
Area: Haharu						Study Case: KGL-noclear			Annex: / 12	
Volt. Level	Generation	Motor Load	Load	Compensation	External Infeed	Interchange to	Power Interchange	Total Losses	Load Losses	No load Losses
[kv]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]		[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]
20.00	0.00	0.00	0.10	0.00	0.00			0.00	0.00	0.00
	0.00	0.00	0.06	0.00	0.00	0.69 kv	-1.68	0.00	0.00	0.00
							0.11	0.02	0.02	0.00
								0.11	0.08	0.02
Total:	0.00	0.00	0.10	0.00	0.00		-0.12	0.02	0.02	0.00
	0.00	0.00	0.06	0.00	0.00		-0.17	0.11	0.08	0.02
						DigSILENT PowerFactory 15.2.1		Project: Date: 9/28/2015		
Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange										
AC Load Flow, balanced, positive sequence					Yes	Automatic Model Adaptation for Convergence			No	
Automatic Tap Adjust of Transformers					No	Max. Acceptable Load Flow Error for			0.01 kVA	
Consider Reactive Power Limits						Nodes Model Equations			0.01 %	
Area Summaries						Study Case: KGL-noclear			Annex: / 13	
Generation	Motor Load	Load	Compensation	External Infeed	Inter Area Flow	Total Losses	Load Losses	No load Losses		
[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	[MW]/[Mvar]	
\pramod\Sumba-V3_HWHL_twowTG_powerstore\Network Model\Network Data\Areas\Kambajava										

	3.956	0.000	3.494	0.000	0.000	0.42	0.04	0.04	0.00
	2.955	0.000	1.692	0.000	0.000	1.08	0.18	0.18	0.00

\pramod\Sumba-V3_HWHL_twowTG_powerstore\Network Model\Network Data\Areas\waingapu	0.220	0.000	2.084	0.000	0.000	-1.88	0.02	0.02	0.00
	0.165	0.000	1.009	0.000	0.000	-0.86	0.02	0.03	-0.00

\pramod\Sumba-V3_HWHL_twowTG_powerstore\Network Model\Network Data\Areas\Haharu	0.000	0.000	0.104	0.000	0.000	-0.12	0.02	0.02	0.00
	0.000	0.000	0.064	0.000	0.000	-0.17	0.11	0.08	0.02

High Wind Low Load (For Two WTGs)

						DigSILENT PowerFactory 15.2.1		Project: Date: 9/28/2015							
Load Flow Calculation						Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange									
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits				Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %					
Grid: Sumba		System Stage: Sumba				Study Case: KGL				Annex: / 1					
rated voltage [kV]		Bus-voltage [p.u.]		Active Power [MW]		Reactive Power [Mvar]		Power Factor [-]		Current [kA]		Loading [%]		Additional Data	
HB(1)															
Haharu		20.00		1.08		21.62		152.18							
Cub_1 /Lod						0.05		0.03		0.85		0.00		P10: 0.05 MW	
Cub_1 /Lne						1.64		-0.12		1.00		0.04		Q10: 0.03 Mvar	
Cub_1 /Lne						-0.00		-0.00		-1.00		0.00		cLod: 0.00 Mvar L: 18.00km	
Cub_1 /Tr2						-0.85		0.05		-1.00		0.02		Pv: 0.00 kW Tap: 0.00 Min: -2 Max: 2	
Cub_1 /Tr2						-0.85		0.05		-1.00		0.02		Tap: 0.00 Min: -2 Max: 2	
K-BB(1)															
K1 400V Bu.40		1.00		0.40		0.00									
Cub_1 /Sym						0.00		0.00		1.00		0.00		Typ: PQ	
Cub_1 /Tr2						0.00		0.00		1.00		0.00		Tap: 3.00 Min: 1 Max: 5	
K-BB(2)															
K3 400V Bu.40		1.00		0.40		0.00									
Cub_1 /Sym						0.00		0.00		1.00		0.00		Typ: PQ	
Cub_1 /Tr2						0.00		0.00		1.00		0.00		Tap: 3.00 Min: 1 Max: 5	
K-BB(3)															
K4 400V Bu.40		1.00		0.40		0.00									
Cub_1 /Sym						0.36		0.83		0.39		1.31		Typ: SL	
Cub_1 /Sym						0.00		0.00		1.00		0.00		Typ: PQ	
Cub_1 /Sym						0.00		0.00		1.00		0.00		Typ: SL	
Cub_1 /Tr2						0.36		0.83		0.39		1.31		Tap: 4.00 Min: 1 Max: 5	
						-----		-----							
						0.36		0.83							
K-BB(4)															
Grid: Sumba		System Stage: Sumba				Study Case: KGL				Annex: / 2					
rated voltage [kV]		Bus-voltage [p.u.]		Active Power [MW]		Reactive Power [Mvar]		Power Factor [-]		Current [kA]		Loading [%]		Additional Data	

Kambajava0.00 1.00 20.02 149.75																			
Cub_1	/Lod	Kambajava Load				1.69	0.56	0.95	0.05		P10:	1.69 MW	Q10:	0.56 Mvar	L:	7.00km			
Cub_1	/Lne	K-H1				-1.51	0.17	-0.99	0.04	4.39	Pv:	26.93 kw	cLod:	0.00 Mvar	L:	7.00km			
Cub_1	/Lne	K-W Tline				1.01	0.33	0.95	0.03	3.08	Pv:	4.47 kw	cLod:	0.00 Mvar	L:	7.00km			
Cub_1	/Tr2	T1				-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5			
Cub_1	/Tr2	T2				-0.00	0.00	-1.00	0.00	0.00	Tap:	5.00	Min:	1	Max:	5			
Cub_1	/Tr2	T3				-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5			
Cub_1	/Tr2	T4				-0.35	-0.82	-0.40	0.03	34.93	Tap:	4.00	Min:	1	Max:	5			
Cub_1	/Tr2	T5				-0.84	-0.24	-0.96	0.03	34.19	Tap:	4.00	Min:	1	Max:	5			
Cub_1	/Tr2	T6				-0.00	-0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5			
Cub_1	/Tr2	T7				-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5			
Cub_1	/Tr2	T8				-0.00	0.00	-1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5			
K-BB(5)																			
K4 400v Bu.40		0.99	0.40	0.80															
Cub_1	/Sym	DOOSAN1				0.42	-0.00	1.00	0.61	80.00	Typ:	PQ							
Cub_1	/Sym	DOOSAN2				0.42	0.26	0.85	0.72	94.12	Typ:	PQ							
Cub_1	/Tr2	T5				0.84	0.26	0.96	1.28	34.19	Tap:	4.00	Min:	1	Max:	5			
Total Generation:						0.84	0.26												
K-BB																			
K2 400v Bu.40		1.00	0.40	0.00															
Cub_1	/Sym	MAN1				0.00	0.00	1.00	0.00	0.00	Typ:	PQ							
Cub_1	/Tr2	T7				0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5			
KBB10																			
K5 400v 0.40		1.00	0.40	0.00															
Cub_1	/Sym	MTU2				0.00	0.00	1.00	0.00	0.00	Typ:	PQ							
Cub_1	/Tr2	T1				0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5			
KBB11																			
K6 400v 0.40		1.00	0.40	0.00															
Cub_1	/Sym	MAN2				0.00	-0.00	1.00	0.00	0.00	Typ:	PQ							
Cub_1	/Tr2	T2				0.00	-0.00	1.00	0.00	0.00	Tap:	5.00	Min:	1	Max:	5			
KBB12																			
K7 400v 0.40		1.00	0.40	0.00															
Cub_1	/Sym	MTU4				0.00	0.00	1.00	0.00	0.00	Typ:	PQ							
Cub_1	/Tr2	T3				0.00	0.00	1.00	0.00	0.00	Tap:	3.00	Min:	1	Max:	5			
Grid: Sumba					System Stage: Sumba					Study Case: KGL					Annex: / 3				
rated voltage		Bus-voltage		Active Power		Reactive Power		Power Factor		Current		Loading		Additional Data					
	[kV]		[p.u.]		[kV]		[deg]		[MW]		[Mvar]		[-]		[kA]		[%]		
Single Busbar(3)																			
K-H2	20.00	1.02	20.36	150.41															
Cub_1	/Lne	K-H1				1.54	-0.16	0.99	0.04	4.39	Pv:	26.93 kw	cLod:	0.00 Mvar	L:	7.00km			
Cub_1	/Lne	K-H2 Tline				-1.54	0.16	-0.99	0.04	4.39	Pv:	99.80 kw	cLod:	0.00 Mvar	L:	18.00km			
WBB(1)																			
W6.3kV	6.30	0.00	0.00	0.00															
Cub_1	/Sym	SWD1				0.00	0.00	1.00	0.00	0.00	Typ:	PQ							
Cub_1	/Sym	SWD2				0.00	0.00	1.00	0.00	0.00	Typ:	PQ							

Load Flow Calculation Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange											
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits						Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations				No 0.01 kVA 0.01 %
Grid: Sumba			System Stage: Sumba			Study Case: KGL			Annex: / 7		
Volt. Level [kV]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]	
0.40	1.20 1.09	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	1.20 1.09	0.00 0.00 0.01 0.04	0.00 0.00 0.01 0.04	0.00 0.00 0.00 0.00	
0.48	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.80 kv 20.00 kv	-0.01 -0.03 0.01 0.03	0.00 0.00 -0.03 0.01 0.03	0.00 0.00 -0.03 0.00 0.00	0.00 0.00 0.00 0.01 0.03	
0.69	1.70 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	20.00 kv	1.70 0.00	0.00 0.00 0.01 0.09	0.00 0.00 0.01 0.04	0.00 0.00 0.00 0.05	
0.80	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.01 0.00	0.48 kv	0.01 0.00	0.00 0.00 -0.03	0.00 0.00 -0.03	0.00 0.00 0.00	
6.30	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00			0.00 0.00	0.00 0.00	0.00 0.00	
Grid: Sumba			System Stage: Sumba			Study Case: KGL			Annex: / 8		
Volt. Level [kV]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]	
20.00	0.00 0.00	0.00 0.00	2.75 0.92	0.00 0.00	0.00 0.00	0.40 kv 0.69 kv	-1.19 -1.06 -1.69 0.09	0.13 0.05 0.01 0.04 0.01 0.09	0.13 0.06 0.01 0.04 0.01 0.04	0.00 -0.01 0.00 0.00 0.00 0.05	
Total:	2.90	0.00	2.75	0.00	0.01		0.00	0.16	0.15	0.01	

1.09		0.00		0.92		0.00		0.00		0.00		0.18		0.11		0.07					
										DigSILENT PowerFactory 15.2.1		Project: Date: 9/28/2015									
Load Flow Calculation										Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange											
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits						Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations						No 0.01 kVA 0.01 %							
Total System Summary										Study Case: KGL						Annex: / 9					
Generation [MW]/ [Mvar]		Motor Load [MW]/ [Mvar]		Load [MW]/ [Mvar]		Compen- sation [MW]/ [Mvar]		External Infeed [MW]/ [Mvar]		Inter Area Flow [MW]/ [Mvar]		Total Losses [MW]/ [Mvar]		Load Losses [MW]/ [Mvar]		No load Losses [MW]/ [Mvar]					
\pramod\Sumba-V3_HWLL_twowTG_powerstore\Network Model\Network Data\Sumba										0.00		0.16		0.15		0.01					
2.90		0.00		2.75		0.00		0.01		0.00		0.18		0.11		0.07					
1.09		0.00		0.92		0.00		0.00													
Total:		2.90		0.00		2.75		0.00		0.01		0.16		0.15		0.01					
		1.09		0.00		0.92		0.00		0.00		0.18		0.11		0.07					
										DigSILENT PowerFactory 15.2.1		Project: Date: 9/28/2015									
Load Flow Calculation										Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange											
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits						Yes No		Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations						No 0.01 kVA 0.01 %							
Area: Kambajava										Study Case: KGL						Annex: / 10					
Volt. Level [kV]		Generation [MW]/ [Mvar]		Motor Load [MW]/ [Mvar]		Load [MW]/ [Mvar]		Compen- sation [MW]/ [Mvar]		External Infeed [MW]/ [Mvar]		Interchange to		Power Interchange [MW]/ [Mvar]		Total Losses [MW]/ [Mvar]		Load Losses [MW]/ [Mvar]		No load Losses [MW]/ [Mvar]	
0.40		1.20		0.00		0.00		0.00		0.00						0.00		0.00		0.00	
		1.09		0.00		0.00		0.00		0.00						0.00		0.00		0.00	
												20.00 kv		1.20		0.01		0.01		0.00	
														1.09		0.04		0.04		0.00	
20.00		0.00		0.00		1.69		0.00		0.00						0.00		0.00		0.00	

	0.00	0.00	0.56	0.00	0.00	0.40 kv	-1.19	0.00	0.00	0.00
						waingapu	-1.06	0.01	0.01	0.00
							1.01	0.04	0.04	0.00
							0.33	0.00	0.00	0.00
								0.01	0.01	-0.00
Total:	1.20	0.00	1.69	0.00	0.00		-0.50	0.01	0.01	0.00
	1.09	0.00	0.56	0.00	0.00		0.50	0.04	0.04	0.00
						waingapu	1.01	0.00	0.00	0.00
							0.33	0.00	0.01	-0.00

						DigSILENT PowerFactory 15.2.1	Project:
							Date: 9/28/2015

Load Flow Calculation	Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange					
AC Load Flow, balanced, positive sequence	Yes	Automatic Model Adaptation for Convergence				No
Automatic Tap Adjust of Transformers	No	Max. Acceptable Load Flow Error for				0.01 kVA
Consider Reactive Power Limits		Nodes				0.01 %
		Model Equations				

Area: Waingapu						Study Case: KGL			Annex:		/ 11
Volt. Level	Generation	Motor Load	Load	Compensation	External Infeed	Interchange to	Power Interchange	Total Losses	Load Losses	No-load Losses	
[kv]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]		[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]	[MW]/ [Mvar]
0.40	0.00	0.00	0.00	0.00	0.00			0.00	0.00	0.00	
	0.00	0.00	0.00	0.00	0.00			0.00	0.00	0.00	
6.30	0.00	0.00	0.00	0.00	0.00			0.00	0.00	0.00	
	0.00	0.00	0.00	0.00	0.00			0.00	0.00	0.00	
20.00	0.00	0.00	1.01	0.00	0.00	Kambajava		0.00	0.00	0.00	
	0.00	0.00	0.33	0.00	0.00			0.00	0.00	0.00	
							-1.01	0.00	0.00	0.00	
							-0.33	0.00	0.01	-0.00	
Total:	0.00	0.00	1.01	0.00	0.00	Kambajava	-1.01	0.00	0.00	0.00	
	0.00	0.00	0.33	0.00	0.00		-0.33	0.00	0.01	-0.00	
							-1.01	0.00	0.00	0.00	
							-0.33	0.00	0.01	-0.00	

						DigSILENT PowerFactory 15.2.1	Project:
							Date: 9/28/2015

Load Flow Calculation	Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange					
AC Load Flow, balanced, positive sequence	Yes	Automatic Model Adaptation for Convergence				No
Automatic Tap Adjust of Transformers		Max. Acceptable Load Flow Error for				

Consider Reactive Power Limits						No	Nodes Model Equations			0.01 kVA 0.01 %	
Area: Haharu						Study Case: KGL			Annex: / 12		
Volt. Level [kv]	Generation [MW]/ [Mvar]	Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Interchange to	Power Interchange [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]	
20.00	0.00 0.00	0.00 0.00	0.05 0.03	0.00 0.00	0.00 0.00	0.69 kv	-1.69 0.09	0.00 0.01 0.09	0.00 0.01 0.04	0.00 0.00 0.00 0.05	
Total:	0.00 0.00	0.00 0.00	0.05 0.03	0.00 0.00	0.00 0.00		-0.06 -0.12	0.01 0.09	0.01 0.04	0.00 0.05	
							DIGSILENT PowerFactory 15.2.1	Project: Date: 9/28/2015			
Load Flow Calculation						Complete System Report: Substations, Voltage Profiles, Grid Interchange, Area Interchange					
AC Load Flow, balanced, positive sequence Automatic Tap Adjust of Transformers Consider Reactive Power Limits						Yes No	Automatic Model Adaptation for Convergence Max. Acceptable Load Flow Error for Nodes Model Equations			No 0.01 kVA 0.01 %	
Area Summaries						Study Case: KGL			Annex: / 13		
Generation [MW]/ [Mvar]		Motor Load [MW]/ [Mvar]	Load [MW]/ [Mvar]	Compensation [MW]/ [Mvar]	External Infeed [MW]/ [Mvar]	Inter Area Flow [MW]/ [Mvar]	Total Losses [MW]/ [Mvar]	Load Losses [MW]/ [Mvar]	No load Losses [MW]/ [Mvar]		
\pramod\Sumba-V3_HWLL_twowTG_powerstore\Network Model\Network Data\Areas\Kambajava							-0.50	0.01	0.01	0.00	
1.198		0.000	1.691	0.000	0.000						
1.095		0.000	0.556	0.000	0.000	0.50	0.04	0.04	0.00		
\pramod\Sumba-V3_HWLL_twowTG_powerstore\Network Model\Network Data\Areas\waingapu							-1.01 -0.33	0.00 0.00	0.00 0.01	0.00 -0.00	
0.000 0.000		0.000 0.000	1.009 0.332	0.000 0.000	0.000 0.000						
\pramod\Sumba-V3_HWLL_twowTG_powerstore\Network Model\Network Data\Areas\Haharu							-0.06 -0.12	0.01 0.09	0.01 0.04	0.00 0.05	
0.000 0.000		0.000 0.000	0.051 0.032	0.000 0.000	0.000 0.000						

Appendix D: List of Dynamic Models

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Wind Turbine Generator Model

Grid: Sumba	Syst. Stage: Sumba	Annex:	/ 125
(WTG) 01 V52 DSL	Common Model	1	/10
Model Definition	... \Library\V52- 0. 85 MW VCS 50 Hz V7. 5. 0		
Out of Service	No		
A-stable integration algorithm	No		
Characteristic Name			
Data source	MAN		
Foreign Key			
Description			
Approval Information			
Status	Not Approved		
Modified		12/31/1969 7: 00: 00 PM	
Modified by			
Parameter			
S_Rated : Base Power [VA]		850000. 0000	
Nunits : Number of Units in wind Park [-]		1. 0000	
TauFud : (Meas.) Shaft Speed Filter Time Constant [s]		0. 1000	
TauP : (Meas.) Active Power Filter Time Constant [s]		0. 1000	
TauQ : (Meas.) Reactive Power Filter Time Constant [s]		0. 1000	
Kp : (Gen. Control) Power Controller Proportional Gain [-]		3. 0025	
Ki : (Gen. Control) Power Controller Integral gain [-]		8. 3264	
Kud : (Gen. Control) Torsion damper Gain [A/rad/s]		100. 0000	
Taucud : (Gen. Control) Torsion damper Time Constant [s]		0. 4000	
RatedRotorInv : Rated Rotor Inverter Current [A]		450. 0000	
IRRated : (Gen. Control) Rated Rotor Current [A]		380. 8300	
Winding_Ratio : (Generator) Nrotor/Nstator [-]		2. 6300	
Xm : (Generator) Magnetizing Reactance [Ohm]		1. 9700	
Xls : (Generator) Stator leakage reactance [Ohm]		0. 0420	
U_Rated : Base Voltage [V]		690. 0000	
Rs : (Generator) Stator resistance [Ohm]		0. 0029	
Xlr : (Generator) Rotor leakage reactance [Ohm]		0. 0430	
Vrmax : (Generator) Maximum Rotor Voltage (referred to the stator) [V]		43	
w1 : (Grid) Nominal Grid Pulsation [rad/s]		314. 1593	
Tfaultclear : (LVRT Logic) Voltage recovery time constant [s]		0. 0600	
Xs : (Generator) Stator reactance [Ohm]		2. 0120	
Xr : (Generator) Rotor reactance [Ohm]		2. 0130	
Xss : (Generator) Transient reactance [Ohm]		0. 0840	
T0 : (Generator) Transient open-circuit time constant [s]		2. 0600	
AG0_enable : (Protection) LVRT Enable/Disable [1/0]		1. 0000	
ULVRT1 : (Protection) LVRT Voltage Limit Stage 1 [pu]		0. 0000	
TLVRT1 : (Protection) LVRT Voltage Timeout Stage 1 [s]		0. 3000	
ULVRT2 : (Protection) LVRT Voltage Limit Stage 2 [pu]		0. 7000	
TLVRT2 : (Protection) LVRT Voltage Timeout Stage 2 [s]		2. 6500	
ULVRT3 : (Protection) LVRT Voltage Limit Stage 3 [pu]		0. 8500	
TLVRT3 : (Protection) LVRT Voltage Timeout Stage 3 [s]		11. 0000	
ULVRT4 : (Protection) LVRT Voltage Limit Stage 4 [pu]		0. 9000	
TLVRT4 : (Protection) LVRT Voltage Timeout Stage 4 [s]		60. 0000	
UV1 : (Protection) Under Voltage Limit Stage 1 [pu]		0. 9000	
Tuv1 : (Protection) Under Voltage Timeout Stage 1 [s]		60. 0000	
UV2 : (Protection) Under Voltage Limit Stage 2 [pu]		0. 8500	
Tuv2 : (Protection) Under Voltage Timeout Stage 2 [s]		11. 0000	
UV3 : (Protection) Under Voltage Limit Stage 3 [pu]		0. 8500	
Tuv3 : (Protection) Under Voltage Timeout Stage 3 [s]		11. 0000	
OV1 : (Protection) Over Voltage Limit Stage 1 [pu]		1. 1000	
Tov1 : (Protection) Over Voltage Timeout Stage 1 [s]		60. 0000	
OV2 : (Protection) Over Voltage Limit Stage 2 [pu]		1. 1800	
Tov2 : (Protection) Over Voltage Timeout Stage 2 [s]		2. 0000	
OV3 : (Protection) Over Voltage Limit Stage 3 [pu]		1. 2000	
Tov3 : (Protection) Over Voltage Timeout Stage 3 [s]		0. 0800	
UF1 : (Protection) Low Frequency Limit [Hz]		47. 0000	
Tuf1 : (Protection) Low Frequency Timeout [s]		0. 2000	
OF1 : (Protection) High Frequency Limit [Hz]		53. 0000	
Tof1 : (Protection) High Frequency Timeout [s]		0. 2000	
Prot_enable : (Protection) Trip Enable/Disable [1/0]		1. 0000	
Krg : (Drive Train) Shaft Stiffness [Nm/rad]		6002. 0000	
Drg : (Drive Train) Shaft damping [Nm/rad/s]		24. 7000	
Wgen : (Drive Train) Nominal Shaft Speed [rad/s]		387. 4631	
Jgen : (Drive Train) Generator Inertia [Kgm2]		31. 0000	
Jrot : (Drive Train) Turbine Rotor Inertia [Kgm2]		158. 0000	
ModeSel : (PQ Limits) PF(=1)or Q(=0) Mode Selector [-]		0. 0000	
PFmin_cap : (PQ Chart) Min Power Factor, Capacitive [-]		0. 2000	
PFmin_ind : (PQ Chart) Min Power Factor, Inductive [-]		-0. 2000	
Qmax_cap : (PQ Chart) Max Q, Capacitive [pu]		0. 5882	
Qmax_ind : (PQ Chart) Max Q, Inductive [pu]		-0. 5882	

PFmax_cap	:(PQ Chart) Max Power Factor,Capacitive [-]	0.9800
PFmax_ind	:(PQ Chart) Max Power Factor,Inductive [-]	-0.9500
PQmax_cap	:(PQ Chart) PQ Corner,Capacitive [pu]	0.6056
PQmax_ind	:(PQ Chart) PQ Corner,Inductive [pu]	0.8405
dPmin	:(PQ Limits) Minimum Slope Limit P ref. [pu/s]	-10.0000
dPmax	:(PQ Limits) Maximum Slope Limit P ref. [pu/s]	1.0000
TauPref	:(PQ Limits) Filter Time Constant P ref. [s]	0.1000
TauQref	:(PQ Limits) Filter Time Constant Q ref [s]	0.1000
F_GS	:(LVRT Logic) WTG type DFIG(=0)/Full Scale (=1) [1/0]	0.0000
RegainPQdelay	:(LVRT Logic) PQ Control Delay [s]	0.2000
RTUdip	:(LVRT Logic) Parameter IRD Calculation [pu]	0.5000
RTIreac	:(LVRT Logic) Parameter IRD Calculation [pu]	1.0000
Tsdfgwashout	:(LVRT Logic) Washout Filter Time Constant [s]	0.0160
Ttimeout	:(LVRT Logic) NO (SDFIG=2) timeout [s]	3.0000
Tbco	:(LVRT Logic) BCO duration [s]	0.0250
Tsrvo	:(LVRT Logic) SRV0 duration [s]	0.0200
Ubco	:(LVRT Logic) BCO triggering level [pu]	0.3500
Usrvo	:(LVRT Logic) SRV0 triggering level [pu]	0.2500
Tmeas	:(LVRT Logic) Voltage measurement time constant [s]	0.0100
Ird_ramplim_neg	:(LVRT Logic) IRD negative ramp limit [pu]	-16.8300
Ird_ramplim_pos	:(LVRT Logic) IRD positive ramp limit [pu]	40.0000
Irq_ramplim_neg	:(LVRT Logic) IRQ negative ramp limit [pu]	-67.3350
Irq_ramplim_pos	:(LVRT Logic) IRQ positive ramp limit [pu]	67.3350
LIP	:(LVRT Logic) IRQ (active power limit during current control [pu]	
Ugrid_delay	:(LVRT Logic) Voltage measurement time delay (Full Scale [s]	
Imag_comp_factor	:(LVRT Logic) Parameter Magnetisation compensation factor	
G_Angle		80.0000
SCR		10.0000

Characteristics

Net Element	Signal Name
-------------	-------------

Figure D-1. WTG detailed control model

Governor Model (GAST)

The governor model was used in all generators.

Grid: Sumba	Syst. Stage: Sumba	Annex:	/ 315
GAST	Common Model	18	/38
Model Definition	... \Library\User Defined Models\gov_GAST		
Out of Service	No		
A-stable integration algorithm	No		
Characteristic Name	MAN		
Data source	MAN		
Foreign Key			
Description			
Approval Information			
Status	Not Approved		
Modified		11/18/2013 4:11:49 AM	
Modified by	Administrator		
Parameter			
R Speed Droop [pu]		0.0470	
T1 Controller Time Constant [s]		0.4000	
T2 Actuator Time Constant [s]		0.1000	
T3 Compressor Time Constant [s]		3.0000	
AT Ambient Temperature Load Limit [pu]		1.0000	
Kt Turbine Factor [pu]		2.0000	
Dturb frictional losses factor pu [pu]		0.0000	
PN Turbine Rated Power(=0->PN=Pgnn) [MW]		0.0000	
Vmin Controller Minimum Output [pu]		0.0000	
Vmax Controller Maximum Output [pu]		1.0000	
Characteristics			
	Net Element	Signal Name

Figure D-2. GAST detailed control model

IEEEET1: AVR Model

The governor model was used in all generators.

Grid: Sumba	Syst. Stage: Sumba	Annex:	/ 131
IEEEET1	Common Model	6	/10
Model Definition	\Library\Standard Models\avr_IEEET1		
Out of Service	No		
A-stable integration algorithm	No		
Characteristic Name	MAN		
Data source	MAN		
Foreign Key			
Description			
Approval Information			
Status	Not Approved		
Modified	3/21/2015 7: 58: 32 PM		
Modified by	pramod		
Parameter			
Tr Measurement Delay [s]	0.0200		
Ka Controller Gain [pu]	200.0000		
Ta Controller Time Constant [s]	0.0300		
Ke Exciter Constant [pu]	1.0000		
Te Exciter Time Constant [s]	0.2000		
Kf Stabilization Path Gain [pu]	0.0500		
Tf Stabilization Path Time Constant [s]	1.5000		
E1 Saturation Factor 1 [pu]	3.9000		
Se1 Saturation Factor 2 [pu]	0.1000		
E2 Saturation Factor 3 [pu]	5.2000		
Se2 Saturation Factor 4 [pu]	0.5000		
Vrmin Controller Output Minimum [pu]	-10.0000		
Vrmax Controller Output Maximum [pu]	10.0000		
Characteristics			
	Net Element	Signal Name

Figure D-3. IEEE T1 detailed control model

Appendix E: Steady-State and Dynamic System Modeling for the Integration of One 850-kW Wind Turbine Generator

This 115 MB file is available at <http://www.nrel.gov/docs/fy16osti/65458-E.pdf>

Appendix F: Report 1—Dynamic System Impact Study by ABB

SYSTEM IMPACT STUDIES OF WIND TURBINE CONNECTION IN SUMBA ISLAND, INDONESIA

Report 1. Dynamic study

DOCUMENT N°: 15SV00931S01R00

EDITION: 1, Rev 0

June 2015

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REVISION HISTORY

Edition n°	Description	Date
1, Rev. 0	Document. First edition	01-06-2015

	Performed	Revised	Approved
Name	LdA, FDF	JM	IRN
Date	02/06/2015	03/06/2015	03/06/2015

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1. OBJECT AND SCOPE

This report shows the dynamic studies conducted on the power grid of the Sumba Island in Indonesia in order to estimate the impact of the commissioning of a wind turbine park in the system.

The study is divided into two scenarios. The first scenario studies the impact of the introduction of a 850 kW wind turbine in the grid of the island that will be scheduled for 2016. The second scenario studies the impact of the introduction of four more 850 kW wind turbine in the east of the island grid and the interconnection of this network with the network of west side of the island by a 92 km overhead line that will be scheduled for 2018.

Is proposed for both scenarios the use of an equipment to provide support to the system stability during transient events. Two technologies are proposed for the selection of this equipment, battery banks and Flywheel.

Figure 1 shows the Sumba Island grid with two separate areas (east and west) and a future grid interconnection between both areas.

Figure 1. Sumba Island grid

2. NETWORK MODEL

Two electrical models for the software tool DigSilent PowerFactory V 15.2 has been provided by the client at the kick-off meeting. The model represents both scenarios and it has been updated in accordance with the data provided to be suitable for the current studies.

The objective of this chapter is to indicate the main elements included in both models. The information concerning this grid has been provided by the client in several emails.

2.1. SCENARIO 1 MODEL

For the scenario 1 just the east side of the grid was included in the model. The model is composed for three main 20 kV substations, Kambajava, Waingapu and Haharu. There are one 850 kW wind turbine on the Kambajava substation and 7412.5 kVA of installed capacity of diesel generation on the Waingapu and Haharu substations. There are also a maximum load capacity of 5682 kW distributed around the system.

Figure 2 shows the Sumba grid model used for the studies of the scenario 1.

Figure 2. Sumba grid model for scenario 1

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2.2. SCENARIO 2 MODEL

For the scenario 2, the east and the west side of the grid was included in the model. The east side is composed for the three main 20 kV substations used on scenario 1, Kambajava, Waingapu and Haharu. And the west side is composed by other three 20 kV substation, Waitabula, Waikabubak and Lokomboro. This model deals with the diesel generation of the whole grid in a consolidated manner in order to facilitate the computer work required.

There are five 850 kW wind turbines on the Kambajava substation (4250 kW of total wind capacity), 6725 kVA of installed capacity of diesel generation on the other east side substations and 8450 kVA of installed capacity of diesel generation on the west side substations. There are also a maximum load capacity of 6876 kW distributed around the east side and 8393 kW distributed around the west side.

Both sides are interconnected with a 92 km overhead line between the Kambajava and the Waitabula substation.

Figure 3 shows the Sumba grid model used for the studies of the scenario 2.

Figure 2. Sumba grid model for scenario 2

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3. STUDY CASES

Three different study cases have been evaluated considering the energy storage solution in and out of service and different operation conditions.

The three study cases have been selected by considered the most extreme cases in a design stage n-1 contingency. The three selected stud cases are:

1. Loss of the largest diesel generator that would be in operation.
2. Loss of the largest load block of the system.
3. Sudden drop of wind, which results in simultaneous loss of all wind generation that would be in operation.

According to the loading description provided by the client, two different loading scenarios have been defined, High Load (HL) and Low Load (LL) scenarios.

Each of the three case studies will be evaluated taking into account the two load levels set (HL and LL) and also all this raised for both future scenarios (2016 and 2018). All this gives a total of 12 simulations to be analyzed.

For all configurations, the use of an equipment to provide support to the system stability also was considered in order to select between battery banks and Flywheel. That means duplicate the number of simulations to be analyzed.

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4. CRITERIA

Based on the documents and the information exchanged with the client, this chapter summarizes the main criteria for the studies.

- Total Priority is given to wind generation over diesel generation whenever the wind is available.
- The utilization voltage to be considered in this study shall be 400 V for diesel generation, 690 V for wind generation and 20 kV for the power grid.
- The voltage operation limits are defined on $\pm 10\%$ of the nominal voltages.
- The limits of low voltage operation for the wind turbine are defined on 0,9 p.u. during 60 s and 0,85 p.u. during 11 s.
- The limits of High voltage operation for the wind turbine are defined on 1,1 p.u. during 60 s, 1,15 p.u. during 2 s and 1,2 p.u. during 80 ms.
- The limits of low frequency operation for the wind turbine are defined on 47 Hz during 200 ms.
- The limits of high frequency operation for the wind turbine are defined on 53 Hz during 200 ms.
- The limits of voltage operation for the diesel generation are defined between 0,9 to 1,1 p.u.
- The limits of frequency operation for the diesel generation are defined between 47 to 53 Hz.

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5. STABILITY ANALYSIS

The main purpose of this chapter is to validate the system frequency stability in terms of loading levels and the characteristics of the wind turbines.

The evaluation is done from a system perspective considering the study cases defined in chapter 3. All cases were simulated with and without using a stability support equipment. For all simulations, the contingency occurs at $t = 0.5$ s. The start-up time of backup generators is limited by the client. For these simulations was taken 10 s for time of cold start-up, but the results are equally applicable to times of start-up higher as discussed in the conclusions.

All simulation result are shown after each analysis by figures. Each figures show graphics (from the top to the bottom) for bus voltage, system frequency, diesel active power and at the last graphic the wind power and the stability support equipment power. Left side of the figures show the graphics simulation using the stability support equipment and the right side show the graphics simulation without using it.

5.1. SCENARIO 1 ANALYSIS

For scenario 1, just the east side of the grid are analyzed using the load and generation expected at 2016. All figures are shown after the whole analysis in order to facilitate reading comprehension.

5.1.1. LOSS OF DIESEL GENERATOR WITH HIGH LOAD

In this event the loss of the largest diesel generator (650 kW) is simulated, then the stability support equipment supplies power (400 kW) for a few seconds until it comes into operation another 550 kW diesel generator and stabilizes the system.

Figure 4 shows how the frequency decreases but is stopped by the action of the stabilizer equipment until comes the backup generator and then the load is shared between the both. When the stabilizer equipment provides no more power, the frequency goes down but is stabilized within acceptable values range (48.65 Hz). The voltages are also kept within the allowable range (between 0.99 to 1.03 p.u.). So the system is stable for this case.

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Without the use of the stability support equipment, the system does not withstand the contingency because the frequency drops so sharply that the wind generator is also lost and there is not enough time to put in service the backup generator.

5.1.2. LOSS OF LOAD WITH HIGH LOAD

In this event the loss of the largest load (3494 kW) is simulated, then the stability support equipment absorbs power (200 kW) for a few seconds and stabilizes the system.

Figure 5 show how the frequency increases but it remains within acceptable values. When the equipment absorbs no more power, the frequency goes up again but is stabilized within acceptable values (51.6 Hz). The voltages are also kept within the allowable range (between 1.01 to 1.06 p.u.). So the system is stable for this case.

Without the use of the stability support equipment, the system withstand the contingency because the generators change their operation point fast enough to compensate for the loss of load. So the use of the stability support equipment is not decisive for the system stability in this case.

5.1.3. LOSS OF WIND GENERATOR WITH HIGH LOAD

In this event the loss of the wind turbine (850 kW) is simulated, then the stability support equipment supplies power (400 kW) for a few seconds until it comes into operation another 550 kW diesel generator and stabilizes the system.

Figure 6 shows how the frequency decreases but is stopped by the actions of the stabilizer equipment until comes the backup generator and then the load is shared between the both. When the equipment provides no more power, the frequency goes down but is stabilized within acceptable values. The frequency is stabilized at a lower value (47.65 Hz) than that obtained in 5.1.1 because the generation loss is greater. The voltages are also kept within the allowable range (between 0.99 to 1 p.u.). So the system is stable for this case.

Without the use of the stability support equipment, the system does not support because the frequency drops so sharply that the backup generator does not have enough power to compensate the loss generation and stabilize the system frequency.

Figure 4. Loss of diesel generator with high load for scenario 1.

Figure 5. Loss of load with high load for scenario 1

Figure 6. Loss of wind generation with high load for scenario 1

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5.1.4. LOSS OF DIESEL GENERATOR WITH LOW LOAD

In this event the loss of the largest diesel generator (420 kW) is simulated, then the stability support equipment supplies power (200 kW) for a few seconds until it comes into operation another 550 kW diesel generator and stabilizes the system.

Figure 7 shows how the frequency decreases but is stopped by the actions of the stabilizer equipment until the backup generator comes in operation and then the load is shared between the both. When the stabilizer equipment provides no more power, the frequency goes down but is stabilized within acceptable values range (49.4 Hz). In this case the backup generator adjusted its operating point to a lower value because the lost generation is smaller than its nominal capacity. The voltages are also kept within the allowable range (between 1 to 1.04 p.u.). So the system is stable for this case.

Without the use of the stability support equipment, the system does not withstand the contingency like in point 5.1.1 because the frequency drops so sharply that the wind generator is also lost and there is not enough time to put in service the backup generator.

5.1.5. LOSS OF LOAD WITH LOW LOAD

In this event the loss of the largest load (1691 kW) is simulated, then the stability support equipment absorbs power (330 kW) for a few seconds and stabilizes the system.

Figure 8 show how the frequency increases but it remains within acceptable values. When the equipment absorbs no more power, the frequency goes up again but is stabilized within acceptable values (52.1 Hz). The voltages are also kept within the allowable range (between 1.01 to 1.06 p.u.). So the system is stable for this case.

Without the use of the stability support equipment, the system withstands the contingency because the generators change its operation point fast enough to compensate for the loss of load. So the use of the stability support equipment is not decisive for the system stability of this case.

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5.1.6. LOSS OF WIND GENERATOR WITH LOW LOAD

In this event the loss of the wind turbine (850 kW) is simulated, then the stability support equipment supplies power (500 kW) for a few seconds until it comes into operation another 550 kW diesel generator and stabilizes the system.

Figure 9 show how the frequency decreases but is stopped by the actions of the stabilizer equipment until the backup generator comes and then the load is shared between the both. When the equipment provides no more power, the frequency goes down but is stabilized within acceptable values. The frequency is stabilized at a lower value (47.9 Hz) than that obtained in 5.1.4 because the generation loss is greater. The voltages are also kept within the allowable range (between 0.99 to 1 p.u.). The system is stable for this case but even so, this case is the most critical in this scenario because the loss of the wind generator represents a large percentage of the load supplied and the spinning reserve available is low.

Without the use of the stability support equipment, the system does not withstand the contingency because the frequency drops so sharply that the backup generator don't have enough power to compensate the loss generation and stabilize the system frequency.

Figure 7. Loss of diesel generator with low load for scenario 1

Figure 8. Loss of load with low load for scenario 1

Figure 9. Loss of wind generation with low load for scenario 1

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5.2. SCENARIO 2 ANALYSIS

For scenario 2, the east and west side of the grid are analyzed using the load and generation expected at 2018. All figures are shown after the whole analysis in order to facilitate reading comprehension.

The consolidated east-west grid have some problems from the voltage stability point of view. The system is more sensitive to disturbances and it takes a longer time to recover the balance. In all simulations can be seen reactive exchanges between the east and west sides after the disturbances.

5.2.1. LOSS OF DIESEL GENERATOR WITH HIGH LOAD

In this event the loss of the largest diesel generator (650 kW) is simulated at the east side, then the stability support equipment supplies power (990 kW) for a few seconds until it comes into operation another 425 kW diesel generator at the east side and stabilizes the system.

In this scenario each generator is represented as a consolidated generator, the loss of a consolidated generator exceed the design stage of n-1 contingency. So, the simulation of the loss of a generator was done by dropping the power supplied by one consolidated generator.

Figure 10 shows how the frequency decreases but is stopped by the actions of the stabilizer equipment until the backup generator comes and then the load is shared between the both. When the stabilizer equipment provides no more power, the frequency goes down but is stabilized within acceptable values range (49.77 Hz). The voltages are also kept within the allowable range (between 0.95 to 1.08 p.u.). So the system is stable for this case.

Without the use of the stability support equipment, the system does not support because the frequency drops so sharply that the wind generator is also lost and there is not enough time to put in service the backup generator.

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5.2.2. LOSS OF LOAD WITH HIGH LOAD

In this event the loss of the largest load (4228 kW) of the system located at east side is simulated, then the stability support equipment absorbs power (100 kW) for a few seconds and stabilizes the system.

Figure 11 shows how the frequency increases but it remains within acceptable values. When the equipment absorbs no more power, the frequency goes up again but is stabilized within acceptable values (50.1 Hz). The voltages are also kept within the allowable range (between 0.90 to 1.09 p.u.). So the system is stable for this case.

Without the use of the stability support equipment, the system withstands the loss of load because the generators change their operation point fast enough to compensate for the loss of load. So the use of the stability support equipment is not decisive for the system stability of this case.

5.2.3. LOSS OF WIND GENERATOR WITH HIGH LOAD

In this event the loss of five wind turbine (4250 kW) is simulated, then the stability support equipment supplies power (4700 kW) for a few seconds until it comes into operation another 2900 kW diesel generator on the east side and 1300 kW on the west side and stabilizes the system.

Figure 12 shows how the frequency decreases after the contingency but is stopped by the actions stabilizer equipment until the backup generators come and then the load is shared between the both. When the stabilizer equipment provides no more power, the frequency goes up but is stabilized within acceptable values. The frequency is stabilized at a value of 50.1 Hz. The voltages are also kept within the allowable range (between 0.92 to 0.97 p.u.). So the system is stable for this case, although there are some issues from the standpoint of voltage stability which are commented in the recommendations and conclusions.

Without the use of the stability support equipment, the system does not withstand the loss of wind generation because the frequency drops so sharply that the backup generator don't have enough power to compensate the loss generation and stabilize the system frequency.

Figure 10. Loss of diesel generator with high load for scenario 2.

Figure 11. Loss of load with high load for scenario 2.

Figure 12. Loss of wind generation with high load for scenario 2

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5.2.4. LOSS OF DIESEL GENERATOR WITH LOW LOAD

In this event the loss of the largest diesel generator (200 kW) is simulated, then the stability support equipment supplies power (140 kW) for a few seconds until it comes into operation another 150 kW diesel generator and stabilizes the system.

In this scenario each generator are represented as consolidated generator, the loss of a consolidated generator exceed the design stage of n-1 contingency. So, the simulation of the loss of a generator was done by dropping the power supplied by one consolidated generator.

Figure 13 shows how the frequency decreases but is stopped by the actions of the stabilizer equipment until the backup generator comes and then the load is shared between the both. When the equipment provide no more power, the frequency goes down but is stabilized within acceptable values range (49.9 Hz). In this case the backup generator adjusted its operating point to a lower value because the lost generation is smaller than its nominal capacity. The voltages are also kept within the allowable range (between 0.9 to 1.01 p.u.). So the system is stable for this case.

Without the use of the stability support equipment, the system does not support because the frequency drops so sharply that the wind generator is also lost and there is not enough time to put in service the backup generator.

5.2.5. LOSS OF LOAD WITH LOW LOAD

In this event the loss of the largest load (2046 kW) is simulated, then the stability support equipment absorbs power (36 kW) for a few seconds and stabilizes the system.

Figure 14 show how the frequency increases but it remains within acceptable values. When the equipment absorbs no more power, the frequency goes up again but is stabilized within acceptable values (50.01 Hz). The voltages are also kept within the allowable range (between 0.9 to 1.01 p.u.). So the system is stable for this case.

Without the use of the stability support equipment, the system withstands the contingency because the generators change their operation point fast enough to compensate for the loss of load. So the use of the stability support equipment is not decisive for the system stability of this case.

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5.2.6. LOSS OF WIND GENERATOR WITH LOW LOAD

In this event the loss of five wind turbine (4250 kW) is simulated, then the stability support equipment supplies power (3600 kW) for a few seconds until it comes into operation another 2000 kW diesel generator on the east side and 1900 kW on the west side and stabilizes the system.

Figure 15 show how the frequency decreases but is stopped by the actions stabilizer equipment until the backup generators come and then the load is shared between all three. When the stabilizer equipment provides no more power, the frequency goes down but is stabilized within acceptable values. The frequency is stabilized at a higher value (50.1 Hz) than that obtained in 5.2.4 because the backup generation is greater. The voltages are also kept within the allowable range (between 0.96 to 0.99 p.u.). The system is stable for this case but even so, this case is the most critical in this scenario because the loss of wind generation represents a large percentage of the load supplied and the spinning reserve available is low.

Without the use of the stability support equipment, the system does not withstand the contingency because the frequency drops so sharply that the backup generator don't have enough power to compensate the loss generation and stabilize the system frequency.

Figure 13. Loss of diesel generator with low load for scenario 2

Figure 14. Loss of load with low load for scenario 2

Figure 15. Loss of wind generation with low load for scenario 2

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6. INTERCONNECTION LINE EVALUATION

In the projected 2018 system is expected to have the east and west sides connected by a 92 km line. In this point is evaluated how the stability of the system is affected by the introduction of this connection.

The interconnection line has the purpose of carry wind power to the load of the west side. But being a relatively long overhead line, it is one of the most vulnerable points in the system. So it is expected a faults occurrence rather high and the system needs to be prepared to deal with the problems this entails.

This system is a typical example of a system with two zones connected by a long line. One side of the system is strong, with more generation that load. While the other side is weak, with more load that generation. All this leads to problems of voltage stability.

For this analysis, a fault is simulated in the interconnection line with a clearance of the line in 0.15 s. The results are shown in Figure 16. With the system operating under the conditions given by the client, the west side collapses due to lack of generation (right side of figure) and the stabilizer equipment is not capable of contributing because it is in the east side.

For the left side of figure 16, the operation of the west side of the system was changed and more spinning reserve was added to that side. This makes that the generation is already available to the line loss and thus not have to depend to stabilizer equipment. For this simulation 1100 kW of spinning reserve was added and with the contingency, the west side frequency goes down but stabilizes at 50.1 Hz. The voltage were also stabilized between 1.07 and 1.09 p.u.

Figure 16 also shows that the east side frequency raises but stabilizes at 50.75 Hz. The voltage was stabilized between 0.94 and 1.1 p.u.

Figure 16. Fault in the interconnection line with high load for scenario 2.

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7. CONCLUSIONS AND RECOMMENDATIONS

This report shows the stability study conducted to the Sumba Island system in Indonesia in order to analyze the impact of the introduction of wind power in the system.

This study has shown that, with the system operating criteria given by the client, it is not possible to introduce just wind turbines. Therefore, is recommended the use of an equipment to provide support to the system stability during transient events. Two technologies were proposed for the selection of this equipment, battery banks and Flywheel.

For scenario 1, 2016, it will be needed an equipment with at least of 500 kW of capacity and for scenario 2, 2018, it will be needed an equipment with at least of 4500 kW in order to supply transitory support to the stability of the system. The contribution time of the additional equipment is determined by the starting time of the back-up diesel generators that were defined as inputs by the client.

Regardless of the time of action, the capacity required for scenario 2 is not met for a single flywheel and the use of several in parallel will significantly increase the cost of the solution and the complexity of the operation. For all this, the use of battery banks are recommended, with capacities of at least 500 kW for 2016 scenario and 4500 kW for 2018 scenario and with a time of action defined by the final starting up process of the back-up diesel generators.

Is has also shown that for scenario 2, the west side of the system is highly vulnerable from the point of view of voltage stability. Without increase the reactive capacity in this area, it would not be able to recover from some contingencies. Then a study is recommended to reassess the dispatch of the system in order to optimize the spinning reserve. Increasing the spinning reserve also reduces the need to use battery banks so the reassessment of the dispatch of the entire system is recommended including a technical-economical assessment of the solutions is also recommended in order to define the optimal solution to ensure system stability.

Appendix G: Steady-State and Dynamic System Modeling for the Integration of Two 850-kW Wind Turbine Generators

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Legends

Table G-1. Legend for All Plots

Line Color	Generator	Line Color	Bus
CAT C32		Haharu
DEUT Z-2		Kambajawa
DOOSAN1		Waingapu
DOOSAN2
DOOSAN3
DOOSAN4
DOOSAN5
MAN1
MTU1
MTU4
VOLVO
YANMAR

Figure G-2. High Wind High Load scenario for the Three-Phase-to-Ground Fault at Kambajawa Bus—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-3. Power output of two WTGs for the High Wind High Load scenario for the Three-Phase-to-Ground Fault at Kambajawa Bus—Self-Clearing of Fault study case

OBSERVATIONS: The system is stable, and the line loadings are within limits. The voltage drops to below 0.1 p.u. at the buses during the fault, and it recovers in 0.18 s. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

High Wind Low Load

Figure G-4. High Wind Low Load scenario for the Three-Phase-to-Ground Fault at Kambajawa Bus—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-5. Power output of two WTGs for the High Wind Low Load scenario for the Three-Phase-to-Ground Fault at Kambajawa Bus—Self-Clearing of Fault study case

OBSERVATIONS: The system is stable, and the line loadings are within limits. The voltage drops to below 0.2 p.u. at the buses during the fault, and it recovers in 0.18 s. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

High Wind High Load with PowerStore

Figure G-6. High Wind High Load with PowerStore scenario for the Three-Phase-to-Ground Fault at Kambajawa Bus—Self-Clearing of Fault study case. (1). Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-7. Active power output of the two WTGs for the High Wind High Load with PowerStore scenario for the Three-Phase-to-Ground Fault at Kambajawa Bus—Self-Clearing of Fault study case

OBSERVATIONS: The system is stable, and the line loadings are within limits. The bus voltages dip below 0.50 p.u. at the H and W buses. The terminal voltage and power outputs of the generators are stable. PowerStore supplies power during the fault. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

High Wind Low Load with PowerStore

Figure G-8. High Wind Low Load with PowerStore scenario for the Three-Phase-to-Ground Fault at Kambajawa Bus—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-9. Power output of two WTGs for the High Wind Low Load with PowerStore scenario for the Three-Phase-to-Ground Fault at Kambajawa Bus—Self-Clearing of Fault study case

OBSERVATIONS: The system is stable, and the line loadings are within limits. The bus voltages dip below 0.50 p.u. at the H and W buses. PowerStore supplies power during the fault when the WTGs are down. It supplies approximately 6 MW at the fault.

Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault

In this study case, a three-phase-to-ground fault at the Waingapu Bus is analyzed with two 850-kW WTGs at Haharu. The fault occurs at 1 s, and it self-clears in 180 ms. The four scenarios for this case are presented below.

High Wind High Load

Figure G-10. Schematic layout for the High Wind High Load scenario for the Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case

Figure G-11. High Wind High Load scenario for the Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-12. Power output of two WTGs for the High Wind High Load scenario for the Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case

OBSERVATIONS: The system is stable, and the line loadings are within limits. The voltage drops to below 0.2 p.u. at the buses during the fault, and it recovers in 0.18 s. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

High Wind Low Load

Figure G-13. High Wind Low Load scenario and Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-14. Power output of two WTGs for the High Wind Low Load scenario for the Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case

OBSERVATIONS: The system is stable, and the line loadings are within limits. The voltage drops to below 0.25 p.u. at the buses during the fault, and it recovers in 0.18 s. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

High Wind High Load with PowerStore

Figure G-15. High Wind High Load with PowerStore scenario for the Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-16. Power output of two WTGs for the High Wind High Load with PowerStore scenario for the Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case

OBSERVATIONS: The system is stable, and the line loadings are within limits. The frequency drops to 0.3 p.u., and it recovers in approximately 0.18 s. The bus voltages dip below 0.30 p.u. at the K and W buses. The terminal voltage and power outputs of the generators are stable. PowerStore supplies power during the fault. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

High Wind Low Load with PowerStore

Figure G-17. High Wind Low Load with PowerStore scenario for the Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-18. Power output of two WTGs for the High Wind Low Load with PowerStore scenario for the Three-Phase-to-Ground Fault at Waingapu Bus—Self-Clearing of Fault study case

OBSERVATIONS: The system is stable, and the line loadings are within limits. The frequency drops to 0.3 p.u., and it recovers in approximately 0.18 s. The bus voltages dip below 0.30 p.u. at the K and W buses. The terminal voltage and power outputs of generators are stable. PowerStore supplies power during the fault. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault

In this study case, the loss of two 850-kW WTGs at the Haharu Bus due to a wind turbine fault is analyzed. The fault occurs at 1 s, and there is no self-clearing.

High Wind High Load

Figure G-19. Schematic layout for the High Wind High Load scenario and Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case

Figure G-20. High Wind High Load scenario for the Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-21. Power output of two WTGs for the High Wind High Load scenario for the Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case

OBSERVATIONS: The frequency keeps falling after the fault, and there is a loss of synchronism in the system. This is expected because the loss of two 850-kW WTGs with no self-clearing is a large loss of generation from which the grid cannot recover.

High Wind Low Load

Figure G-22. High Wind Low Load scenario for the Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-23. Power output of two WTGs for the High Wind Low Load with PowerStore scenario for the Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case

OBSERVATIONS: The frequency keeps falling after the fault, and there is a loss of synchronism in the system. This is expected because the loss of two 850-kW WTGs with no self-clearing is a large loss of generation from which the grid cannot recover.

High Wind High Load with PowerStore

Figure G-24. High Wind High Load scenario with PowerStore for the Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-25. Power output of two WTGs for the High Wind High Load scenario with PowerStore for the Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case

OBSERVATIONS: The system stabilizes because PowerStore supplies power when the two 0.85-MW WTGs go down. It supplies approximately 1.5 MW of active power from 1 s to 10 s. After 10 s, CAT32 starts supplying 0.55 MW of power, thus reducing the contribution of PowerStore to 0.95 MW. After 30 s, when PowerStore had depleted energy, there is a frequency runaway because there is a large loss of power. To prevent a frequency runaway, two additional CAT32 generators with capacities of 0.55 kW and 10-s cold-start times are required in reserve, or a plan to implement load-shedding in such cases is required.

High Wind Low Load with PowerStore

Figure G-26. High Wind Low Load with PowerStore scenario for the Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-27. Power output of two WTGs for the High Wind Low Load with PowerStore scenario for the Wind Power Plant Outage at Haharu Bus—No Self-Clearing of Fault study case

OBSERVATIONS: The system stabilizes because PowerStore supplies power when the two 0.85-MW WTGs go down. It supplies approximately 1.8 MW of active power from 1 s to 10 s. After 10 s, CAT32 starts supplying 0.55 MW of power, thus reducing the contribution of PowerStore to 1.2 MW. After 30 s, when PowerStore had depleted energy, there is a frequency runaway because there is a large loss of power. To prevent a frequency runaway, two additional CAT32 generators with capacities of 0.55 kW and 10-s cold-start time are required in reserve, or a plan to implement load-shedding in such cases is required.

Partial Generator Outage at Kambajawa Bus—No Self-Clearing of Fault

In this study case, a generation loss of 650 kW during high load and a loss of 420 kW during low load at Kambajawa Bus is analyzed. The fault occurs at 1 s, and there is no self-clearing. The four scenarios for this case are presented below.

High Wind High Load

Figure G-28. Schematic layout for the High Wind High Load scenario for the Partial Generator (650 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case

Figure G-29. High Wind High Load scenario for the Partial Generator (650 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-30. Power output of two WTGs for the High Wind High Load scenario for the Partial Generator (650 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case

OBSERVATIONS: A frequency runaway is observed because the system loses 650 kW of generation. There is not enough headroom available to compensate for this loss. Due to this, the frequency falls for 10 s by an amount large enough to cause the WTGs to disconnect. This results in a loss of 2.35 MW in the system. When the CAT32 generator starts supplying power at 10 s, the generator is not able to synchronize and the system as a whole loses synchronism.

High Wind Low Load

Figure G-31. High Wind Low Load scenario for the Partial Generator (420 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-32. Power output of two WTGs for the High Wind High Load scenario for the Partial Generator (420 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case

OBSERVATIONS: A frequency runaway is observed because the system loses 420 kW of generation. There is not enough headroom available to compensate for this loss. Due to this, the frequency falls for 10 s by an amount large enough to cause the WTGs to disconnect. This results in a loss of 2.35 MW in the system. When the CAT32 generator starts supplying power at 10 s, the generator is not able to synchronize and the system as a whole loses synchronism.

High Wind High Load with PowerStore

Figure G-33. High Wind High Load with PowerStore scenario for the Partial Generator (650 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-34. Active power output of the two WTGs for the High Wind High Load with PowerStore scenario for the Partial Generator (650 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case

OBSERVATIONS: At the fault, PowerStore starts supplying approximately 600 kW, thus stabilizing the system until the reserve generator CAT C32 starts supplying power at 10 s. At 30 s, when PowerStore shuts down, the system is still stable.

High Wind Low Load with PowerStore

Figure G-35. High Wind Low Load with PowerStore scenario for the Partial Generator (420 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-36. Active power output of the two WTGs for the High Wind Low Load with PowerStore scenario for the Partial Generator (420 kW) Outage at Kambajawa Bus—No Self-Clearing of Fault study case

OBSERVATIONS: At the fault, PowerStore starts supplying approximately 500 kW, thus stabilizing the system until the reserve generator CAT32 starts supplying power at 10 s. There is enough power generation available in the system to compensate for this loss.

In this study case, the loss of the total load at the Kambajawa Bus is analyzed. The fault occurs at 1 s, and there is no self-clearing.

High Wind High Load

Figure G-37. Schematic layout for the High Wind High Load scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case

Figure G-38. High Wind High Load scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-39. Active power output of the two WTGs for the High Wind High Load scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case

OBSERVATIONS: In this study case, a load of 3.494 MW is lost at 1 s at Kambajawa Bus. The bus frequency increases to 1.04 p.u. and the bus voltages by 0.02 p.u., but overall the system is stable. As shown, the generators reduce their generation by 60%–70% of their initial value. In reality, the diesel generator sets would be disconnected to attain stability.

High Wind Low Load

Figure G-40. High Wind Low Load scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-41. Active power output of the two WTGs for the High Wind High Load scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case

OBSERVATIONS: In this study case, a load of 1.691 MW is lost at 1 s at Kambajawa Bus. The bus frequency and bus voltages increase by a very small value, but overall the system is stable. As shown, the generators reduce their generation and reach a negative value. In reality, the diesel generator sets would be disconnected to attain stability.

High Wind High Load with PowerStore

Figure G-42. High Wind High Load with PowerStore scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-43. Active power output of the two WTGs for the High Wind High Load with PowerStore scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case

OBSERVATIONS: In this study case, a load of 3.494 MW is lost at 1 s at Kambajawa Bus. The bus frequency increases to 1.04 p.u., but overall the system is stable. Because there is PowerStore in the system, it starts absorbing at 1 s. As shown, the generators reduce their generation by 60%–70% of their initial value when the PowerStore shuts down at 30 s. In reality, the diesel generator sets would be disconnected to attain stability.

High Wind Low Load with PowerStore

Figure G-44. High Wind Low Load with PowerStore scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-45. Active power output of the two WTGs for the High Wind Low Load with PowerStore scenario for the Total Load Loss at Kambajawa Bus—No Self-Clearing of Fault study case

OBSERVATIONS: In this study case, a load of 1.691 MW is lost at 1 s at Kambajawa Bus. The bus frequency and bus voltages increase by a very small value, but overall the system is stable. PowerStore in the system starts absorbing at 1 s. In reality, the diesel generator sets would be disconnected to attain stability.

Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault

In this study case, a three-phase short circuit in the transmission line between Kambajawa and Haharu is analyzed. The fault occurs at 1 s, and it self-clears in 180 ms. The four scenarios for this case are presented below.

High Wind High Load

Figure G-46. Schematic layout for High Wind High Load scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case

Figure G-47. High Wind High Load scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-48. Active power output of the two WTGs for the High Wind High Load scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case

OBSERVATIONS: Islanding of Haharu occurs, and the Haharu load goes offline for 180 ms. After the fault clears, the system is stable—line loadings, voltages, and frequency are within limits. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

High Wind Low Load

Figure G-49. High Wind Low Load scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-50. Active power output of the two WTGs for the High Wind High Load scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case

OBSERVATIONS: Islanding of Haharu occurs, and the Haharu load goes offline for 180 ms. After the fault clears, the system is stable—line loadings, voltages, and frequency are within limits. The low-voltage ride-through capability of the WTGs prevents them from going offline, and they recover to normal operation quickly after the fault clears.

High Wind High Load with PowerStore

Figure G-51. High Wind High Load with PowerStore scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-52. Active power output of the two WTGs for the High Wind High Load with PowerStore scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case

OBSERVATIONS: Islanding of Haharu occurs, and the Haharu load goes offline for 180 ms. After the fault clears, the system is stable—line loadings, voltages, and frequency are within limits. PowerStore supplies power as the WTGs recover from the low-voltage ride-through.

High Wind Low Load with PowerStore

Figure G-53. High Wind Low Load with PowerStore scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case. (1) Rotor angle of generators, (2) bus frequency, (3) generator frequency, (4) bus voltage, (5) terminal voltage, and (6) real power of generators

Figure G-54. Active power output of the two WTGs for the High Wind Low Load with PowerStore scenario for the Kambajawa-Haharu Transmission Line Fault—Self-Clearing of Fault study case

OBSERVATIONS: Islanding of Haharu is occurring, and the Haharu load goes offline for 180 ms. After the fault clears, the system is stable—line loadings, voltages, and frequency are within limits. PowerStore supplies power as the WTGs recover from the low-voltage ride-through.

Appendix H: Indonesian Translation

List of Acronyms

Units of Measure

Hz	hertz
km	kilometer
kV	kilovolt
kW	kilowatt
MVA	megavolt ampere
MW	megawatt
MWh	megawatt hour
pu	per unit

Acronyms

AVR	automatic voltage regulator
FRT	fault ride-through
HWHL	High Wind High Load
HWLL	High Wind Low Load
IWE	Innovative Wind Energy, Inc
KG1	Kambajawa Generator Set 1
KG2	Kambajawa Generator Set 1
LVRT	low-voltage ride-through
NREL	National Renewable Energy Laboratory
NWHL	No Wind High Load
NWLL	No Wind Low Load
PLN	Perusahaan Listrik Negara
WG1	Waingapu Generator Set 1
WG2	Waingapu Generator Set 1
WTG	wind turbine generator

Executive Summary

Tujuan dari proyek ini adalah untuk mempelajari dampak dari pemasangan satu dan dua turbin angin berdaya 850kW dalam jaringan distribusi Sumba Timur, Indonesia. Model ini dibuat untuk jaringan 20kV seperti yang ada pada kuartal pertama 2015, dengan beban puncak 5.682MW. Data rinci jaringan dikumpulkan untuk setiap komponen jaringan. Aliran daya, analisa short circuit, dan analisa transien dilakukan dengan menggunakan DIgSILENT PowerFactory 15.2.1.

Analisis aliran daya menunjukkan bahwa untuk jaringan dasar saat ini (tanpa turbin angin) dan dengan satu atau dua 850kW PLTB, tidak terjadi overloading generator, tidak terjadi overloading konduktor, dan semua tegangan bus berada dalam batas normal.

Analisis short-circuit menunjukkan bahwa short-circuit power ratio untuk satu PLTB sebesar 850kW cukup berada di atas persyaratan minimum di bus Haharu - titik penyambungan PLTB. Selain itu, karena kontribusi dari arus short-circuit dari PLTB adalah minimal, daya terpasang perangkat di gardu listrik tidak terpengaruh.

Analisis trasien menunjukkan bahwa dengan satu PLTB sebesar 850-kW, sistem ini tidak stabil di bawah skenario gangguan sebagai berikut: kehilangan pembangkitan daya sebesar 400-kW di Kambajawa tanpa dihubungkan kembali, kehilangan pembangkitan daya sebesar 400-kW di Waingapu tanpa dihubungkan kembali dan kehilangan daya penuh yang dibangkitkan PLTB tanpa dihubungkan kembali. Dengan penambahan daya sebesar 500kW/4.17 kWh berupa energy storage ditambah dengan kemampuan auto-start dari generator cadangan kemampuan start-up dalam 10 detik setelah gangguan, jaringan sistim akan stabil.

Hasil dari analisa mengintegrasikan satu 850-kW WTG di bus Haharu di grid timur Pulau Sumba, perubahan-perubahan berikut ini dapat dipertimbangkan:

1. Pengadaan energy storage sebesar 500-kW/4.17kWh di bus Haharu ditambah dengan autostart untuk diesel CAT32 diesel yang berkapasitas 550kW di Waingapu. Untuk skenario kecepatan angin yang tinggi (diperkirakan kemungkinan terjadi dengan probabilitas 2% dari seluruh kecepatan angin) dan berbagai gangguan - misalnya terputusnya PLTB, terputusnya satu generator di Kambajawa - urutan kejadian berikut harus terjadi untuk menjaga stabilitas sistem:
 - A. Unit storage akan menyediakan energi maksimum mulai saat gangguan selama 10 detik, sehingga akan mengurangi tingkat penurunan frekuensi jaringan dan meningkatkan nadir frekuensi dip selama hilangnya sebagian daya jaringan.
 - B. Controller mengirimkan sinyal autostart untuk CAT32 ketika gangguan terjadi
 - C. Diesel unit CAT32 segera mulai jalan dalam waktu 10 detik
 - D. Unit storage terus memberikan daya selama 30 detik dan kemudian dilepas dari jaringan
 - E. Sesudah 30 detik, jika ada kekurangan daya, generator lain dalam sistem akan meningkatkan daya dengan memanfaatkan kapasitas yang tersisa untuk memberikan daya tambahan yang dibutuhkan

2. Jika tidak ada storage yang digunakan maka pengaturan jaringan bisa sulit dijalankan. Strategi berikut dapat mengatasi tantangan itu, tetapi akan menyebabkan genset diesel berjalan pada efisiensi yang lebih rendah:

- A. Generator diesel harus dijalankan dengan memanfaatkan kapasitas daya yang cukup tinggi sehingga dapat menggantikan daya sekitar 850 kW jika kecepatan angin tiba tiba menurun saat PLTB memproduksi maksimum. Operasi semacam ini akan menjadi tantangan jika kecepatan angin tinggi dan permintaan daya rendah karena scenario semacam ini mengharuskan daya genset diesel bekerja dibawah 90% daya mampu; memang hal ini dapat menyediakan daya cadangan cukup, tapi akan mengorbankan efisiensi diesel. Praktek pada saat ini adalah menjalankan genset diesel pada 100% daya mampu (tidak ada daya cadangan).

Kesimpulannya, tambahan satu 850kW PLTD di Sumba Timur ditambah dengan unit storage sebesar 500kW, pengendali pembangkit listrik hybrid, 550kW genset diesel cadangan dengan kemampuan 10 detik start-up dan komunikasi kecepatan tinggi adalah solusi yang akan meningkatkan keandalan pasokan energi, peningkatan stabilitas system, dan mengurangi emisi greenhouse gas.

Analisis transien menunjukkan bahwa dengan dua PLTB (2x850-kW) terletak di wilayah yang sama, sistem tidak stabil di bawah skenario gangguan seperti berikut: hilangnya pembangkitan daya di bus Kambajawa tanpa dihubungkan kembali, dan hilangnya dua PLTB tanpa dihubungkan kembali. Dengan penambahan berikut ini, sistem akan menjadi stabil: (1) 1.500 kW / 25 kWh storage, (2) satu 550-kW cadangan diesel generator dengan kemampuan start-up secepat 10 detik, (3) generator cadangan tambahan dengan kemampuan start up secepat 60 - detik, (4) perinkan kontroler hybrid untuk mengelola semua unit pembangkit, dan (5) jaringan komunikasi berkecepatan tinggi. Kebanyakan sistem storage komersial lithium-ion dan beberapa sistem flywheel storage memiliki sumber energi selama 60 detik dengan aliaran daya penuh; Oleh karena itu, kombinasi menambahkan (1) sampai (5) adalah tepat untuk meningkatkan keandalan pasokan energi, meningkatkan stabilitas sistem, dan mengurangi emisi greenhouse gas.

Laporan gangguan (yang disediakan oleh PLN) untuk tahun 2014 menunjukkan bahwa jumlah pemadaman dan pemutusan listrik sangatlah tinggi: sekitar satu per hari. Analisis awal menunjukkan alasan-alasan berikut (1) Short circuit yang tidak dibetulkan dalam Batas waktu yang sudah ditentukan pada jaringan pemutus, (2) Generator yang dijalankan mendekati kapasitas daya mampu (daya cadangan sangat rendah), (3) Kurangnya pemangkasan tumbuh tumbuhan yang dapat menyebabkan short circuit pada jalur penyulang, dan (4) banyaknya diesel generator terpasang yang sudah termasuk tua umurnya. Perbaikan terhadap (1) sampai (4) ditambah dengan pemasangan energy storage akan mengurangi jumlah pemadaman dan pemutusan listrik, sehingga dapat meningkatkan keandalan jaringan system daya.

Untuk mencapai tujuan jangka panjang dengan 100% sumber energi terbarukan di Pulau Sumba, laporan ini menganalisa: sumber daya bervariasi (angin / solar) + energy storage (dengan kandungan energi minimal, berkisar dari 30 detik sampai beberapa menit) + generator diesel dengan kemampuan start-up secepat (10-20 detik) + peringkat controller hybrid untuk mengatur semua pembangkitan daya. Jika diterapkan, proyek angin 850-kW akan menjadi proyek percontohan untuk ini. Sebagai catatan, ada beberapa jalan lain yang belum dijajaki, seperti

misalnya pembangkitan daya tanpa diesel. Bila proyek PLTB ini diperbesar, mendistribusikan energy storage di dekat pusat beban harus dipertimbangkan, sehingga tidak membuat PLTB dan energy storage menjadi titik kegagalan bila terjadi gangguan; penempatan PLTB dan energy storage secara terpisah akan meningkatkan kandalan jaringan daya. Demikian pula, untuk mengintegrasikan dua PLTB, PLTB yang kedua harus ditempatkan di lokasi sumber daya angin yang berbeda dari yang pertama, dan dihubungkan pada bus yang berbeda, untuk menghindari titik kegagalan tunggal dan dengan demikian lebih meningkatkan keandalan jaringan terhadap gangguan.

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1 Latar Belakang

Tujuan dari proyek ini adalah untuk mempelajari dampak dari mengintegrasikan satu atau dua PLTB berdaya 850-kW dari Vestas dengan model Tipe 3 (doubly fed induction generator - DFIG) pada jaringan sistem tenaga Pulau Sumba bagian timur, di Indonesia. Pulau Sumba terpilih sebagai pulau terpilih untuk energi terbarukan berdasarkan studi yang dilakukan oleh Hivos International bekerjasama dengan Winrock International, Inc Sumba dipilih karena pertimbangan sebagai berikut:

- Akses penggunaan listrik sangat rendah (rasio elektrifikasi 24,5% pada tahun 2010);
- Hingga kini, Sumba sangat tergantung pada pembangkit listrik tenaga diesel - PLTD (85% dari bahan bakar minyak Diesel);
- Bahan bakar minyak dikirim dari daerah lain di Indonesia, memakan biaya transportasi yang tinggi.
- Sumba kaya akan sumber daya energi terbarukan termasuk air, bio-energi, angin, dan surya/PV.
- Sekitar 20% dari penduduk Sumba dianggap berpenghasilan rendah (miskin).

Pertumbuhan beban puncak di Sumba seperti yang ditunjukkan di Figure H-1, diperkirakan akan mencapai 13MW minimal pada tahun 2025, dengan pertumbuhan sekitar 300%. Maksimal, beban puncak diperkirakan dapat mencapai sekitar 20MW pada tahun 2025 (pertumbuhan sekitar 500%).

Figure H-1. Perkiraan pertumbuhan daya puncak di Pulau Sumba. Image from Hivos International (2011)

Peta sumber daya angin ada di Figure H-2. Di gambarkan bahwa sumber daya angin pada umumnya baik untuk keseluruhan pulau Sumba mencapai ketinggian sebesar 7.5m/detik pada tempat tempat tertentu tidak jauh dari pusat beban.

Figure H-2. Sumber daya angin rata-rata per tahun di Pulau Sumba.

Image from Hirsch et al. (2015)

Proyek ini merupakan kerjasama antara NREL, Winrock International Inc, dan PLN (perusahaan listrik di Indonesia). Dalam panduan “Steady-State and Dynamic System Model Validation” dianjurkan oleh North American Electric Reliability Corporation untuk mengembangkan dan menerapkan proses validasi data secara tercatat untuk memvalidasi model steady-state dan model sistem dinamis. Untuk itu, team ini telah mengembangkan proses tersebut, yang dijelaskan di sini, dan harus digunakan untuk memvalidasi model steady-state dan model dinamis. Sebagai catatan, langkah-langkah validasi ini belum dilaksanakan untuk proyek ini.

2 Analisa Steady-State

Analisa steady state dilakukan untuk menganalisa kondisi steady-state dari sistim jaringan daya termasuk tegangan, aliran daya melalui cabang cabang dan transformator dengan mempertimbangkan bermacam macam kasus yang mengancam kelangsungan sistim daya yang beroperasi dibawah stress.

2.1 Proses

Proses yang digunakan untuk menganalisa model steady-state yang didasarkan pada North American Electric Reliability Corporation (NERC) "Procedures for Validation of Powerflow and Dynamics Cases". Beberapa perubahan yang dilakukan dengan prosedur berdasarkan Peraturan Daerah (PLN) dan berdasarkan pertimbangan teknis. Berikut ini data yang diperoleh dari PLN di Sumba Timur. Data lengkap pada Lampiran A.

3. Data didapatkan dari PLN.
 - B. Jaringan penyulang
 - i. Status
 - C. Transformator
 - i. Status
 - ii. Load tap changer (LTC) position
 - iii. Tipe (transformator dengan LTCs diganti dengan tipe 1 untuk mengunci LTC)
 - D. Beban
 - i. Daya aktif
 - ii. Daya reaktif
 - E. Generator
 - i. Daya aktif
 - ii. Daya reaktif
4. Semua genset dan PLTB yang terhubung dengan jaringan di sambung melalui jaringan 20-kV sebagai generator pada bus-bus tertentu.

2.2 Analisa Aliran Daya

Data data jaringan sistim daya, data beban, data lengkap pembangkit daya - PTL, semuanya diperlukan untuk menganalisa model sistim daya. Appendix B berisi input data untuk setiap scenario (kasus), dan Appendix C terdiri dari hasil analisa aliran daya untuk setiap scenario (kasus).

Table H-1. Data-data bus/gardu-listrik untuk Sumba Timur

No.	Nama Gardu Listrik	Tingkat Tegangan dalam kV	Daya Pemutus (kA)	Daerah/zona	Nama Distrik
1	Haharu	20	16	Hambapraing	Haharu
2	Kambajawa	20	16	East Sumba	Kambajawa
3	Waingapu	20	16	Waingapu	Waingapu

Catatan: MHaharu adalah bus diantara Haharu dan Kambajawa. Bus ini diperkenalkan karena tipe kawat yang digunakan tidak sama — sepanjang 17 Km kawat dari satu tipe dan 8Km berikutnya kawatnya dari tipe yang berbeda. Didalam diagram yang ada, bus ini di label sebagai “Single busbar(3)/K-H2” seperti tertera dibawah bus Haharu.

Table H-2. Daftar dari generator di Haharu Bus #1

No.	Nama Generator	Tegangan (kV)	Kapasitas Daya MVA
1	WTG1	0.69	0.85
2	WTG2	0.69	0.85

Note: Generator kedua tidak dipakai jika hanya mengintegrasikan satu PLTB 850-kW.

Table H-3. Daftar dari generators di Kambajawa Bus #2

SNo.	Nama Generator	Tegangan (kV)	Kapasitas Daya MVA
1	Volvo	0.4	0.22
2	MTU1	0.4	0.65
3	MAN1	0.4	0.43
4	MTU2	0.4	0.43
5	MTU4	0.4	0.43
6	MAN2	0.4	0.32
7	DOOSAN1	0.4	0.42
8	DOOSAN2	0.4	0.42
9	DOOSAN3	0.4	0.42
10	DOOSAN4	0.4	0.42
11	DOOSAN5	0.4	0.42
Total:			4.58

Table H-4. Daftar dari generators di Waingapu Bus #3

SNo.	Nama Generator	Tegangan (kV)	Kapasitas Daya MVA
1	CAT	0.4	0.55
2	YANMAR	6.3	0.22
3	DEUTZ1	0.4	0.18
4	DEUTZ2	0.4	0.18
5	SWD1	6.3	0.22
6	SWD2	6.3	0.22
7	SWD3	6.3	0.22
Total			1.79

2.2.1 Aliran Daya Dasar

Aliran daya dasar menganalisa sistim daya sebelum PLTB terpasang dengan kondisi beban rendah dan beban puncak.

Menurut informasi yang didapat, total beban maksimum dalam sistim adalah 5.682 MW sekitar jam 6:00pm sore dan the total beban minimum dari system adalah 2.751 MW pada siang hari. Beban masing masing termasuk beban maksium dan minimum untuk setiap bus diberikan pada table H-5. Informasi tentang power factor beban juga diberikan untuk kondisi yang bersangkutan.

Table H-5. Beban daya dan power factor untuk beban pada ketiga gardu listrik

Nomor Bus	Nama of gardu-listrik	Level Tegangan dalam kV	Beban Maximum (MW), beban puncak	Power factor, beban puncak	Beban Minimum (MW), beban minimum	Power factor, beban minimum
1	Haharu	20	0.104	0.85	0.051	0.85
2	Kambajawa	20	3.494	0.9	1.691	0.95
3	Waingapu	20	2.084	0.9	1.0086	0.95
	Total		5.682		2.751	

Dari informasi yang didapat selama pengumpulan data dari PLN Sumba, selama beban minimum, hanya generator di Kambajawa yang di operasikan. Selama beban puncak hanya generator di Waingapu yang di operasikan. Selama beban puncak, beberapa generator di Waingapu di operasikan tergantung dari tambahan daya yang diperlukan. Urutan operasi ini berdasarkan dari efisiensi bahan bakar dari generator nya. Prioritas pertama adalah CAT C32 disusul oleh Yanmar, DEUTZ, SWD.

Untuk memodel tipe pembangkitan daya seperti ini, beberapa pilihan untuk mewakili slack bus digunakan untuk bermacam macam scenario.

Table H-6. Skenario untuk Slack bus

Scenario	Slack Bus
Tanpa Angin Beban Tinggi	MTU 1
Tanpa Angin Beban Rendah	MAN 1
Angin Tinggi (1) ^a Beban Tinggi	MTU 1
Angin Tinggi (2) Beban Rendah	DOOSAN 3
Angin Tinggi (2) Beban Tinggi	MAN 1
Angin Tinggi (2) Beban Rendah	DOOSAN 3

^a Angka dalam tanda kurung menunjukkan jumlah PLTB dalam jaringan yang di analisa

Data yang dikumpulkan dari PLN Sumba menunjukkan bahwa semua generator di operasikan dengan power factor sebesar 0.8. Untuk model power factor seperti ini menyebabkan aliran daya reaktif yang besar dibandingkan dengan beban, sehingga menyebabkan penyerapan daya reaktif yang tinggi pada slack-bus. Untuk mengatasi hal ini, beberapa generator di operasikan pada PF=1 untuk memastikan penyerapan daya reaktif yang minimal pada slack-bus. Tabel H-7 adalah daftar generator yang di matikan dan dioperasikan dengan PF=1 dalam empat scenario. Hasil dari analisa dasar menunjukkan bahwa generator di Kambajawa tidak mengalami overload, and semua tegangan berada dalam batasan yang ditentukan.

Table H-7. Status On atau Off generator dan power factor nya untuk satu PLTB dan dua PLTB

Nama Generator	Daya Mampu	Tanpa Angin Beban Tinggi		Tanpa Angin Beban Rendah		Angin Tinggi (1) Beban Tinggi		Angin Tinggi (1) Beban Rendah		Angin Tinggi (2) Beban Tinggi		Angin Tinggi (2) Beban Rendah	
		Status	PF	Status	PF	Status	PF	Status	PF	Status	PF	Status	PF
MTU2	430	ON	0.8	ON	0.8	ON	0.8	OFF	0	ON	0.8	OFF	0
DOOSAN1	420	ON	1	ON	1	ON	1	ON	1	ON	1	ON	1
DOOSAN2	420	ON	1	ON	1	ON	0.8	ON	0.8	ON	0.8	ON	0.8
DOOSAN3	420	ON	0.8	ON	1	ON	0.8	ON	0.8	ON	0.8	ON	0.8
DOOSAN4	420	ON	0.8	ON	0.8	ON	0.8	ON	0.8	ON	0.8	OFF	0
DOOSAN5	420	ON	0.8	ON	0.8	ON	0.8	ON	0.8	ON	0.8	OFF	0
VOLVO	220	ON	0.8	OFF	0	ON	0.8	OFF	0	ON	0.8	OFF	0
MAN1	430	ON	0.8	ON	0.8	ON	0.8	OFF	0	ON	0.8	OFF	0
MTU1	650	ON	0.8	OFF	0	ON	0.8	OFF	0	ON	0.8	OFF	0
MTU4	430	ON	0.8	OFF	0	ON	0.8	OFF	0	OFF	0	OFF	0
CAT	550	ON	0.8	OFF	0	ON	0.8	OFF	0	ON	0.8	OFF	0
YANMAR	220	ON	0.8	OFF	0	ON	1	OFF	0	OFF	0	OFF	0
MAN2	320	ON	0.8	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
DEUTZ-1	180	ON	1	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
DEUTZ-2	180	ON	0.8	OFF	0	ON	1	OFF	0	OFF	0	OFF	0
SWD-1	220	ON	1	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
SWD-2	220	ON	0.8	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
SWD-3	220	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0	OFF	0
WTG	850	OFF	0	OFF	0	ON	1	ON	1	ON	1	ON	1

Figure H-3. Aliran daya – Beban Tinggi, Tanpa PLTB, MTU1 =Slack Bus

Figure H-4. Aliran daya – Beban rendah, Tanpa PLTB, MAN 1 =Slack Bus

2.2.2 Aliran Daya dengan PLTB Terpasang

Sistim ini dianalisa dengan PLTB terpasang dalam dua scenario yang sama seperti terdahulu sehubungan dengan pemasangan satu dan dua PLTB dengan kapasitas sebesar 850 kW dengan tegangan sebesar 0.69 kV. Analisa sistim daya di lakukan dengan kondisi beban yang sama seperti analisa dasar dengan scenario yang sama. Hasilnya di berikan di Tabel 8.

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Table H-8. Perbandingan Berbagai Skenario Aliran Daya

	High Load Scenario			Low Load Scenario		
	Without WTG(s)	With 1 WTG	With 2 WTGs	Without WTG(s)	With 1 WTG	With 2 WTGs
INPUT						
Load, PF at Kambajawa	3.494 MW, 0.9	3.494 MW, 0.9	3.494 MW, 0.9	1.691 MW, 0.95	1.691 MW, 0.95	1.691 MW, 0.95
Load, PF at Waingapu	2.084 MW, 0.9	2.084 MW, 0.9	2.084 MW, 0.9	1.009 MW, 0.95	1.009 MW, 0.95	1.009 MW, 0.95
Load, PF at Haharu	0.104 MW, 0.85	0.104 MW, 0.85	0.104 MW, 0.85	0.051 MW, 0.85	0.051 MW, 0.85	0.051 MW, 0.85
OUTPUT						
Real Power Generated by WTG(s)	0	0.85 MW	1.7 MW	0	0.85 MW	1.7 MW
Reactive Power Generated by WTG(s)	0	0 MVAR	0 MVAR	0	0.085 MVAR	0 MVAR
Real Power Generated by Kambajawa Generators	4.171 MW	3.988 MW	3.956 MW	2.779 MW	1.954 MW	1.198 MW
Reactive Power Generated by Kambajawa Generators	2.108 MVAR	2.64 MVAR	2.955 MVAR	1.022 MVAR	1.031 MVAR	1.095 MVAR
Real Power Generated by Waingapu Generators	1.567 MW	0.94 MW	0.22 MW	0	0	0
Reactive Power Generated by Waingapu Generators	0.876 MVAR	0.412 MVAR	0.165 MVAR	0	0	0
PU Voltage at Haharu (20 kV)	0.984	1.032	1.084	0.986	1.04	1.081
PU Voltage at MHaharu (20 kV)	0.99	1.003	1.025	0.989	1.008	1.018
PU Voltage at Kambajawa (20 kV)	0.992	0.996	1.009	0.99	0.999	1.001
PU Voltage at Waingapu (20 kV)	0.989	0.988	0.997	0.984	0.994	0.996

	High Load Scenario			Low Load Scenario		
	Without WTG(s)	With 1 WTG	With 2 WTGs	Without WTG(s)	With 1 WTG	With 2 WTGs
Real Power Consumed by Line between Kambajawa and MHaharu	0 MW	0.006 MW	0.025 MW	0 MW	0.007 MW	0.027 MW
Reactive Power Consumed by Line between Kambajawa and MHaharu	0.004 MVAR	0.001 MVAR	0.01 MVAR	0.004 MVAR	0.001 MVAR	0.011 MVAR
Real Power Consumed by Line between MHaharu and Haharu	0.001 MW	0.022 MW	0.092 MW	0 MW	0.025 MW	0.1 MW
Reactive Power Consumed by Line between MHaharu and Haharu	0.003 MVAR	0.005 MVAR	0.033 MVAR	0.004 MVAR	0.006 MVAR	0.036 MVAR
Real Power Consumed by Line between Kambajawa and Waingapu	0.001 MW	0.007 MW	0.016 MW	0.004 MW	0.004 MW	0.004 MW
Reactive Power Consumed by Line between Kambajawa and Waingapu	0.002 MVAR	0.005 MVAR	0.017 MVAR	0.001 MVAR	0.001 MVAR	0.001 MVAR
Haharu-Kambajawa Line Loading in kA (3.18 MVA)*	0.004	0.021	0.042	0.002	0.022	0.044
Kambajawa-Waingapu Line Loading in kA (7.4 MVA)*	0.016	0.05	0.059	0.031	0.031	0.031

2.2.3 Hasil dari Aliran Daya dengan PLTB Terpasang

Hasil-hasil nya menunjukkan bahwa:

- Tegangan di semua bus berada dalam batas Peraturan Listrik (grid code)
- Beban pada penyulang berada dalam batas pemanasan (thermal limit) dari kawat yang dipakai

Dari perspektif aliran daya, pemasangan satu atau dua PLTB sebesar 850kW tidak akan menyebabkan dampak yang merusak/jelek pada jaringan.

2.3 Analisa Short – Circuit

Dua tipe analisa short-circuit dilakukan:

- Penghitungan Short-circuit power ratio untuk mengukur kekuatan dari jaringan pada titik pertemuan. Section 2.3.1 menjelaskan analisa ini.
- Penghitungan of kontribusi short-circuit dari PLTB. Section 2.3.2 menjelaskan analisa ini.

2.3.1 Gangguan Short Circuit pada titik pertemuan (Point of Common Coupling - PCC) dari PLTB (sebelum PLTB terpasang)

Skenario apa adanya, short-circuit power di Haharu bus (PCC dari PLTB) dihitung.

Table H-9. Perbandingan Berbagai Skenario Short Circuit di PCC

	Tanpa WTG	
	3- Phase Gangguan saat Beban Tinggi	3- Phase Gangguan saat Beban Rendah
INPUT PARAMETERS		
Pembangkitan Daya di Kambajawa	4.171 MW	2.779 MW
Pembangkitan Daya di Waingapu	1.567 MW	0 MW
OUTPUT		
Short-Circuit Power di Haharu bus	14.8 MVA	12.3 MVA
Short-Circuit Power Ratio di Haharu bus (untuk PLTB 0.85MW)	17.41	14.47
Kontribusi Saat Gangguan dari Generator di Kambajawa	11.3 MVA	12.3 MVA
Kontribusi Saat Gangguan dari Generator di Waingapu	3.5 MVA	0 MVA

Catatan, terminology yang dipakai dalam bagian ini dijelaskan disini.

- *Short-circuit power* sebetulnya adalah short circuit-daya penuh output dari generator dengan unit terpakai MVA. Ini menunjukkan bahwa sebetulnya saat short-circuit, “daya aktif” sebetulnya sangatlah kecil, “daya penuh” yang tercantum sebagian besar di serap sebagai “daya reaktif” yang diserap dalam reaktansi didalam generator, transformator, dan reaktansi penyulang.
- *Short-Circuit Power ratio (SCPR)* dinyatakan dalam satuan per-unit. $SCPR = 17.41$ selama beban tinggi dan 14.47 selama beban rendah. Ini semua jauh diatas SCPR yang diperlukan untuk memasang PLTB. Di semua grid codes yang ada, SCPR yang diperlukan biasanya berkisar 5 (dihitung saat PLTB off) atau lebih tinggi untuk menghindari variasi tegangan di PCC pada saat PLTB beroperasi dengan kecepatan angin yang tinggi.

Figure H-8. Analisa Short Circuit untuk gangguan 3-phase pada PCC (Beban Rendah)

2.3.2 Gangguan Short Circuit di PCC dari PLTB (sebelum dan sesudah PLTB terpasang)

Table H-10. Perbandingan Kontribusi dari Short Circuit Power dari PLTB

	Beban Tinggi		Beban Rendah	
	Short Circuit di Kambajawa	Short Circuit di Waingapu	Short Circuit di Kambajawa	Short Circuit di Waingapu
Satu PLTB berdaya 850 kW				
Short-Circuit Power pada Bus yang Terganggu	41.8 MVA	34.1 MVA	30.8 MVA	26.4 MVA
Kontribusi Gangguan dari PLTB	1.8 MVA	1.5MVA	1.9 MVA	1.6 MVA
Dua PLTB masing masing berdaya 850 kW				
Short-Circuit Power pada Bus yang Terganggu	34 MVA	39.8 MVA	17.9 MVA	16.3 MVA
Kontribusi Gangguan dari PLTB	2.8 MVA	3.4 MVA	3.6 MVA	3.2 MVA

Seperti diduga, kontribusi short-circuit power dari PLTB sangatlah minimal. Kesimpulannya adalah Daya Terpasang (MVA) dari sistim pengaman yang terpasang dan equipment terpasang lainnya di gardu listrik seharusnya cukup untuk memadai satu atau dua PLTB masing masing berdaya 850kW.

2.4 Pedoman untuk Mengidentifikasi dan Mengatasi Perbedaan yang Tidak Dapat Diterima

Tabel dibawah ini dapat dipakai untuk menidentifikasi dan mengatasi perbedaan dalam proses memvalidasi steady state model. Table 11 dibawah ini bisa dipakai untuk perbedaan dalam bentuk prosentase dan perbedaan dalam harga mutlak untuk aliran daya aktif, daya reaktif, dan power factor dalam jaringan distribusi dengan tegangan 20kV atau tegangan yang lebih rendah untuk renewable energy power plants berkapasitas 10MW atau lebih rendah¹.

Table H-11. Pedoman untuk mengidentifikasi perbedaan yang dapat diterima untuk jaringan 20kV

Quantity	Acceptable Differences
Bus Voltage Magnitude	85% to 110%
Frequency	51 to 47.5 Hz
Power factor	0.9 leading to 0.85 lagging

¹ "Guidelines for Connecting Renewable Energy Generation Plants (REGP) to PLN's Distribution System," Feb 2014, approved by PLN Board of Directors as DK. Dir. PLN No.0357/2014.

Table H-12. Guidelines to resolve unacceptable differences

Quantity	Resolution Guidelines
Bus Voltage Magnitude Real Power Flow Reactive Power Flow	<p>Verify that the generation should be modeled as gross instead of net values.</p> <p>Verify that shunt capacitors are sized correctly.</p> <p>Verify that all state estimator loads are accounted for.</p> <p>Verify that the network configuration is modeled appropriately based on the circuit breaker and switch status (e.g., does a bus need to be modeled as a split bus due to an open circuit?).</p> <p>Verify that the modeled line and transformer impedances are correct.</p> <p>Verify that no-load tap changers are modeled appropriately for all transformers.</p> <p>Verify that all other system elements are modeled appropriately.</p> <p>Consider whether PI data should be used when state estimator data are questionable.</p> <p>Consider whether differences are caused by measurement error.</p>

3 Analisa Sistim Dinamis

3.1 Proses

Proses yang digunakan untuk menganalisa model steady-state yang didasarkan pada North American Electric Reliability Corporation (NERC) "Procedures for Validation of Powerflow and Dynamics Cases". Beberapa perubahan yang dilakukan dengan prosedur berdasarkan Peraturan Daerah (PLN) dan berdasarkan pertimbangan teknis.

Pada intinya, analisa sistem dinamis dilakukan dengan menggunakan kondisi sistem yang tercatat pada pada hari dan waktu tertentu sebagai data masukan untuk melihat apakah output (tegangan bus dan aliran daya aktif dan reaktif) yang dihasilkan oleh model yang dipakai sesuai dengan kondisi sistem yang diukur di lapangan. Lebih penting lagi, analisa ini harus termaksud analisa sebelum terjadi gangguan, pada saat gangguan, dan sesudah gangguan terutama mencakup tegangan, frekuensi, overload penyulang atau transformator) di bus yang penting.

Berbagai gangguan harus dipertimbangkan dengan masukan dari PLN lokal. Pertimbangan harus dimulai dengan kemungkinan gangguan terbanyak berdasarkan data historis yang dicatat oleh PLN. Beberapa contoh kontinjensi untuk beban puncak / ringan, dan dengan / tanpa generator PLTB harus diikuti sertakan:

- Pemutusan PLTB (mencakup kecepatan angin rendah dan kecepatan angin tinggi)
- Pemutusan sebagian dari beban dari jaringan
- Pemutusan salah satu atau beberapa diesel genset dari jaringan
- Gangguan pada bus-bus tertentu

Untuk analisa ini, digunakan metoda electromechanical transient simulation metoda dari PowerFactory dengan menggunakan harga effective (rms). Dalam metoda ini "A-Stable" algorithm dipakai untuk step-size yang bisa di adaptasi didalam perhitungan integrasi.

3.2 Data Dinamis of Komponen-komponen Jaringan

Data dinamis yang dipakai untuk simulasi dinamis di cantumkan di Appendix E. Untuk komponen komponen yang datanya tidak disediakan oleh PLN, atau yang tidak tersedia untuk Sumba Timur, kami memakai data dinamis umum (generic).

3.2.1 Gangguan Transien dan Kondisi dari Sistim Daya

Kasus-kasus berikut ini akan di periksa dan diamati:

- Sebelum Gangguan: Analisa dasar tanpa PLTB (beban puncak dan beban rendah). In di beri nama "Tanpa Angin Beban Tinggi" dan "Tanpa Angin Beban Rendah"
- Sebelum Gangguan: Satu PLTB terpasang (beban puncak dan beban rendah). In di beri nama "Angin Tinggi Beban Tinggi" dan "Angin Tinggi Beban Rendah"
- Terminologi "gangguan" dipakai untuk menunjukkan adanya "short-circuit" atau "pemutusan" beban ataupun generator.
- Analisa gangguan diikuti oleh:

- Self-clearing dimana tidak satupun (beban, generator, penyulang) di putuskan dari jaringan. Kasus-kasus ini tidak memiliki label tambahan. Hal ini diasumsikan bahwa gangguan hilang dengan sendirinya sebelum pemutus sirkuit diaktifkan.
- No Self-Clearing. Kasus-kasus ini diberi label dengan kata-kata "No Self-Clearing". Hal ini diasumsikan bahwa gangguan bertahan tanpa ada upaya untuk menghapus gangguan ini. Jika gangguan ini tidak diisolasi, akhirnya sistem jaringan listrik dapat mengalami "black out".

Waktu gangguan akan dipilih selama 9 cycles atau 0,18 detik (untuk 50Hz) seperti yang biasa digunakan di Amerika Serikat.

Macam gangguan pertama yang akan dianalisa adalah gangguan pada bus tertentu (di masing-masing tiga bus-Haharu, Kambajawa dan Waingapu).

3.2.2 Hilangnya Sebagian Beban

Gangguan yang dapat menyebabkan hilangnya beban umumnya karena overload atau short-circuit. Biasanya urutan peristiwa yang terjadi adalah akibat dari kerja sistem pengamanan. Skenario yang paling mungkin terjadi dimulai sistem pengamanan berusaha untuk mengisolasi (supaya tidak menyebar ke seluruh jaringan) dan memutuskan ke sekelompok beban dari jaringan, dengan demikian, dampaknya pada sistem daya nampak sebagai hilangnya beban dari jaringan. Karena generasi daya total adalah sekitar 6 MW beban puncak dan 3.8MW beban rendah, ukuran dipilih untuk mewakili hilangnya beban 400kW, yaitu ukuran rata-rata diesel gen-set di Sumba Timur. DIGSILENT hanya memungkinkan untuk mewujudkan kehilangan beban dalam prosentase dari beban total, bukannya kehilangan beban sebesar 400kW tepat, Tabel di bawah ini berisi daftar skenario kehilangan beban yang dipakai dalam analisa.

Table H-13. Skenario Beban Hilang

Bus	Scenario	High Load (MW)	Low Load (MW)
Haharu	Sebelum Gangguan	0.104	0.069
	Setelah Gangguan	0	0
	Prosentase hilang (100 %)	0.104	0.069
Kambajawa	Sebelum Gangguan	3.494	2.085
	Setelah Gangguan	2.981	1.776
	Prosentase hilang (15 %)	0.513	0.309
Waingapu	Sebelum Gangguan	2.084	1.782
	Setelah Gangguan	1.676	1.434
	Prosentase hilang (20 %)	0.408	0.348

3.2.3 Hilangnya Sebagian Pembangkitan Daya

Dalam skenario ini, diasumsikan bahwa hilangnya pembangkitan daya setara dengan pemutusan generator diesel tunggal dari jaringan, dan ukuran khas generator diesel di Sumba Timur adalah 400kW. Dengan demikian, pemutusan generator dari jaringan dipilih untuk memiliki kapasitas

sebesar 400kW. Di Kambajawa dan Waingapu, pembangkitan daya di wakilih oleh dua generator yaitu, satu generator mewakili kelompok generator yang akan tetap terhubung selama dan setelah gangguan, sedangkan generator kedua (400kW) merupakan generator yang akan terputus selama gangguan.

3.3 Batasan Tegangan dan Trekuensi Dalam Studi Ini.

PLN memberikan batas normal untuk tegangan dan frekuensi di jaringan Sumba Timur; batas lainnya didasarkan atas praktek yang digunakan dibanyak tempat. Berikut ini adalah batas yang digunakan untuk penelitian ini:

- Batas tegangan operasi didefinisikan pada $\pm 10\%$ dari tegangan nominal.
- Batas-batas operasi frekuensi untuk semua komponen grid didefinisikan antara 0,97-1,03 pu
- Batas-batas operasi tegangan rendah untuk turbin angin yang didefinisikan pada 0,9 pu selama 60 second (detik) dan 0,85 p.u. selama 11 second (detik).
- Batas-batas operasi tegangan tinggi untuk turbin angin yang didefinisikan pada 1.1 pu selama 60 s, 1,15 p.u. untuk 2 s dan 1,2 p.u. untuk 80 ms.
- Batas-batas operasi frekuensi rendah dan tinggi untuk turbin angin didefinisikan sebagai 47 Hz dan 53 Hz untuk 200 ms.
- Batas-batas operasi tegangan untuk pembangkit diesel didefinisikan antara 0,9-1,1 pu
- Batas-batas operasi frekuensi untuk pembangkit diesel didefinisikan antara 47-53 Hz untuk 200 ms.
- Prioritas yang lebih tinggi diberikan untuk PLTB melebihi pembangkitan dari diesel setiap saat tenaga angin tersedia. Untuk semua skenario diselidiki, tidak ada satupun situasi yang tidak dapat diterima.

3.4 Skenario untuk Mengintegrasikan Satu PLTB Berdaya 850-kW

Ringkasan analisis transien dari skenario dan kinerja yang diamati untuk jaringan diberikan di Tabel H-14. Angka-angka ini terkandung dalam Lampiran E. Kasus kasus yang dianggap penting di tulis dengan huruf tebal dan digarisbawahi sesuai dengan macam ketidakstabilan; jenis ketidakstabilan dijelaskan dalam kolom pengamatan.

Table H-14. Skenario and pengamatan untuk analisa dinamis dengan satu PLTB

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
Gangguan tiga fasa ke tanah pada bus Haharu. Gangguan terjadi pada 1 detik & dan dihilangkan pada 1.18 detik.			
1	Tanpa Angin Beban Tinggi	Figure E-1, E-2	Sistem stabil; pembebanan penyulang dalam batas normal. Pembebanan penyulang dalam batasan normal. Tegangan di bus turun sampai sekitar 0.65 pu.

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
			Frekwensi turun sampai 0.97 p.u. dan kembali pada 12 detik.
1	Tanpa Angin Beban Rendah	Figure E-3, E-4	Sistem stabil. Pembebanan penyulang dalam batasan normal. Tegangan di bus turun sampai sekitar 0.625 pu. dan kembali dalam 0.18 detik.
3	Angin Tinggi Beban Tinggi	Figure E-5, E-6, dan E-7	Sistem stabil Pembebanan penyulang dalam batas normal. Frekuensi turun mencapai 0.965pu dan pulih kembali dalam waktu sekitar 2.5 detik. Tegangan di bus turun sampai sekitar 0.6 pu di bus K dan W. Tegangan terminal dan daya output dari semua generator semuanya stabil
4	Angin Tinggi Beban Rendah	Figure E-8, E-9, dan E-10	Sistem stabil Pembebanan penyulang dalam batas normal. Frekuensi turun mencapai 0.96pu dan pulih kembali dalam waktu sekitar 2 detik. Tegangan di bus turun sampai sekitar 0.45 pu di bus K dan W. Tegangan terminal dan daya output dari semua generator semuanya stabil
Gangguan tiga fasa ke tanah pada bus Kambajawa. Gangguan terjadi pada 1 detik dan dihilangkan pada 1.18 detik.			
5	Tanpa Angin Beban Tinggi	Figures E-11, E-12	Sistem stabil Pembebanan penyulang dalam batas normal. Tegangan terminal di generator turun dibawah 0.3 p.u. selama gangguan. Tegangan di bus Haharu dang Waingapu turun dibawah 0.1 pu.selama gangguan. Tegangan kembali segera sesudah gangguan dihilangkan
6	Tanpa Angin Beban Rendah	Figure E-13	Sistem stabil Pembebanan penyulang dalam batas normal. Tegangan terminal di generator turun dibawah 0.3 p.u. selama gangguan.

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
			Tegangan di bus Haharu dan Waingapu turun dibawah 0.1 pu. selama gangguan. Tegangan kembali segera sesudah gangguan dihilangkan
7	Angin Tinggi Beban Tinggi	Figures E-14, E-15	Sistem stabil Pembebanan penyulang dalam batas normal. Frekwensi jatuh sampai 0.99 p.u. dan kembali dalam waktu 2.5 detik. Tegangan di bus K dan W turun di bawah 0.1 pu. Tegangan terminal dan daya output dari semua generator semuanya stabil
8	Angin Tinggi Beban Rendah	Figure E-16 dan E-17	Sistem stabil. Pembebanan penyulang dalam batas normal. Frekuensi turun sampai 0.99 pu dan pulih dalam waktu sekitar 8 detik. Tegangan jatuh di bawah 0.2 pu di bus K dan bus W. Tegangan dan daya output generator stabil.
Gangguan tiga fasa ke tanah pada bus Waingapu. Gangguan terjadi pada 1 detik & dan dihilangkan pada 1.18 detik.			
9	Tanpa Angin Beban Tinggi	Figure E-18, E-19	Tegangan pada terminal generator turun di bawah 0.1pu selama gangguan, Tegangan bus di Haharu dan Kambajawa turun sampai di bawah 0.2 pu selama gangguan. Tegangan segera pulih kembali setelah gangguan dihilangkan
10	Tanpa Angin Beban Rendah	Figure E-20	Tegangan di terminal generator jatuh di bawah 0.1pu selama gangguan. Tegangan di bus Haharu dan Kambajawa jatuh dibawah 0.2 p.u. selama gangguan. Tegangan segera kembali sesudah gangguan dihilangkan.
11	Angin Tinggi Beban Tinggi	Figure E-21 and E-22	Tegangan pada terminal generator turun di bawah 0.3pu selama gangguan Tegangan bus di Haharu dan Kambajawa turun sampai di bawah 0.2 pu selama gangguan. Tegangan segera pulih kembali

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
			setelah gangguan dihilangkan
12	Angin Tinggi Beban Rendah	Figure E-23 and E-24	Tegangan di terminal generator turun di bawah 0.3pu selama gangguan. Tegangan di bus Haharu dan Kambajawa turun dibawah 0.2 p.u. selama gangguan. Tegangan segera kembali sesudah gangguan dihilangkan.
Gangguan pada PLTB. Gangguan terjadi pada 1 detik dan dihilangkan pada 1.18 detik			
13	Angin Tinggi Beban Tinggi	Figure E-25, E-26 and E-27	Sistim stabil Pembebanan penyulang, tegangan dan frekwensi jaringan berada dalam batasan normal. Tegangan transien pada bus Haharu dan PLTB output transien sesudah gangguan di hilangkan.
14	Angin Tinggi Beban Rendah	Figure E-28 and E-29	Sistim stabil. Pembebanan penyulang, tegangan dalam batasan normal. Tegangan transien pada bus Haharu dan PLTB daya transient nampak setelah gangguan dihilangkan.
Gangguan pada PLTB. Gangguan terjadi pada 1 detik dan tidak dihilangkan (PLTB tidak disambung kembali)..			
15	Angin Tinggi Beban Tinggi	Figure E-30, E-31 and E-32	Dalam kasus ini terlihat hilangnya sinkronisasi. Ini dapat terjadi karena menghilangnya daya PLTB sebesar 850kW dari jaringan. Storage bila dipasang dengan PLTB dapat menyediakan daya sementara sampai adanya tambahan daya dari diesel genset tambahan untuk mengganti kehilangan daya yang besar.
16	Angin Tinggi Beban Rendah	Figure E-33 and E-34	Dalam kasus ini terlihat hilangnya sinkronisasi. Ini dapat terjadi karena menghilangnya daya PLTB sebesar 850kW dari jaringan. Storage bila dipasang dengan PLTB dapat menyediakan daya sementara sampai adanya tambahan daya dari diesel genset tambahan untuk mengganti kehilangan daya yang besar.
Gangguan pada sebagian generator di bus Kambajawa. Gangguan terjadi pada 1 detik, dan dihilangkan pada 1.18 detik.			

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
17	Tanpa Angin Beban Tinggi	Figure E-35 and E-36	Sistim stabil Pembebanan penyulang, tegangan berada dalam batasan normal.
18	Tanpa Angin Beban Rendah	Figure E-37	Sistim stabil Pembebanan penyulang, tegangan berada dalam batasan normal. Setelah gangguan, frekwensi mencapai 1.015p.u dan 0.985 p.u. sedikit diluar batasan normal.
19	Angin Tinggi Beban Tinggi	Figure E-38 and E-39	Sistim stabil Pembebanan penyulang, tegangan berada dalam batasan normal. Setelah gangguan, frekwensi mencapai 1.015p.u dan 0.985 p.u. sedikit diluar batasan normal.
20	Angin Tinggi Beban Rendah	Figure E-40 and E-41	Sistim stabil Pembebanan penyulang, tegangan berada dalam batasan normal. Setelah gangguan, frekwensi mencapai 1.015p.u dan 0.985 p.u. sedikit diluar batasan normal.
Gangguan pada sebagian generator di bus Kambajawa. Gangguan terjadi pada 1 detik, dan tidak dihilangkan			
21	Tanpa Angin Beban Tinggi	Figure E-42 dan E-43	Sistem tidak stabil. Sesudah gangguan terjadi, frekwensi terus turun, dan frekwensi tak terkendalikan.
22	Tanpa Angin Beban Rendah	Figure E-44	Sistem tidak stabil. Sesudah gangguan terjadi, frekwensi terus turun, dan frekwensi tak terkendalikan. Tegangan pada bus dan terminal generator juga terus menurun.
23	Angin Tinggi Beban Tinggi	Figure E-45 and E-46	Sistem tidak stabil. Sesudah gangguan terjadi, frekwensi terus turun, dan frekwensi tak terkendalikan.
24	Angin Tinggi Beban Rendah	Figure E-47 and E-48	Sistem tidak stabil. Sesudah gangguan terjadi, frekwensi terus turun, dan frekwensi tak terkendalikan. Tegangan pada bus dan terminal generator juga terus menurun.
Gangguan pada sebagian generator di bus Waingapu. Gangguan terjadi pada 1 detik, dan dihilangkan pada 1.18 detik.			

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
25	Tanpa Angin Beban Tinggi	Figure E-49 and E-50	Sistim stabil. Pembebanan penyulang dan tegangan pada bus ada dalam batasan normal.
26	Angin Tinggi Beban Tinggi	Figure E-51 and E-52	Sistim stabil. Pembebanan penyulang dan tegangan pada bus ada dalam batasan normal. Selama gangguan, frekwensi keluar dari batasan 1% dua kali, tapi akhirnya kembali 1 detik sesudah gangguan.
Gangguan pada sebagian generator di bus Waingapu. Gangguan terjadi pada 1 detik, dan gangguan tidak dihilangkan.			
27	Tanpa Angin Beban Tinggi	Figure E-53, and E-54	Sistim tidak stabil. Setelah gangguan, frekwensi terus jatuh, dan frekwensi tak terkendalikan. Dalam kasus ini tidak cukup daya cadangan tersedia pada generator yang jalan.
28	Angin Tinggi Beban Tinggi	Figure E-55 and E-56	Sistim tidak stabil. Setelah gangguan, frekwensi terus jatuh, dan frekwensi tak terkendalikan. Dalam kasus ini tidak cukup daya cadangan tersedia pada generator yang jalan.
Hilangnya beban di bus Haharu. Gangguan terjadi pada 1 detik dan beban disambung kembali pada 1.18 detik			
29	Tanpa Angin Beban Tinggi	Figure E-57 and E-58	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
30	Tanpa Angin Beban Rendah	Figure E-59	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
31	Angin Tinggi Beban Tinggi	Figure E-60 and E-61	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
32	Angin Tinggi Beban Rendah	Figure E-62 and E-63	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
Hilangnya beban di bus Haharu. Gangguan terjadi pada 1 detik dan beban tidak disambung kembali			
33	Tanpa Angin Beban Tinggi	Figure E-64	Sistim stabil

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
		and E-65	Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
34	Tanpa Angin Beban Rendah	Figure E-66	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
35	Angin Tinggi Beban Tinggi	Figure E-67 and E-68	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
36	Angin Tinggi Beban Rendah	Figure E-69 and E-70	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
Hilangnya beban di bus Kambajawa. Gangguan terjadi pada 1 detik dan beban disambung kembali pada 1.18 detik			
37	Tanpa Angin Beban Tinggi	Figure E-71 and E-72	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
38	Tanpa Angin Beban Rendah	Figure E-73	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
39	Angin Tinggi Beban Tinggi	Figure E-74 and E-75	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
40	Angin Tinggi Beban Rendah	Figure E-76 and E-77	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
Hilangnya beban di bus Kambajawa. Gangguan terjadi pada 1 detik dan beban tidak disambung kembali.			
41	Tanpa Angin Beban Tinggi	Figure E-78 and E-79	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
42	Tanpa Angin Beban Rendah	Figure E-80	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
43	Angin Tinggi Beban Tinggi	Figure E-81	Sistim stabil

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
		and E-82	Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
44	Angin Tinggi Beban Rendah	Figure E-83 and E-84	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
Hilangnya beban di bus Waingapu. Gangguan terjadi pada 1 detik dan beban disambung kembali pada 1.18 detik			
45	Tanpa Angin Beban Tinggi	Figure E-85 and E-86	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
46	Tanpa Angin Beban Rendah	Figure E-87	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
47	Angin Tinggi Beban Tinggi	Figure E-88 and E-89	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
48	Angin Tinggi Beban Rendah	Figure E-90 and E-91	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
Hilangnya beban di bus Waingapu. Gangguan terjadi pada 1 detik dan beban tidak disambung kembali.			
49	Tanpa Angin Beban Tinggi	Figure E-92 and E-93	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
50	Tanpa Angin Beban Rendah	Figure E-94	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
51	Angin Tinggi Beban Tinggi	Figure E-95 and E-96	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
52	Angin Tinggi Beban Rendah	Figure E-97 and E-98	Sistim stabil Pembebanan penyulang, tegangan, dan frekuensi berada dalam batas normal.
Short-circuit pada penyulang Kambajawa-Haharu. Gangguan terjadi pada 1 second, dan			

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
dihilangkan dalam 180 msecond.			
53	Tanpa Angin Beban Tinggi	Figure E-99 and E-100	Terjadi islanding (terlepas dari jaringan) di Haharu; beban di Haharu dilepas selama 180 ms. Sesudah gangguan dihilangkan, sistim daya stabil Frekwensi jatuh sampai 0.97 p.u., diluar batas normal, selama 4 detik, dan kemudian kembali ke normal.
54	Tanpa Angin Beban Rendah	Figure E-101	Terjadi islanding (terlepas dari jaringan) di Haharu; beban di Haharu dilepas selama 180 ms. Sesudah gangguan dihilangkan, sistim daya stabil Frekwensi jatuh sampai 0.97 p.u., diluar batas normal, selama 4 detik, dan kemudian kembali ke normal.
55	Angin Tinggi Beban Tinggi	Figure E-102 and E-103	Terjadi islanding (terlepas dari jaringan) di Haharu; beban di Haharu dilepas selama 180 ms. Sesudah gangguan dihilangkan, sistim daya stabil Frekwensi jatuh sampai 0.97 p.u., diluar batas normal, selama 4 detik, dan kemudian kembali ke normal. PLTB tetap terhubung ke jaringan.
56	Angin Tinggi Beban Rendah	Figure E-104 and E-105	Terjadi islanding (terlepas dari jaringan) di Haharu; beban di Haharu dilepas selama 180 ms. Sesudah gangguan dihilangkan, sistim daya stabil Frekwensi jatuh sampai 0.97 p.u., diluar batas normal, selama 4 detik, dan kemudian kembali ke normal. PLTB tetap terhubung ke jaringan.
Short-circuit pada penyulang Kambajawa-Haharu. Gangguan terjadi pada 1 second, dan tidak dihilangkan.			
57	Tanpa Angin Beban Tinggi	Figure E-106 and E-107	Relay tidak di model, jadi gangguan short circuit bertahan pada saluran penyulang menyebabkan hlangnya sinkronisasi
58	Tanpa Angin Beban Rendah	Figure E-108	Relay tidak di model, jadi gangguan short circuit bertahan pada saluran penyulang menyebabkan hlangnya sinkronisasi
59	Angin Tinggi Beban Tinggi	Figure E-109	Relay tidak di model, jadi gangguan

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
		and E-110	short circuit bertahan pada saluran penyulang menyebabkan hilang sinkronisasi
60	Angin Tinggi Beban Rendah	Figure E-111 and E-112	Relay tidak di model, jadi gangguan short circuit bertahan pada saluran penyulang menyebabkan hilang sinkronisasi
Gangguan short circuit pada penyulang antara Kambajawa-Waingapu. Gangguan terjadi pada 1 detik dan dihilangkan dalam waktu 180 msecond			
61	Tanpa Angin Beban Tinggi	Figure E-113 and E-114	Terjadi islanding di Waingapu Sesudah gangguan dihilangkan, sistim stabil. Pembebanan penyulang, tegangan, dan frekwensi berada dalam batasan normal.
<u>62</u>	Tanpa Angin Beban Rendah	Figure E-115	Terjadi islanding di Waingapu Sesudah gangguan dihilangkan, sistim stabil. Pembebanan penyulang, tegangan, dan frekwensi berada dalam batasan normal.
63	Angin Tinggi Beban Tinggi	Figure E-116 and E-117	Terjadi islanding di Waingapu Sesudah gangguan dihilangkan, sistim stabil. Pembebanan penyulang, tegangan, dan frekwensi berada dalam batasan normal.
64	Angin Tinggi Beban Rendah	Figure E-118 and E-119	Terjadi islanding di Waingapu Sesudah gangguan dihilangkan, sistim stabil. Pembebanan penyulang, tegangan, dan frekwensi berada dalam batasan normal.
Gangguan short circuit pada penyulang antara Kambajawa-Waingapu. Gangguan terjadi pada 1 detik dan tidak dihilangkan.			
<u>65</u>	Tanpa Angin Beban Tinggi	Figure E-120 and E-121	Relay tidak dimodel, jadi gangguan short circuit pada jaringan penyulang menyebabkan sistim daya kehilangan sinkronisasi
<u>66</u>	Tanpa Angin Beban Rendah	Figure E-122	Relay tidak dimodel, jadi gangguan short circuit pada jaringan penyulang menyebabkan sistim daya kehilangan sinkronisasi
<u>67</u>	Angin Tinggi Beban Tinggi	Figure E-123 and E-124	Relay tidak dimodel, jadi gangguan short circuit pada jaringan penyulang menyebabkan sistim daya kehilangan

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
			sinkronisasi
68	Angin Tinggi Beban Rendah	Figure E-125 and E-126	Relay tidak dimodel, jadi gangguan short circuit pada jaringan penyulang menyebabkan sistim daya kehilangan sinkronisasi

Gambar-gambar yang disebut dalam table diatas ada di Appendix E.

3.5 Analisa Sistim dengan Tambahan Energy Storage

Penelitian ini meliputi analisa energy storage sebagai metode untuk menghindari ketidakstabilan sistem di Sumba Timur yang dapat terjadi dengan pemasangan 850kW PLTB. Energy storage Power Store dari ABB dipakai dalam analisa ini. Model untuk controller dari ABB untuk energy storage juga dipakai disini. Energy storage ini dimodel sebagai sumber arus (current source), dan arus aktif (I_R) dan arus reaktif (I_I) dapat di atur secara langsung dan independen. Pengatur daya aktif-frekwensi (P-f), dan pengatur daya reaktif-tegangan (Q-V) memakai frekwensi jaringan dan tegangan terminal untuk mengatur arus daya aktif dan arus daya reaktif. Pengatur daya aktif-frekwensi dapat dipakai untuk menyediakan daya pembantu inersia (inertial support) dan dapat dipakai mengatur droop dari pembangkit daya. Dua macam energy storage tersedia dari PowerStore buatan ABB: Flywheel dan Li-ion Battery.

Sebagai catatan, bahkan sebelum adanya PLTB di jaringan, banyak terjadi pemadaman seperti tercatat dalam laporan gangguan (yang disediakan oleh PLN) untuk tahun 2014, yang menunjukkan bahwa jumlah pemadaman dan pemadaman listrik sangatlah tinggi (sekitar satu per hari). Analisa awal menunjukkan alasan-alasan berikut: (1) Short circuit yang tidak dibetulkan dalam batas waktu yang sudah ditentukan pada jaringan pemutus, (2) Generator yang dijalankan mendekati kapasitas daya mampu (cadangan daya sangat rendah), (3) Kurangnya pemangkasan tumbuh tumbuhan yang dapat menyebabkan short circuit pada jalur penyulang, dan (4) banyaknya diesel generator terpasang yang sudah termasuk tua umurnya. Perbaikan terhadap (1) sampai (4) ditambah dengan pemasangan energy storage akan mengurangi jumlah pemadaman dan pemutusan listrik, sehingga dapat meningkatkan keandalan jaringan system daya,

Untuk analisa dinamis dengan energy storage anggapan berikut ini dipakai dalam analisa:

- 550kW CAT C32 diesel generator di Waingapu tersedia sebagai generator cadangan dilengkapi dengan saklar autostart. Satu atau beberapa generator semacam ini akan dibutuhkan.
- Adanya supervisory control yang memonitor gangguan, dan suatu daftar standar gangguan yang mungkin terjadi (parameter sistem), supervisory control ini akan mengirimkan sinyal autostart ke generator cadangan di atas.
- Generator cadangan memiliki kemampuan auto-start dalam 10 detik, yang berarti akan mampu untuk memulai, sinkronisasi dengan grid, dan memberikan daya penuh dalam waktu 10 detik.

Manfaat utama energy storage yang dianalisa dalam skenario ini adalah untuk memenuhi daya sementara antara terjadinya gangguan dan awal pembangkitan daya oleh generator cadangan.

Manfaat lainnya dari energy storage jangka pendek ini adalah untuk meratakan variabilitas daya angin dan meratakan beban pada generator diesel selama daya yang dibangkitkan oleh PLTB naik dan turun. Untuk 850kW PLTB di Sumba Timur, kelompok generator diesel yang sekarang terpasang (dengan inersia, AVR dan Governor model yang di simulasi) akan mampu mengatasi variabilitas kecepatan angin dan mencukupi kebutuhan naik turunnya kecepatan angin (ramping requirement seperti yang di berikan pada Appendix E- Figures 127-136). Namun, harus dicatat bahwa usia kebanyakan generator yang sekarang terpasang menunjukkan bahwa variabilitas tambahan diluar variasi daya beban yang normal akan membutuhkan pemeliharaan (terjadwal maupun tidak) yang lebih sering. Jadi, tambahan energy storage akan memperbaiki keandalan dan ketahanan sistim jaringan terhadap gangguan.

Tabel 15 berisi hasil studi stabilitas untuk berbagai skenario setelah penambahan energy storage. Analisa ini dilakukan oleh kantor konsultan ABB di Madrid, Spanyol. Laporan lengkap dilampirkan sebagai Lampiran F.

Untuk menentukan ukuran yang optimal dari energy storage, informasi berikut digunakan: (1) jumlah daya yang diperlukan untuk mengganti hilangnya daya jika terjadi gangguan besar dalam sistem dan putaran inersia yang tersedia dalam sistem, dan (2) waktu yang dibutuhkan sampai generator cadangan dapat masuk ke jaringan dan memenuhi kebutuhan daya. Ilustrasi berikut adalah untuk satu PLTB berdaya 850-kW. Proses yang sama dapat dilakukan untuk pemasangan dua PLTB masing-masing berdaya 850-kW.

1. Gangguan kritis yang dipakai dalam penelitian ini adalah hilangnya daya dari PLTB (850 kW). Daya cadangan yang harus disediakan dari generator untuk skenario beban tinggi dan rendah masing-masing adalah 597,8 kW dan 377,3 kW. Jadi, ada kekurangan daya sebesar 252,1 kW dan 472 kW di skenario beban tinggi dan beban rendah, yang harus disediakan oleh energy storage untuk menstabilkan sistem. Oleh karena itu, energy storage dengan kapasitas daya 500 kW yang dipilih.
2. Untuk menentukan berapa lama energy storage diperlukan untuk memenuhi kekurangan daya ini, waktu start-up dari generator cadangan perlu diperhitungkan. Sebagaimana ditunjukkan, generator cadangan dengan waktu start-up 10 detik dipilih dalam penelitian ini. Karena generator ini berusia 15 tahun, waktu start-up diperpanjang menjadi 30 detik, yang termasuk waktu untuk start-up, sinkronisasi, dan kenaikan daya sampai dengan kapasitas penuh. Kapasitas energi dari energy storage adalah

$$500 \text{ kW} \times (30/3600) \text{ jam} = 4.17 \text{ kWh}$$

Ukuran energy storage yang dibutuhkan untuk mengintegrasikan dua PLTB masing-masing berdaya 850 kW di bus Haharu di jaringan Sumba Timur dapat di perinci sebagai berikut:

1. Gangguan kritis yang dipakai dalam penelitian ini adalah hilangnya daya dari kedua PLTB (1700-kW). Berdasarkan daya cadangan yang harus disediakan oleh generator dan ukuran energy storage yang tersedia adalah 500kW/unit, total energy storage yang dipakai dalam penelistian ini adalah 1500-kW.

2. Untuk menentukan berapa lama energy storage diperlukan untuk memenuhi kekurangan daya ini, generator cadangan dengan waktu start-up 10 detik dibantu oleh generator cadangan yang lain dengan kemampuan start-up 60 detik. Berdasarkan situasi ini, energy storage harus memiliki energy untuk selama 60 detik:

$$1500 \text{ kW} \times (60/3600) \text{ jam} = 25 \text{ kWh}$$

Karena itu, energy storage dengan kapasitas daya dan energi dari 500 kW dan 4.17 kWh, dibutuhkan untuk kasus mengintegrasikan satu PLTB (850-kW) dan 1.500 kW dan 25 kWh, untuk kasus mengintegrasikan dua PLTB (masing-masing 850-kW). Pemilihan energy storage (flywheel atau baterai teknologi-lithium-ion [Li-ion], lead acid, atau kimia lainnya) dan spesifikasi rinci dan ukuran energy storage tidak termasuk dalam proyek ini. Daya penuh yang ditentukan diatas adalah persyaratan untuk energy storage; Namun, energy storage yang tersedia secara komersial antara 500 kW dan 1.500 kW akan memiliki kandungan energi (kWh) yang jauh lebih besar. Sebagai contoh, Beacon Flywheel 500 kW memiliki kandungan energi dari 50 kWh, sebuah SAFT IM20P Li-ion 500-kW baterai memiliki kandungan energi sekitar 160 kWh, Beacon Flywheel 1.500 kW memiliki kandungan energi dari 150 kWh, dan SAFT IM20P baterai Li-ion 1500-kW memiliki kandungan energi sekitar 500 kWh.

Figure 10. Power flow display: low load with WTGs and PowerStore. DOOSAN 5 = slack bus

Gambar-gambar yang disebut dalam table ini ada di Appendix F. Studi sistim dinamis dilakukan oleh ABB.

Table 15. Skenario and pengamatan untuk analisa dinamis dengan energy storage (ABB powerstore™).

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
Hilangnya pembangkitan daya dari Diesel Generator (650 kW)			
1	Angin Tinggi Beban Tinggi	Figure 4 (Appendix F)	Peralatan pendukung stabilitas membangkitkan daya (400 kW) selama 10 detik sampai generator CAT C32 mulai membangkitkan daya dan menstabilkan sistem. Frekuensi dan tegangan turun, tetapi stabil dan dalam batas normal. Untuk kasus ini, sistem stabil.
2	Angin Tinggi Beban Rendah	Figure 7 (Appendix F)	<p>Peralatan pendukung stabilitas membangkitkan daya (400 kW) selama 10 detik sampai generator CAT C32 mulai membangkitkan daya dan menstabilkan sistem. Frekuensi dan tegangan turun, tetapi stabil dan dalam batas normal. Untuk kasus ini, sistem stabil.</p> <p>Tanpa adanya peralatan pendukung stabilitas, sistim tidak bisa bertahan terhadap gangguan semacam ini karena frekuensi jaringan jatuh secara tajam sehingga PLTB juga terlepas dari jaringan dan tidak cukup waktu untuk menghubungkan generator cadangan ke jaringan.</p>
Hilangnya beban			
3	Angin Tinggi Beban Tinggi	Figure 5 (Appendix F)	Hilangnya beban terbesar (3.494 kW) dari jaringan disimulasikan, segera peralatan pendukung stabilitas menyerap daya (200 kW) untuk 10 detik dan menstabilkan sistem. Jadi sistemnya stabil untuk kasus ini. Penggunaan peralatan dukungan stabilitas bukanlah factor penentu stabilitas system dalam kasus ini karena generator yang lain dengan cepat menyesuaikan titik operasi nya untuk mengadaptasi situasi.
4	Angin Tinggi Beban Rendah	Figure 8 (Appendix F)	Hilangnya beban terbesar (1.691 kW) dari jaringan disimulasikan. Dengan segera peralatan pendukung stabilitas menyerap daya (330 kW) untuk 10 detik dan menstabilkan sistem. Jadi sistem stabil untuk kasus ini.

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
			Penggunaan peralatan pendukung stabilitas bukanlah factor penentu stabilitas system dalam kasus ini karena generator yang lain dengan cepat menyesuaikan titik operasi nya untuk mengadaptasi situasi.
Hilangnya pembangkitan daya PLTB (850 kW) dari jaringan (misalnya karena kecepatan angin menghilang)			
5	Angin Tinggi Beban Tinggi	Figure 6 (Appendix F)	Peralatan pendukung stabilitas daya (sebesar 400 kW) dapat memenuhi pembangkitan daya untuk 10 detik sampai generator cadangan memulai pembangkitan daya dan menstabilkan sistem. Tanpa menggunakan peralatan dukungan stabilitas daya, sistem ini tidak stabil karena frekuensi turun dengan tajam terutama jika generator cadangan tidak memiliki daya yang cukup untuk mengkompensasi hilangnya pembangkitan daya dan menstabilkan frekuensi sistem.
6	Angin Tinggi Beban Rendah	Figure 9 (Appendix F)	Peralatan pendukung stabilitas daya (500 kW) dapat menyediakan daya untuk 10 detik sampai generator cadangan mulai membangkitkan daya dan menstabilkan sistem. Tanpa menggunakan peralatan dukungan stabilitas, sistem ini tidak bisa stabil karena frekuensi turun dengan tajam sehingga generator cadangan tidak memiliki daya pembangkitan yang cukup untuk mengkompensasi hilangnya jaringan daya dan menstabilkan frekuensi sistem.
Variasi daya output dari PLTB			
7	Angin Tinggi Beban Tinggi	Figure E-127, E-128 and E-129	Variasi daya output dari PLTB menyebabkan output dari diesel genset ber variasi sebesar 5% untuk generator genset yang beroperasi pada daya mampu dan bervariasi 10% untuk generator yang beroperasi dibawah daya mampu. Perbedaan ini dipenuhi oleh energy storage. Frekwensi dan tegangan ber variasi dalam batasan normal. .
8	Angin Tinggi Beban Rendah	Figure E-130 and E-131	Variasi daya output dari PLTB menyebabkan output dari diesel genset ber variasi sebesar 2.5% (diesel genset ini beroperasi dengan

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
			daya mampu – tidak ada headroom lagi). Perbedaan ini dipenuhi oleh energy storage. Frekwensi dan tegangan ber variasi dalam batasan normal.
Turunnya daya secara perlahan (ramping down) output dari PLTB			
9	Angin Tinggi Beban Tinggi	Figure E-132, E-133 and E-134	Selama PLTB output menurun, Diesel genset yang mempunyai daya cadangan dan energy storage “Power Store” menaikkan daya secara bersamaan untuk menutup kekurangan daya.
10	Angin Tinggi Beban Rendah	Figure E-135 and E-136	Selama PLTB output menurun, Diesel genset yang mempunyai daya cadangan dan energy storage “Power Store” menaikkan daya secara bersamaan untuk menutup kekurangan daya. Sesudah 18 detik, diesel genset mencapai daya puncak, sesudah itu, Power Store memenuhi kekurangan daya.

Sistim dapat juga kehilangan stabilitas jika terjadi gangguan-gangguan berikut ini: short-circuit pada penyulang Kambajawa-Haharu tanpa upaya menghilangkan gangguan dari jaringan. Juga short-circuit pada penyulang antara Kambajawa-Waingapu dapat menyebabkan kehilangan stabilitas jaringan. Jika gangguan tidak dihilangkan dalam waktu 180 mili-detik, sistim akan kehilangan sinkronisme. Untuk mengatasi hal ini, relay sistim pengaman harus di program untuk mengisolasi gangguan supaya tidak menyebar.

3.6 Skenario Untuk Mengintegrasikan Dua PLTB (Masing-masing Berdaya 850-kW)

Gambar gambar yang tercantum dalam Tabel H-16 ada di dalam Appendix G. Angka-angka yang tercantum dalam grafik-grafik di rincikan dibawah ini.

Table 1. Skenario and pengamatan untuk analisa dinamis Analisa Dampak Sistim untuk mengintegrasikan dua PLTB

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
Gangguan tiga fasa ketanah di bus Kambajawa. Gangguan terjadi pada 1 detik dan dihilangkan pada 1.18 detik.			
1	Angin Tinggi Beban Tinggi	Figure G-1, G-2 and G-3	Sistim stabil. Pembebanan penyulang ada dalam batasan normal. LVRT (low voltage ride through – ketahanan menghadapi tegangan rendah) dari PLTB menghindarkan PLTB terlepas dari jaringan. PLTB kembali normal segera sesudah gangguan dihilangkan.
2	Angin Tinggi Beban Rendah	Figure G-4 and G-5	Sistim stabil. Pembebanan penyulang ada dalam batasan normal. LVRT (low voltage ride through – ketahanan menghadapi tegangan rendah) dari PLTB menghindarkan PLTB terlepas dari jaringan. PLTB kembali normal segera sesudah gangguan dihilangkan.
3	Angin Tinggi Beban Tinggi dengan Energy Storage	Figure G-6 and G-7	Sistim stabil. Pembebanan penyulang ada dalam batasan normal. Tegangan di terminal dan daya output dari generator semuanya stabil Energy storage memenuhi daya selama gangguan.
4	Angin Tinggi Beban Rendah dengan Energy Storage	Figure G-8 and G-9	Sistim stabil. Pembebanan penyulang ada dalam batasan normal. Tegangan pada bus jatuh dibawah 0.50 p.u. di bus H dan W. Energy storage memenuhi daya selama gangguan ketika PLTB down.
Gangguan tiga fasa ketanah di bus Waingapu. Gangguan terjadi pada 1 detik dan dihilangkan pada 1.18 detik.			
5	Angin Tinggi Beban Tinggi	Figure G-10, G-11 and G-12	Sistim stabil. Pembebanan penyulang ada dalam batasan normal. LVRT (low voltage ride through – ketahanan menghadapi tegangan rendah) dari PLTB menghindarkan PLTB terlepas dari jaringan. PLTB kembali normal segera sesudah gangguan dihilangkan.

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
6	Angin Tinggi Beban Rendah	Figure G-13 and G-14	Sistim stabil. Pembebanan penyulang ada dalam batasan normal. LVRT (low voltage ride through – ketahanan menghadapi tegangan rendah) dari PLTB menghindarkan PLTB terlepas dari jaringan. PLTB kembali normal segera sesudah gangguan dihilangkan.
7	Angin Tinggi Beban Tinggi dengan Energy Storage	Figure G-15 and G-16	Sistim stabil. Pembebanan penyulang ada dalam batasan normal. Tegangan di terminal dan daya output dari generator semuanya stabil Energy storage memenuhi daya selama gangguan.
8	Angin Tinggi Beban Rendah dengan Energy Storage	Figure G-17 and G-18	Sistim stabil. Pembebanan penyulang ada dalam batasan normal. Tegangan pada bus jatuh dibawah 0.50 p.u. di bus H dan W. Energy storage memenuhi daya selama gangguan ketika PLTB down.
Gangguan pada kedua PLTB. Gangguan terjadi pada 1 detik, dan tidak dihilangkan.			
9	Angin Tinggi Beban Tinggi	Figure G-19, G-20 and G-21	Frekwensi terus menurun sesudah gangguan, dan terjadi kehilangan sinkronisasi. Ini memang diharapkan, karena hilangnya daya dari dua PLTB masing masing berdaya 850-kW tanpa adanya pengganti merupakan kehilangan daya yang besar dari jaringan. Sehingga jaringan daya tidak bisa kembali normal.
10	Angin Tinggi Beban Rendah	Figure G-22 and G-23	Frekwensi terus menurun sesudah gangguan, dan terjadi kehilangan sinkronisasi. Ini memang diharapkan, karena hilangnya daya dari dua PLTB masing masing berdaya 850-kW tanpa adanya pengganti merupakan kehilangan daya yang besar dari jaringan. Sehingga jaringan daya tidak bisa kembali normal.

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
11	Angin Tinggi Beban Tinggi dengan Energy Storage	Figure G-24 and G-25	<p>Energy storage memenuhi daya ketika kedua PLTB (masing masing berdaya 850-kW) terlepas dari jaringan. Energy storage memenuhi daya sebesar 1.5MW sampai generator yang ditentukan CAT C32 mulai menghasilkan daya sebesar 0.55MW pada 10 detik. Hal ini mengurangi kontribusi dari Energy storage ke 0.95MW.</p> <p>Sesudah 30 detik, ketika energy dalam storage sudah habis, terjadi penurunan frekuensi yang tak terkendalikan karena hilangnya daya yang besar dari jaringan daya.</p> <p>Untuk menghindari penurunan frekwensi tak terkendalikan, perlu ditambahkan dua unit generator cadangan CAT C32 ber kapasitas 0.55MW dengan kemampuan start-up 10 detik, Atau, pemutusan beban terencana (load shedding) harus di rencanakan jika hal ini terjadi.</p>
12	Angin Tinggi Beban Rendah dengan Energy Storage	Figure G-26 and G-27	<p>Energy storage memenuhi daya ketika kedua PLTB (masing masing berdaya 850-kW) terlepas dari jaringan. Energy storage memenuhi daya sebesar 1.8MW sampai generator yang ditentukan CAT C32 mulai menghasilkan daya sebesar 0.55-MW pada 10 detik. Hal ini mengurangi kontribusi dari Energy storage ke 1.2MW.</p> <p>Sesudah 30 detik, ketika energy dalam storage sudah habis, terjadi penurunan frekuensi yang tak terkendalikan karena hilangnya daya yang besar dari jaringan daya.</p> <p>Untuk menghindari penurunan frekwensi tak terkendalikan, perlu ditambahkan dua unit generator cadangan CAT C32 ber kapasitas 0.55MW dengan kemampuan start-up 10 detik, Atau, pemutusan beban terencana (load shedding) harus di rencanakan jika hal ini terjadi.</p>
Gangguan pada generator di bus Kambajawa. Gangguan terjadi pada 1 detik, dan tidak dihilangkan.			

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
13	Angin Tinggi Beban Tinggi	Figure G-28, G-29 and G-30	Frekwensi menurun tak terkendalikan karena hilangnya daya sebesar 650kW dari generator. Tidak cukup daya cadangan dari generator lainnya untuk mengganti kehilangan daya ini. Karena hal ini, frekwensi turun selama 10 detik sampai rendah sekali sehingga PLTB terlepas (under frequency relay protection) dari jaringan. Hal ini menyebabkan hilangnya daya total sebesar 2.35 MW dari sistim jaringan. Sehnigga ketika generator CAT C32 mulai memasok daya pada 10 detik, generatornya tidak bisa sinkron, dan seluruh sisim jaringan terlepas dari sinkronisasi.
14	Angin Tinggi Beban Rendah	Figure G-31 and G-32	Frekwensi menurun tak terkendalikan karena hilangnya daya sebesar 420kW dari generator. Tidak cukup daya cadangan dari generator lainnya untuk mengganti kehilangan daya ini. Karena hal ini, frekwensi turun selama 10 detik sampai rendah sekali sehingga PLTB terlepas (under frequency relay protection) dari jaringan. Hal ini menyebabkan hilangnya daya total sebesar 2.35 MW dari sistim jaringan. Sehnigga ketika generator CAT C32 mulai memasok daya pada 10 detik, generatornya tidak bisa sinkron, dan seluruh sisim jaringan terlepas dari sinkronisasi.
15	Angin Tinggi Beban Tinggi dengan Energy Storage	Figure G-33 and G-34	Pada saat gangguan, energy storage segera menenuhi daya sebesar 600kW. Hal ini menyebabkan sistim stabil sampai generator cadangan, CAT C32, mulai memasok daya pada 10 detik. Pada 30 detik, ketika energy storage down, sistim nya tetap stabil.
16	Angin Tinggi Beban Rendah dengan Energy Storage	Figure G-35 and G-36	Pada saat gangguan, energy storage segera menenuhi daya sebesar 500kW. Hal ini menyebabkan sistim stabil sampai generator cadangan, CAT C32, mulai memasok daya pada 10 detik. Ada cukup banyak daya tersedia dari generator yang ada untuk mengganti daya yang hilang dari jaringan.
Hilangnya beban di bus Kambajawa. Gangguan terjadi pada 1 detik, dan beban tidak disambung kembali.			

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
17	Angin Tinggi Beban Tinggi	Figure G-37, G-38 and G-39	Beban sebesar 3.494MW terlepas dari jaringan pada 1 detik di bus Kambajawa. Frekwensi di bus meningkat sampai 1.04 p.u., dan tegangan bus meningkat sebanyak 0.02 p.u., tetapi secara keseluruhan sistim stabil. Seperti yang tergambar, generator mengurangi daya nya sebesar 60%-70% dari daya awal. Dalam prakteknya, beberapa diesel genset akan dilepas dari jaringan untuk mengatur stabilitas.
18	Angin Tinggi Beban Rendah	Figure G-40 and G-41	Beban sebesar 1.691MW terlepas dari jaringan pada 1 detik di bus Kambajawa. Frekwensi dan tegangan di bus meningkat sedikit, tetapi secara keseluruhan sistim stabil. Seperti yang tergambar, generator mengurangi daya nya sampai negative. Dalam prakteknya, satu atau beberapa diesel genset akan dilepas dari jaringan untuk mengatur stabilitas.
19	Angin Tinggi Beban Tinggi dengan Energy Storage	Figure G-42 and G-43	Beban sebesar 3.494MW terlepas dari jaringan pada 1 detik di bus Kambajawa. Frekwensi di bus meningkat sampai 1.04 p.u., tetapi secara keseluruhan sistim stabil. Karena adanya Energy Storage dalam jaringan, terlihat energy storage mulai menyerap daya pada 1 detik. Seperti yang tergambar, generator mengurangi daya nya sebesar 60%-70% dari daya awal sampai energy storage dilepas pada 30 detik. Dalam prakteknya, beberapa diesel genset akan dilepas dari jaringan untuk mengatur stabilitas.
20	Angin Tinggi Beban Rendah dengan Energy Storage	Figure G-44 and G-45	Beban sebesar 1.691 MW terlepas dari jaringan pada 1 detik di bus Kambajawa. Frekwensi di bus meningkat sampai 1.04 p.u., dan tegangan bus meningkat sedikit, tetapi secara keseluruhan sistim stabil. Energy storage mulai menyerap daya pada 1 detik. Dalam prakteknya, satu atau beberapa diesel genset akan dilepas dari jaringan untuk mengatur stabilitas.
Gangguan pada penyulang Kambajawa-Haharu. pada 1.18 detik			Gangguan terjadi pada 1 detik dan dihilangkan
21	Angin Tinggi Beban Tinggi	Figure G-46, G-47 and G-48	Terjadi islanding di bus Haharu (bus Haharu terisolasi). Beban di Haharu Iterlepas dari jaringan selama 180 ms. Setelah gangguan dihilangkan, sistim stabil = pembebanan penyulang, tegangan dan frekwensi kembali normal.

Kasus #	Tipe dari Gangguan	Tampilan #	Pengamatan
22	Angin Tinggi Beban Rendah	Figure G-49 and G-50	Terjadi islanding di bus Haharu (bus Haharu terisolasi). Beban di Haharu lterlepas dari jaringan selama 180 ms. Sesudah gangguan dihilangkan, sistim stabil = pembebanan penyulang, tegangan dan frekwensi kembali normal.
23	Angin Tinggi Beban Tinggi dengan Energy Storage	Figure G-51 and G-52	Terjadi islanding di bus Haharu (bus Haharu terisolasi). Beban di Haharu lterlepas dari jaringan selama 180 ms. Sesudah gangguan dihilangkan, sistim stabil = pembebanan penyulang, tegangan dan frekwensi kembali normal. Energy storage memenuhi daya selama PLTB mulai normal setelah LVRT.
24	Angin Tinggi Beban Rendah dengan Energy Storage	Figure G-53 and G-54	Terjadi islanding di bus Haharu (bus Haharu terisolasi). Beban di Haharu lterlepas dari jaringan selama 180 ms. Sesudah gangguan dihilangkan, sistim stabil = pembebanan penyulang, tegangan dan frekwensi kembali normal. Energy storage memenuhi daya selama PLTB mulai normal setelah LVRT.

4 Kesimpulan

Jaringan Sumba Timur telah dianalisa untuk aliran daya, short circuit, dan analisa transien.

Analisa aliran daya menunjukkan bahwa analisa dasar dan dalam analisa dengan satu PLTB, tidak ada overloading dari generator, tidak ada overloading dari konduktor, dan semua tegangan bus berada dalam batas normal.

Analisis short circuit menunjukkan bahwa short-circuit power ratio ada dalam batasan normal di atas persyaratan minimum untuk bus Haharu – titik pertemuan penyulang untuk PLTB. Selain itu, karena kontribusi arus short circuit dari PLTB sangatlah kecil, kapasitas daya perangkat di gardu listrik tidak terdampak.

Studi stabilitas transien dilakukan untuk menganalisa dampak dari pengadaan satu 850-kW WTG menunjukkan adanya masalah stabilitas. Penambahan energy storage pada jaringan listrik, ditambah dengan generator cadangan, controller hybrid, dan komunikasi berkecepatan tinggi dalam jaringan akan menjamin stabilitas sistem. Energy storage berkapasitas setidaknya 500 kW kapasitas dan 4,17 kWh energi akan cukup untuk memastikan stabilitas jaringan daya. Disamping penambahan storage, diesel genset, CAT C32, dengan kapasitas 550 kW dengan kemampuan start-up dalam 10 detik harus dipakai sebagai generator cadangan. Ini semua harus dikontrol oleh controller hybrid yang dapat semua diesel genset, PLTB, dan energy storage berdasarkan data-data jaringan, output dari PLTB, kondisi tenaga (state of charge) energy storage, dan faktor lainnya. Ini juga akan membutuhkan komunikasi kecepatan tinggi antara controller hybrid dan semua unit peringkat yang dikontrol yang ada pada jaringan.

Kesimpulannya, bahwa penambahan satu PLTD berdaya 850kW di Sumba Timur dengan energy storage berkapasitas 500kW (dengan setidaknya 4.17kWh), 550kW genset diesel cadangan dengan kemampuan 10 detik start-up, pengendali pembangkit listrik hybrid controller, dan komunikasi kecepatan tinggi dalam jaringan adalah solusi yang akan meningkatkan keandalan pasokan energi, meningkatkan stabilitas sistem dan mengurangi emisi greenhouse gas.

Untuk penambahan dua PLTB yang masing-masing berkapasitas 850-kW akan membutuhkan penambahan energy storage sebesar 1.500 kW, (sedikit di bawah kapasitas total dua PLTB). Energy storage ini dirancang untuk menyediakan tenaga listrik selama 60 detik, waktu yang cukup untuk start-up diesel genset cadangan. Selain energy storage, satu CAT C32 diesel genset generator dengan kapasitas 550 kW dan kemampuan start-up dalam waktu 10 detik dan generator lainnya dengan total kapasitas 950 kW dengan kemampuan start-up 60-detik harus dipakai sebagai generator cadangan. Perhatikan bahwa peningkatan daya PLTB dari 850 kW ke 1.700 kW menyebabkan penambahan yang cukup besar untuk pengadaan energy storage dan generator cadangan, dan akan memakan biaya yang cukup tinggi untuk memperkuat jaringan daya (storage, generator cadangan, dan hybrid controller). Disarankan bahwa sebagai langkah pertama hanya satu PLTB berkapasitas 850-kW diintegrasikan ke jaringan. Setelah semua masalah pemasangan diselesaikan, data-data baru harus dikumpulkan berdasarkan penambahan satu PLTB, dan analisa jaringan teknis untuk penambahan skenario dua turbin harus dijalankan lagi. Pilihan-pilihan lain seperti penempatan dua PLTB di kawasan yang sama atau memilih lokasi yang berbeda antara kedua PLTB harus dievaluasi lagi. Data data baru dan pengalaman

yang diperoleh dari integrasi PLTB pertama akan membuat analisa dampak pada jaringan untuk PLTB yang berikutnya akan lebih tepat dan teliti.

5 Referensi

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