

Impact of the 3Cs of Batteries on PHEV Value Proposition: Cost, Calendar Life, and Cycle Life

**The 9th Advanced Automotive Battery Conference
Long Beach, California
June 10-12, 2009**

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NREL/PR-540-45887

Funded by Energy Storage R&D (David Howell)
Vehicle Technologies Program
U.S. Department of Energy

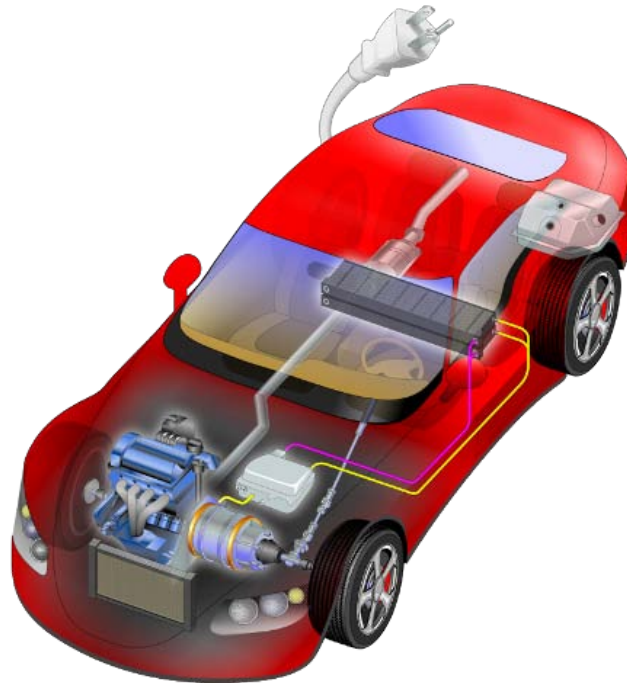


Overview

- Introduction and background
- Motivation for PHEV battery trade-off analysis
- Battery calendar and cycle life models
- Battery cost model
- Battery life/cost trade-off results
- Impact of temperature on battery life and cost
- Summary

Introduction

- PHEVs have the potential to significantly reduce (imported) petroleum consumption (and GHG emissions) by improving efficiency and use of electricity
- Capacity, c-rate, cost, cycle life, and calendar life are all critical in making batteries for PHEVs commercially viable
- Incremental cost of the long-lasting batteries could be offset with government incentives and high petroleum prices



Introduction

- PHEVs have the potential to significantly reduce (imported) petroleum consumption (and GHG emissions) by improving efficiency and use of electricity
- Capacity, c-rate, cost, cycle life, and calendar life are all critical in making batteries for PHEVs commercially viable
- Incremental cost of the long-lasting batteries could be offset with government incentives and high petroleum prices
- Cost, calendar life, and cycle life are the least known and have the biggest impact on PHEV value proposition
- Cost, fuel savings, and battery degradation characteristics at beginning of life vs. end of life must be evaluated
- The spectrum of battery degradation rates due to both cycle life and calendar life in various climates and operating states of charge (SOCs) are needed
- NREL has been studying trade-offs between the performance, life, and cost of batteries



Major Battery Requirements (5Cs)



Requirements of End of Life Energy Storage Systems for PHEVs

Characteristics at EOL (End of Life)		High Power/Energy Ratio Battery	High Energy/Power Ratio Battery
Reference Equivalent Electric Range	miles	10	40
Peak Pulse Discharge Power - 2 Sec / 10 Sec	kW	50 / 45	46 / 38
Peak Regen Pulse Power (10 sec)	kW	30	25
Available Energy for CD (Charge Depleting) Mode, 10 kW Rate	kWh	3.4	11.6
Available Energy for CS (Charge Sustaining) Mode	kWh	0.5	0.3
Minimum Round-trip Energy Efficiency (USABC HEV Cycle)	%	90	90
Cold cranking power at -30°C, 2 sec - 3 Pulses	kW	7	7
CD Life / Discharge Throughput	Cycles/MWh	5,000 / 17	5,000 / 58
CS HEV Cycle Life, 50 Wh Profile	Cycles	300,000	300,000
Calendar Life, 35°C	year	15	15
Maximum System Weight	kg	60	120
Maximum System Volume	Liter	40	80
Maximum Operating Voltage	Vdc	400	400
Minimum Operating Voltage	Vdc	>0.55 x Vmax	>0.55 x Vmax
Maximum Self-discharge	Wh/day	50	50
System Recharge Rate at 30°C	kW	1.4 (120V/15A)	1.4 (120V/15A)
Unassisted Operating & Charging Temperature Range	°C	-30 to +52	-30 to +52
Survival Temperature Range	°C	-46 to +66	-46 to +66
Maximum System Production Price @ 100k units/yr	\$	\$1,700	\$3,400



Major Battery Requirements (5Cs)



Requirements of End of Life Energy Storage Systems for PHEVs

		Low Energy/Power Ratio Battery	High Energy/Power Ratio Battery
Peak Power Discharge (2S/10S) = 46/38 kW C-rate ~ 10-15 kW			
Peak Pulse Discharge Power (2 sec / 10 sec)	kW	50 / 45	46 / 38
Peak Regen Pulse Power (10 sec)	kW	30	25
Available Energy (ΔSOC = 70%) Capacity (EOL) = 16.6 kWh	kWh	3.4	11.6
Minimum Capacity	kWh	0.5	0.3
Cold cranking power at -30°C, 2 sec - 3 Pulses	kW	7	7
Cycle Life / Discharge Throughput	Cycles/MWh	5,000 / 17	5,000 / 58
Cycle Life (depleting) = 3K-5K cycles Cycle Life (sustaining) = 200K-300K cycles		500,000	300,000
Calendar Life at 35°C = 15 Years		15	15
Maximum System Volume	Liter	60	120
Maximum Operating Voltage	V	40	80
Minimum Operating Voltage	V	400	400
Maximum Self-Discharge	%/yr	>0.55 x Vmax	>0.55 x Vmax
System Recharge Rate at 30°C	kW	50	50
Unassisted Operating & Charging Temperature Range	°C	1.4 (120V/15A)	1.4 (120V/15A)
Survival Temperature Range	°C	-30 to +52	-30 to +52
Maximum System Production Price @ 100k units/yr	\$	66	-46 to +66
		Cost (system) = \$3,400	
		\$1,700	\$3,400

The Three Important Cs of Batteries

- Cost
- Cycle Life
- Calendar Life

These three attributes vary significantly from supplier to supplier, are not consistently reported, and dramatically affect the market potential of PHEVs and EVs.

C³ Data Is Critical to Many Analysis Efforts

Performance
Modeling

Vehicle
Systems
Simulation

Cost

Cycle
Life

Calendar
Life

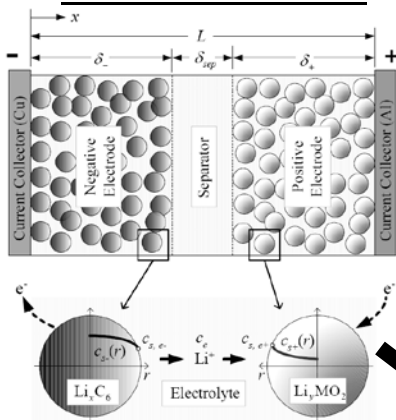
Linkage
with
Renewables

Economic Analysis
& Value Proposition

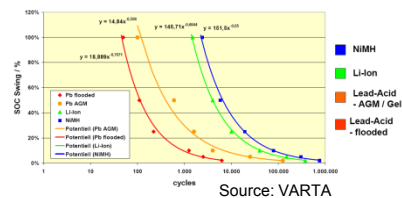
PHEV Battery Design Optimization

Design/size PHEV batteries to meet USABC technical goals/requirements at minimum cost.

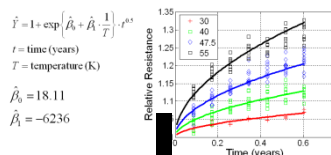
Capacity and C-rate Performance



Cycle Life, Calendar Life

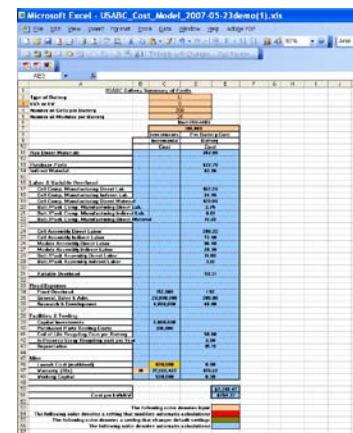


Source: VARTA

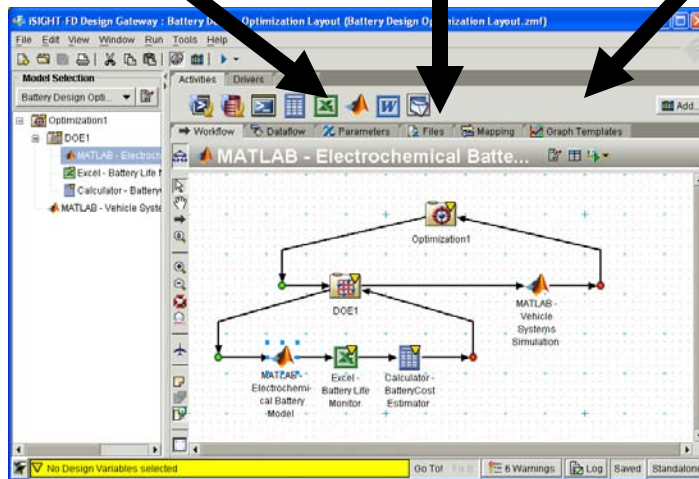


Source: ANL, INL, LBNL, SNL

Cost



Optimization with vehicle simulations under realistic driving cycles and environments



Life prediction represents greatest uncertainty

Complex dependency on $t^{1/2}$, t , # cycles, T , V , ΔDOD

Motivation: Minimize Battery Cost, Maximize Life

How?

- 0) Select a high-quality, low-cost cell
- 1) Size battery appropriately so as not to overstress/overcycle, but with minimum cost and mass**
 - 1) Accelerated calendar and cycle life testing
 - 2) Accurate life and DOD predictive models
- 2) Minimize time spent at high temperatures**
 - 1) Standby thermal management (vehicle parked!)
 - 2) Active thermal management (vehicle being driven)
- 3) Use proper electrical management, control design

Component
design/
selection

**System
design**



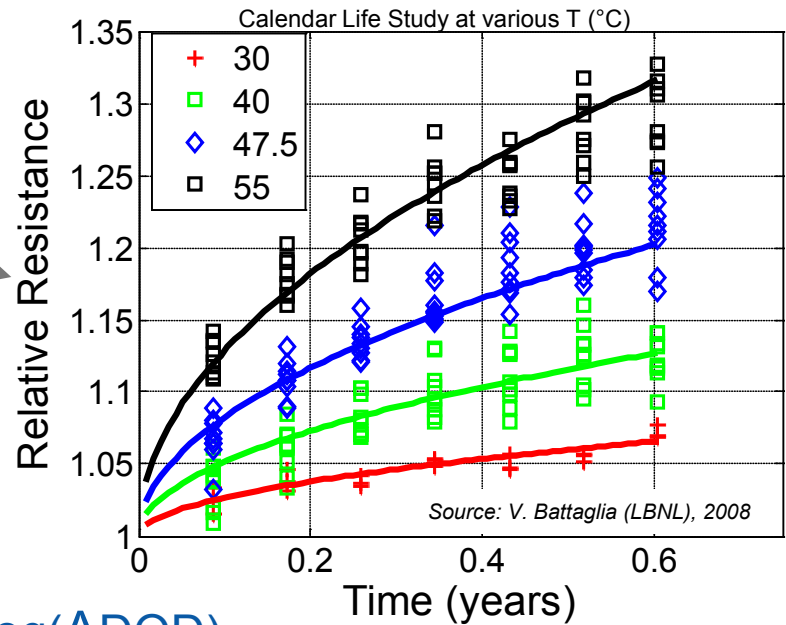
Overview

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Modeling to Predict Battery Life

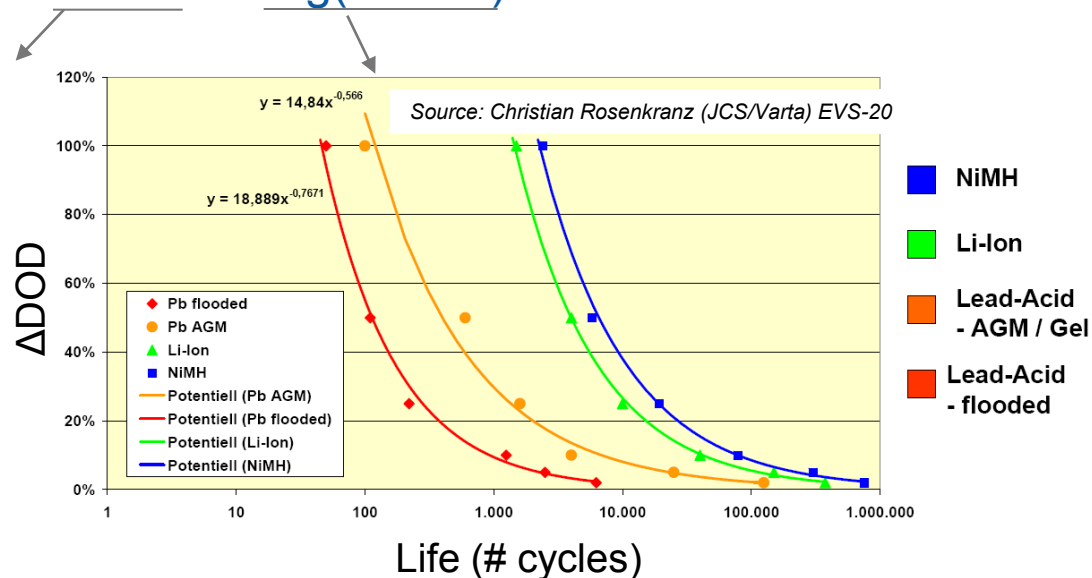
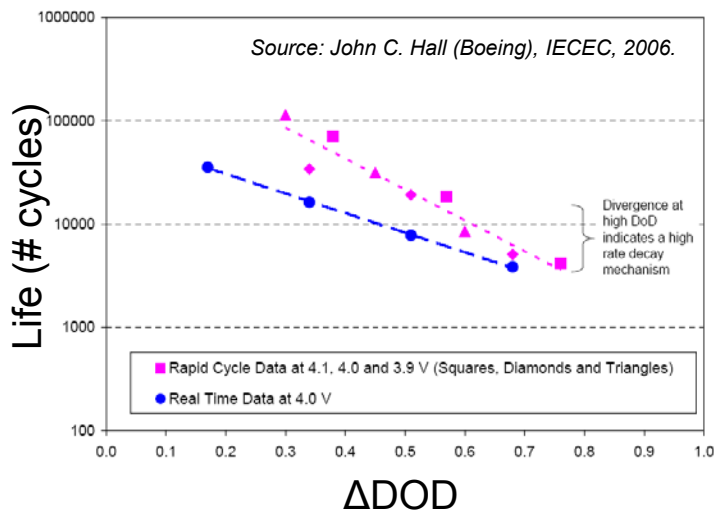
Calendar (Storage) Fade

- Relatively well established & understood
- Typical $t^{1/2}$ time dependency
- Arrhenius relation describes T dependency



Cycling Fade

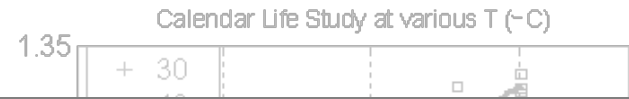
- Poorly understood
- Typical t or N dependency
- Often correlated $\log(\# \text{ cycles})$ with ΔDOD or $\log(\Delta\text{DOD})$



Objectives for Battery Life Modeling

Develop a power and energy degradation model that —

1. Uses both accelerated and real-time calendar and cycle life data as inputs.
2. Is mathematically consistent with all calendar and cycle life empirical data.
3. Is extendable to arbitrary usage scenarios (i.e., it is predictive).



Life (# cycles)



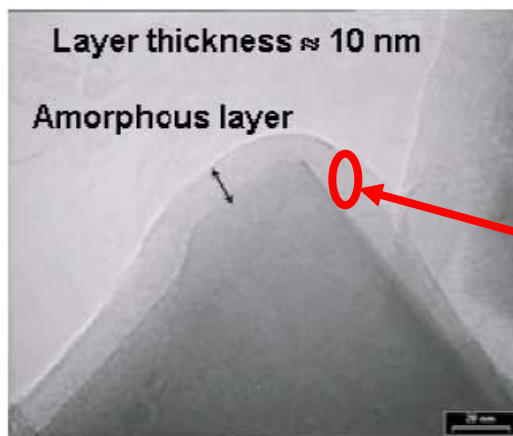
Impedance Growth Mechanisms: Complex Calendar and Cycling Dependency

NCA chemistry: Different types of electrode surface film layers can grow.

(1) “Electrolyte film” or SEI layer (2) “Solid film”

SEM Images: John C. Hall, IECEC, 2006.

Cell stored
at 0°C

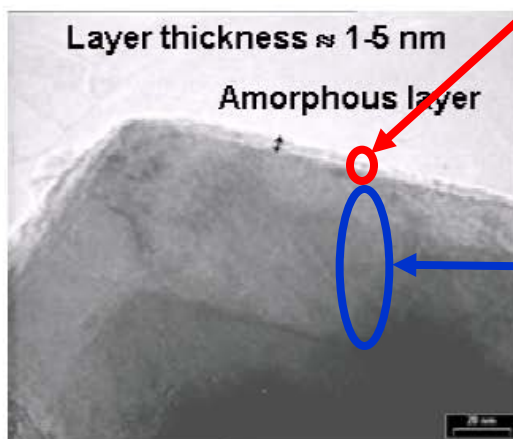


Electrolyte film*

- grows during storage $\propto t^{1/2}$
- suppressed by cycling

*Often called Solid-Electrolyte Inter-phase (SEI) layer

Cell cycled
1 cycle/day
at 80% DOD
and 0°C



Solid film

- grows only with cycling $\propto t$ or N

Life Model Summary (equations & coefficients)

Impedance Growth Model

- Temperature
- Voltage
- Δ DOD
- Calendar Storage ($t^{1/2}$ term)
- Cycling (t & N terms)

Capacity Fade Model

- Temperature
- Voltage
- Δ DOD
- Calendar Storage (Li loss)
- Cycling (Site loss)

Life Model Summary (equations & coefficients)

Impedance Growth Model

- Temperature
- Voltage
- ΔDOD
- Calendar Storage ($t^{1/2}$ term)
- Cycling (t & N terms)

$$k_1 = k_{1,ref} \exp(-E_{a1} \times (T^{-1} - T_{ref}^{-1}) / R)$$

$$k_2 = k_{2,ref} \exp(-E_{a2} \times (T^{-1} - T_{ref}^{-1}) / R)$$

$$a_1 = a_{1,ref} k_1 \exp(\alpha_1 F / RT \times V)$$

$$a_2 = a_{2,ref} k_2 \exp(\alpha_2 F / RT \times V)$$

$$a_1 = b_0 + b_1 (1 - \Delta DOD)^{b2}$$

$$a_2 / a_1 = \max[0, c_0 + c_1 (\Delta DOD)]$$

$$a_{2,t} = a_2 (1 - \alpha_N)$$

$$a_{2,N} = a_2 \alpha_N$$

$$R = a_1 t^{1/2} + a_{2,t} t + a_{2,N} N$$

Capacity Fade Model

- Temperature
 - Voltage
 - ΔDOD
 - Calendar Storage (Li loss)
 - Cycling (Site loss)
- From impedance growth model

$$Q_{Li} = d_0 + d_1 \times (a_1 t^{1/2})$$

$$Q_{sites} = e_0 + e_1 \times (a_{2,t} t + a_{2,N} N)$$

$$Q = \min(Q_{Li}, Q_{sites})$$

Reasonably fits available data

Actual interactions of degradation mechanisms may be more complex.

Details of Calendar and Cycle Life Models Are Presented by Kandler Smith in the Poster Session for AABC-09

Modeling of Nonuniform Degradation in Large-Format Li-ion Batteries

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Abstract

An empirical degradation model, capturing the effects of both storage and cycling, was developed for the Li-ion Nickel-Cobalt-Aluminum chemistry. The degradation model is coupled with NREL's multi-dimensional multi-scale (MMS) cell model to explore the impacts of nonuniform cycling and temperature inside a cylindrical 20 Ah PHEV cell over the course of an accelerated cycle-life test. Results show significant differences compared to a lumped analysis that neglects the cell's real geometry.

Background and Approach

Background
Context: Trend towards larger cells
PHEV → PHEV → EV
Reduced cell count reduces cost & complexity
Drawback: Greater internal nonuniformity
Elevated temperature, Regions of localized cycling

Objectives
Understand impact of large-format cell design features on battery useful life
Improve battery engineering models to include realistic geometry and physics
Reduce make-and-break iterations, accelerate design cycle

Multiscale approach for computational efficiency

Length scales:
1. Lithium-ion (1-100 μm)
2. Heat & electron transport (1-20 cm)

Time scales
1. Repeated cycling profile (minutes)
2. Degradation effects (months)

Empirical degradation model considers both storage and cycling effects

Storage (Calendar) fade
Typical t^2 time dependency
Arrhenius relation describes T dependency

Cycling fade
Typical t or N dependency
Often correlated log (if cycled) with ΔDOO

Degradation Model

Empirical model fit to test data for the Li-ion NCA chemistry¹⁸

ΔDOO Effect
Model includes t^2 (storage) and N (cycling) dependencies
 a_1 (storage) and a_2 (cycling) coefficients vary with ΔDOO

Voltage and temperature acceleration
Increased degradation due to elevated voltage and temperature described using Tafel and Arrhenius equations

Model for 1 cycle/day, $N = 3$

ΔDOO	a_1 (days ⁻²)	a_2 (days)	R ²
10%	0.00010e-4	1.54E10e-7	0.9847
15%	1.00010e-4	3.70E10e-7	0.9888
20%	1.00010e-4	9.88E10e-7	0.9920
25%	1.00010e-4	1.120E11e-7	0.9716

Li-ion (C/NCA) degradation model summary

Impedance Growth Model

- Temperature: $k_1 = k_{1,0} \exp(-E_a / (R(T_1 - T_0)))$
 $k_2 = k_{2,0} \exp(E_a / (R(T_1 - T_0)))$
- Voltage: $A_1 = a_{1,0} \exp(\alpha_1 FRT / V)$, $A_2 = a_{2,0} (1 - \alpha_2)$
 $A_3 = a_{3,0} \exp(\alpha_3 FRT / V)$, $A_4 = a_{4,0}$
- ΔDOO: $A_1 = b_1 (1 - \Delta DOO)$
 $A_2 / A_3 = \max(S, c_1 + c_2 (\Delta DOO))$

Calendar Storage (t^2 term) + Cycling (t & N terms) → $R = a_1 t^2 + a_2 t + a_3 N$

Capacity Fade Model

- Temperature
- Voltage
- ΔDOO
- Calendar Storage (t term): $Q_t = Q_0 + \alpha_1 t + \beta_1 t^2$
- Cycling rate load: $Q_c = \alpha_2 + \alpha_3 + \beta_2 (t + t_0)$
- $Q = \min(Q_t, Q_c)$

Results

Modeling investigation: Accelerated cycling of 20 Ah PHEV-type cylindrical cell

- Cell Dimensions: 48 mm diameter, 120 mm height
- Well designed for thermal & cycling uniformity, low capacity fade rate
- Thermal: 30°C ambient, $h = 20 \text{ W/m}^2\text{K}$
- ΔDOO: 90% SOC_{max} to 30% SOC_{min}
- Actual Cycling: Various discharge (shown below), 10 min rest, 1°C charge, 60 min rest, repeat.

Capacity fade & resistance growth for various repeated discharge profiles (1C, 5C, 10C, U50%)

Temperature rise accelerates degradation

Significant growth in internal temperature during U50% and 10C discharge cycling
Internal temperature remains constant for 1C discharge cycling

Abundance

- Early in life, inner core and terminal areas are cycled the most
- Later in life, those same areas are most degraded and are cycled least
- Abundance continually grows throughout life

US06 - Nonuniform degradation

Relative Capacity

- Regions near terminals suffer most significant capacity loss
- Large temperature → excessive cycling
- Inner core loses capacity faster than outer cylinder wall
- High temperature → Material degradation

0 months → 8 months → 16 months
3.1% Ah imbalance → 1.7% Ah imbalance → 2.8% Ah imbalance

Nonuniform degradation effects important for predicting cell performance fade

- Lumped temperature model overpredicts (all level fade) (1-D) electro-thermal model also overpredicts fade
- Illustrates strong coupling between multidimensional degradation and cell performance

Conclusions

- For 20 Ah cylindrical cell with good thermal & cycling uniformity at beginning of life...
 - Abundance grows throughout life (T, Ah throughput, capacity loss)
 - Acceleration mechanism apparent for high-rate cycling (Ah): Higher impedance → Higher temperature → Faster degradation
 - Major factors leading to nonuniform degradation: Nonuniform temperature (degrades inner core), Nonuniform potential (degrades terminal region)
 - Regions heavily used at beginning of life (inner core, terminal region) are used less and less as life progresses
 - 1-D electro-thermal model not suited to predict performance degradation for large cells: For a given electrode-level degradation mechanism, overpredicts cell-level capacity fade and impedance growth

Acknowledgements

- U.S. Department of Energy, Office of Vehicle Technologies
- Case Howard, Energy Storage Program

References

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2. J. C. Kim, K. Smith, "Multi-Scale Multi-Dimensional Model for Battery Cell Design and Management," 13th Electrochem. Soc. Pacific Rim Meeting, Honolulu, HI, October 19-21, 2008
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4. J. Kim, T. Kim, G. Brown, "Design Innovation and Life Prediction for Lithium Ion Sealed Cells," 4th International Energy Conversion Engineering Conference & Exhibit, San Diego, CA, June 24-28, 2006
5. J. Kim, A. Simon, S. Pappas, P. Liu, K. Kraljic, "Resistance Growth in Lithium Ion Sealed Cells," 1. New Zealand Battery Analysts', 2009 Electrochem. Soc. Mtg., Los Angeles, CA, October 16-21, 2009
6. J. P. Christopoulos, J. Blawie, J. J. Thomas, K. J. Spring, S. J. Hankins, V. S. Arifovic, D. Rowell, "Advanced Technology Development Program for Lithium Ion Batteries: DOE Gen 2 Performance Evaluation Final Report," Idaho National Laboratory, INEL/EV-ET-00010, July 2006
7. M. C. Ventur, K. B. Cho, L. D. Westerman, S. V. Sathuluri, "Storage Characterization of Li-ion Batteries," NASSA Advanced Battery Workshop, Huntsville, AL, November 16, 2006
8. J. Sulzer, "Accelerated Testing of Advanced Battery Technologies in PHEV Applications," 13th Electrochem. Soc. Meeting, Anaheim, CA, December 1-5, 2008
9. F. Baranov, K. Borzhomishvili, "LiPF₆ Li-ion Space Batteries Roadmap," NASSA Advanced Battery Workshop, Huntsville, AL, November 17-20, 2007

Life Model Summary

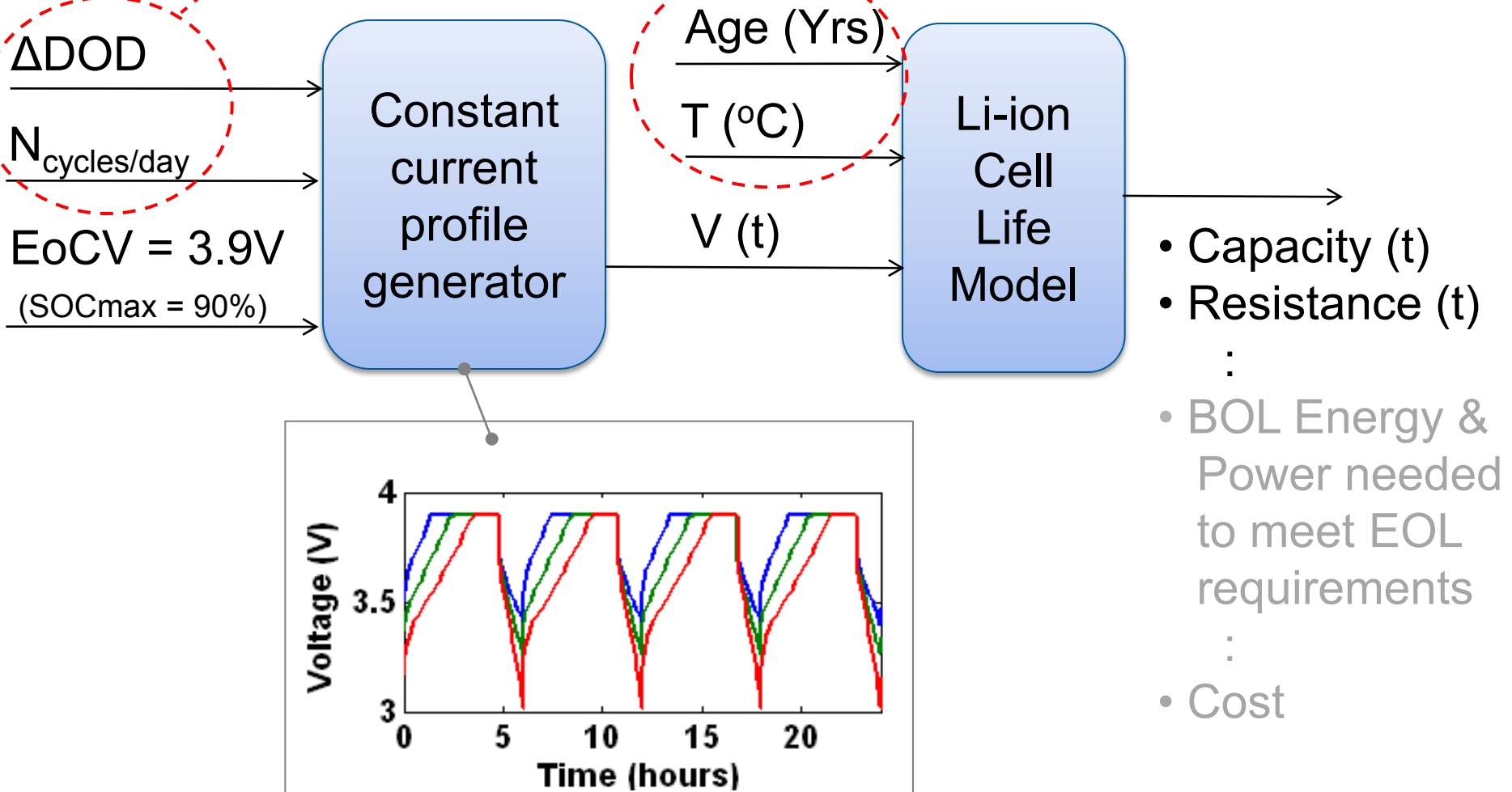
- Model structure set by Boeing satellite battery dataset^{1,2}
 - Difficult to decouple Δ DOD and voltage degradation effects from cell-level dataset
- Model adjusted to reflect more recent experience with NCA-graphite cells from various Labs³⁻⁶
 - 4.5 years storage at 40°C, 50% SOC → 10% capacity fade⁴
 - 13.7 years storage at 35°C → 110% resistance growth⁵
 - 2700 PHEV charge depletion cycles at 25°C → 8% capacity fade, 50% resistance growth⁶
- The following analysis illustrates trade-offs for a cell with low capacity fade but high resistance growth over life.

References:

1. J. Hall, T. Lin, G. Brown, "Decay Processes and Life Predictions for Lithium Ion Satellite Cells," 4th International Energy Conversion Engineering Conference & Exhibit, San Diego, CA, June 26-29, 2006.
2. J. Hall, A. Schoen, A. Powers, P. Liu, K. Kirby, "Resistance Growth in Lithium Ion Satellite Cells. I. Non Destructive Data Analyses," 208th Electrochem. Soc. Mtg., Los Angeles, CA, October 16-21, 2005.
3. J.P. Christophersen, I. Bloom, E.V. Thomas, K.L. Gering, G.L. Henriksen, V.S. Battaglia, D. Howell, "Advanced Technology Development Program for Lithium-Ion Batteries: DOE Gen 2 Performance Evaluation Final Report," Idaho National Laboratory, INL/EXT-05-00913, July, 2006.
4. M.C. Smart, K.B. Chin, L.D. Whitcanack, B.V. Ratnakumar, "Storage Characteristics of Li-Ion Batteries," NASA Aerospace Battery Workshop, Huntsville, AL, November 14-16, 2006.
5. P. Biensan, Y. Borthomieu, "Saft Li-Ion Space Batteries Roadmap," NASA Aerospace Battery Workshop, Huntsville, AL, November 27-29, 2007.
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Life Analysis Conducted Using Simplified Cycling Profiles

Major input parameters that are varied.



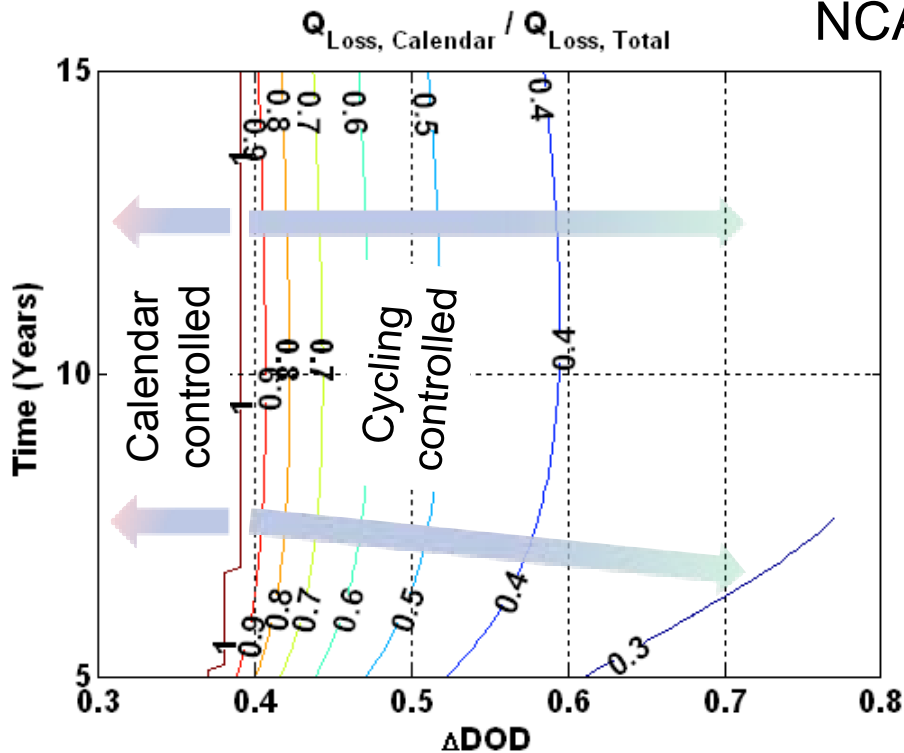
Results: Which Dominates — Calendar or Cycling?

Capacity Fade – Energy

Generally cycling controlled, though it depends on temperature

Moderate Climate

- 20°C, 1 cycle/day, SOC_{max} = 90%

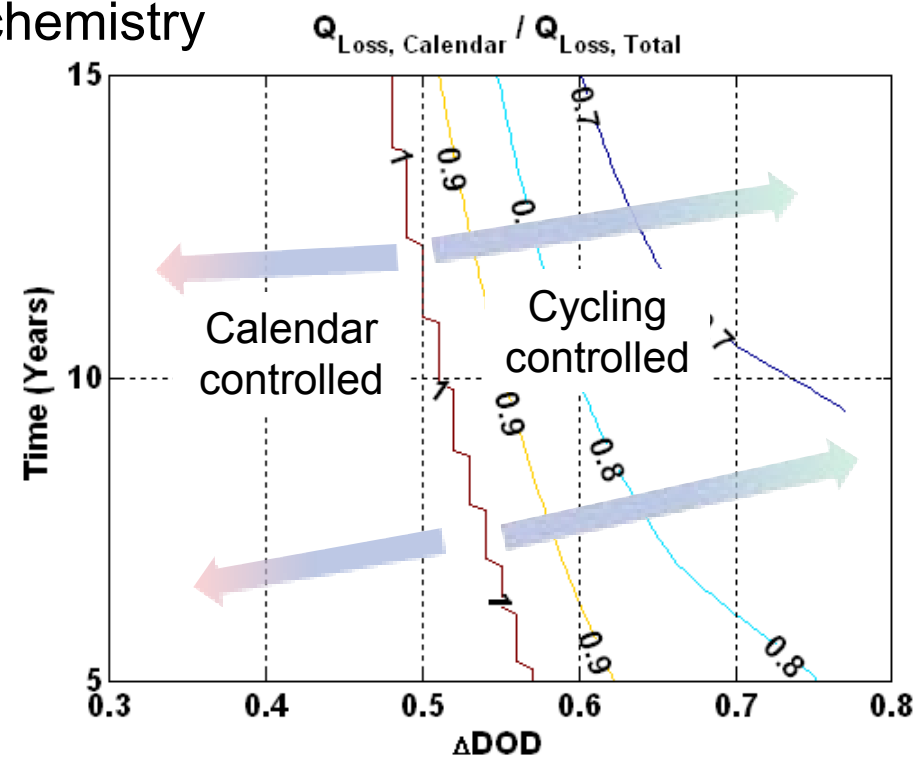


- Predominantly cycling controlled
(calendar fade just 30% to 40% of cycling fade)

Hot Climate

- 35°C, 1 cycle/day, SOC_{max} = 90%

NCA chemistry



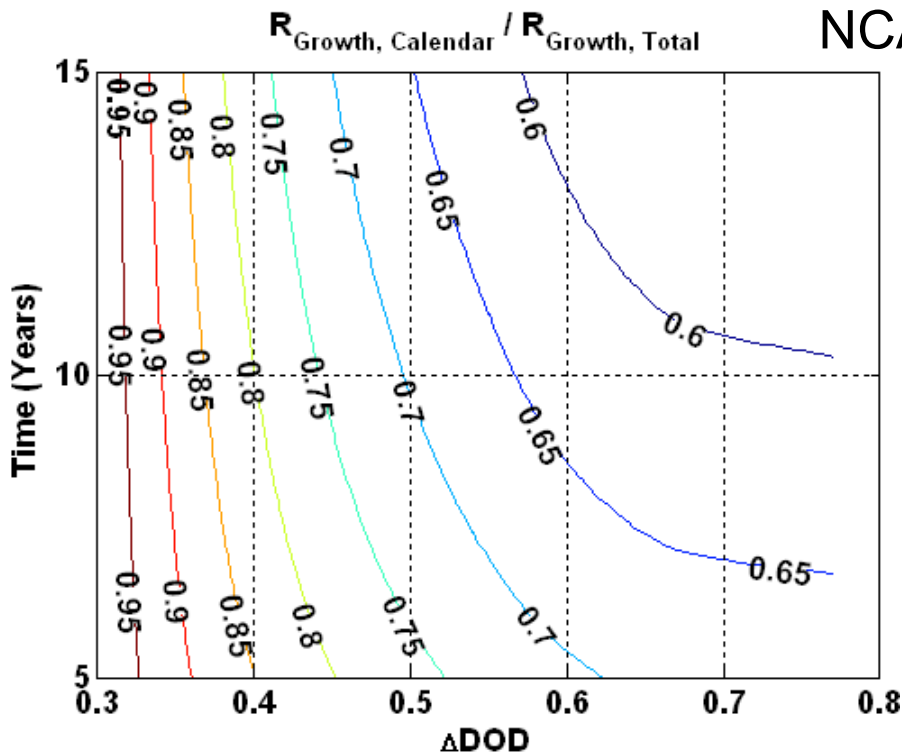
- Cycling controlled for High ΔDOD
- Calendar controlled for Low ΔDOD

Results: Which Dominates — Calendar or Cycling? Resistance Growth – Power

Calendar effect dominates, though both are important.

Moderate Climate

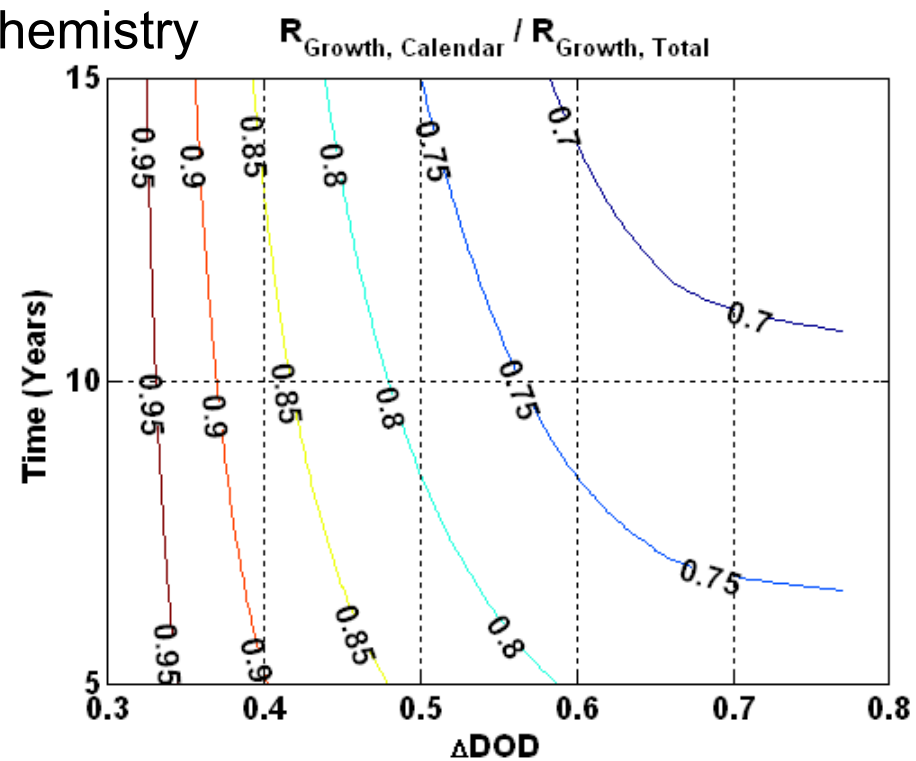
- 20°C, 1 cycle/day, SOC_{max} = 90%



- Calendar degradation:
> 60% of total resistance growth

Hot Climate

- 35°C, 1 cycle/day, SOC_{max} = 90%



- Calendar degradation:
> 70% of total resistance growth

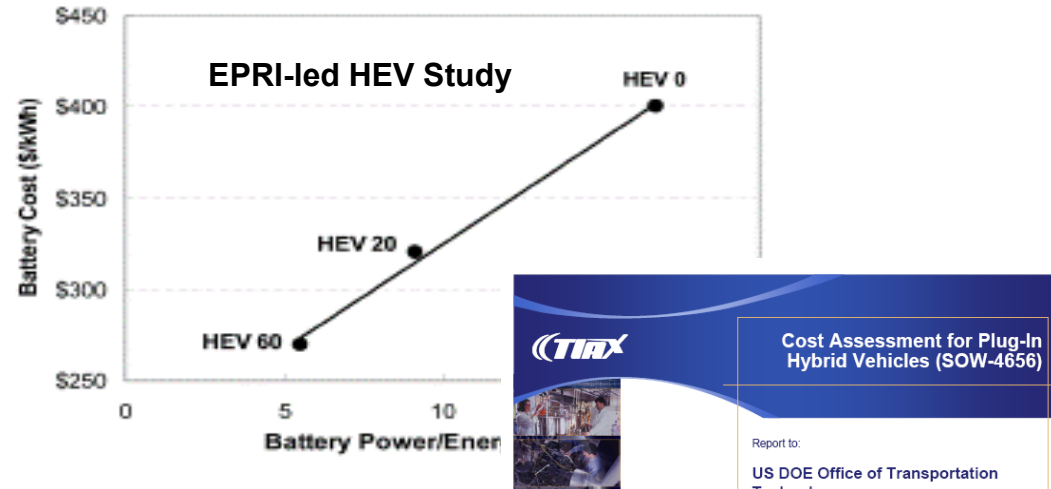
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Developing a Simplified Cost Model

Estimating Manufacturer Pack Cost

- Battery cost estimates from EPRI-led HEV study as original source¹
- EPRI HEV cost model used for NREL's EVS-22 paper on PHEV Cost Benefit Analysis²
- DOE-sponsored TIAX study reviewed cost details of two Li-ion cathodes (NCA and NCM) manufacturing³
- Modified fixed costs to include a per-cell component based on TIAX estimates (this study)
- Cost at volume manufacturing at 2007 materials' prices



Nominal Energy (kWh)	P/E	Detailed Model: ³ NCM	Detailed Model: ³ NCA	Simple Model: ^{1,2} \$=11*kW+224 *kWh+680
6.9	5.8	\$3120	\$2600	\$2660
8.5	4.7	\$3510	\$2860	\$3020
11.6	3.5	\$4290	\$3500	\$3680

NCA - Nickel Cobalt Alumina; NCM- Nickel Cobalt Manganese

Simplified Pack Cost Model

$$\$/\text{pack} = 11.1 * \text{kW} + 224.1 * \text{kWh} + 4.53 * \text{BSF} + 340$$

BSF = Battery Size Factor

1. Graham, R. et al. "Comparing the Benefits and Impacts of Hybrid Electric Vehicle Options," Electric Power Research Institute (EPRI), 2001.
 2. Simpson, A., "Cost Benefit Analysis of Plug-In Hybrid Electric Vehicle Technology," 22nd International Electric Vehicle Symposium, Yokohama, Japan, Oct. 2006.
 3. "Cost Assessment for Plug-In Hybrid Vehicles," TIAX LLC, Oct. 2007.

Life-Cost Trade-Off Study: Approach

- Choose a cycle life model and a calendar life model
 - We picked curve fits from slide 13 for NCA chemistry
- Choose a cost model
 - Manufacturing cost of a complete pack at high-volume production
 - We picked the equation on slide 18 for NCA chemistry
- Select the required battery energy and power
 - Energy: 3.4 kWh PHEV10; 11.6 kWh PHEV40 (USABC requirements)
- Select the required battery life
 - Cycles (charge depleting): 5000 CD cycles (USABC requirements)
 - Calendar life: 10 years at 30°C (less aggressive than 15-year USABC)
- Perform analysis to answer the following questions:
 - What Δ DOD & P/E meet life at minimum cost?
 - Which controls life? Calendar or cycle life?
 - What environmental parameters cause greatest life sensitivity?

Life-Cost Trade-Off: Energy and Power Margin to Meet EOL Performance Requirements

Battery Sizing Metrics:

$$\text{BOL Energy Margin} = \left[\frac{\text{BOL Total Energy}}{\text{EOL Available Energy Requirement}} - 1 \right] \times 100\%$$

$$\text{BOL Power Margin} = \left[\frac{\text{BOL Total Power}}{\text{EOL Available Power Requirement}} - 1 \right] \times 100\%$$

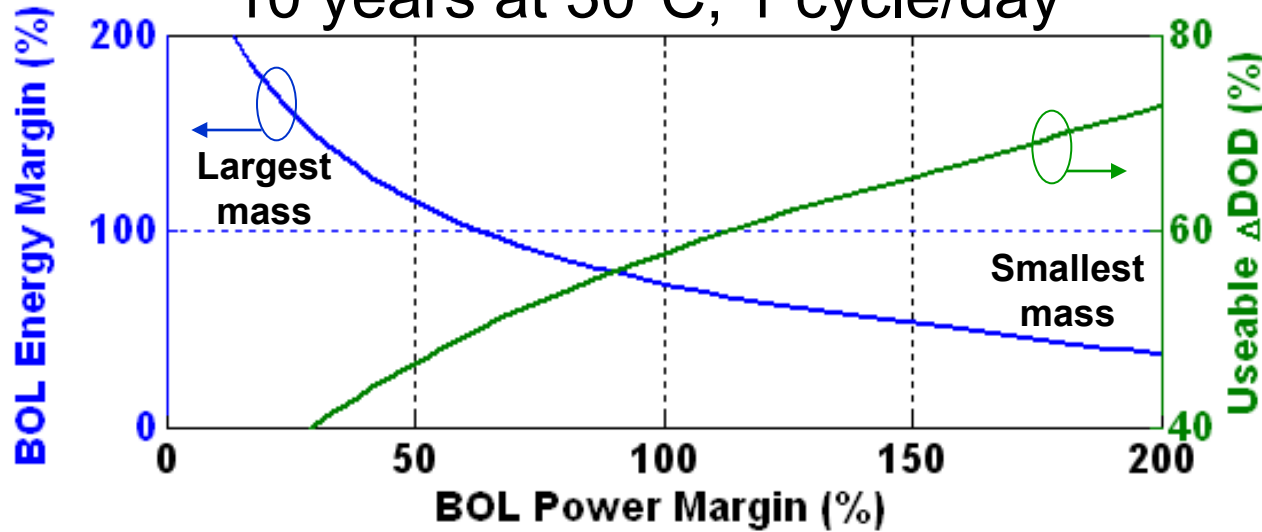
BOL = Beginning of Life
EOL = End of Life

Next slides give results for **typical** Li-ion NCA chemistry and include fade for a chosen Δ DOD window (1 cycle/day, 30°C).

Example Results: Life-Cost Trade-Off Study

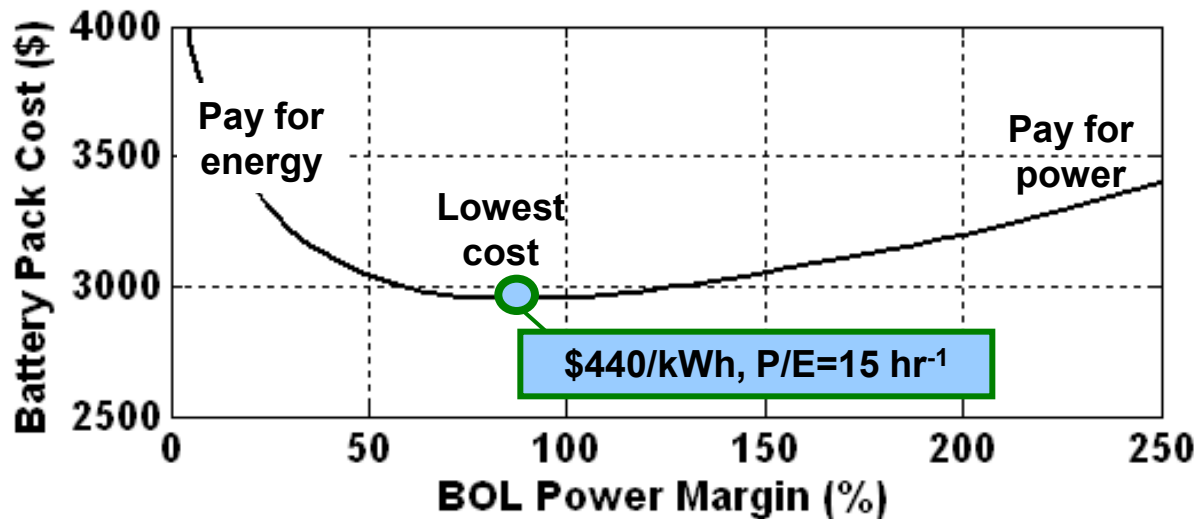
(Energy & Power Margin, Usable Δ DOD)

PHEV10 battery sized for
10 years at 30°C, 1 cycle/day*



NCA chemistry

- PHEV10 batteries can require >100% excess power at BOL
- Allows ~60% usable Δ DOD (More usable Δ DOD is possible with even more excess power)



- Too much power is preferable to too little
 - small increase in cost
 - reduces mass

Today's costs at volume production

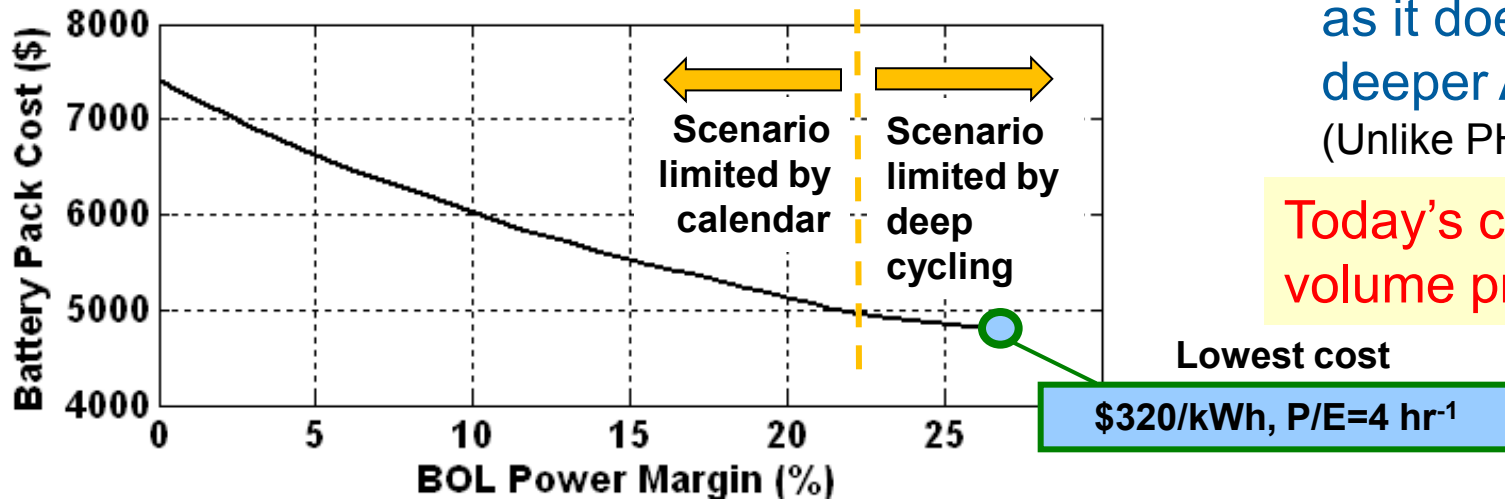
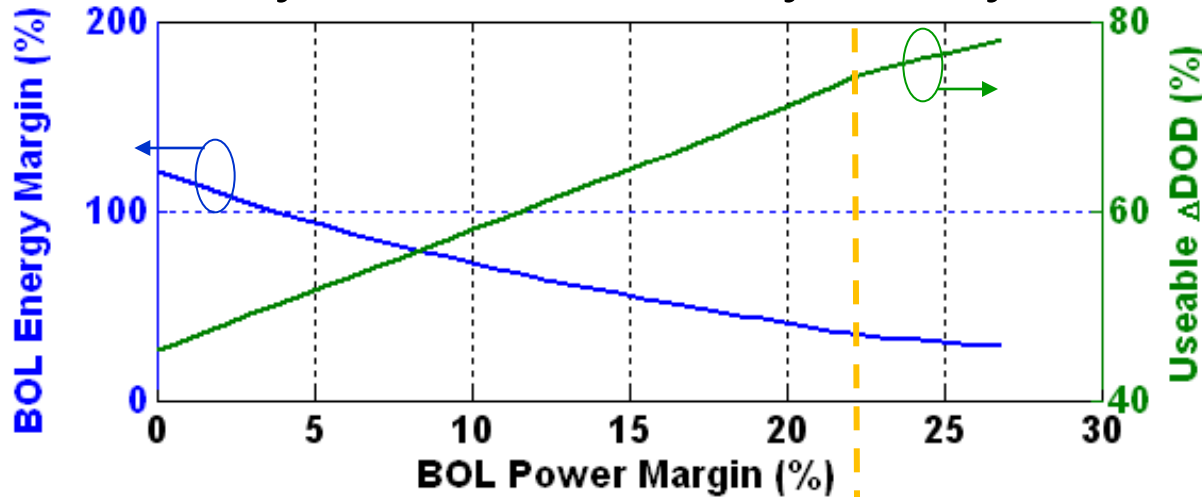
* 3.9 EoCV (90% SOC_{max})

** Excess power and energy relative to 50kW and 3.4 kWh PHEV 10 requirements

Example Results: Life-Cost Trade-Off Study

(Energy & Power Margin, Usable Δ DOD)

PHEV40 battery sized for 10 years at 30°C, 1 cycle/day*



NCA chemistry

- PHEV40 batteries can require ~25% excess power at BOL
- Less power sensitivity compared with PHEV10
- Higher excess power is not advantageous as it does not allow deeper Δ DOD cycling (Unlike PHEV10)

Today's costs at volume production

* 3.9 EoCV (90% SOC_{max})

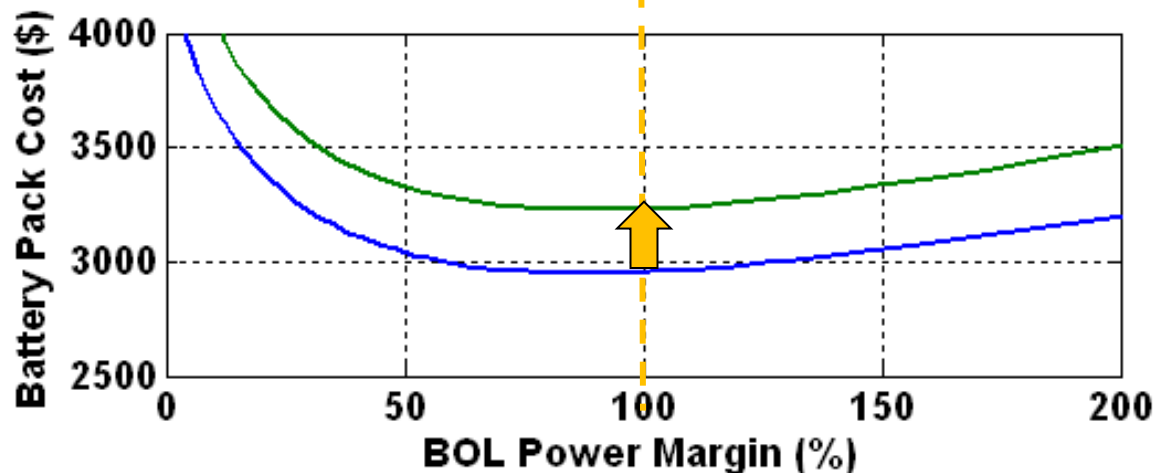
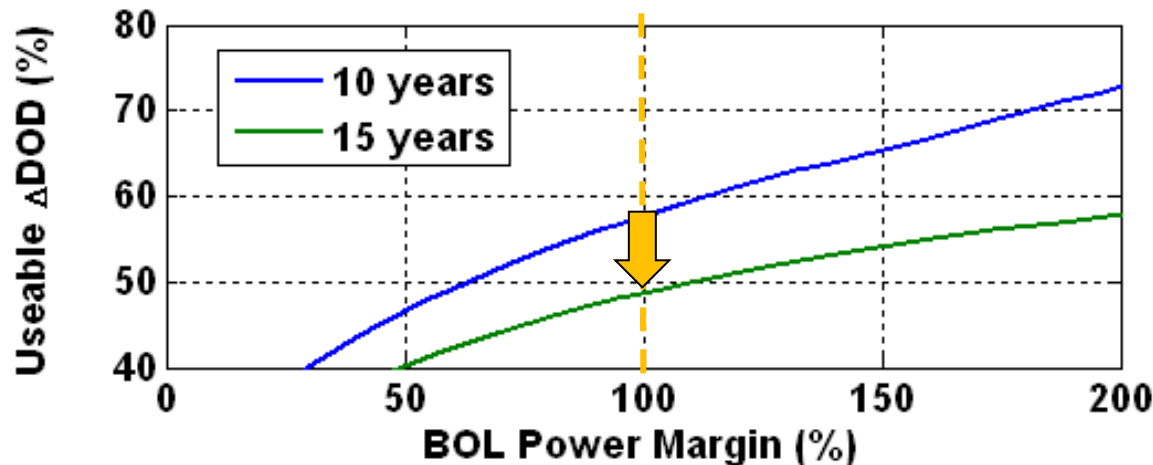
** Excess power and energy relative to 46kW and 11.6 kWh PHEV 40 requirements

Example Results: Life-Cost Trade-off Study

(Sensitivity to Years of Life)

PHEV10 battery sized for
10, 15 years at 30°C*

NCA chemistry



Increasing life requirement from 10 to 15 years means:

- 10% less Δ DOD is usable
- \$250 greater cost

* 1 cycle/day, 3.9 EoCV (90% SOC_{max})

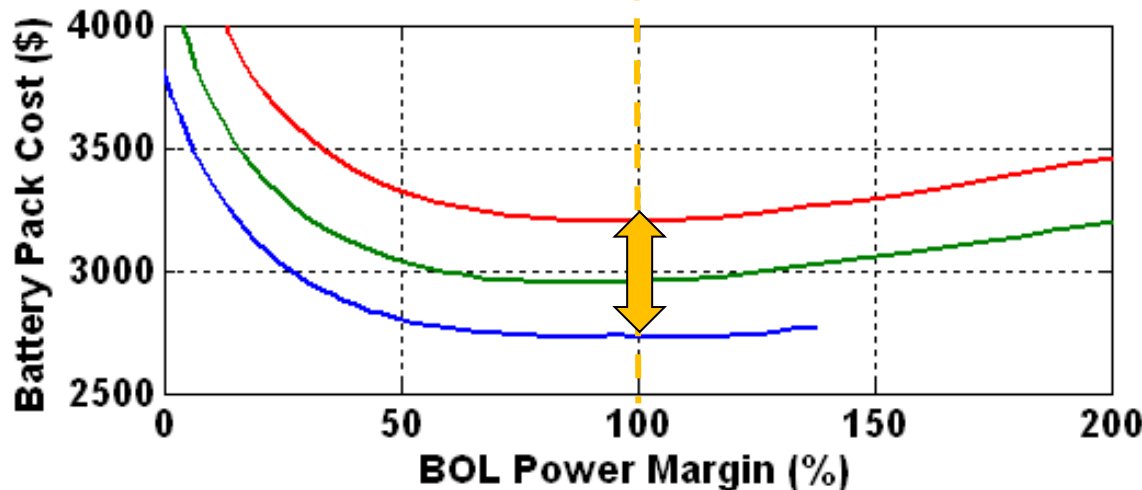
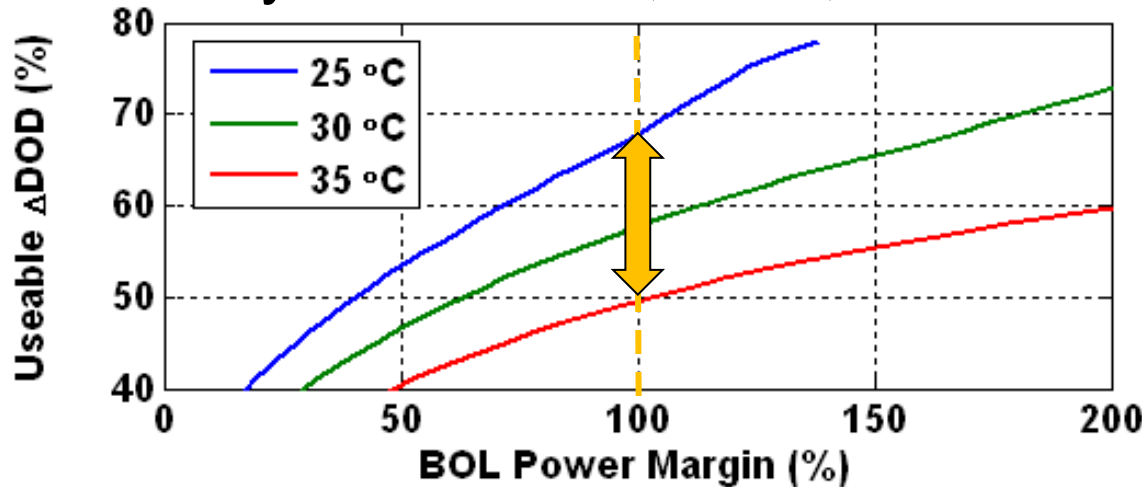
** Excess power relative to 50kW PHEV 10 requirement

Example Results: Life-Cost Trade-Off Study

(Temperature Sensitivity)

PHEV10 battery sized for 10 years at 25°C, 30°C, & 35°C*

NCA chemistry



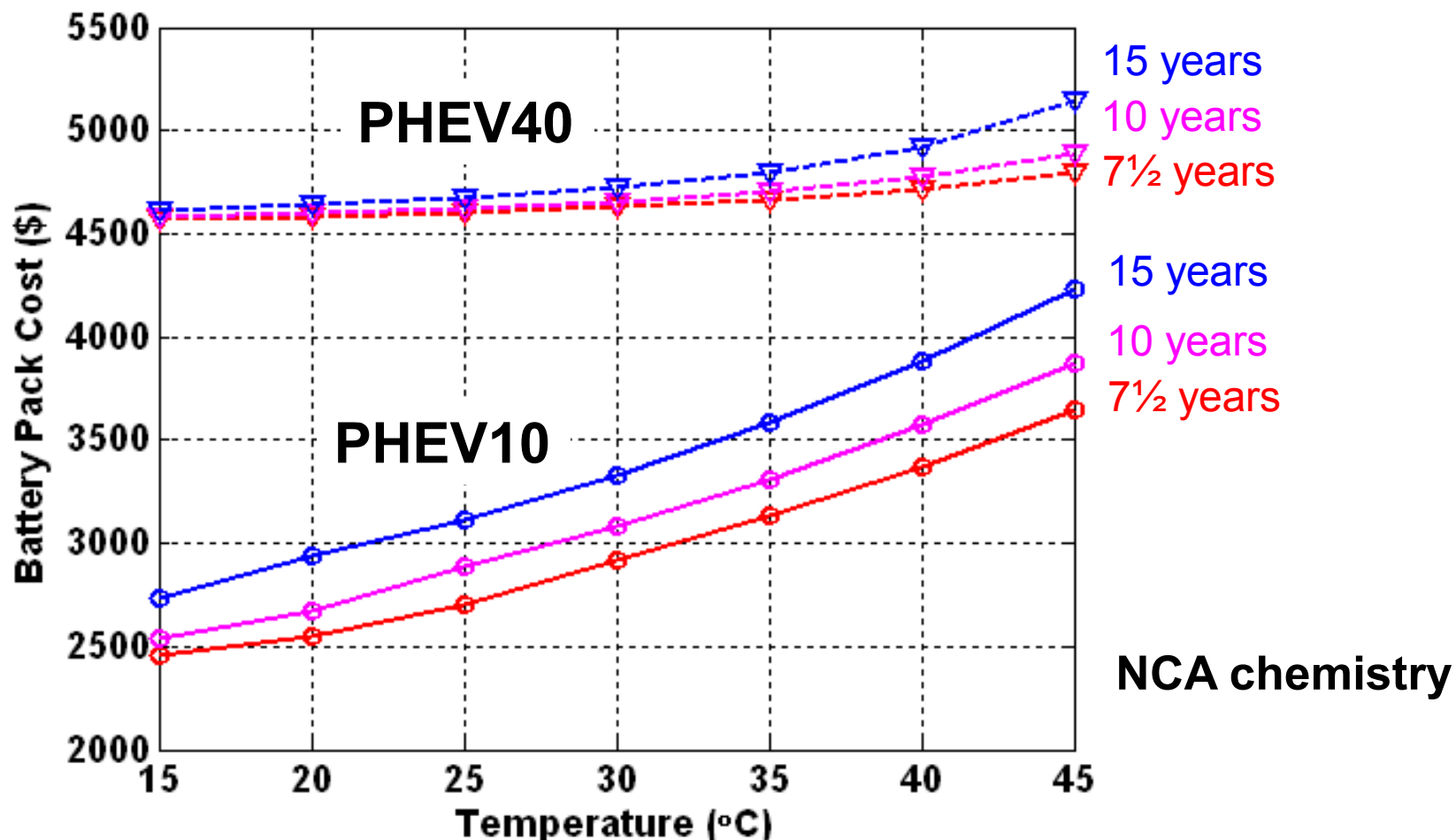
- Temperature exposure drastically impacts system size necessary to meet goals at end of life
 - 25°C: 70% ΔDOD is usable
 - 35°C: 50% ΔDOD is usable
- Modifying life requirements from 10 years at 25°C to 10 years at 35°C increases battery cost by >\$500

* 1 cycle/day, 3.9 EoCV (90% SOC_{max})

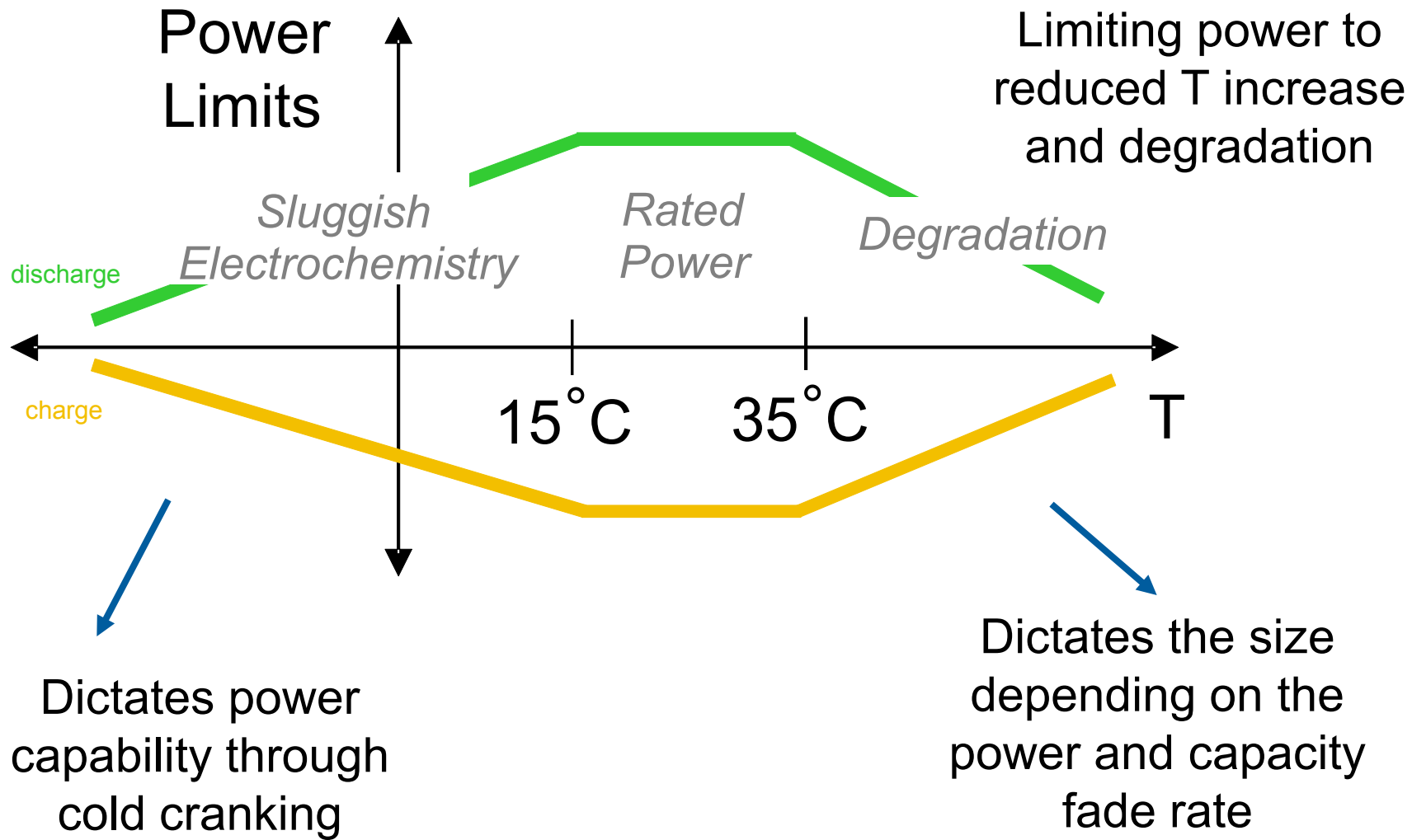
** Excess power relative to 50kW PHEV 10 requirement

Summary: Comparison of Battery Minimum Cost Designs for Varying Years of Life and Temperature

- Battery replacement not economically justified
- Cost can be more sensitive to temperature than years life
(Especially true for small PHEV batteries with high power requirement)



Temperature Impacts Cost (Sizing & Life)

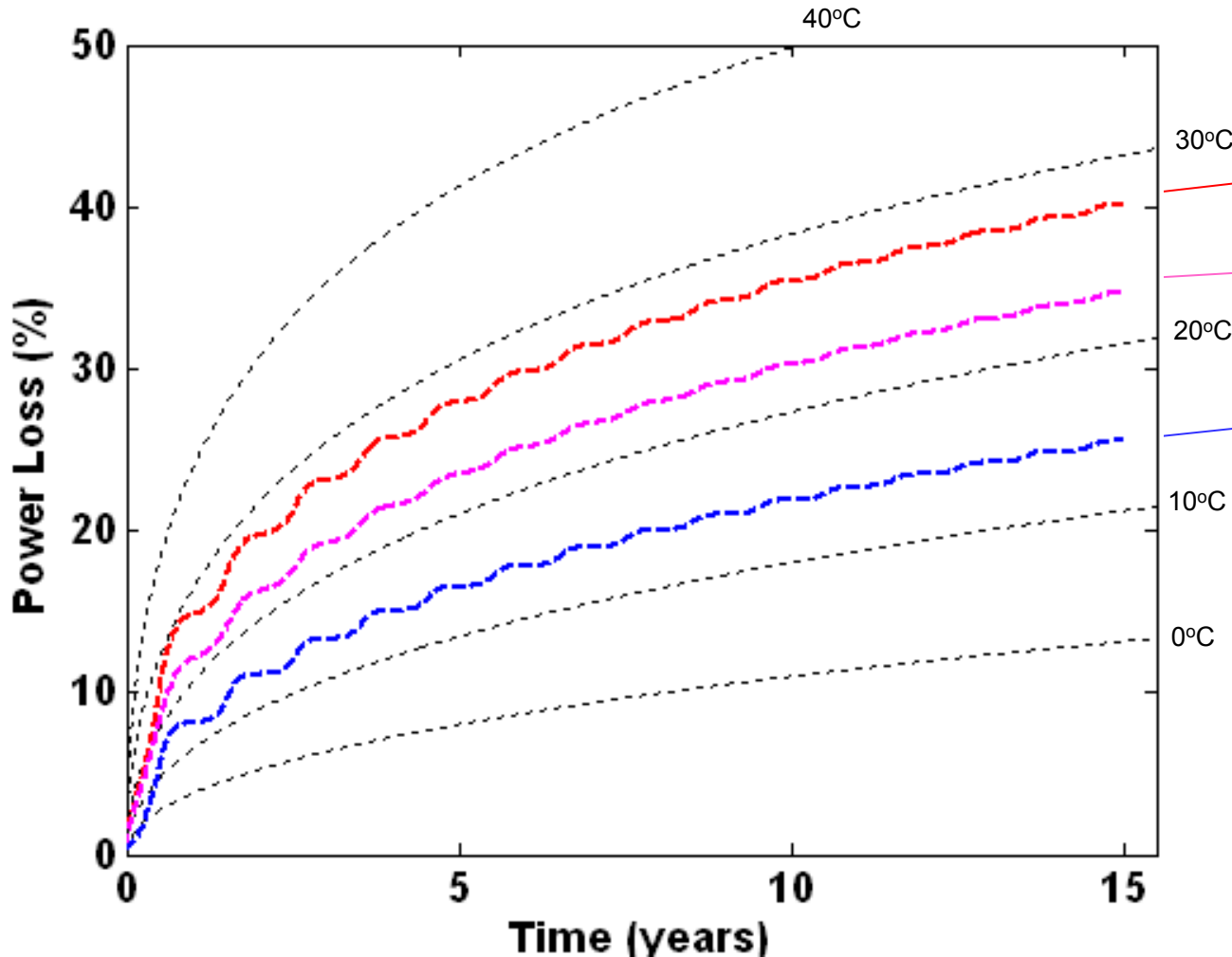


Impact of Temperature on Battery in a Parked Car

(Battery T = Ambient T)

- Used typical metrological year (TMY) as the hourly temperature
- Power fade model reformulated as rate law, integrated for temperature profile.
- PHEV10 with a typical quality NCA chemistry.

Most passenger vehicles are parked >90% of time.



Phoenix
44°C max, 24°C avg

Houston
39°C max, 20°C avg

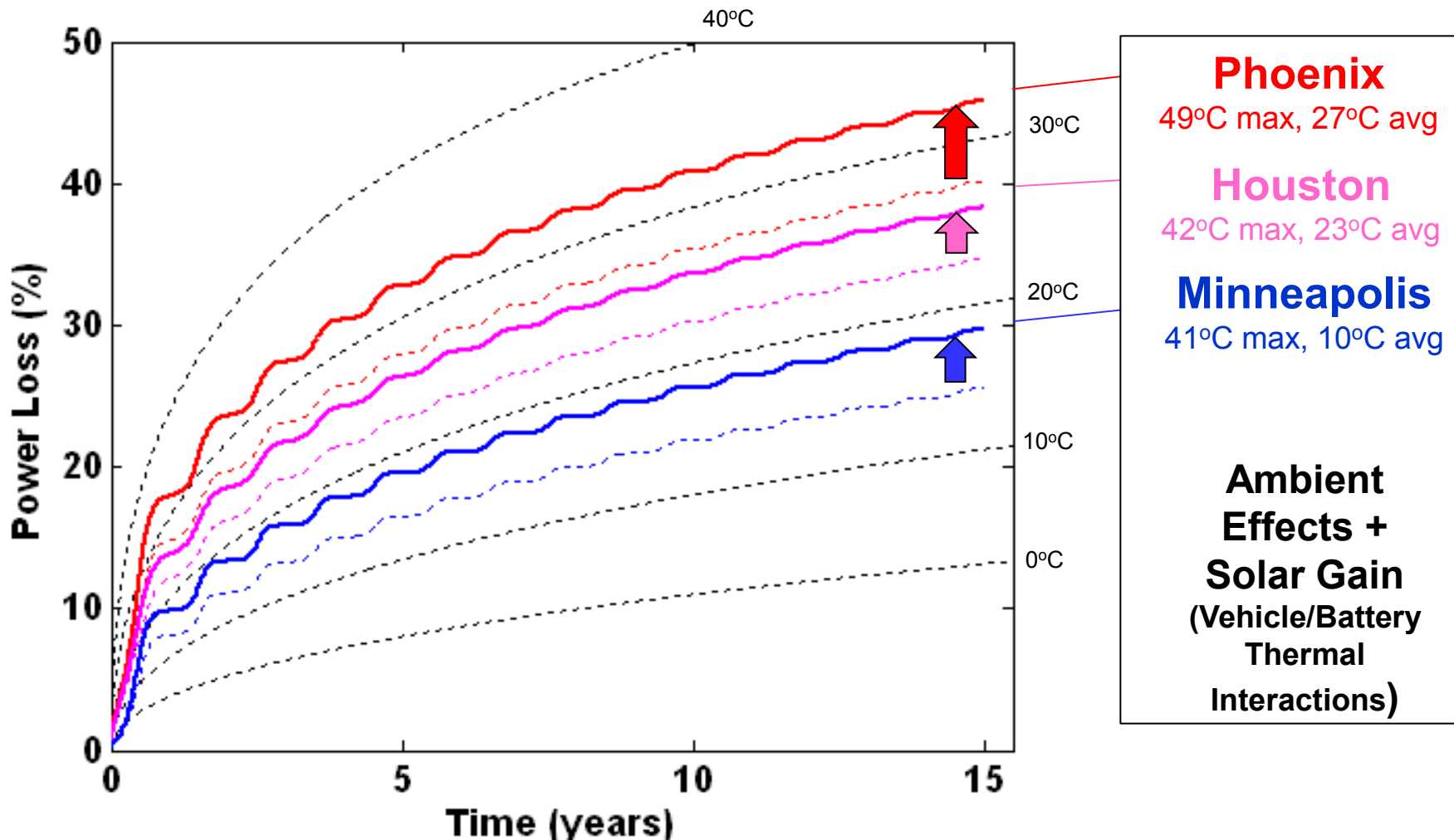
Minneapolis
37°C max, 8°C avg

Ambient Effects Only

Impact of Temperature on Battery in a Parked Car

(Battery T = Ambient T + Solar Gain)

- The same as previous slide (PHEV10, NCA chemistry and TYM weather)
- Developed a vehicle-battery-ambient model to predict the battery temperature
- Results show significant fade due to the ambient temperature and solar gain



Analysis Shows Keeping Peak Battery Temperature below Extremes Could Greatly Improve Battery Life

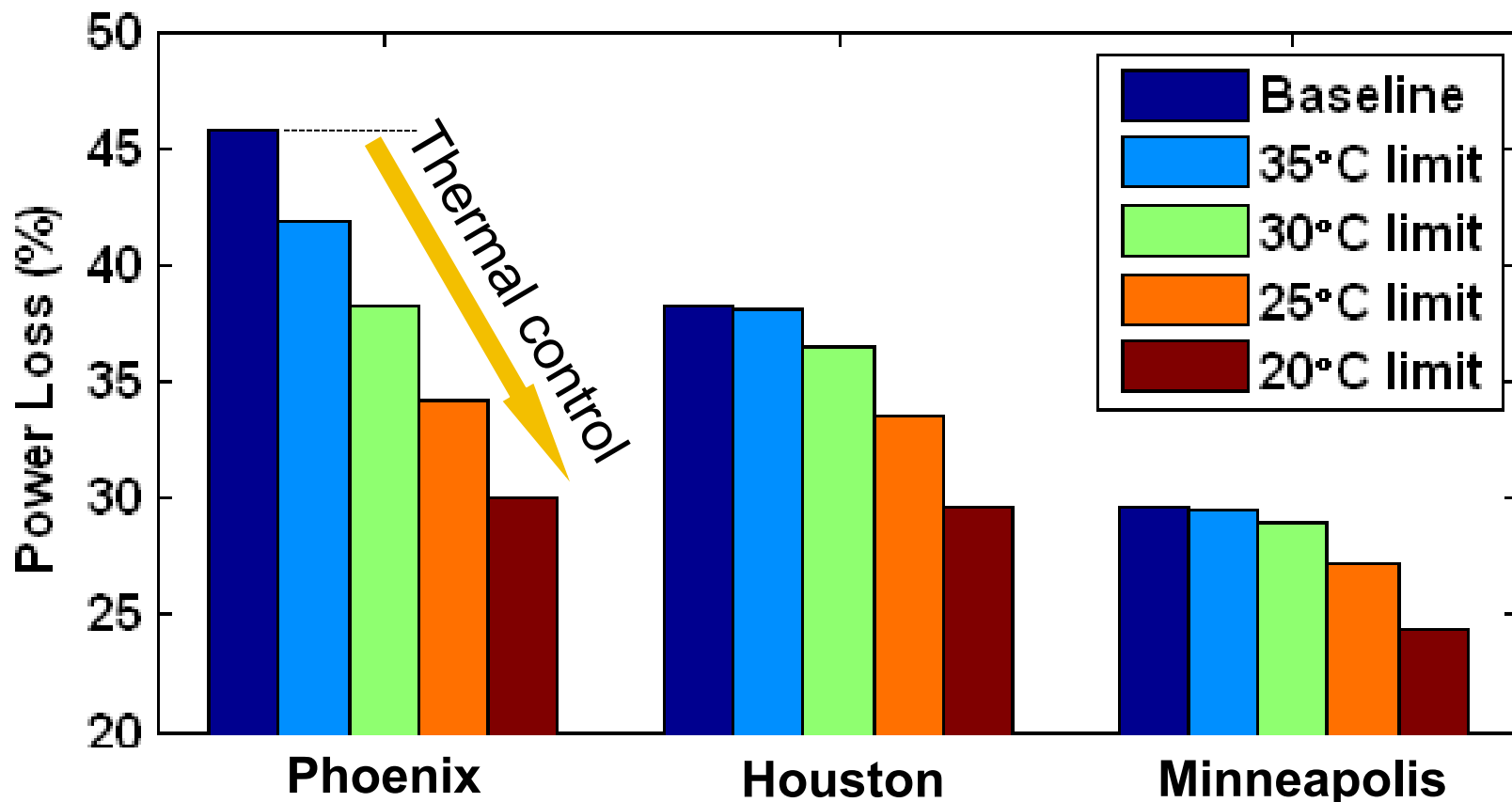
PHEV10 – Power loss after 15 years

Ambient temperature & solar radiation climate data input to vehicle/battery thermal model.

Assume peak battery temperatures can be eliminated.

Typical Quality Current NCA Li-ion Technology

How much is it worth to spend on thermal control (parked too)?



Summary

- Battery cost, cycle life, and calendar life must be optimized to achieve maximum value for PHEV commercialization.
 - A process/approach such as the one discussed here is needed.
- Useful life of a given pack design is dictated by complex interaction of parameters ($t^{1/2}$, t , N , T , V , DOD).
 - Different chemistries have different behaviors.
- Battery life is extremely sensitive to temperature exposure; solar loading can cause further battery heating and lower life.
- Thermal control (when parked or driving) could be a cost-effective method to reduce oversizing of battery for the beginning of life.
- PHEV battery “standby” thermal control can reduce power loss, particularly for PHEV10.
- Accurate degradation prediction requires a large experimental matrix (for different chemistries).

Thank You!

