

# Pyrgometer Calibration for DOE-Atmospheric System Research program using NREL Method



**Science Team Meeting**

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# Overview to address some ECR comments

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Thermocouple/thermopile

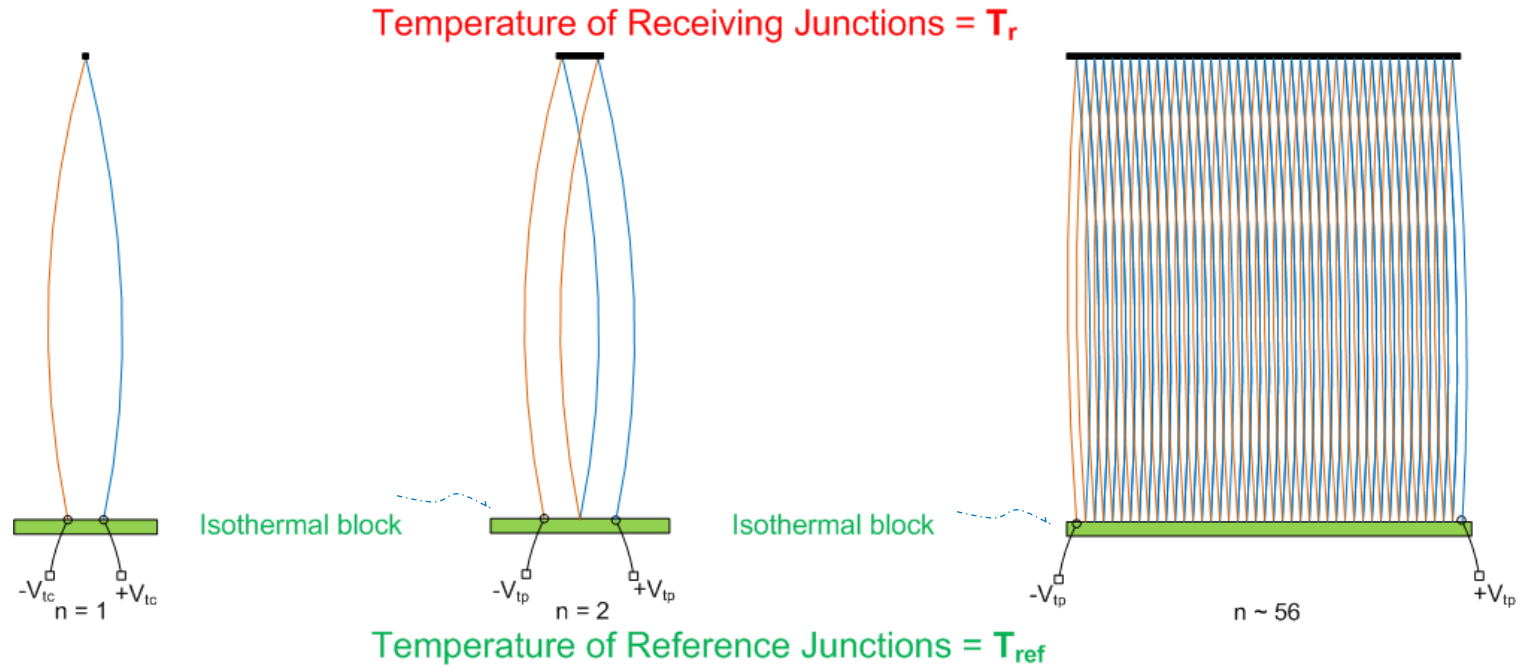
Pyrgeometer thermodynamics

NREL & PMOD equations

NREL calibration method

Conclusion.

# Effect of increased junctions on thermopile



$$V_{tp} = n \cdot s \cdot e (T_r - T_{ref})$$

where,

$n$  = number of junctions

$s$  = Seebeck coefficient

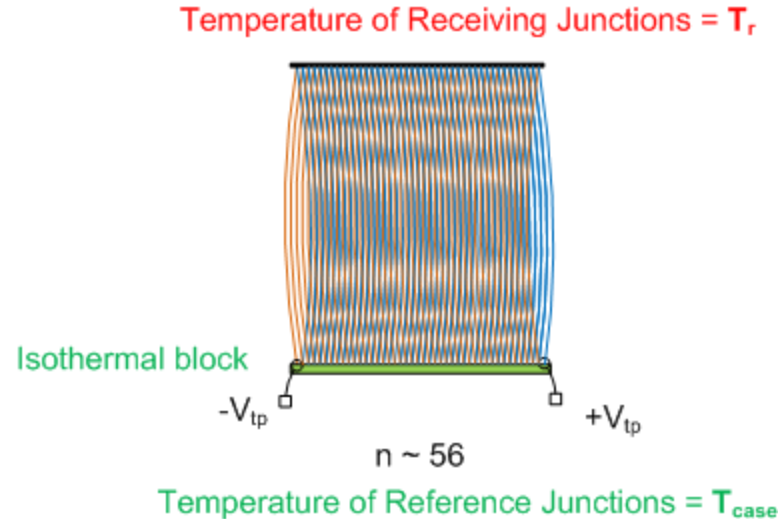
$e$  = thermopile efficiency.  $e=1$  for  $n = 1, 2$ , or small number

$n \uparrow$  to increase signal/noise ratio, thermal conductivity between receiving&reference junctions  $\uparrow$ ,  $T_{ref}$  effect on  $T_r \uparrow$ , therefore  $e \neq 1$

If  $n$  is not optimum  $\rightarrow V_{tp} \downarrow$ ,  $n$  too large  $V_{tp} \sim$  zero volt

# Effect of increased thermal conductivity on PIRs

Not to scale



$$V_{tp} = n \cdot s \cdot e (T_r - T_{case})$$

where  $e = 0.65$  for PIRs, measured by John Hickey for PIRs with  $n \sim 56$  junctions and Seebeck coefficient  $\sim 39 \mu\text{V/K}$ , reported in:

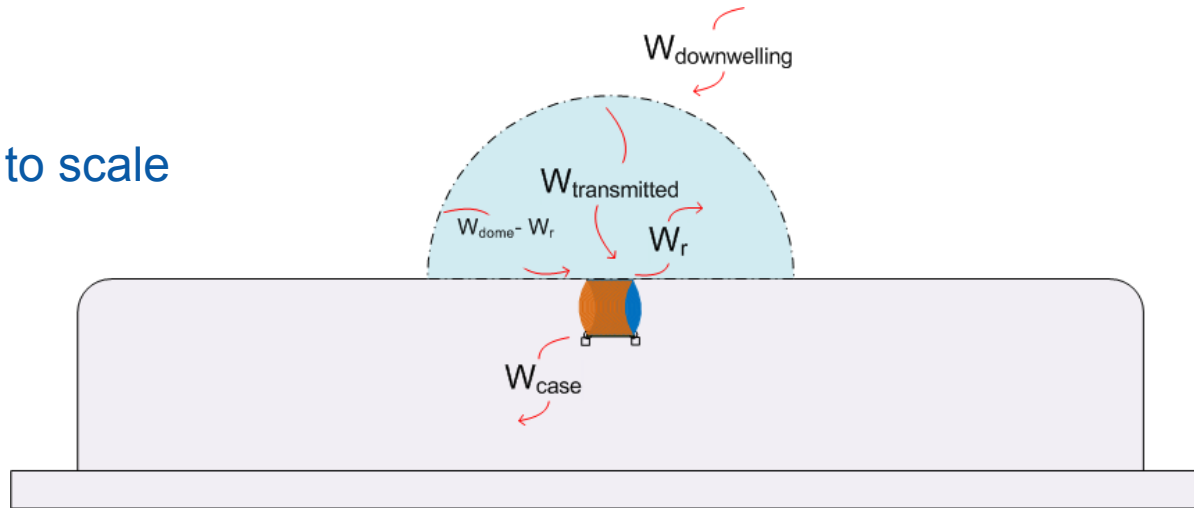
Reda et al., (2002). [Pyrgometer Calibration at the National Renewable Energy Laboratory \(NREL\)](#). Journal of Atmospheric and Solar-Terrestrial Physics. Vol. 64(15), 2002; pp. 1623-1629.

therefore,

$$T_r = T_{case} + 0.0007044 V_{tp}$$

# Simplified pyrgemeter thermodynamics

Not to scale



- Net Irradiance =  $W_{\text{net}} = K_1 \cdot V_{\text{tp}}$   
 $= W_{\text{incoming}} - W_{\text{outgoing}} = W_{\text{transmitted}} + K_3 \cdot (W_{\text{dome}} - W_r) - K_2 \cdot W_r$   
 where  $W_{\text{transmitted}} = \tau \cdot W_{\text{downwelling}}$ , and  $\tau = \text{Dome+Filter transmittance}$  .. assumed to be constant

Other equations are based on assumptions:  $e = 1$  and  $W_{\text{outgoing}} = W_{\text{case}}$  instead of  $W_r$  !?!

- Arrange the above equation and Re-name constants, therefore,

$$W_{\text{downwelling}} = K_1 \cdot V_{\text{tp}} + K_2 \cdot W_r - K_3 \cdot (W_{\text{dome}} - W_r)$$

This is NREL's equation without  $K_0$ , Reda et al., (2002). *Pyrgemeter Calibration at the National Renewable Energy Laboratory (NREL)*. Journal of Atmospheric and Solar-Terrestrial Physics. Vol. 64(15), 2002; pp. 1623-1629.

$K_0$  is reserved for troubleshooting regressions & blackbody calibrations only

# Comparing NREL and PMOD equations

## NREL Equation:

$$W_{\text{downwelling}} = K_1 \cdot V_{\text{tp}} + K_2 \cdot W_r - K_3 (W_{\text{dome}} - W_r)$$

## Expansion of NREL Equation to compare with PMOD equation:

1.  $T_r = T_{\text{case}} + 0.0007044 V_{\text{tp}} \dots$  for PIRs

2.  $W_{\text{downwelling}} = K_1 \cdot V_{\text{tp}} + K_2 \cdot \sigma (T_{\text{case}} + 0.0007044 V_{\text{tp}})^4 - K_3 [W_{\text{dome}} - \sigma (T_{\text{case}} + 0.0007044 V_{\text{tp}})^4]$   
Expand  $(T_{\text{case}} + 0.0007044 V_{\text{tp}})^4$  using  $(a + b)^4 = a^4 + 4a^3b + 6a^2b^2 + 4ab^3 + b^4$

3. Arrange terms and re-name coefficients,

$$W_{\text{downwelling}} = K_1 \cdot V_{\text{tp}} + k'_1 \cdot T_{\text{case}}^3 \cdot V_{\text{tp}} + k_2 \cdot W_{\text{case}} - k_3 (W_{\text{dome}} - W_{\text{case}}) + k_4 \cdot T_{\text{case}}^2 \cdot V_{\text{tp}}^2 + k_5 \cdot T_{\text{case}} \cdot V_{\text{tp}}^3 + k_6 \cdot V_{\text{tp}}^4$$

## PMOD Equation:

$$W_{\text{downwelling}} = V_{\text{tp}} (1 + k_1 \cdot \sigma \cdot T_{\text{case}}^3) / c + k_2 \cdot W_{\text{case}} - k_3 (W_{\text{dome}} - W_{\text{case}}) \\ = K_1 \cdot V_{\text{tp}} + k'_1 \cdot T_{\text{case}}^3 \cdot V_{\text{tp}} + k_2 \cdot W_{\text{case}} - k_3 (W_{\text{dome}} - W_{\text{case}})$$

**! PMOD equation = NREL equation without  $k_4$ ,  $k_5$ , and  $k_6$  terms !**

From many comparisons,  $U_{g5}$  using NREL or PMOD equation = (1 to 3)  $W/m^2$  w.r.t. WISG

# NREL Calibration Procedure

Procedure is developed after many comparisons/validations with PMOD/NOAA  
Calibration is performed outdoor using a group of reference pyrgeometers with traceability to consensus reference, WISG

Recommended Measurement Equation:

$$W_{\text{downwelling}} = K_1 \cdot V_{\text{tp}} + K_2 \cdot W_r - K_3(W_{\text{dome}} - W_r)$$

Process:

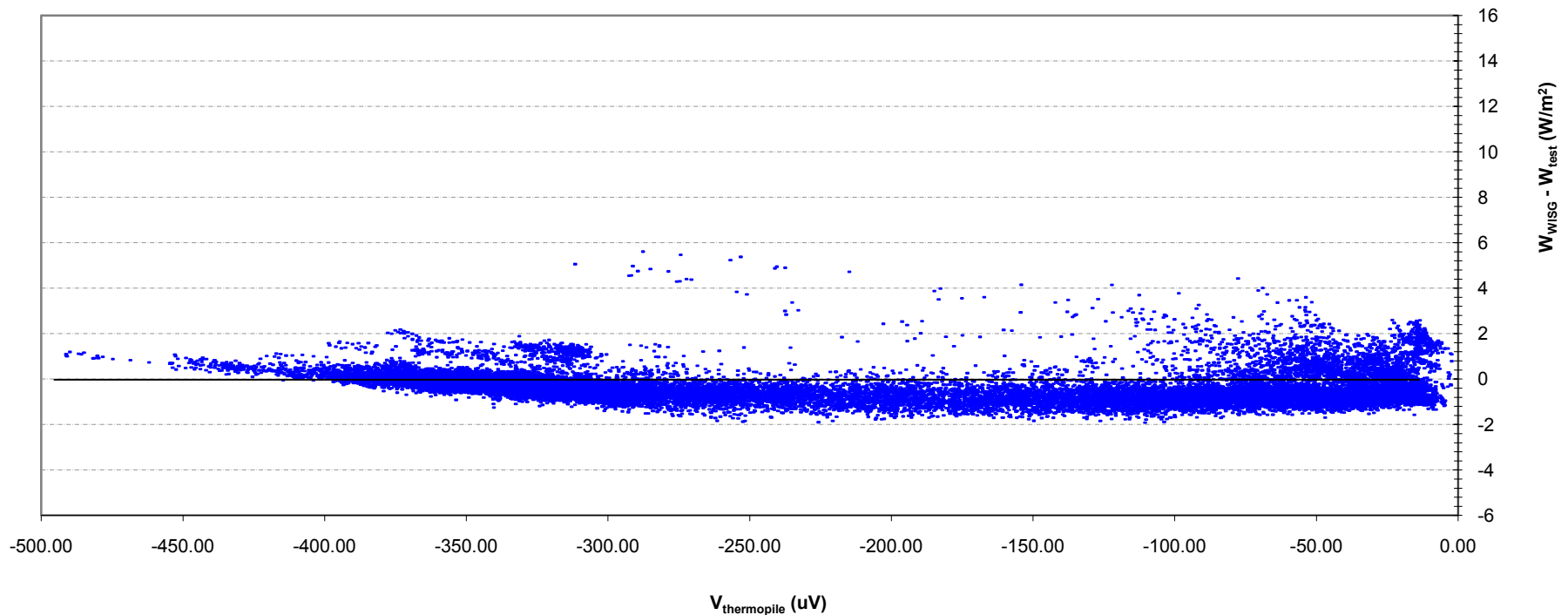
1.  $V$  = minimum negative magnitude (Cloudy sky), adjust  $K_2$  to minimize the difference between pyrgeometer under test (PUT) irradiance and reference irradiance
2.  $V$  = maximum negative magnitude (Clear sky), adjust  $K_1$  to minimize the difference between the PUT irradiance and reference irradiance
3. Adjust  $K_3$  to minimize the scatter of the differences between PUT irradiance and reference irradiance.

Future software development might include/evaluate regression, with uniform sets of data!!, to calculate the calibration coefficients

# NREL Calibration Method Validation

At least 40 pyrgeometers were calibrated using NREL method with uncertainty  $U_{95} < 3 \text{ W/m}^2$  with respect to WISG, for all sky conditions, e.g.

Difference between the reference irradiance and the irradiance measured by 31197F3 using NREL method/equation





# Conclusions

NREL method achieves uncertainty of  $< 3 \text{ W/m}^2$  for all sky conditions

NREL equation accounts for the pyrgeometer thermodynamics

Since  $T_r = T_{\text{case}} + 0.0007044 V_{\text{tp}}$ , and response time of thermopile is faster than case temperature response, therefore, NREL equation reduces response time of measuring  $W_{\text{downwelling}}$  .... needed for fast changes in sky conditions

At present, with the instruments/data-acquisition limitations, all equations might achieve  $U_{95} = (1 \text{ to } 3) \text{ W/m}^2$  w.r.t. WISG

In the future, when  $U_{95}$  of measuring instruments and consensus reference is reduced, NREL equation might be a good candidate when uncertainty of fractions of  $\text{W/m}^2$  is needed

Manufacturers specifications to include thermopile efficiency,  $e$ , for accurate  $K_2$  and  $K_3$  derivation.