

# Advances in Concentrating Solar Power Collectors: Mirrors and Solar Selective Coatings

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# Outline

- Solar Market Potential
- Solar Reflectors
- Solar Selective Coating
- Conclusion



# Concentrating Solar Power Technologies

Parabolic Trough



Power Tower



Dish-Stirling



Solar concentration allows tailored design approaches

Compact Linear Fresnel Reflector (CLFR)



100kW LCPV Tracking



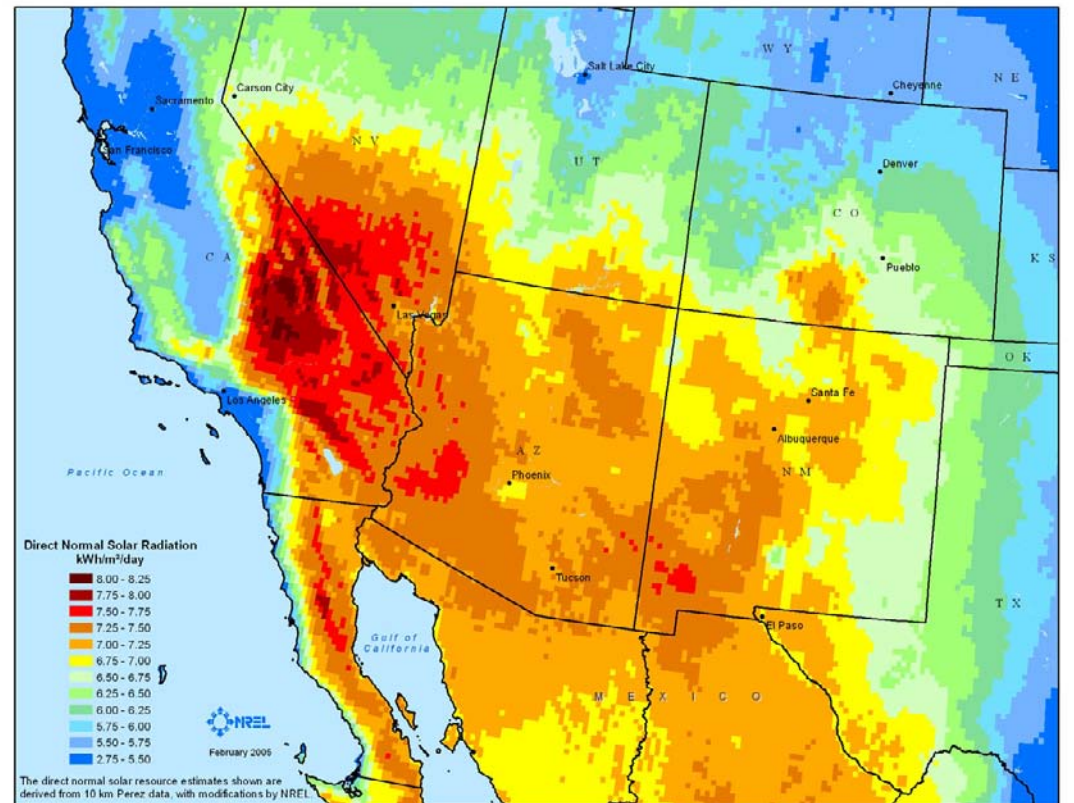
CPV Heliostat



CPV Winston Collector

# DOE & WGA determined feasibility of 1000MW in SW

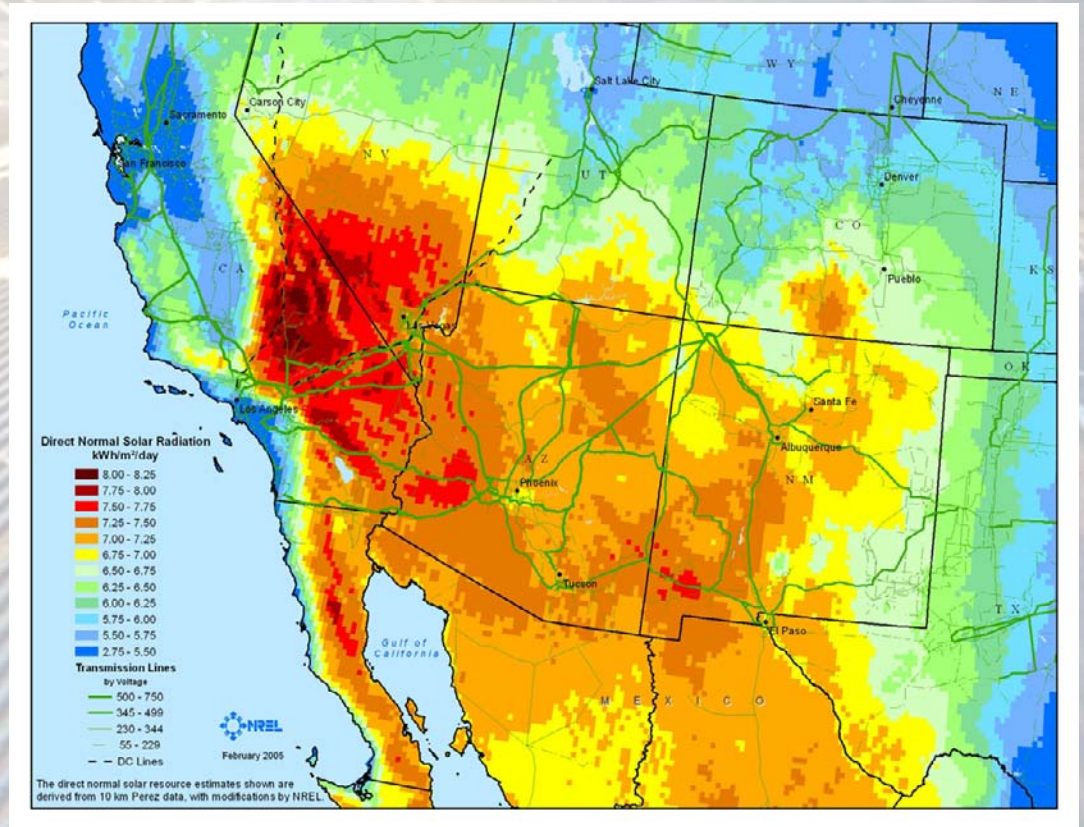
## Southwest Solar Resources



# DOE & WGA determined feasibility of 1000MW in SW

## Southwest Solar Resources

## Transmission Overlay

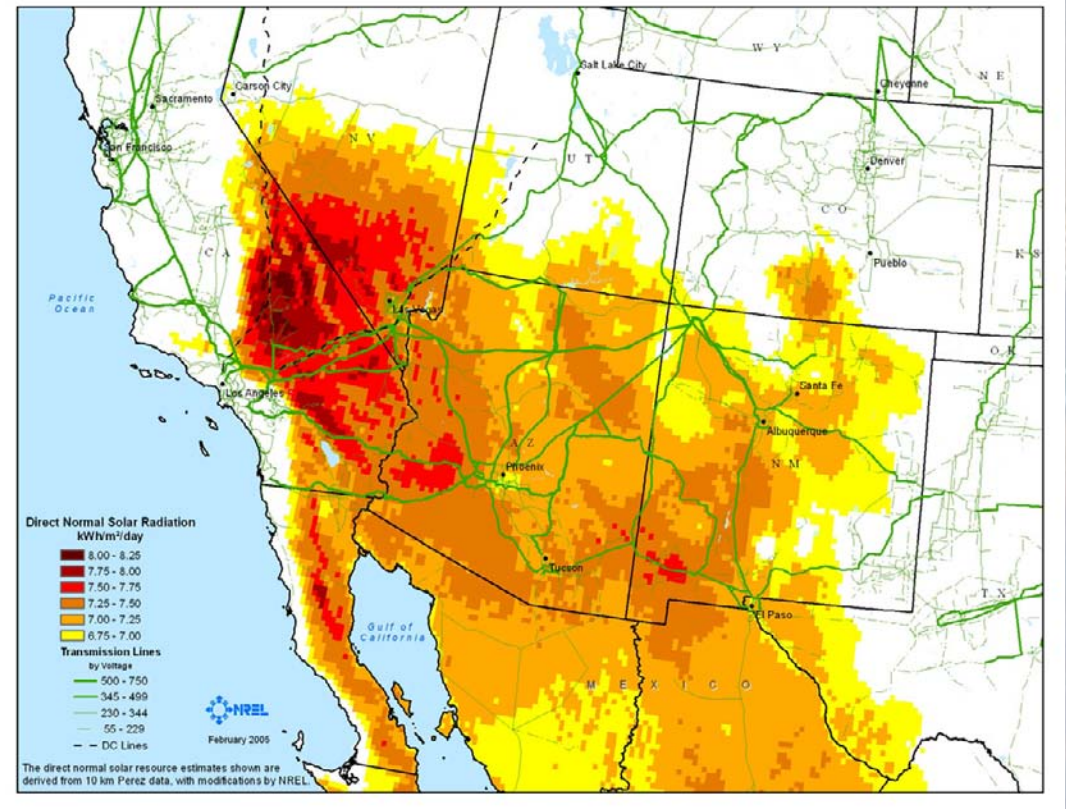


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## Southwest Solar Resources

## Transmission Overlay

Eliminate locations  
< 6.75 kwh/m<sup>2</sup>/day



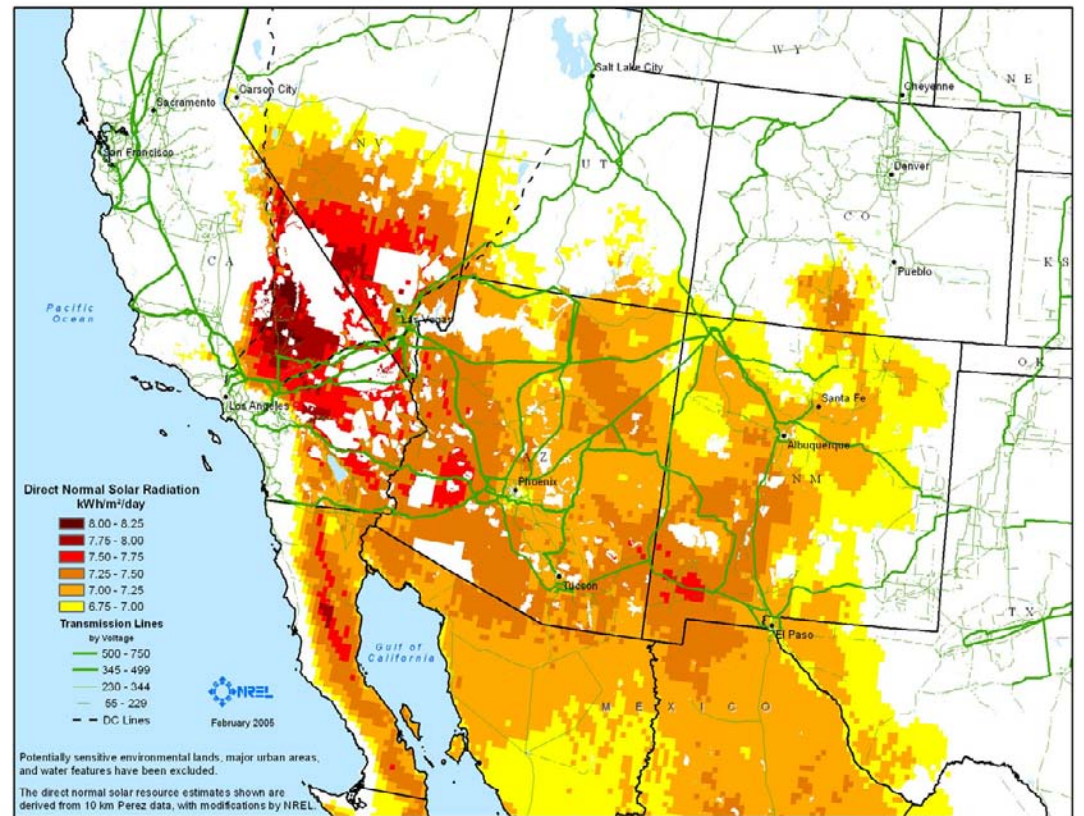
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## Southwest Solar Resources

### Transmission Overlay

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Exclude environmentally  
sensitive lands, major  
urban areas, and water  
features



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## Southwest Solar Resources

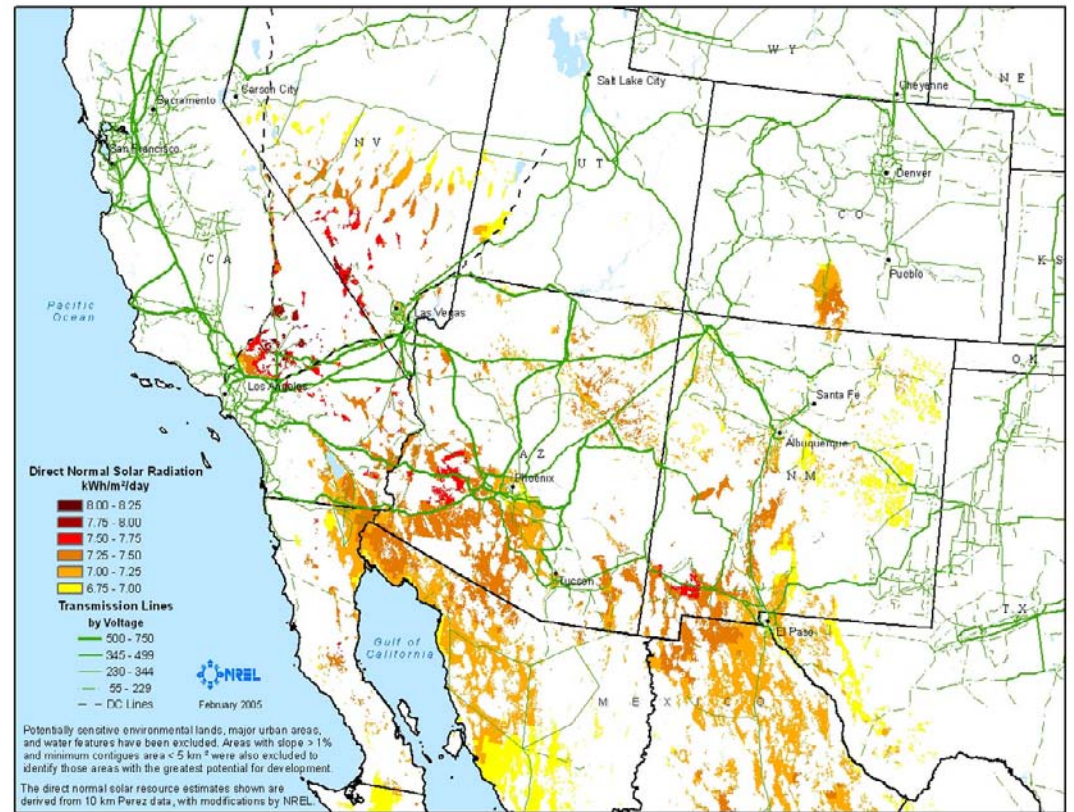
### Transmission Overlay

Eliminate locations  
< 6.75 kwh/m<sup>2</sup>/day

Exclude environmentally  
sensitive lands, major  
urban areas, and water  
features

Remove land areas >  
(3%) & 1% average  
land slope

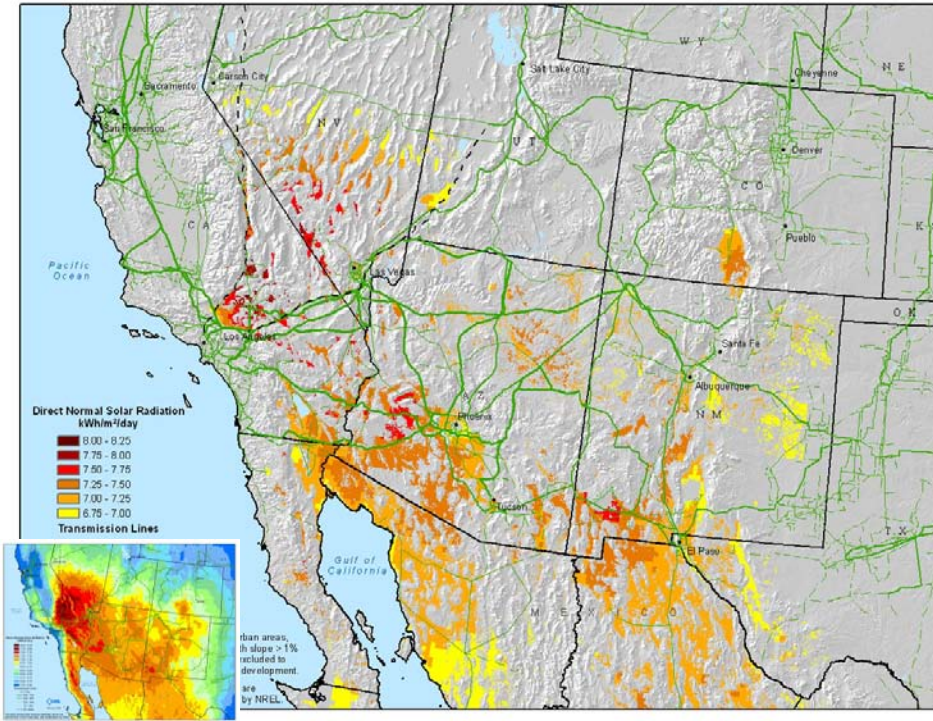
Remove land <5 contiguous km<sup>2</sup>





# SW Solar Energy Potential

State	Land Area (mi <sup>2</sup> )	Solar Capacity (MW)	Solar Generation Capacity GWh
AZ	19,279	2,467,663	5,836,517
CA	6,853	877,204	2,074,763
CO	2,124	271,903	643,105
NV	5,589	715,438	1,692,154
NM	15,156	1,939,970	4,588,417
TX	1,162	148,729	351,774
UT	3,564	456,147	1,078,879
<b>Total</b>	<b>53,727</b>	<b>6,877,055</b>	<b>16,265,611</b>

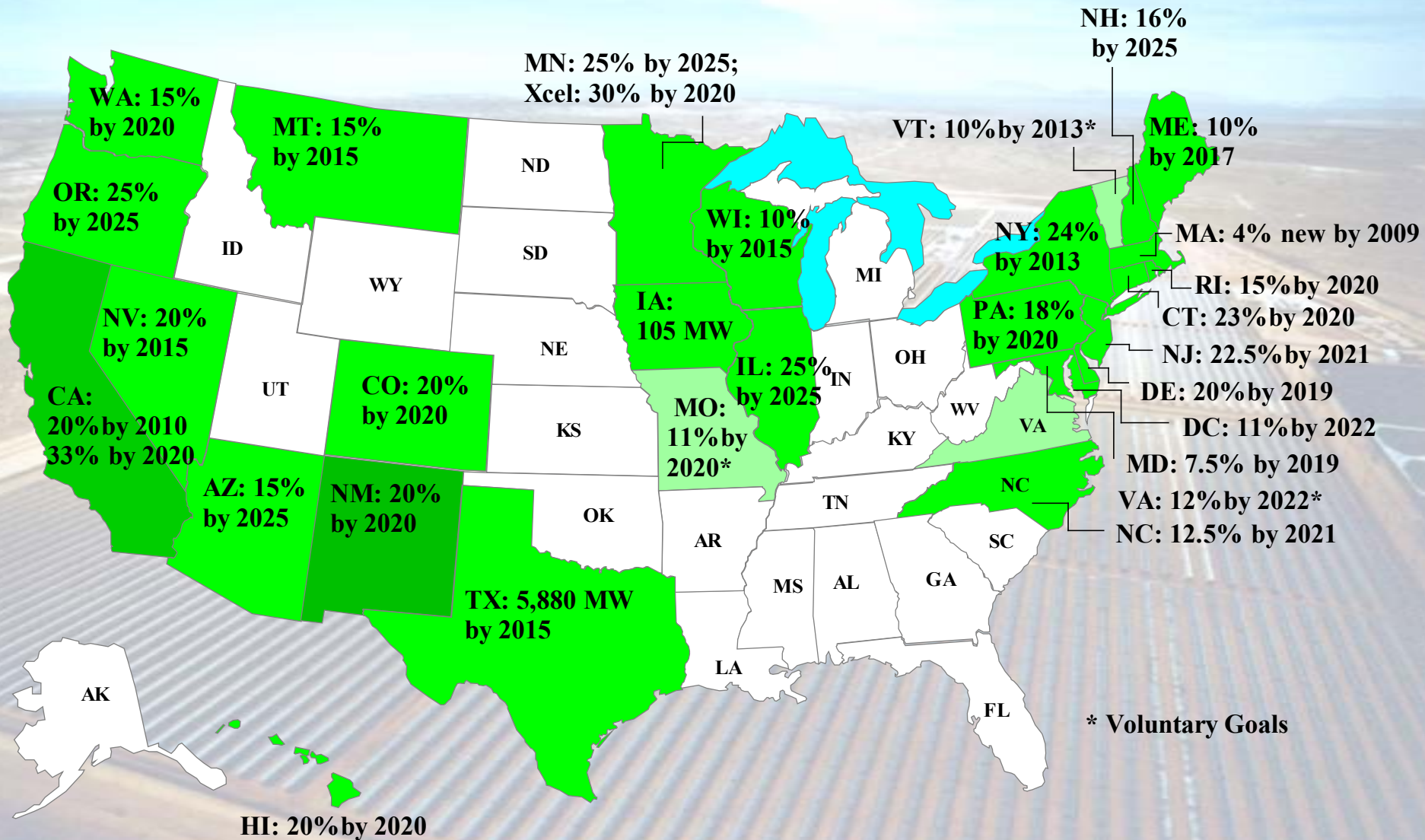


The table and map represent land that has no primary use today, exclude land with slope > 1%, <5 contiguous km<sup>2</sup>, & sensitive lands.

Solar Energy Resource  $\geq 6.75$  kwh/m<sup>2</sup>/day  
 Capacity assumes 5 acres/MW  
 Generation assumes 27% annual capacity factor

- **Current total generation in the U.S. is 1,000GW w/ generation approximately 3,800 TWh**

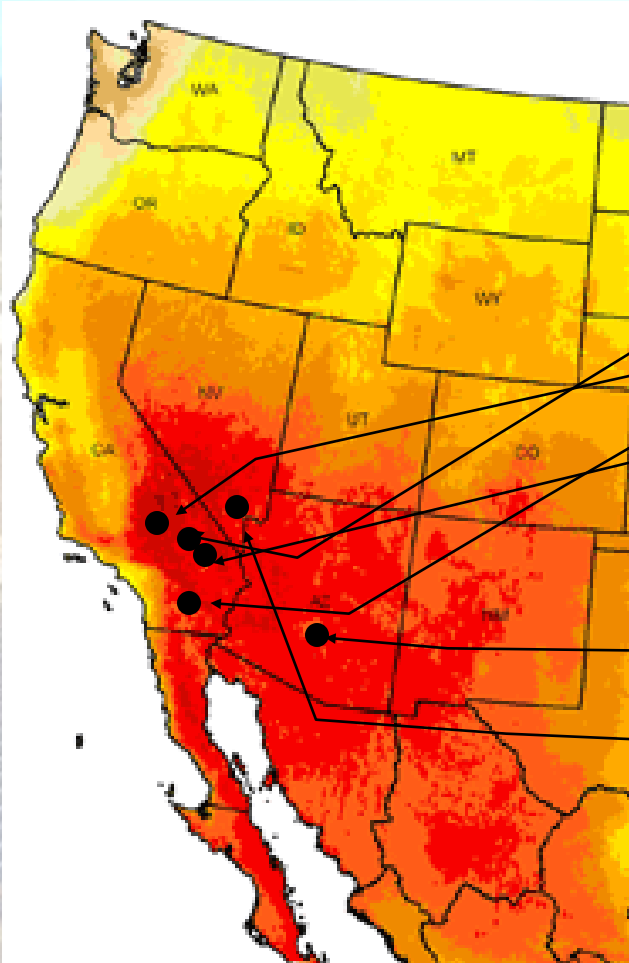
# Renewable Portfolio Standards



State RPS mandates successfully jump-starting desirable growth

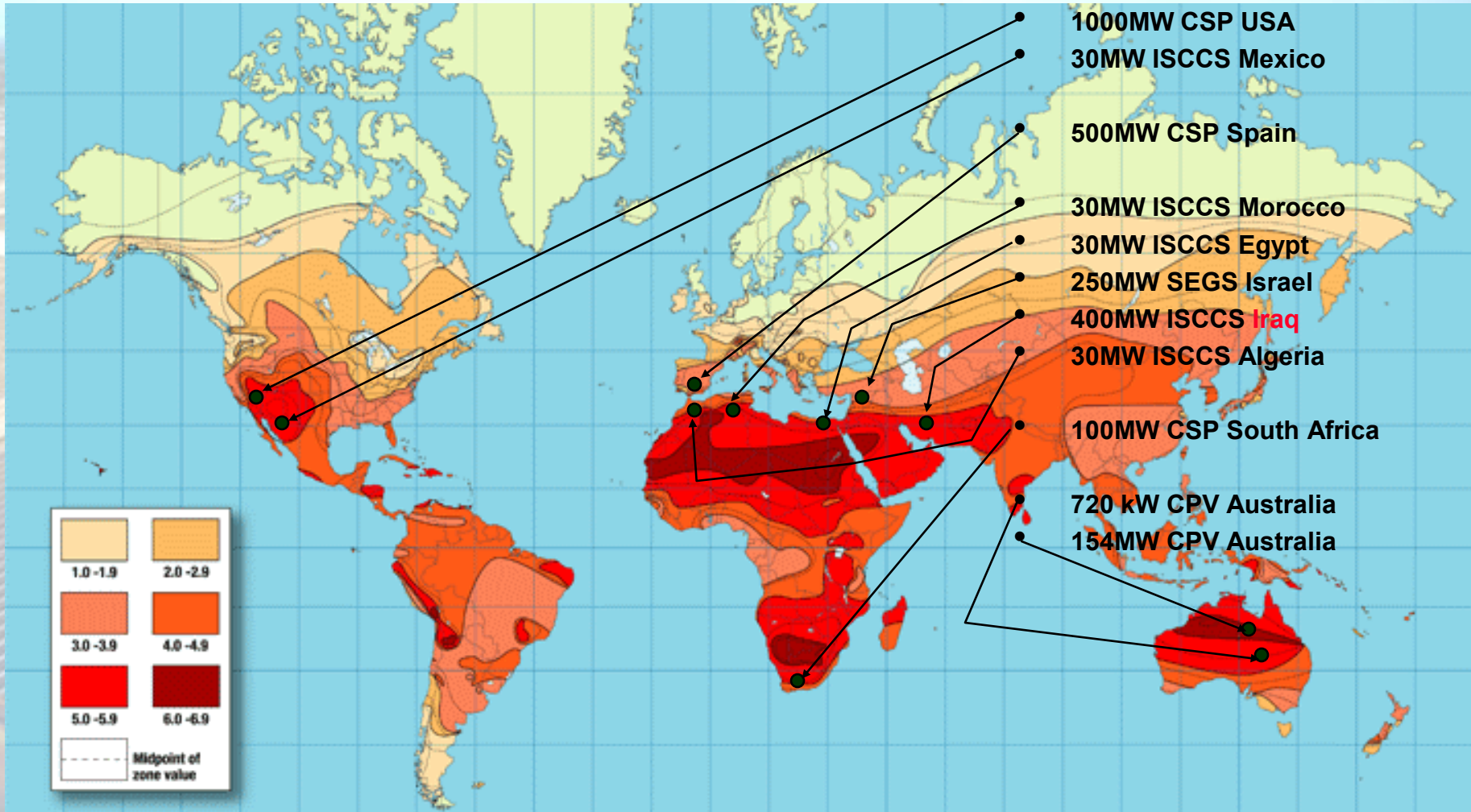
# Market for Solar in US SW

## 10,000 MW of CSP by 2020



- California:
  - 500 MW by 2010
  - 8,000 MW by 2020 –peaking demand
    - 354 MW SEGS trough plants in CA
    - 2 PPAs for 1.75 GW Dish Stirling plants in Southern CA
      - 500 MW (option to expand to 850 MW) – Mojave Desert
      - 300 MW (two options to expand to 900 MW) – Imperial Valley
    - 553 MW PPA signed PGE, CA
    - 300 MW PGE, CA Pending contractual announcement
    - 175 MW PGE/FPL CLFR (commitment)
    - 200 MW FPL CLFR (commitment)
    - 1000 MW PGE (commitment) probably in CA
- Arizona: 2,000 MW
  - 1 MW trough plant in AZ
- Nevada: 1,500 MW
  - 64 MW trough project in NV
- New Mexico: TBD
- West Texas: 1,000 + MW
- Colorado: 500 MW after 2010
  - Numerous RFP's in CO, TX, AZ,
- Florida: 300 MW CLFR (FPL Commitment)
  - 10 MW initial (w/ option to expand to 300 MW)
  - 500 MW FPL (commitment) in CA, FL, & other states

# International CSP Project Developments

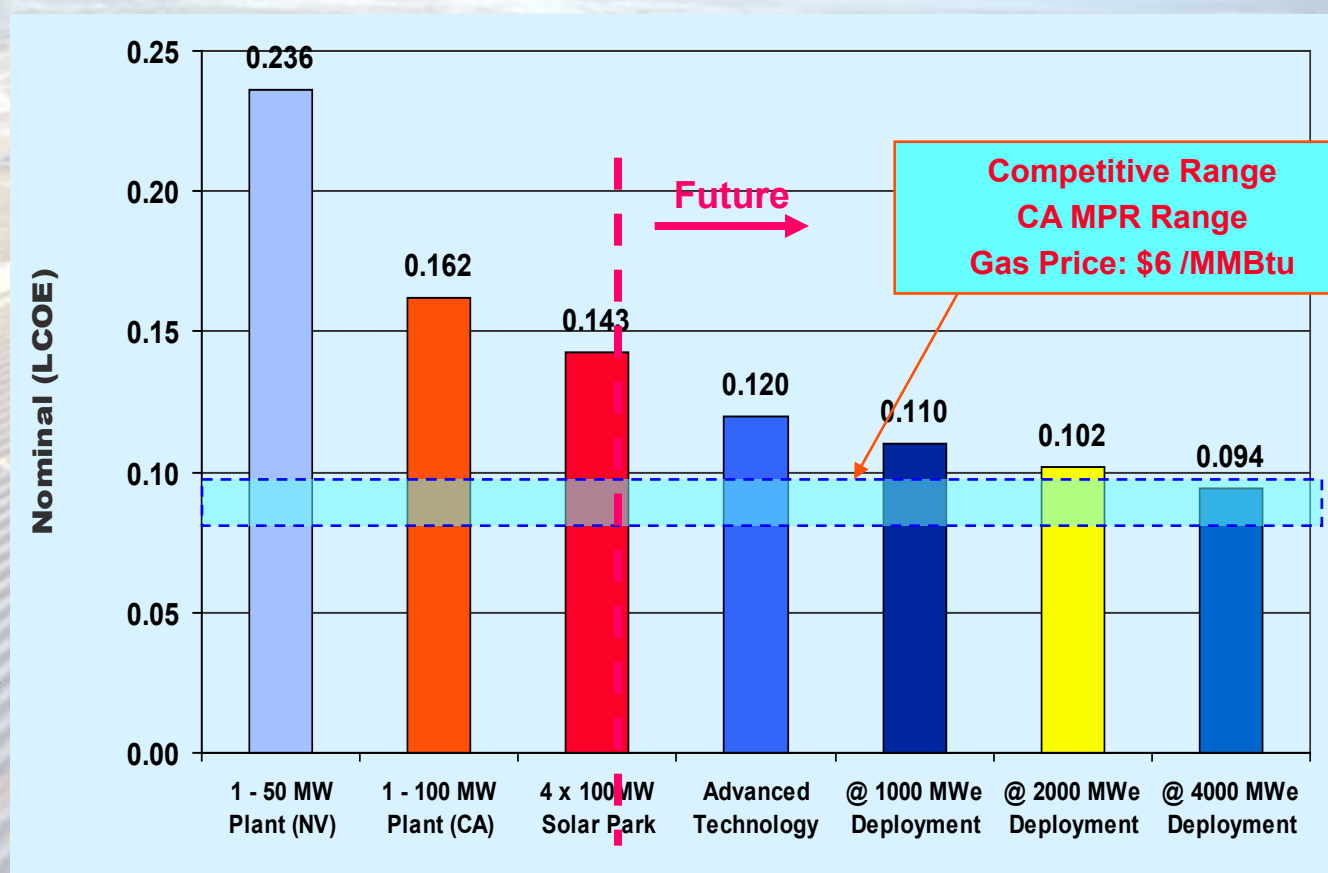


# Parabolic Trough Plants



# Parabolic Trough Cost Reduction Scenario

- Good Solar Resource Site
- Advanced Technology
- Learning & Competition
- Increasing Plant Size
- Alternative Financing
- Tax Neutrality for Solar Fuels
- Tax Incentives

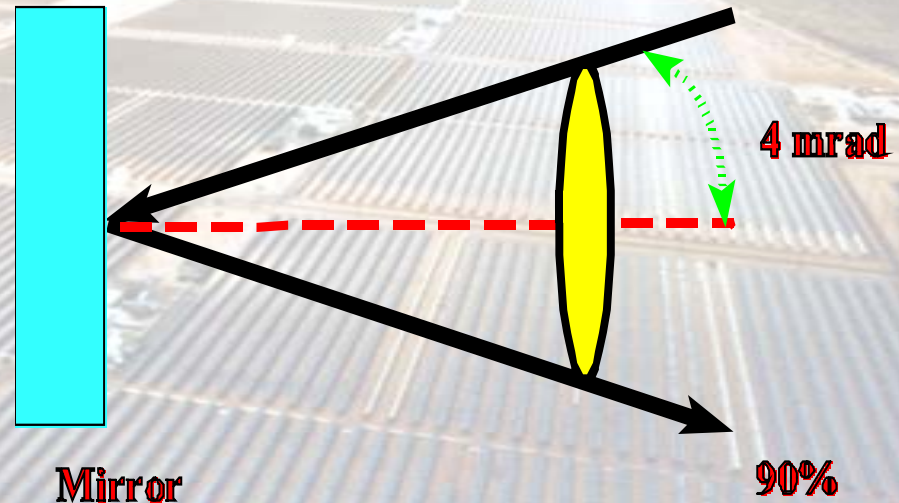


Location: Barstow, CA  
 Incentives: Current California  
 Deployment Assumes:  
 - 90% PR in Solar Field  
 - 95% PR in Power Plant

# Goals for Improved Optical Materials



- >90% Specular reflectance into a 4-mrad cone angle
  - Unofficially 95%
- 10 - 30 year lifetime
  - Unofficially 30 y
- Manufacturing cost \$10.76/m<sup>2</sup> (\$1/ft<sup>2</sup>)
  - 1992 Cost Goal
  - Adjusted for inflation to \$15.46/m<sup>2</sup> (\$1.44/ft<sup>2</sup>)
  - Structural (self-supporting) mirror to \$27/m<sup>2</sup> (\$2.50/ft<sup>2</sup>)



# Technical Approach

- **Samples supplied by:**

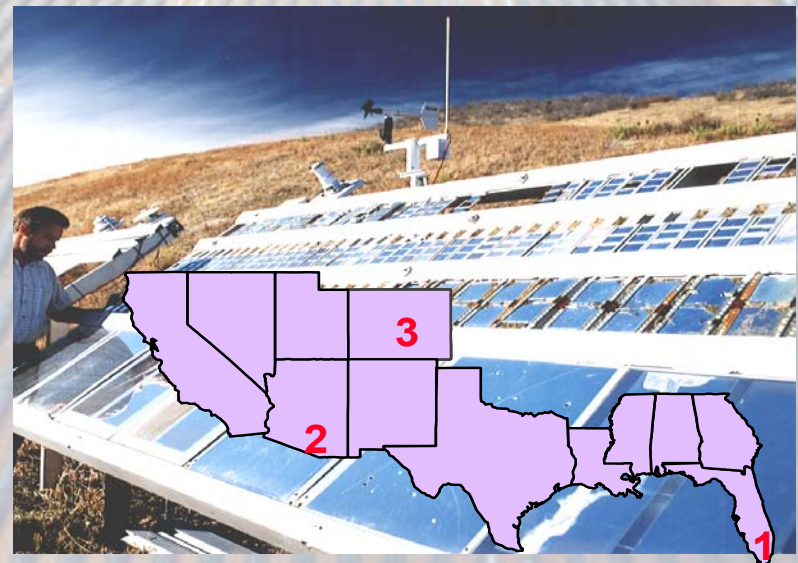
- Industry
- Subcontracts
- Developed in-house

- **Optical Characterization:**

- Perkin-Elmer (PE) Lambda 9 & 900 UV-VIS-NIR spectrophotometers (250-2500 nm) w/ integrating spheres
- PE IR 883 IR spectrophotometer (2.5-50  $\mu\text{m}$ )
- Devices & Services (D&S) Field Portable Specular Reflectometer (7, 15, & 25-mrad cone angle at 660 nm)

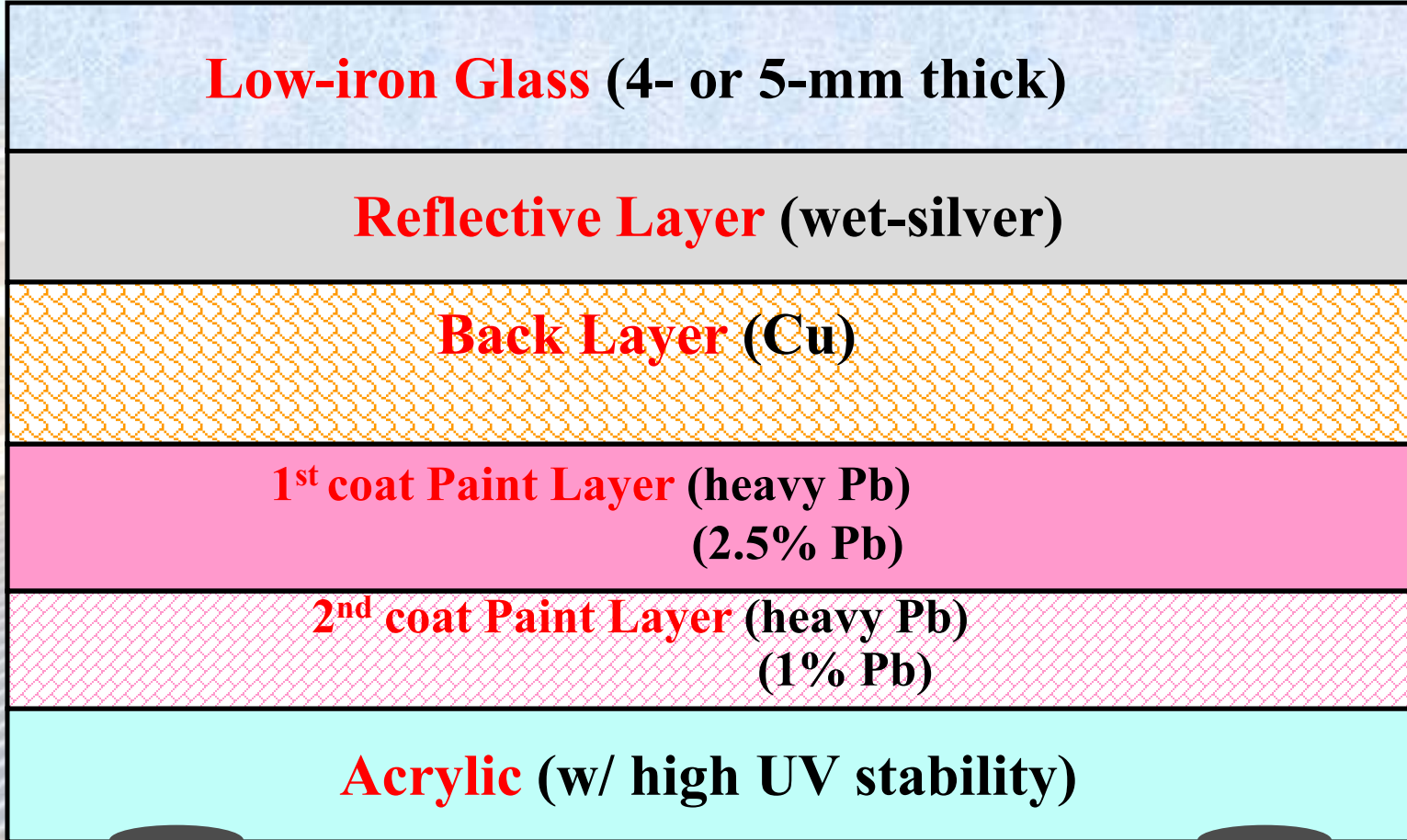
- **Outdoor (OET) & Accelerated Exposure Testing (AET):**

- Atlas Ci65 & Ci5000 WeatherOmers (WOM) (1X & 2X Xenon Arc/60°C/60%RH)
- QPanel QUV (UVA 340@ 290- 340 nm/ 4 h UV at 40° / 4 h dark at 100%RH)
- 1.0 & 1.4 kW Solar Simulators (SS) ( $\approx$ 5X Xenon 300-500 nm. 1.0-kW SS 80°C/ 80% RH, 1.4 kW-SS-4 quadrants 2 RH &T, light /dark)
- BlueM damp heat (85°C/85%RH/dark)
- 3 meteorologically monitored sites at Golden, Colorado (NREL), Miami, Florida (FLA), and Phoenix, Arizona (APS)





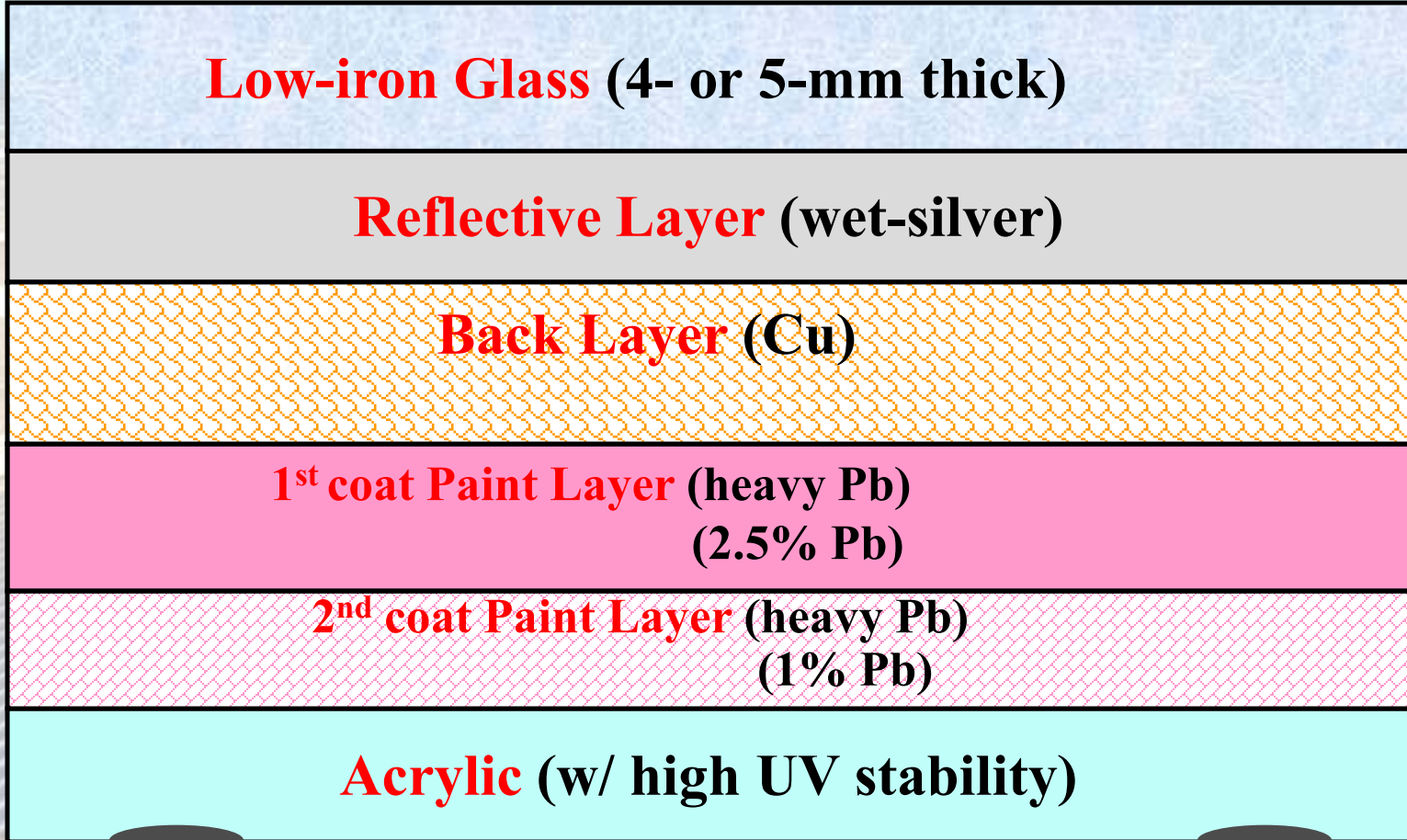
# Parabolic Trough Glass Mirror Architecture



Thick glass is slumped  
Flabeg mirrors still use Cu back protection  
Three-coat paint system designed for outdoor applications,  
Mactac adhesive  
Ceramic pad



# Parabolic Trough Glass Mirror Architecture

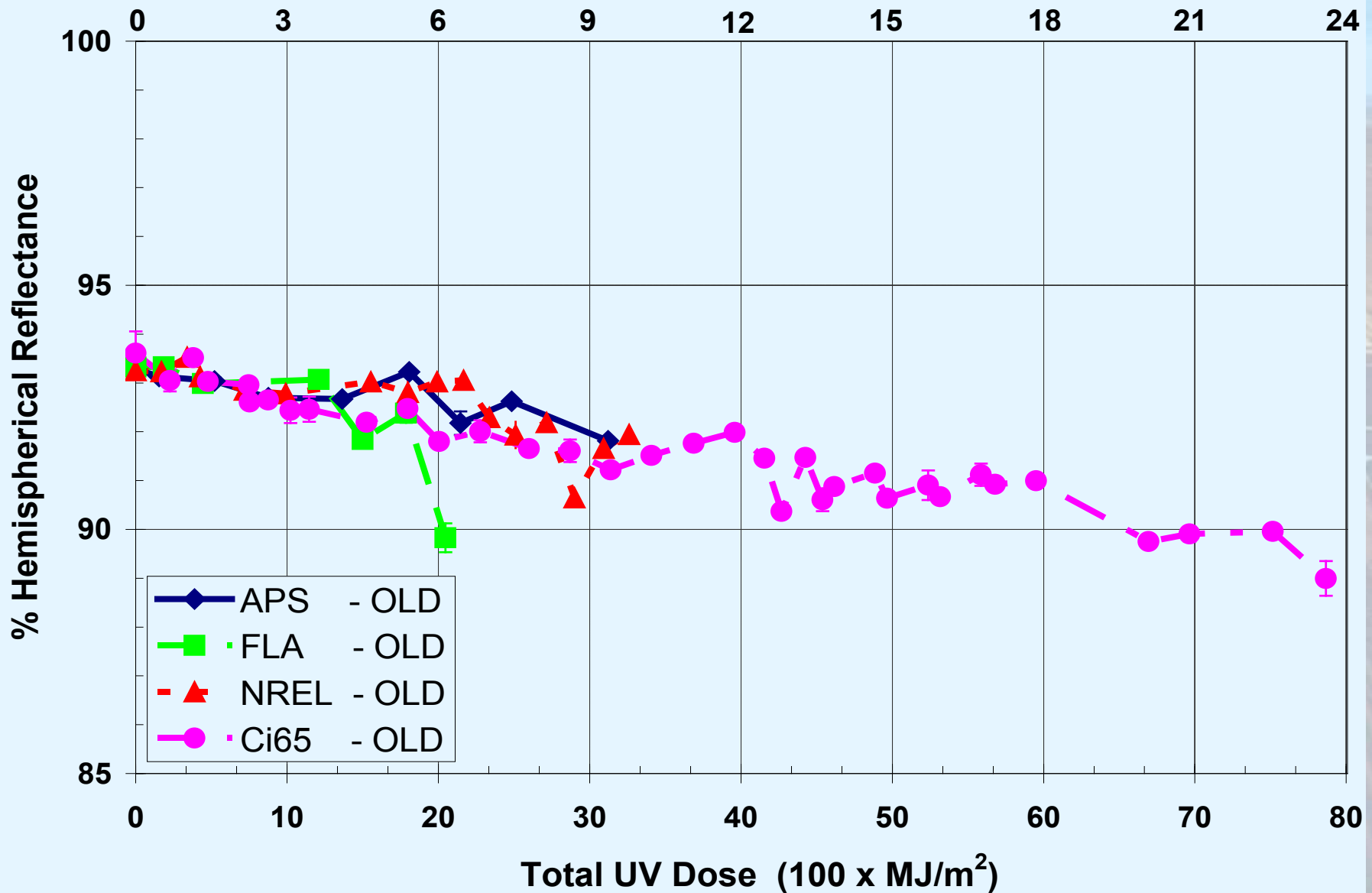


Thick glass is slumped  
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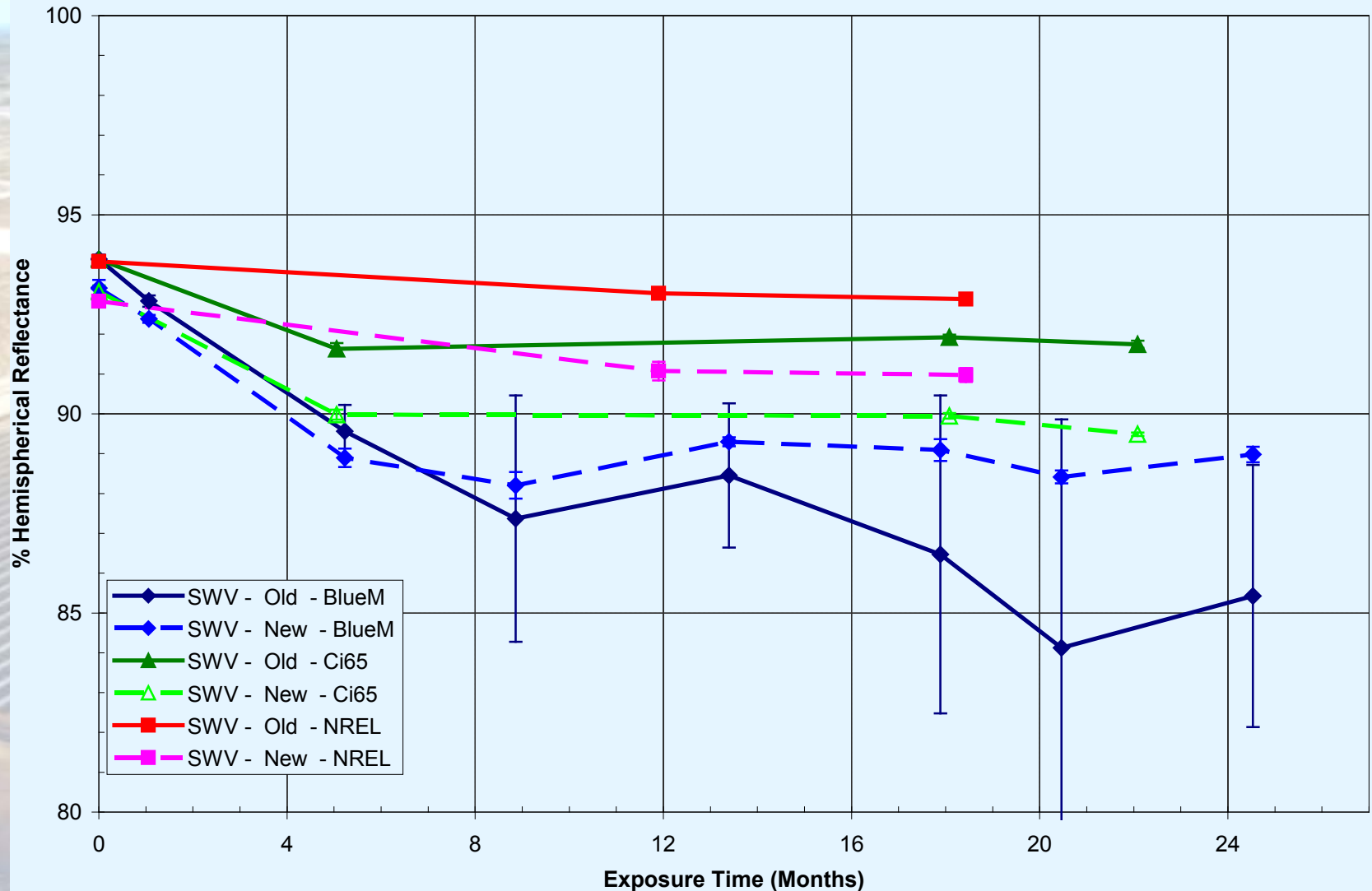
# Original Flabeg Mirror

Equivalent NREL Exposure Time (years)



# Original vs. New Flabeg Mirror

% Hemispherical Reflectance of Old Flabeg (w/Cu & Pb paint) vs New Flabeg (w/ Cu & low-Pb paint) Mirrors as a function of accelerated exposure in Ci65 WOM (65°C/65%RH/~3sun light exposure) and BlueM (85°C/85%RH/dark), and outdoors in Colorado



# Alternate Thick Glass Mirror Architecture

**Low-iron Glass** (3- or 4-mm thick flat)

**Reflective Layer** (wet-silver)

**Back Layer** (Cu-less)

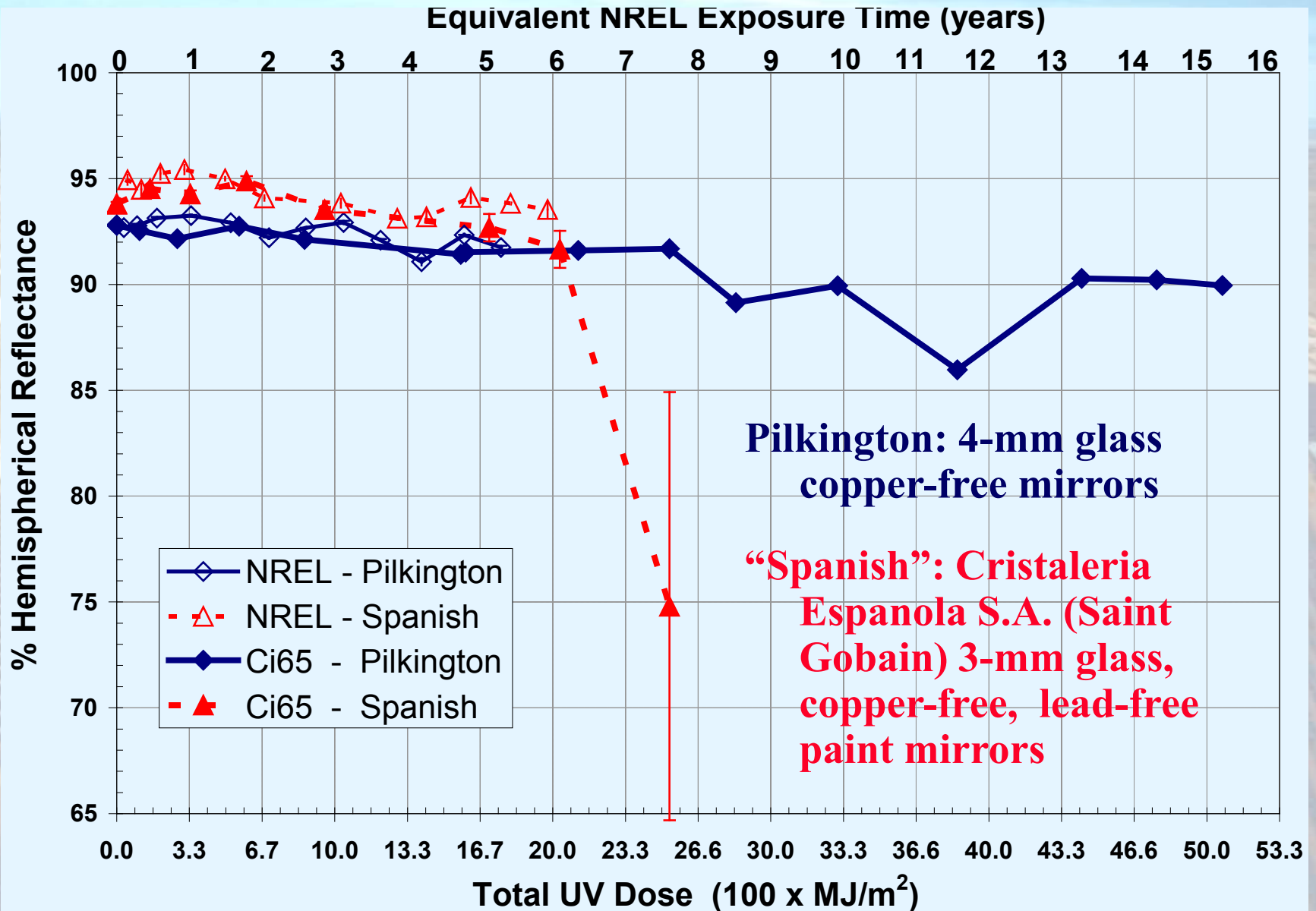
**1<sup>st</sup> coat Paint Layer** (lead-free <0.15% Pb)

**2<sup>nd</sup> coat Paint Layer** (lead-free <0.15% Pb)

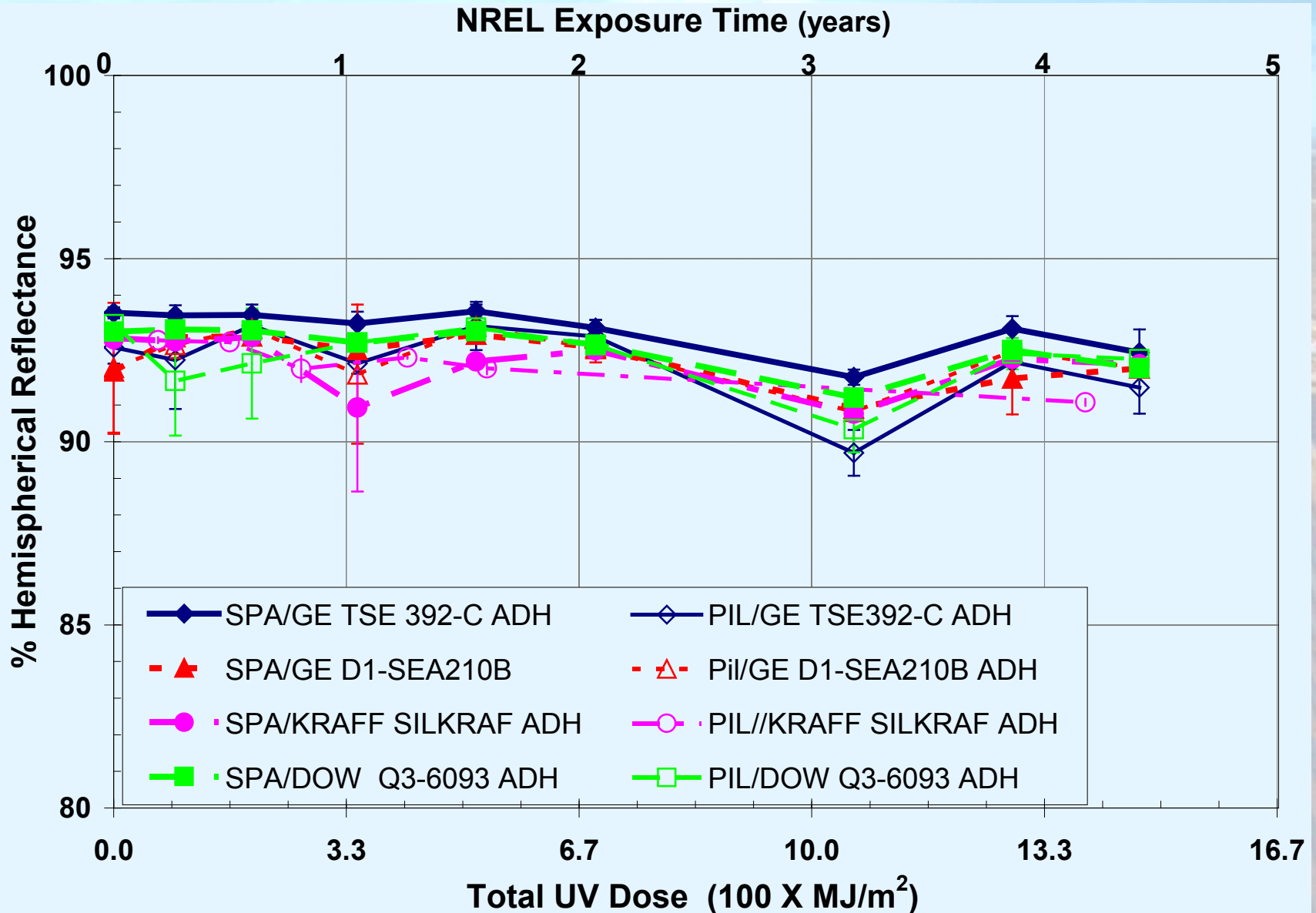
**Adhesive** (PS, spray)

**Substrate** (SS, Al)

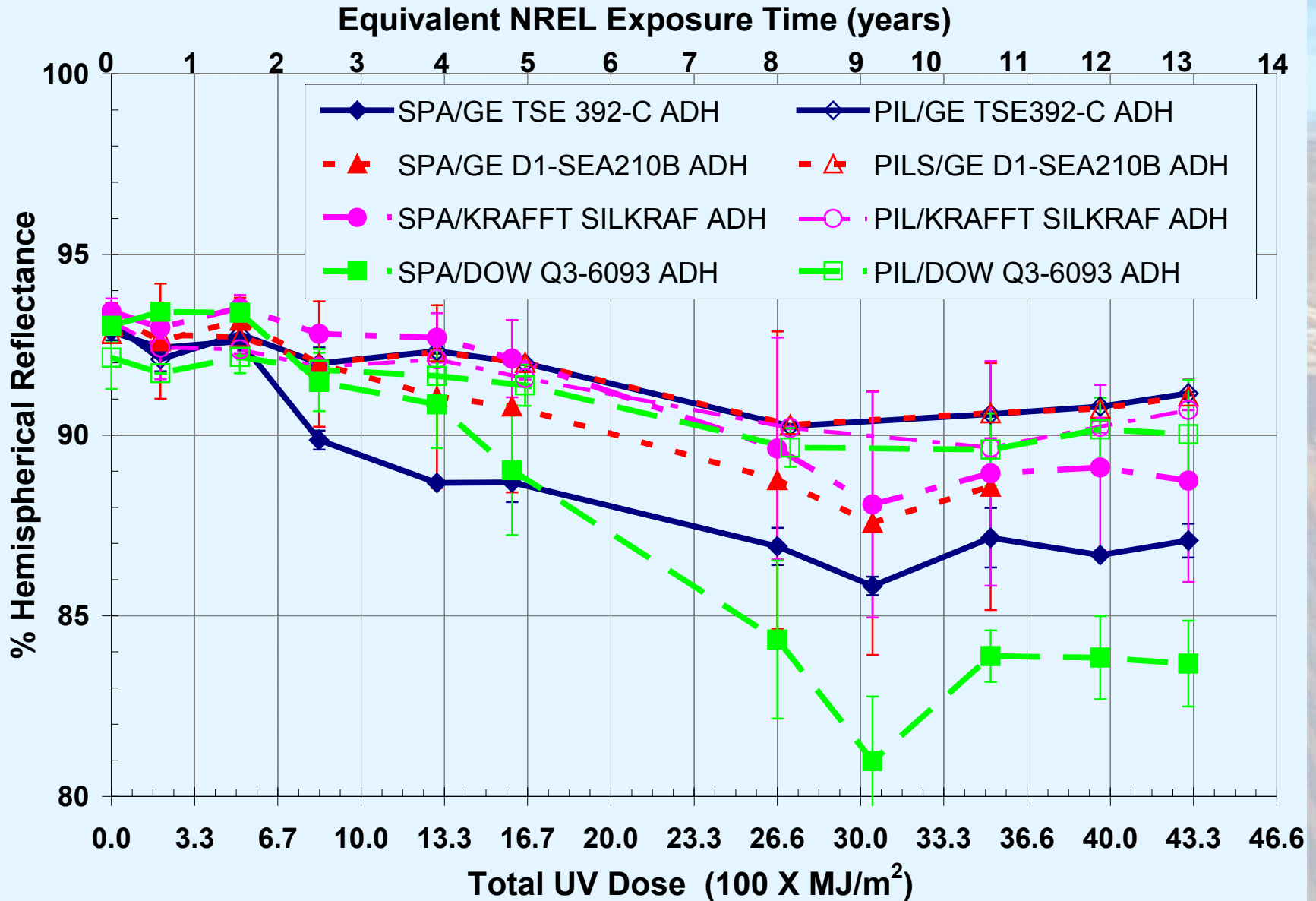
# Alternate Thick Glass Mirror



# Effect of Adhesive on Thick Glass Mirror

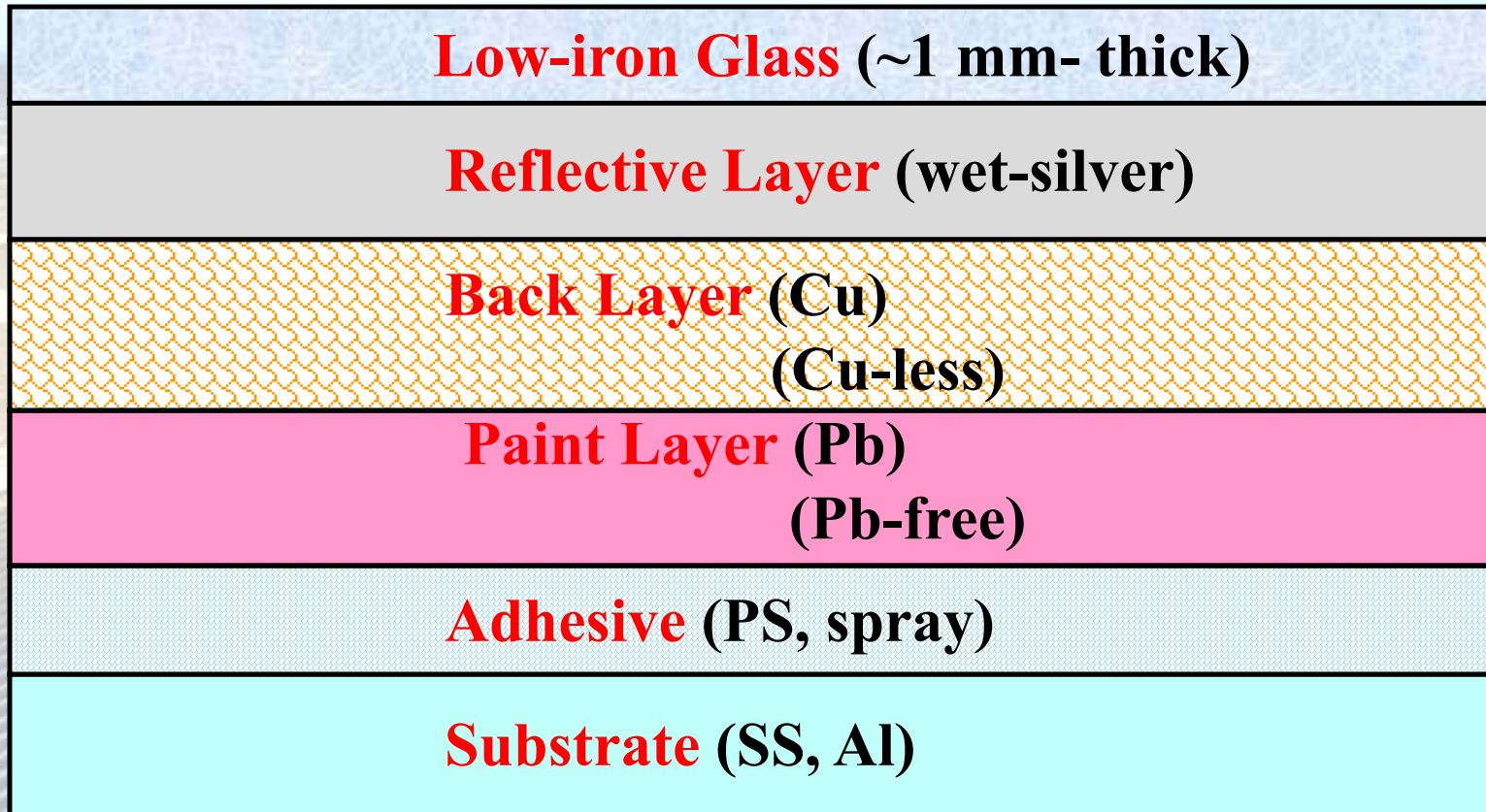


# Effect of Adhesive on Thick Glass Mirror



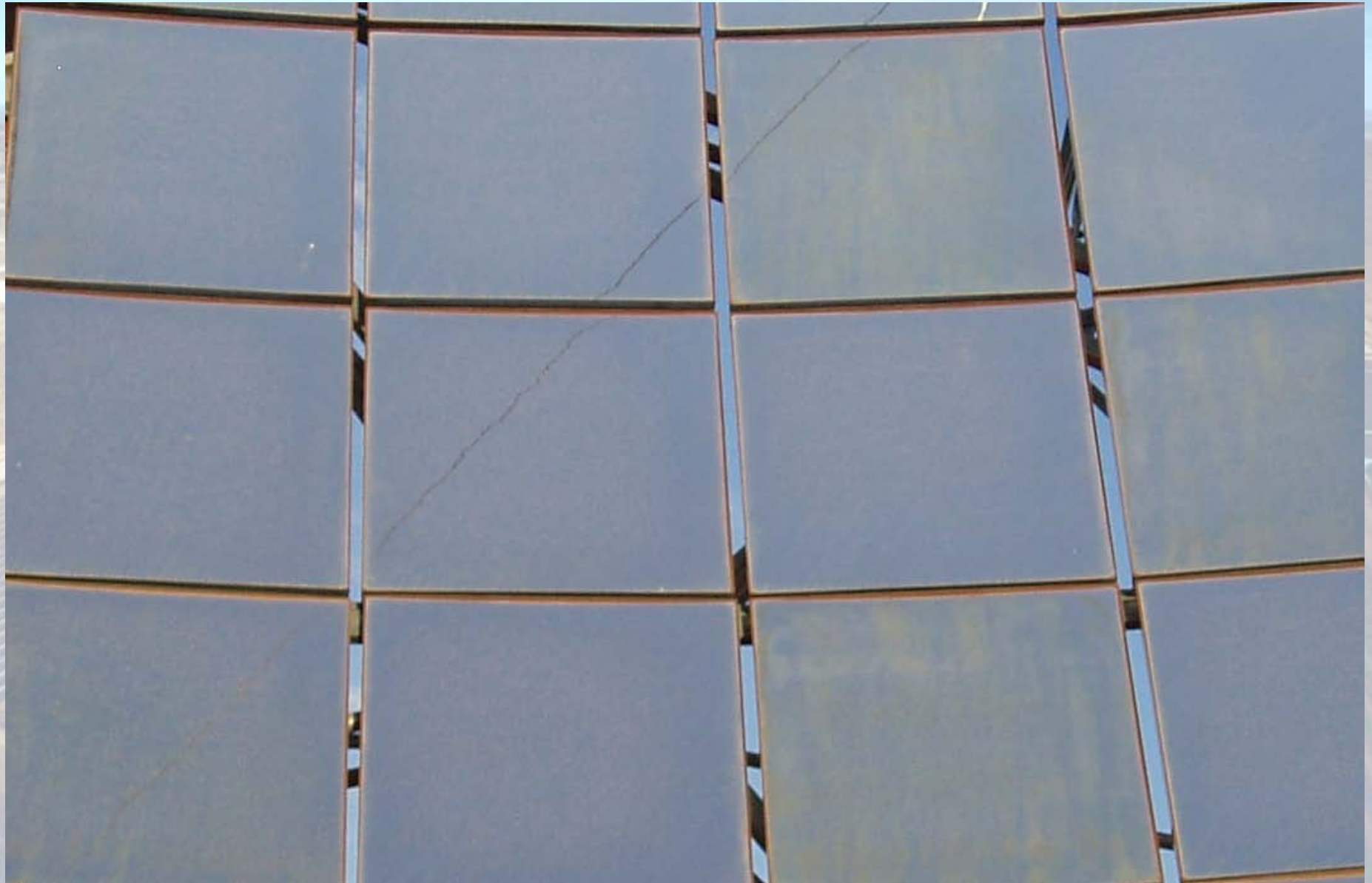


# Thin Glass Mirror Architecture



**Thin glass mirrors are designed for indoor applications.**

# Thin Glass Corrosion



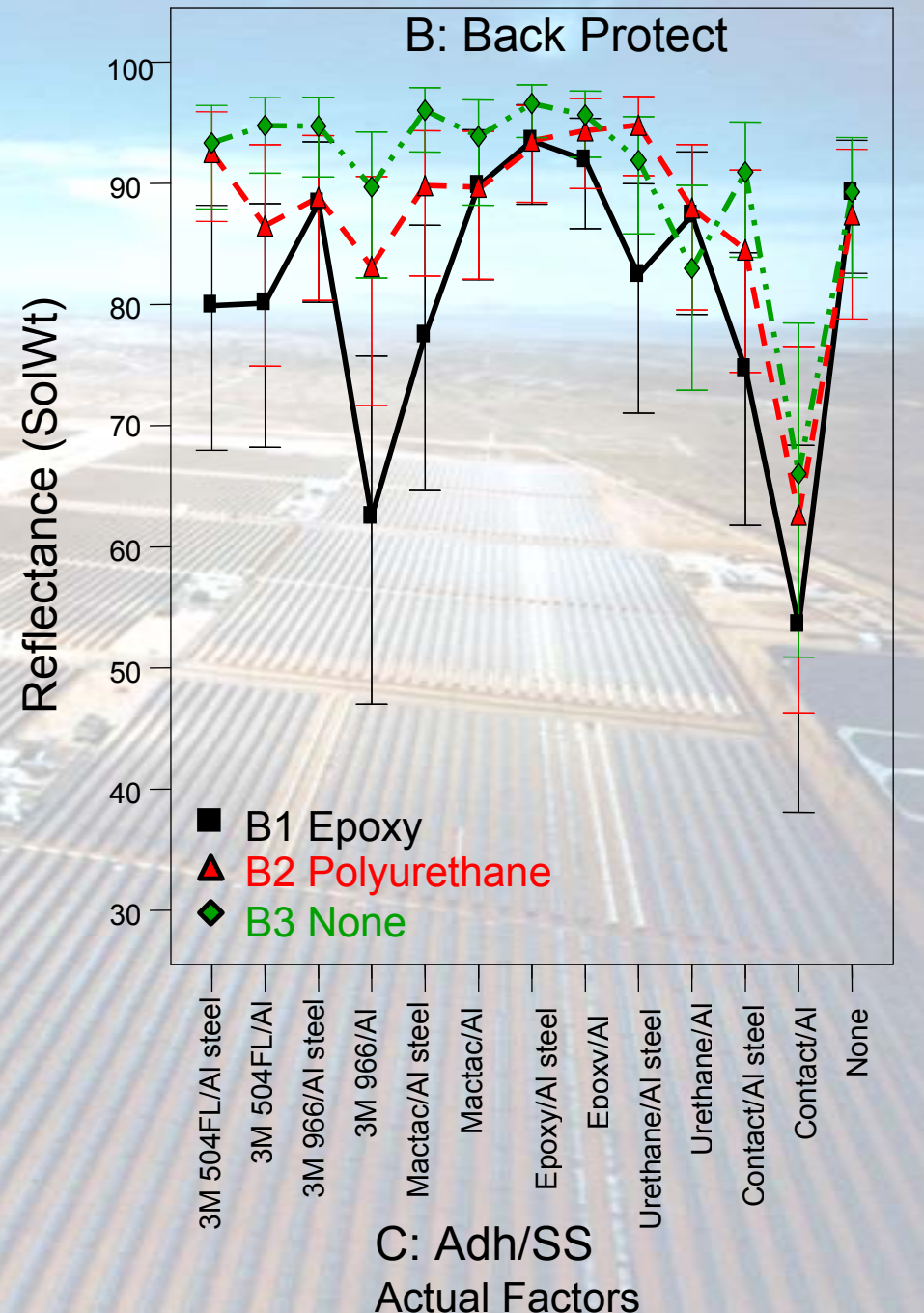
# Thin Glass Mirror Matrix

D-optimal fractional factorial algorithm using Design-Expert® software

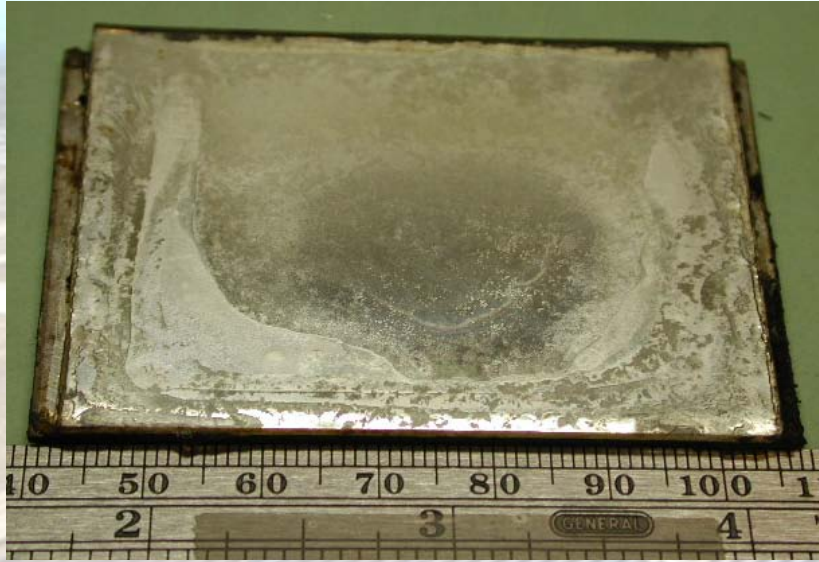
Levels	Factors					
	Mirror Type	Back Protection	Adhesive / Substrate	Edge Protection	Substrate Cleaning	Back Priming
1	Naugatuck/Cu	Epoxy	3M504FL/AL steel	None	SAIC	3M
2	Naugatuck/ No Cu	Polyurethane	3M504FL/AL	Exuded Adh.	SES	None
3	Glaverbel	None	3M966/AL steel	CPFilm		
4			3M966/AL			
5			Mactac/AL steel			
6			Mactac/AL			
7			Epoxy/AL steel			
8			Epoxy/AL			
9			Urethane /AL steel			
10			Urethane /AL			
11			Contact /AL steel			
12			Contact /AL			
13			None			

# ANOVA Analysis

- Glaverbel - best overall mirror in Mirror matrix test
  - Commercial vs. prototype
  - 1- vs. 2-coat paint system
  - Difference in EU and US lead-free regulations
- Epoxy-based adhesive – probably good choice
- No additional back protection - survive the longest
- Polyurethane – poor choice
- BlueM - more accelerated exposure chamber

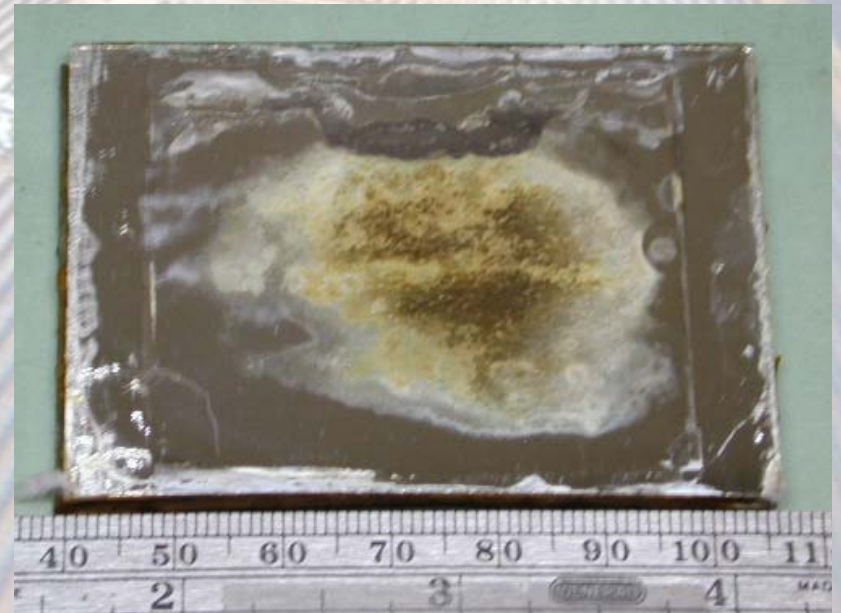


# Damp-Heat results similar but ~6X faster than Ci5000



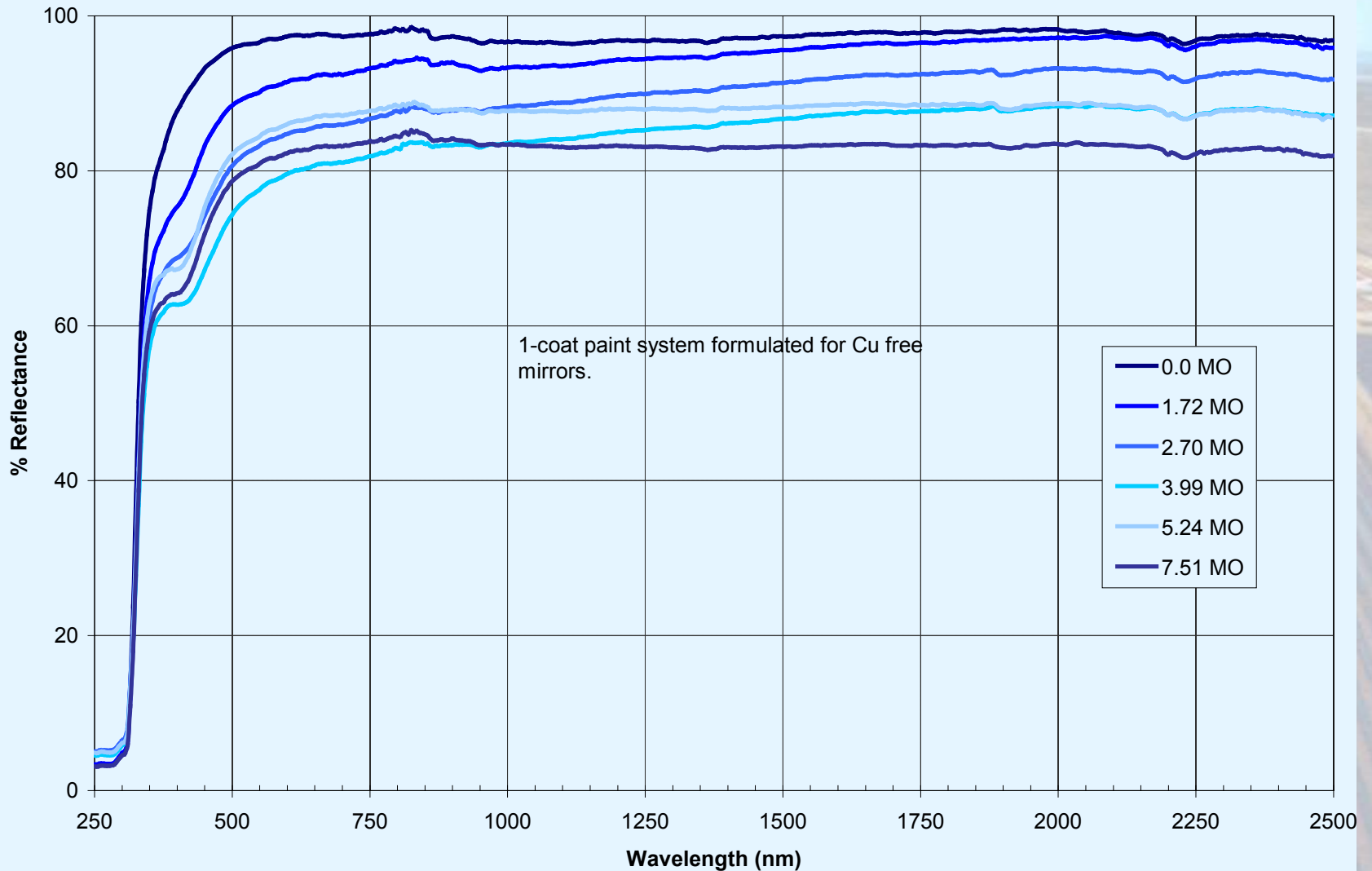
**Discontinued in  
Damp-Heat 5.9 MO**

**Discontinued in  
Ci5000 18.9 MO**

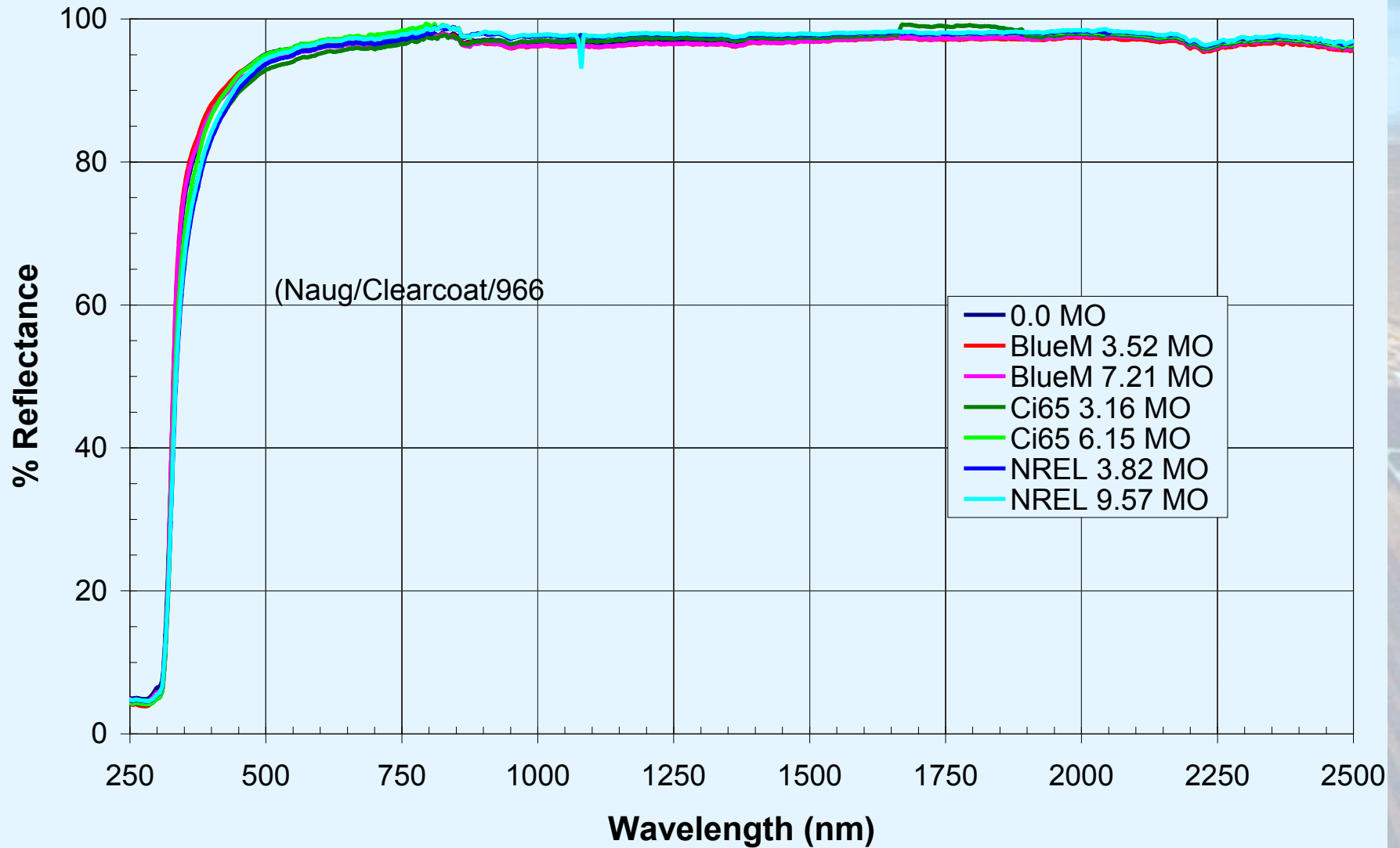


# Thin Glass Mirror

Spectral Reflectance of Naugatuck copperless mirrors with 1 coat paint system after accelerated exposure in Blue M (dark / 85°C / 85%RH) chamber



# Thin Glass Mirror



# Aluminized Reflector Architecture

**Protective Overcoat**

**Protective Oxide Topcoat**

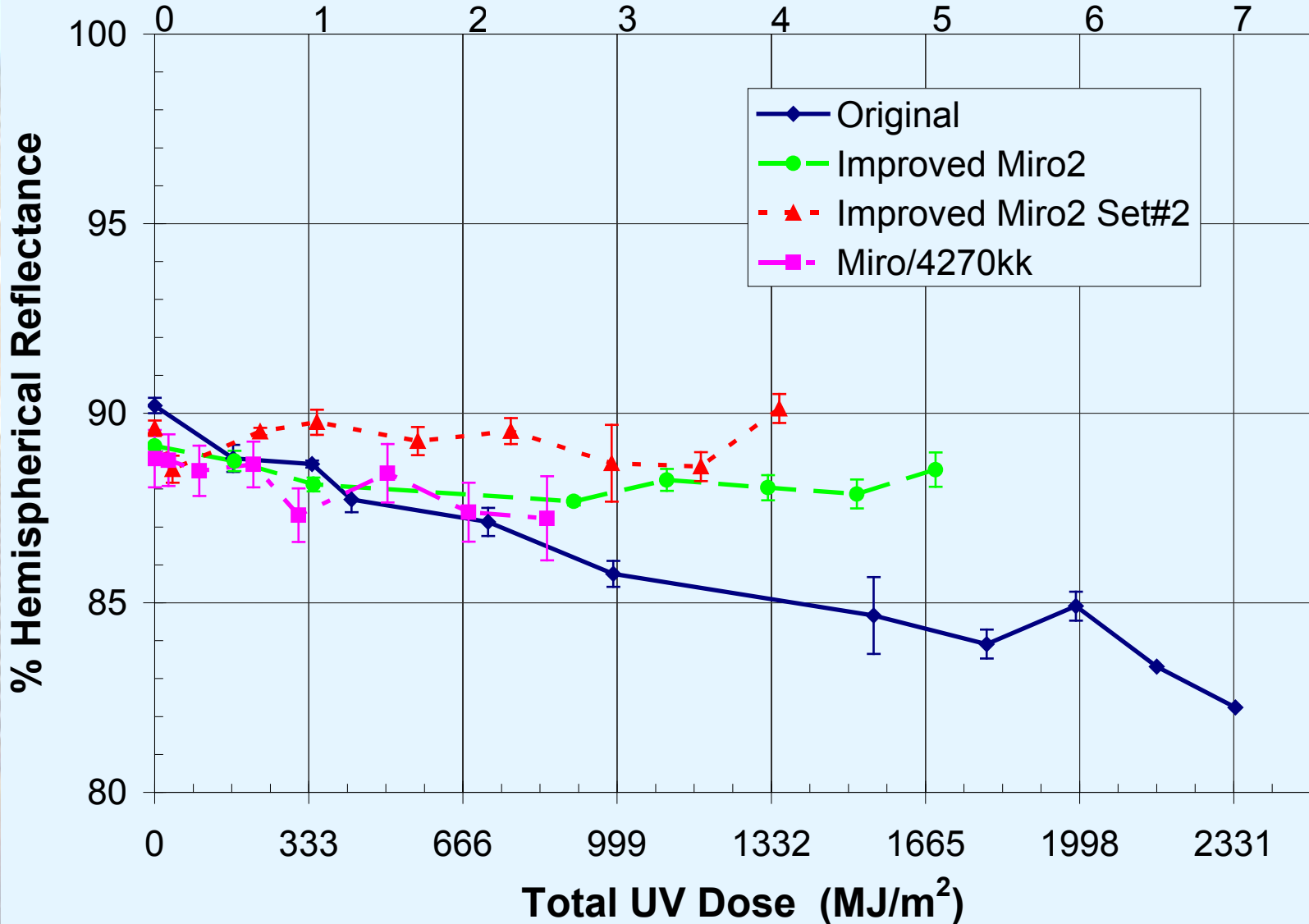
**Enhanced Al Reflective Layer**

**Polished Aluminum Substrate**



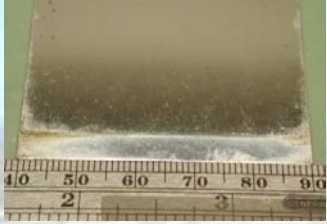
# Aluminized Reflectors

NREL Exposure Time (y)



# Aluminized Reflector Specularity

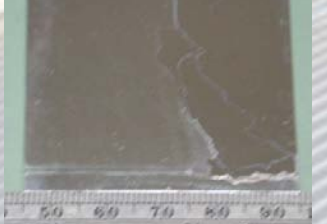
FLA 11.8 m



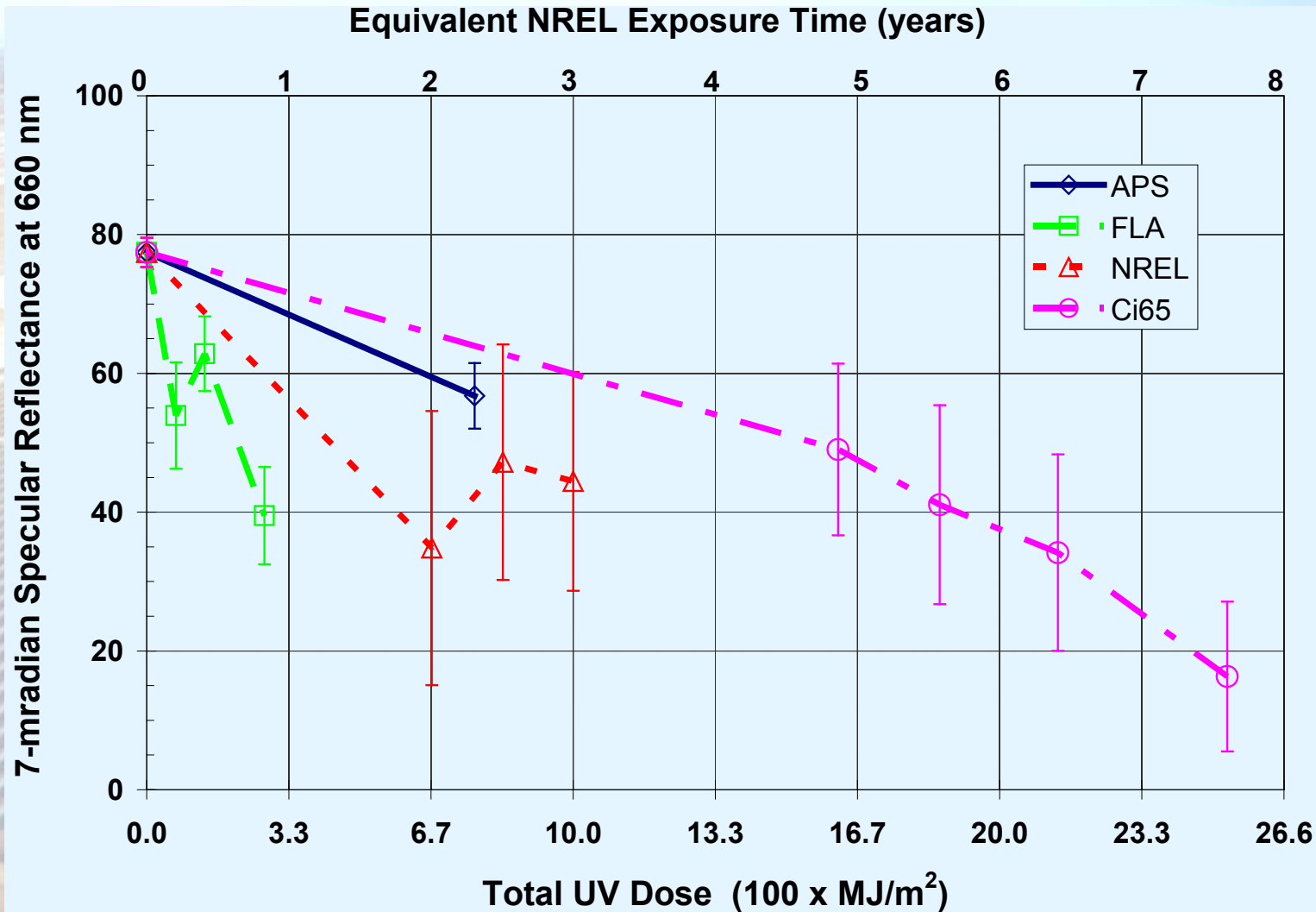
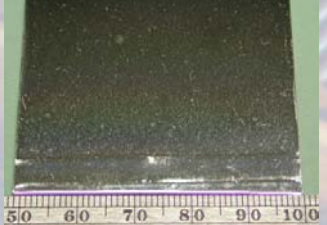
NREL 11 m



APS 27.7 m

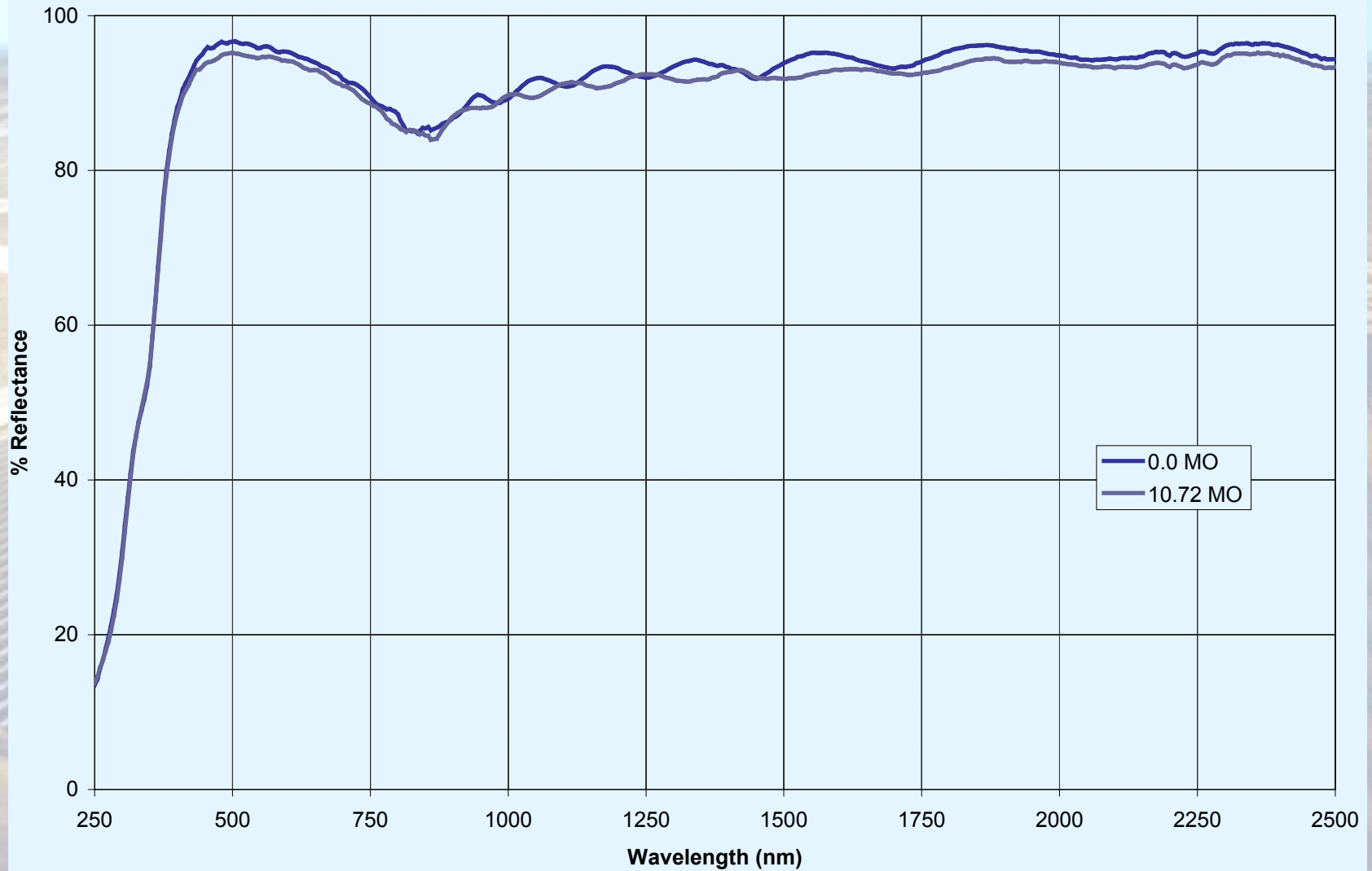


WOM 10.2 m



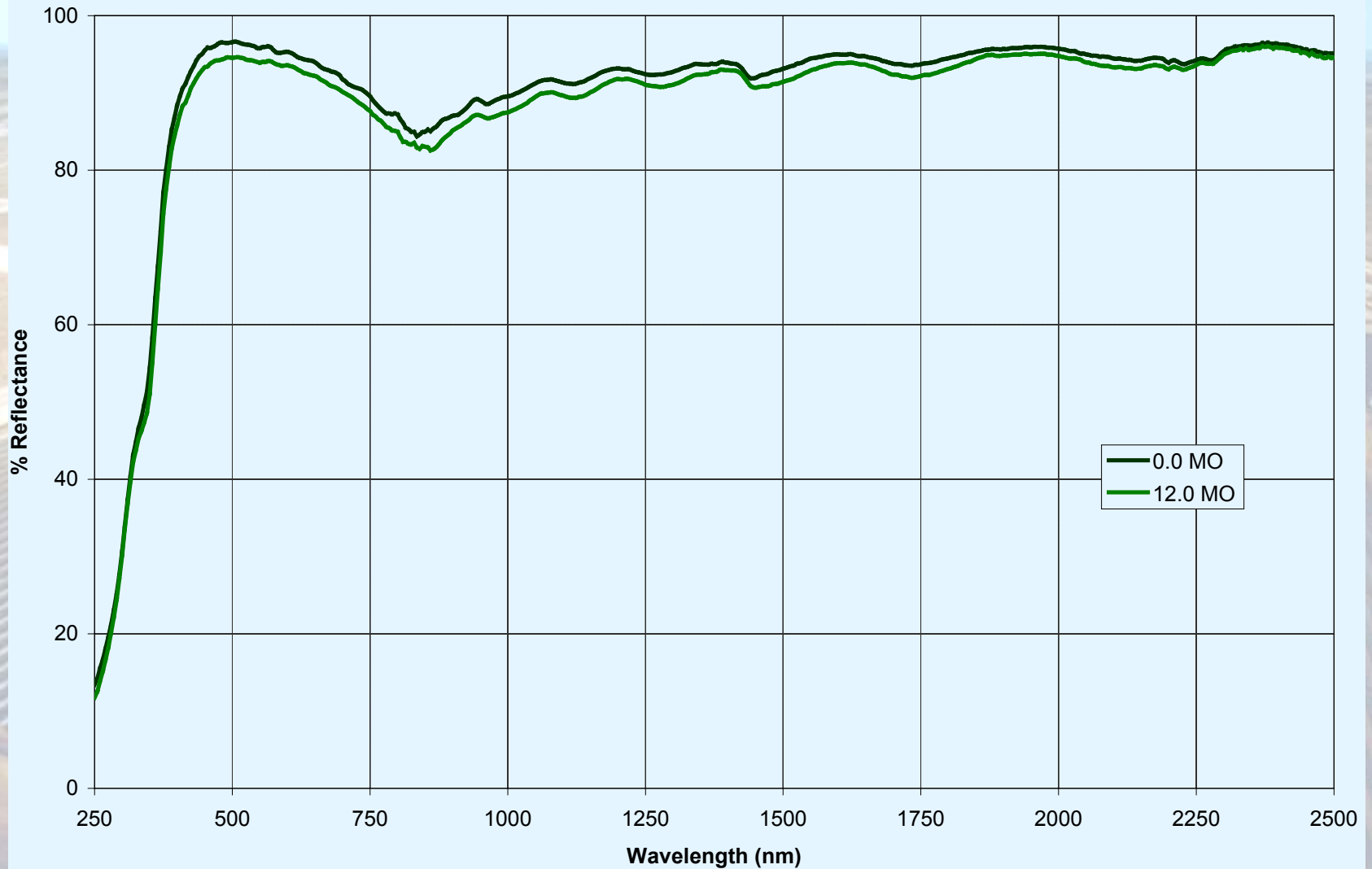
# Aluminized Reflector

Spectral Reflectance of Alanod MiroSun mirrors after outdoor exposure in Phoenix, AZ at APS



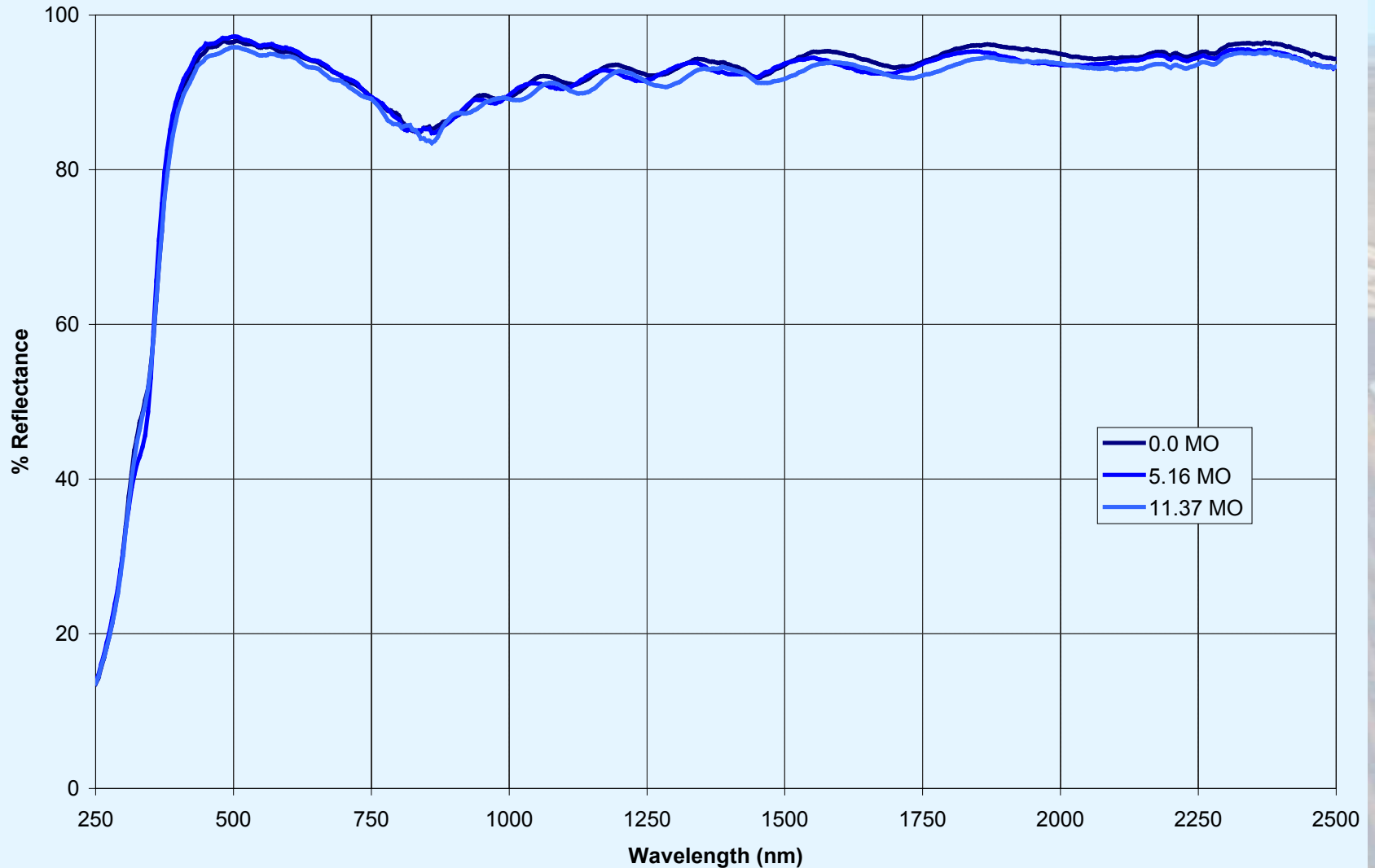
# Aluminized Reflector

Spectral Reflectance of AlanoD MiroSun mirrors after outdoor exposure in Miami, FL at FLA



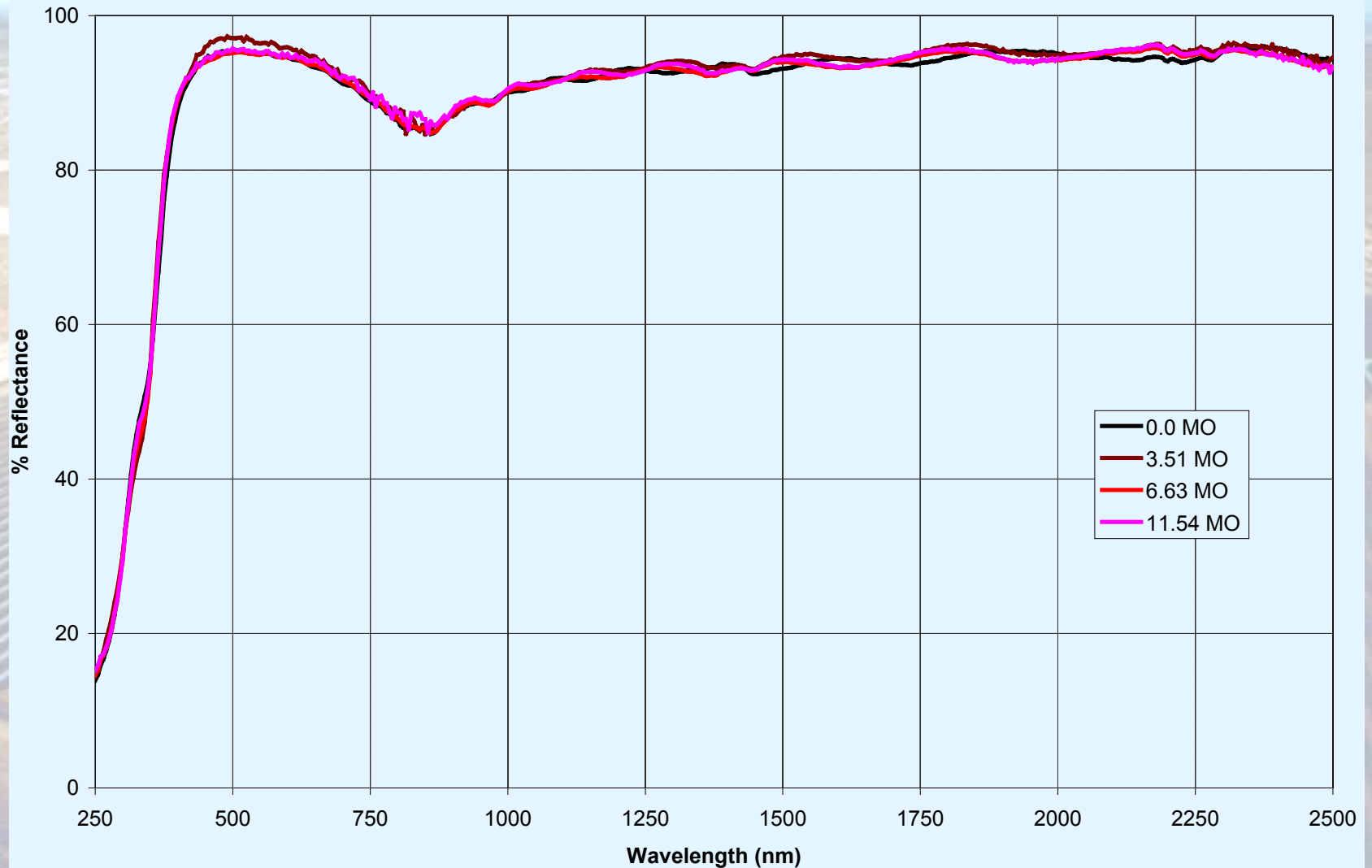
# Aluminized Reflector

Spectral Reflectance of Alanod MiroSun mirrors after outdoor exposure in Golden, CO at NREL



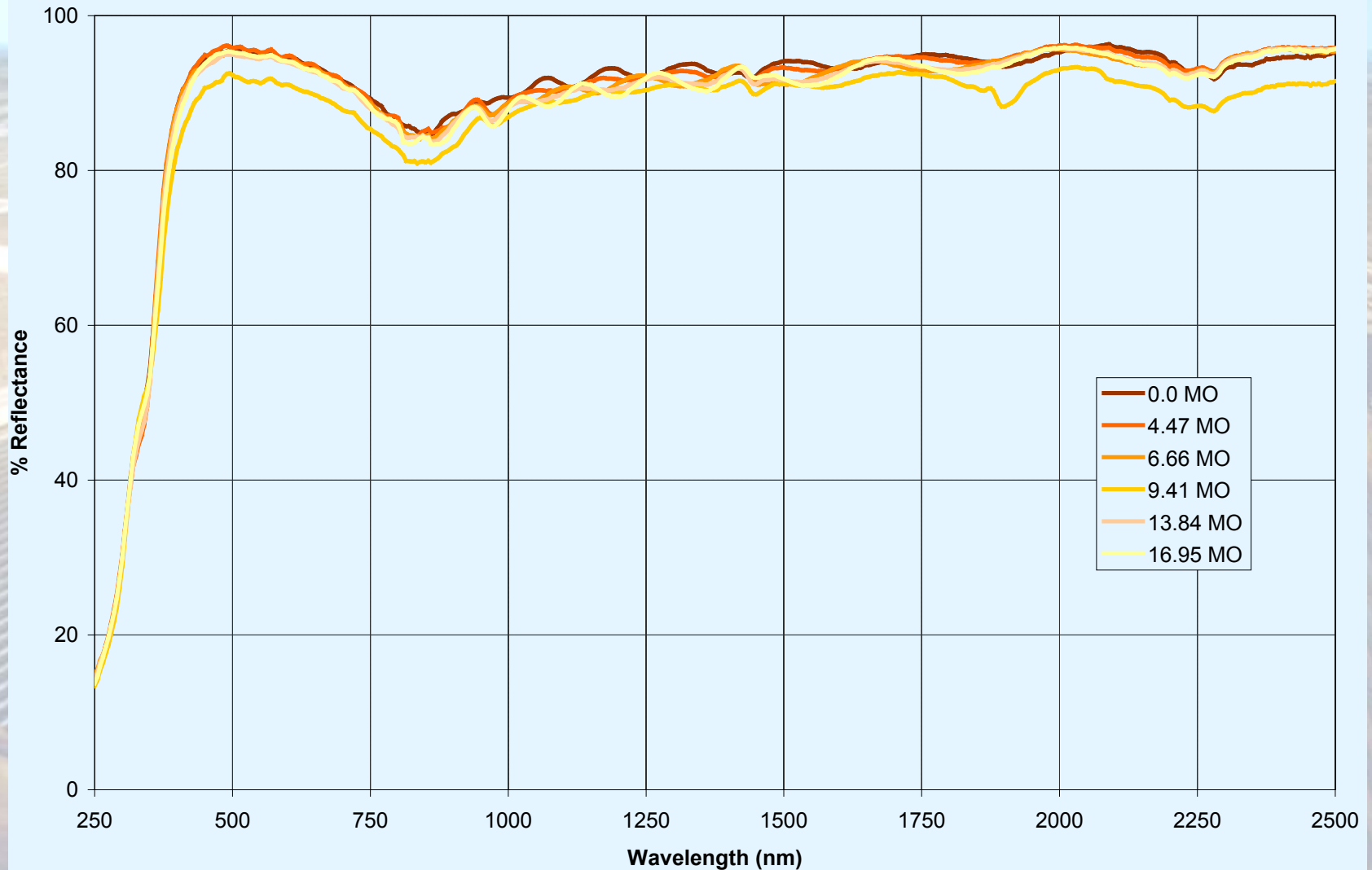
# Aluminized Reflector

Spectral Reflectance of Alanod MiroSun mirrors after accelerated exposure in Ci65 WOM  
(1 sun / 60°C / 60%RH) chamber



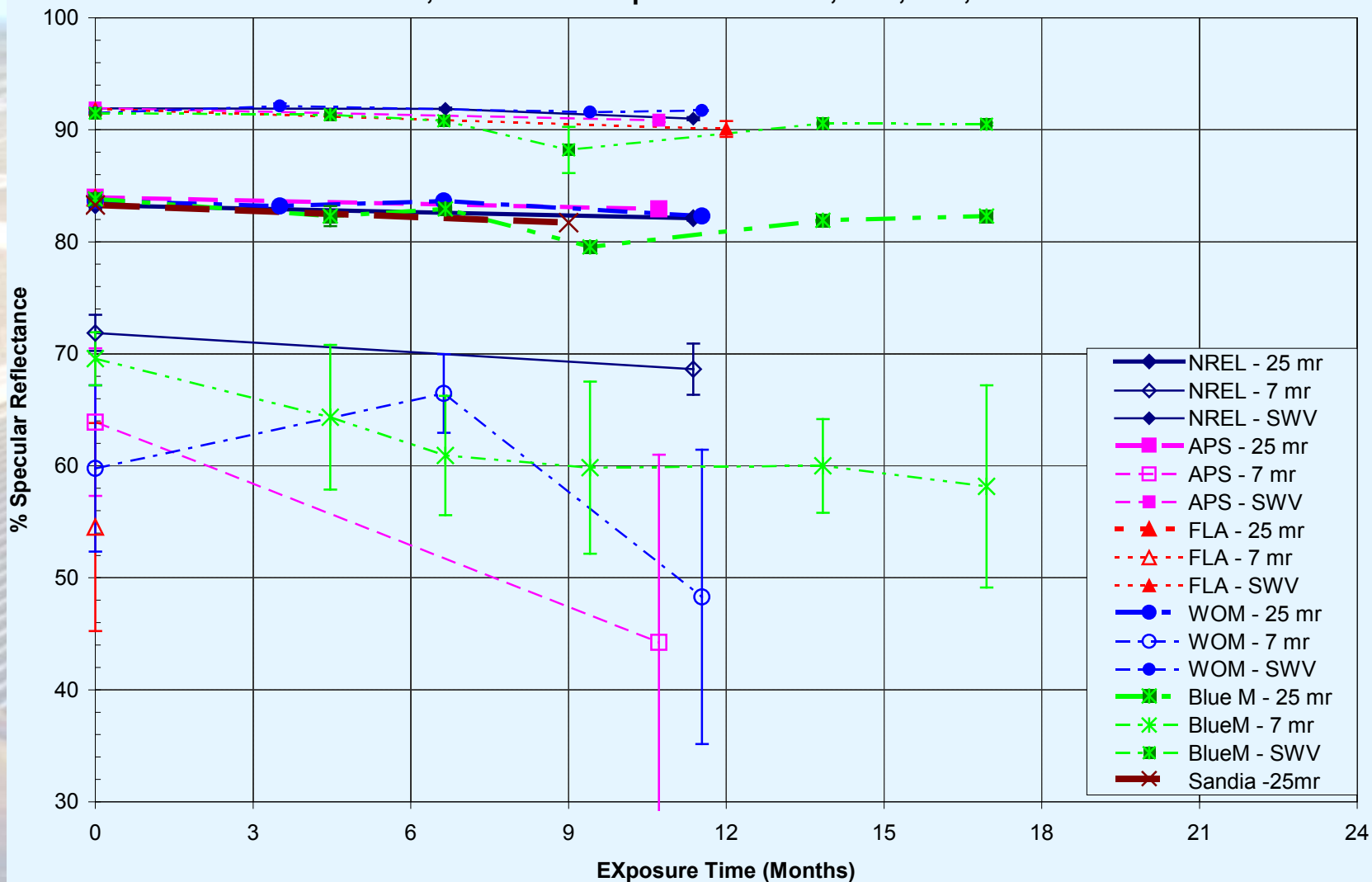
# Aluminized Reflector

Spectral Reflectance of Alanod MiroSun mirrors after accelerated exposure in Blue M (dark / 85°C / 85%RH) chamber



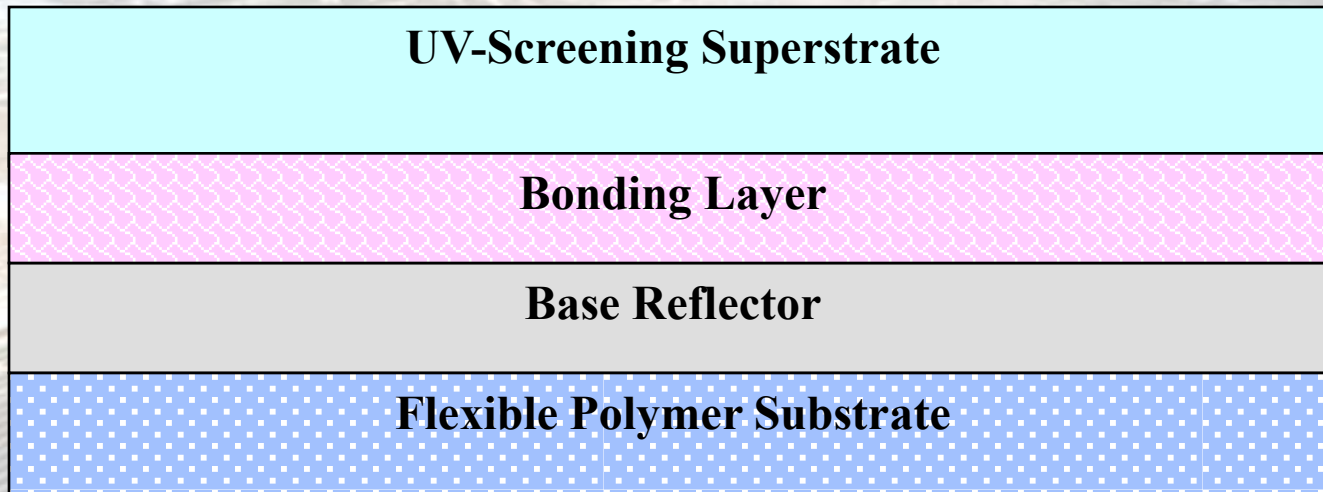
# Aluminized Reflector

Specular Reflectance at 7- and 25-mradians at 660 nm of Alanod MiroSun mirrors after accelerated exposure in Blue M (dark / 85°C / 85%RH), WOM (1 sun / 60°C / 60%RH) chambers, and outdoor exposure at NREL, APS, FLA, and Sandia

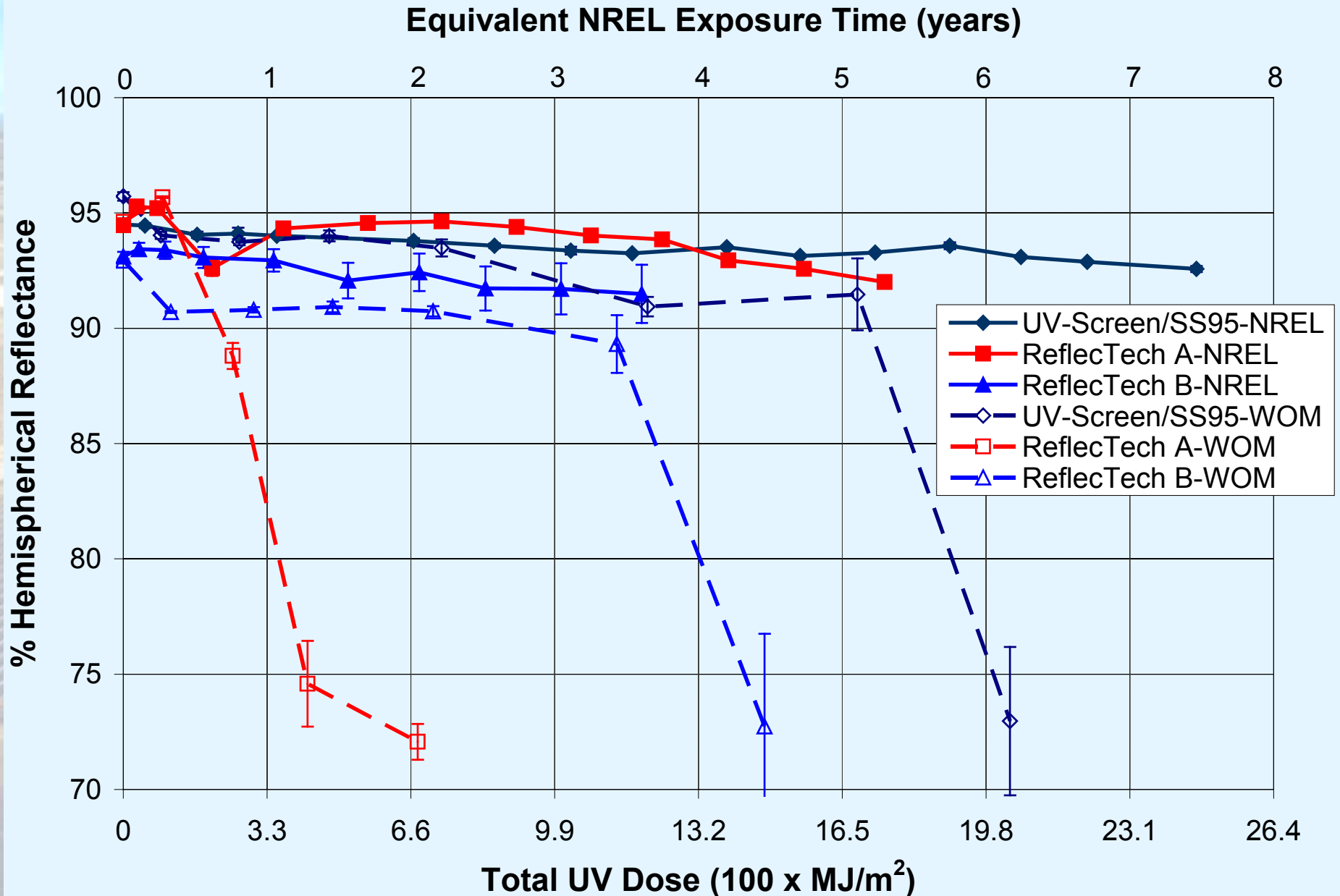




# ReflecTech - Silvered Polymer Reflector Architecture

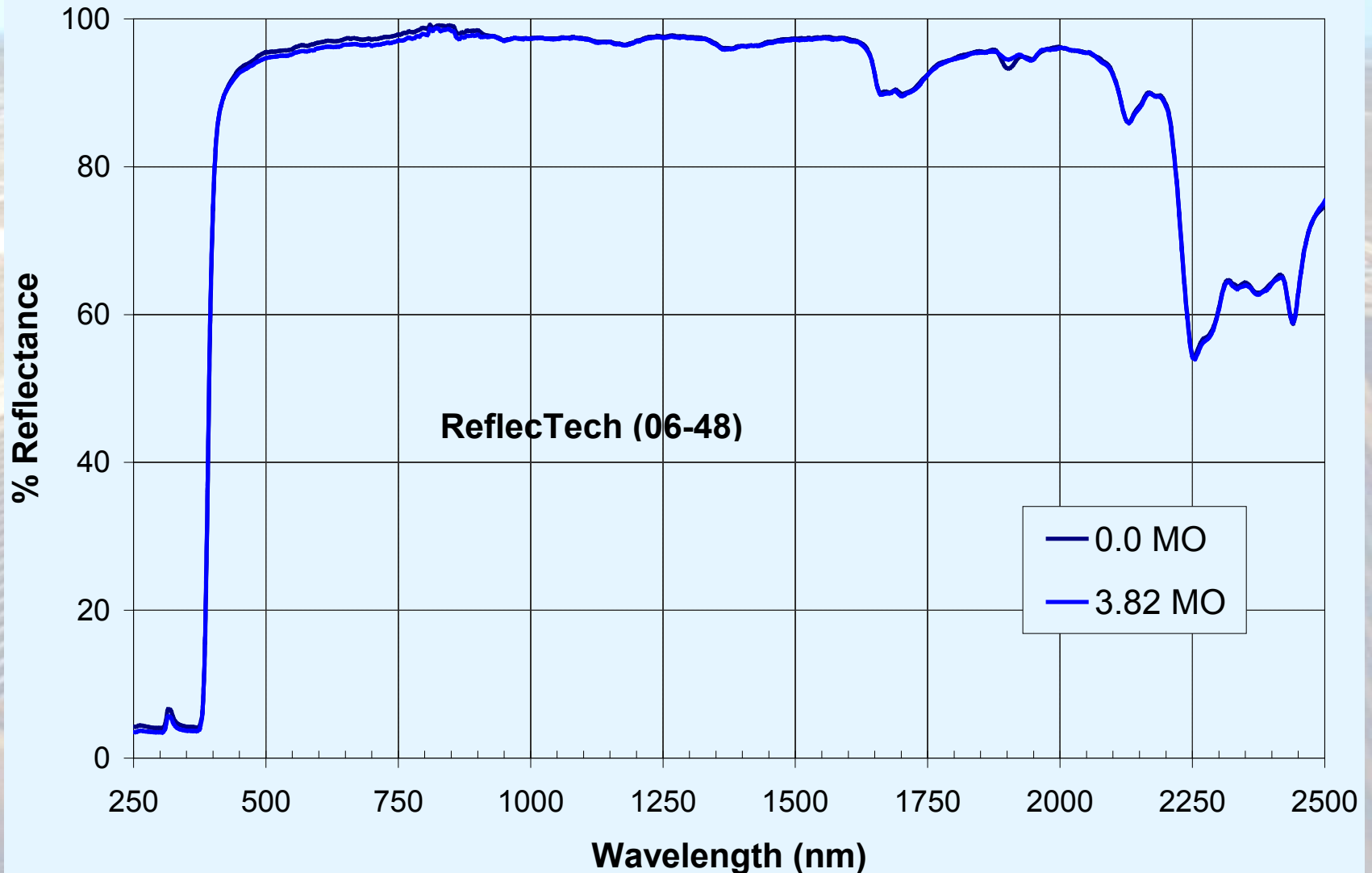


# ReflecTech Prototypes



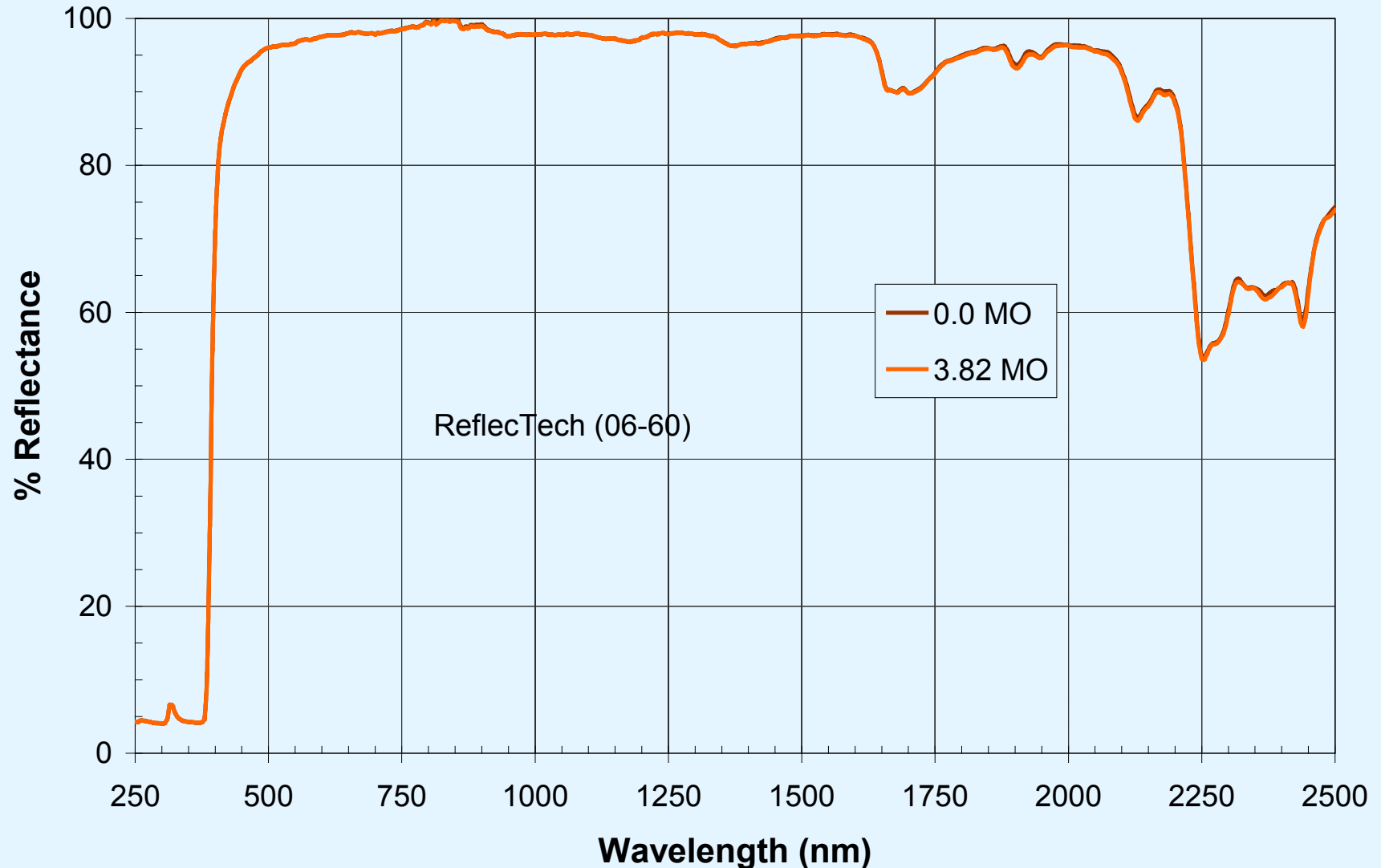
# ReflecTech III -NREL

Spectral Reflectance of ReflecTech pilot-run#3 (06-48) silver polymer mirrors after outdoor exposure in Golden, CO at NREL



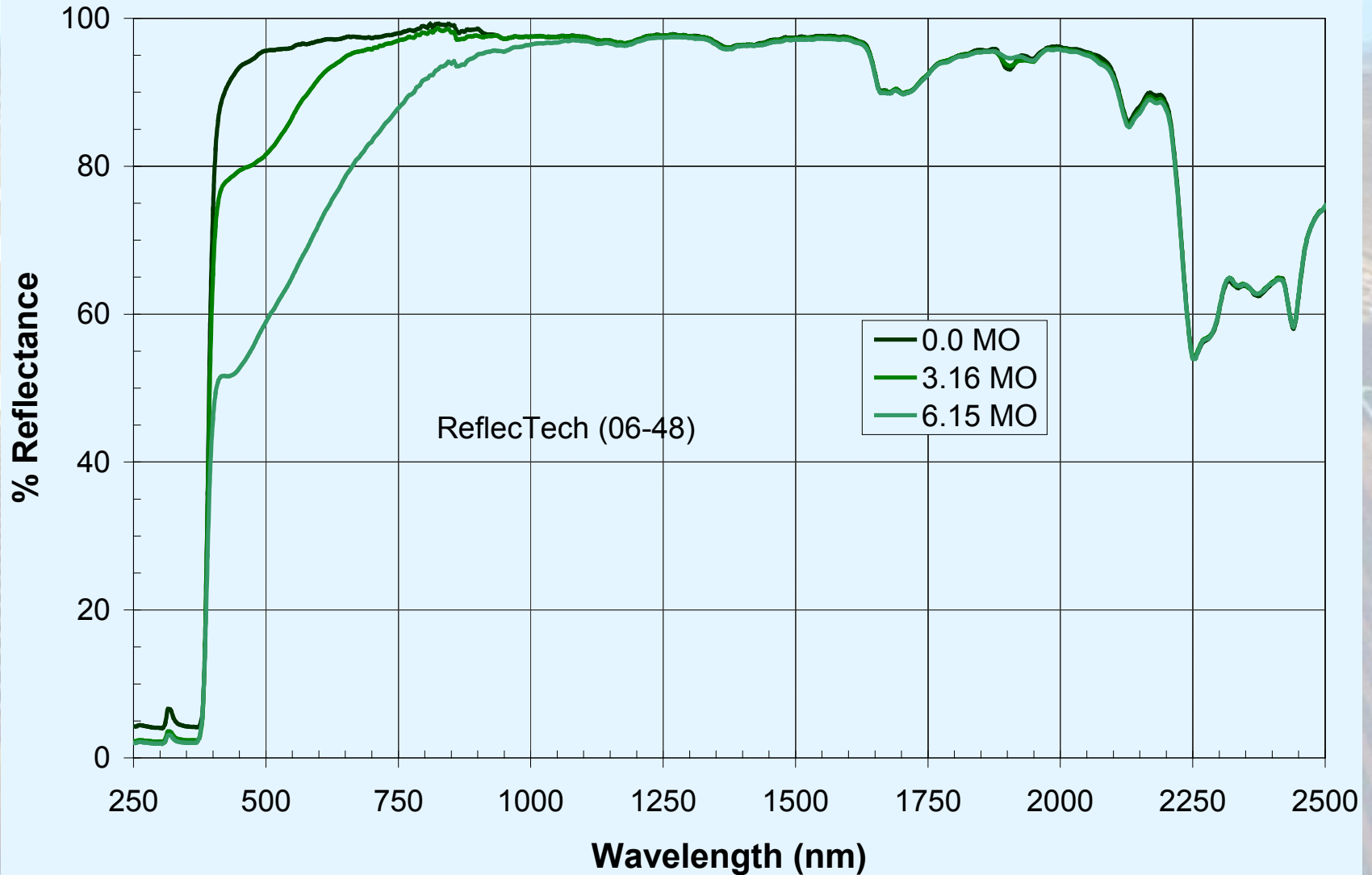
# ReflecTech III -NREL

Spectral Reflectance of ReflecTech pilot-run#3 (06-60) silver polymer mirrors after outdoor exposure in Golden, CO at NREL



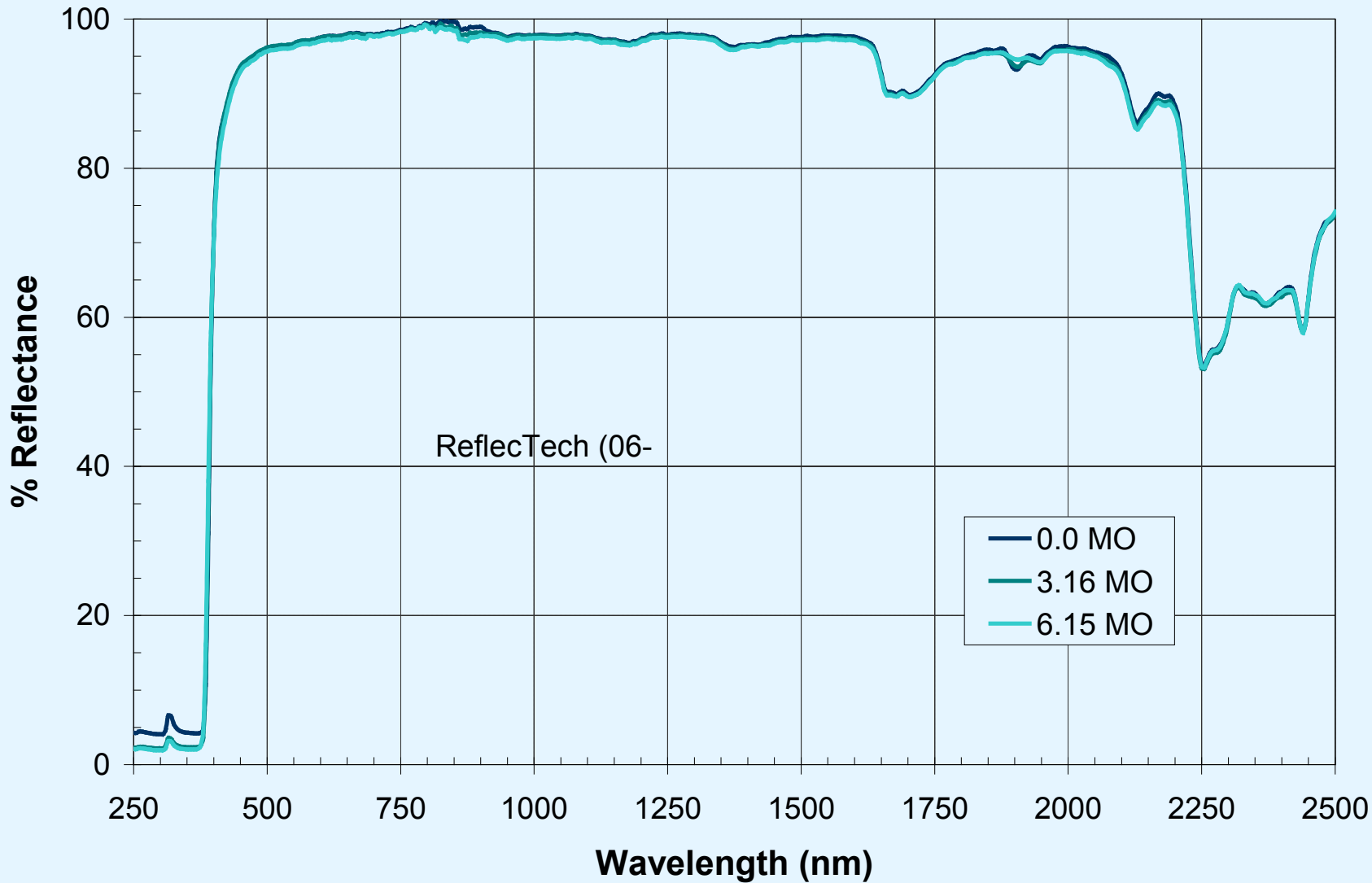
# ReflecTech III –Ci65 WOM

Spectral Reflectance of ReflecTech pilot-run#3 (06-48) silver polymer mirrors after accelerated exposure in Ci65 (1 sun / 60°C / 60%RH) chamber



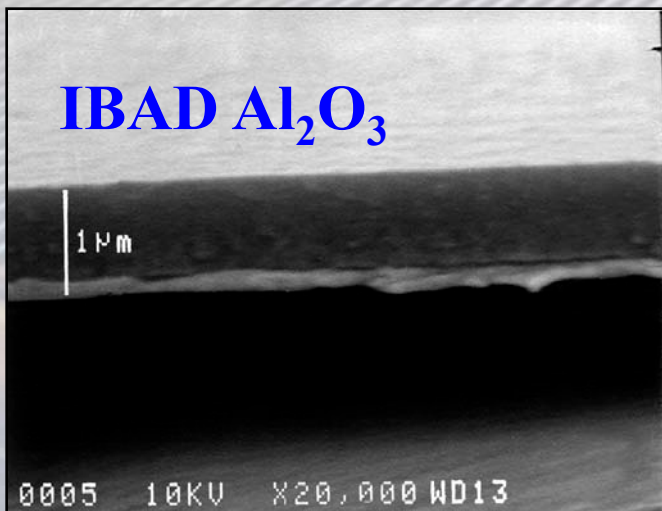
# ReflecTech III –Ci65 WOM

Spectral Reflectance of of ReflecTech pilot-run#3 (06-60) silver polymer mirrors after accelerated exposure in Ci65 (1 sun / 60°C / 60%RH) chamber



# Front Surface Solar Reflector Architecture

**Top Protective Layer (1-4 $\mu\text{m}$   $\text{Al}_2\text{O}_3$ )**



# Front Surface Solar Reflector Architecture

**Top Protective Layer** (1-4 $\mu\text{m}$   $\text{Al}_2\text{O}_3$ )

**Reflective Layer** (100 nm Ag)

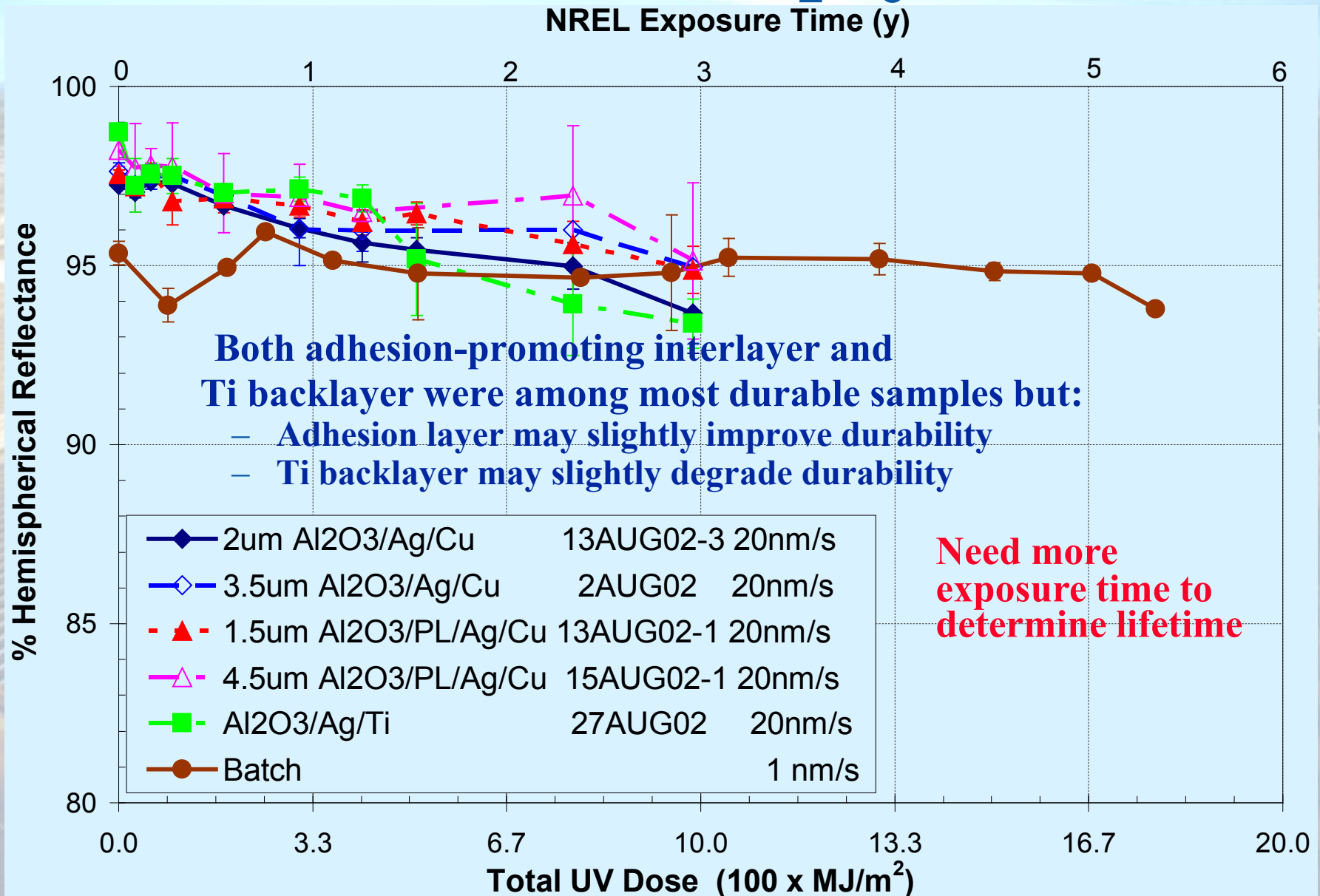
**Substrate** (PET)



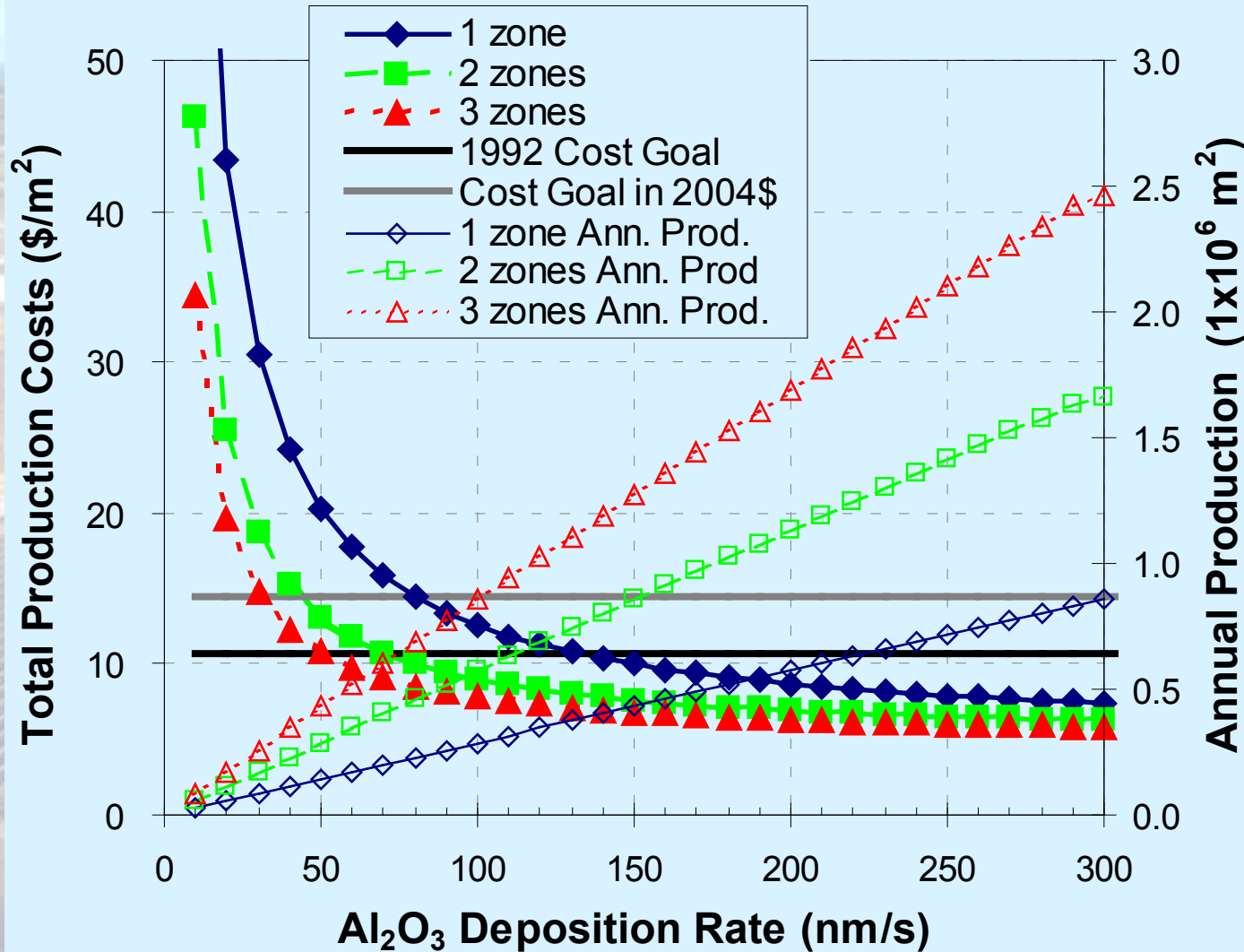
# Front Surface Solar Reflector Architecture

<b>Anti-soiling Layer</b> (100 nm $\text{TiO}_2$ )	
<b>Top Protective Layer</b> (1-4 $\mu\text{m}$ $\text{Al}_2\text{O}_3$ )	
<b>Adhesion Promoting Layer (APL)</b> (1-10 nm)	
<b>Reflective Layer</b> (100 nm Ag)	
<b>Metal Back Layer</b> (30 nm Cu —optional)	
<b>Substrate</b> (PET)	(Chrome Plated Steel, Levelled Stainless Steel, or Aluminum)

# Outdoor exposure at NREL of Roll-Coated IBAD $\text{Al}_2\text{O}_3$ Samples



# Cost Analysis

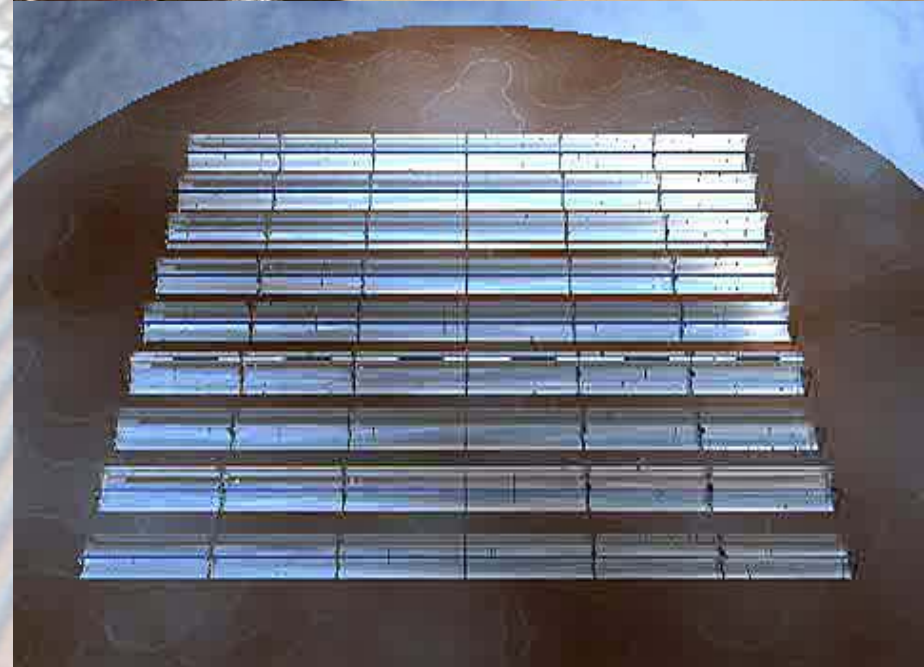


- 30% yield
  - Coating 79% time
  - 10 to 200 nm/s rate
  - Machine cost: \$2M-\$4.1M
  - Loan%/length: 12% for 5 yrs
  - PET substrate
  - 1- $\mu\text{m}$  Al<sub>2</sub>O<sub>3</sub>
  - Modified ASRM
  - \$200/h machine burden
  - 1200-mm web
  - High-purity High-volume (i.e., \$200/kg) Al<sub>2</sub>O<sub>3</sub>
- ✓ 1 vs. 2 vs. 3 zones in 1 machine

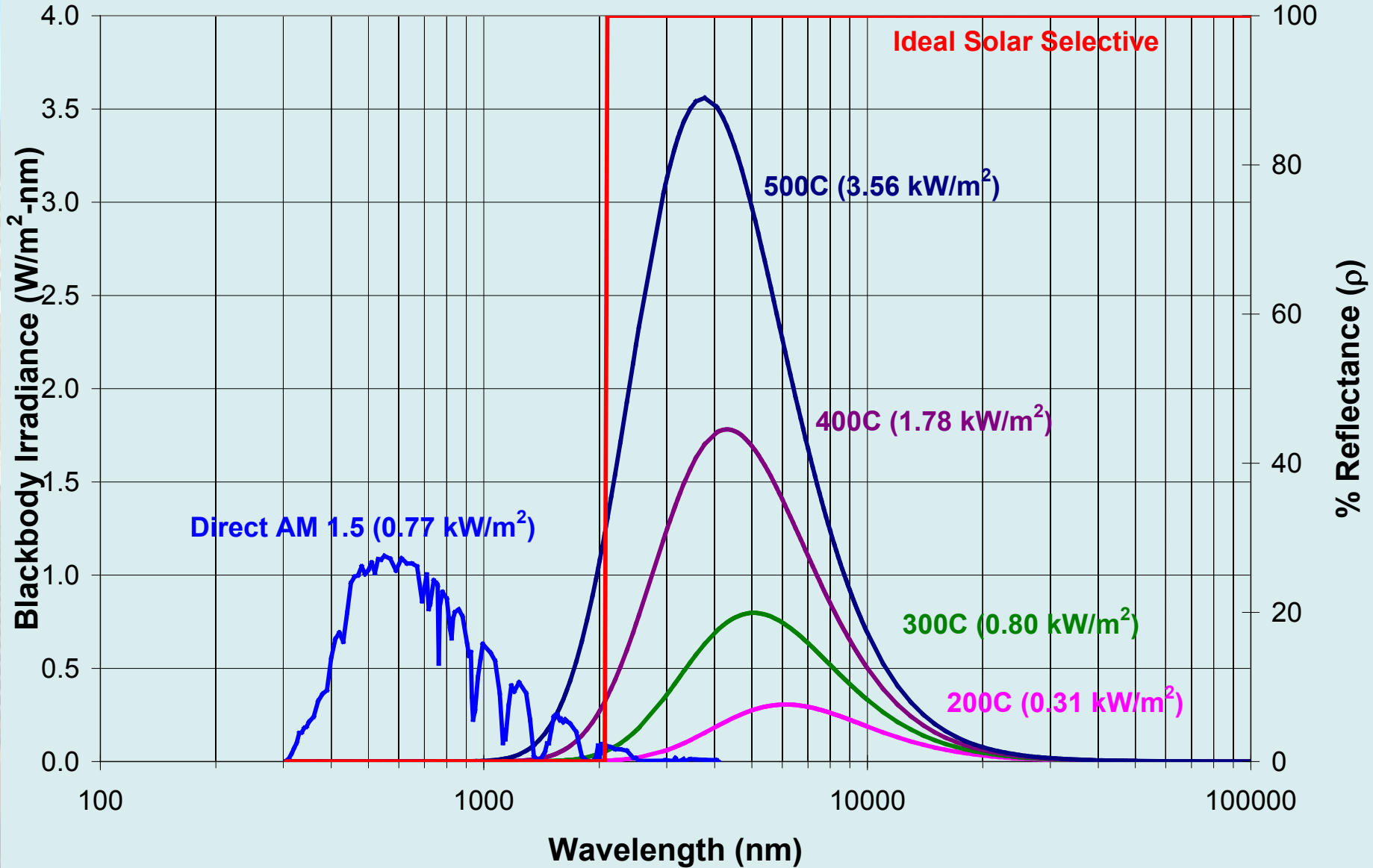
# Field Requirements for Advanced Receivers

- Receivers:

- 4 m (13.1 ft) long
- 70 mm (2.25 in) diameter
- New 64 MWe Nevada plant
  - 820 collectors and each collector has 24 (96 m) receivers
  - 19,680 receivers
  - 82 km of receivers (50 mi)
- Existing SEGS plants have 5x this many receivers
- New 553 MW plant will need 8.5x this many receivers
- 3-4%/yr Failure Rate
- ~\$1000/tube

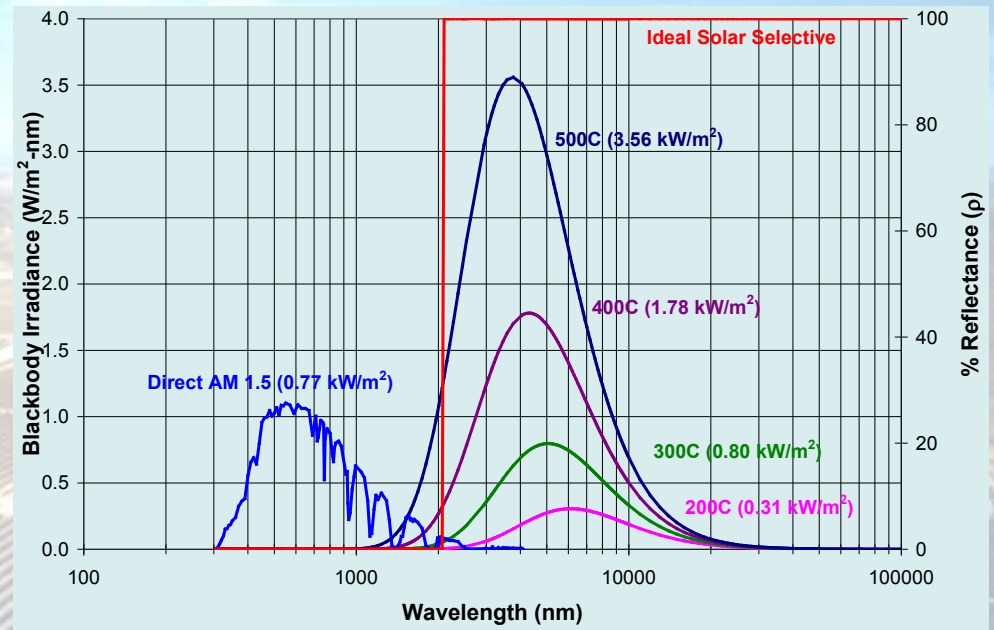


# Advanced Selective Coating Goals



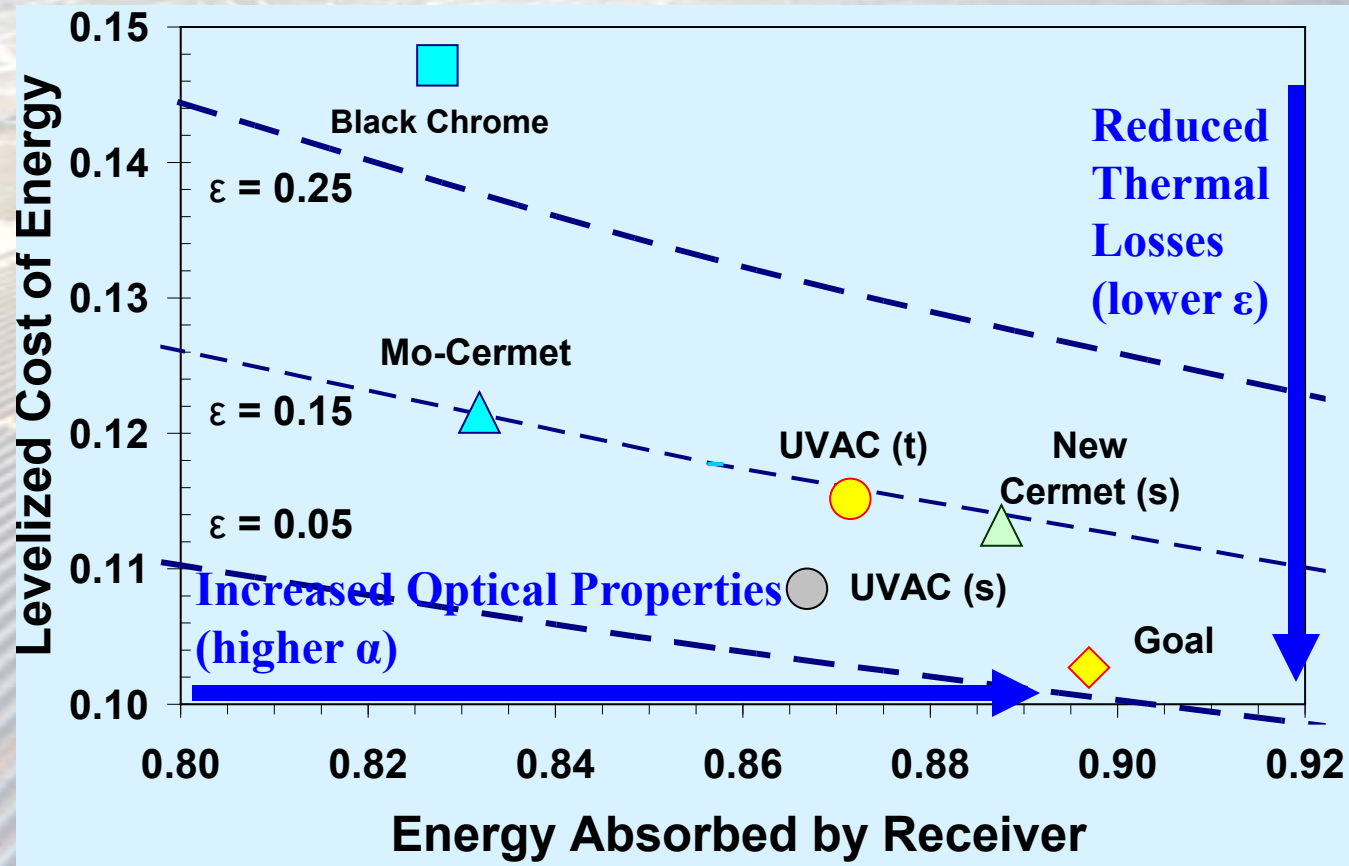
# Advanced Selective Coating Goals

- To develop receiver coatings that have:
  - Good optical and thermal performance: absorptance ( $\alpha$ )  $\geq 96\%$ , & emittance ( $\epsilon$ )  $\leq 7\%$   $>400^\circ\text{C}$
  - High temperature stability in air at temperatures  $\geq 550^\circ\text{C}$
  - Manufacturing processes with improved quality control
  - Lower cost

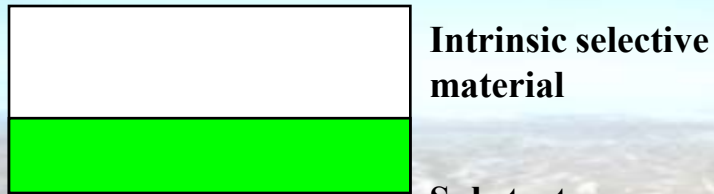


# High Temperature Solar Selective Coating Development

- Selective coating properties impact collector optical performance and thermal losses.
- Improvements in the receiver can enhance collector efficiency & lower cost.
- The international community currently leads this area and there exists minimal US research & no US manufacturer of high-temperature selective coatings.



# Types of Selective Coatings



Intrinsic selective material

Substrate

*Intrinsic absorber*



Dielectric

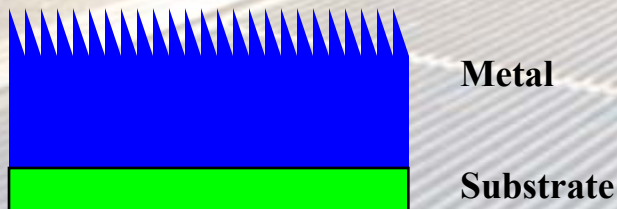
Metal

Dielectric

Metal

Substrate

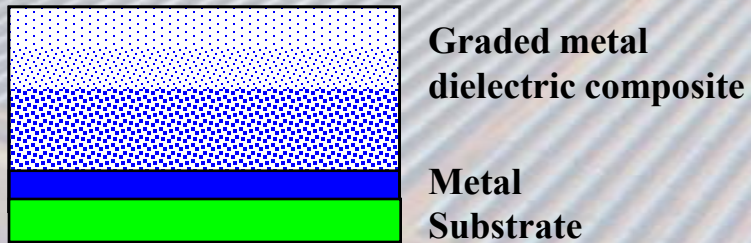
*Multilayer absorbers*



Metal

Substrate

*Surface texturing*

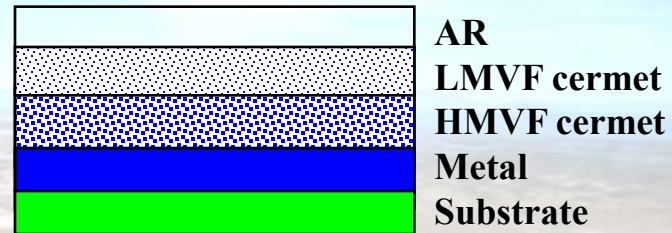


Graded metal dielectric composite

Metal

Substrate

*Graded cermet*



AR

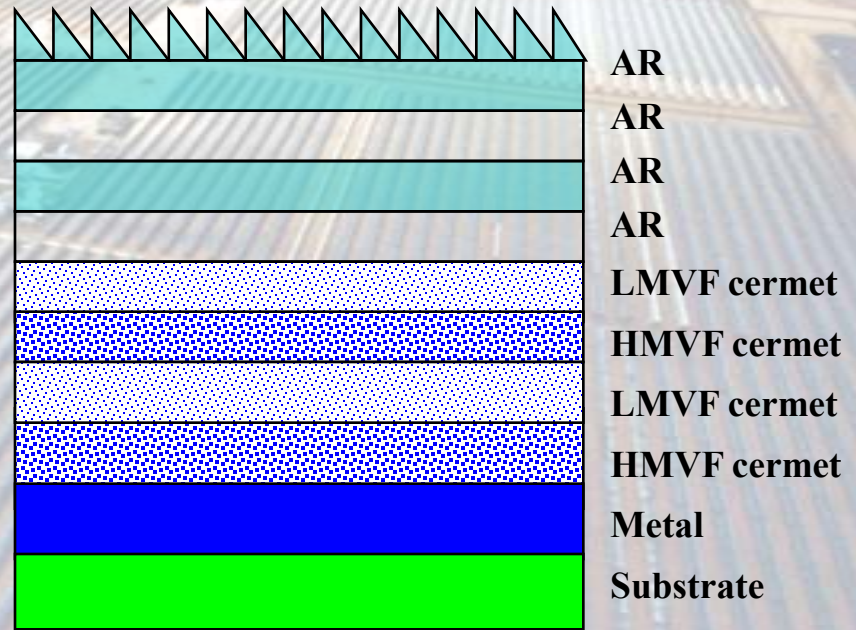
LMVF cermet

HMVF cermet

Metal

Substrate

*Double cermet*



AR

AR

AR

AR

LMVF cermet

HMVF cermet

LMVF cermet

HMVF cermet

Metal

Substrate

*Multiple cermet*



# Literature Review of Candidate High-temperature ( $> 400^{\circ}\text{C}$ ) Solar Selective Materials

- Graded Mo,W, ZrB, Pt-  $\text{Al}_2\text{O}_3$  cermets
- Si tandem absorber
- Black Co, Mo,W
- Double cermets- SS-AlN, AlN/Mo, or AlN/W
- 4-layer V- $\text{Al}_2\text{O}_3$ , W- $\text{Al}_2\text{O}_3$ , Cr- $\text{Al}_2\text{O}_3$ , Co- $\text{SiO}_2$ , Cr- $\text{SiO}_2$ , Ni- $\text{SiO}_2$
- Double AR
- Multilayers; Al-AlN<sub>x</sub>-AlN
- Au/ $\text{TiO}_2$  cermet
- $\text{ZrC}_x\text{N}_y/\text{Ag}$
- $\text{Ti}_{1-x}\text{Al}_x\text{N}$
- *Quasicrystals* multilayers & cermets
- Surface Texturing

# Desirable Properties for Stable Coating in Air > 400°C

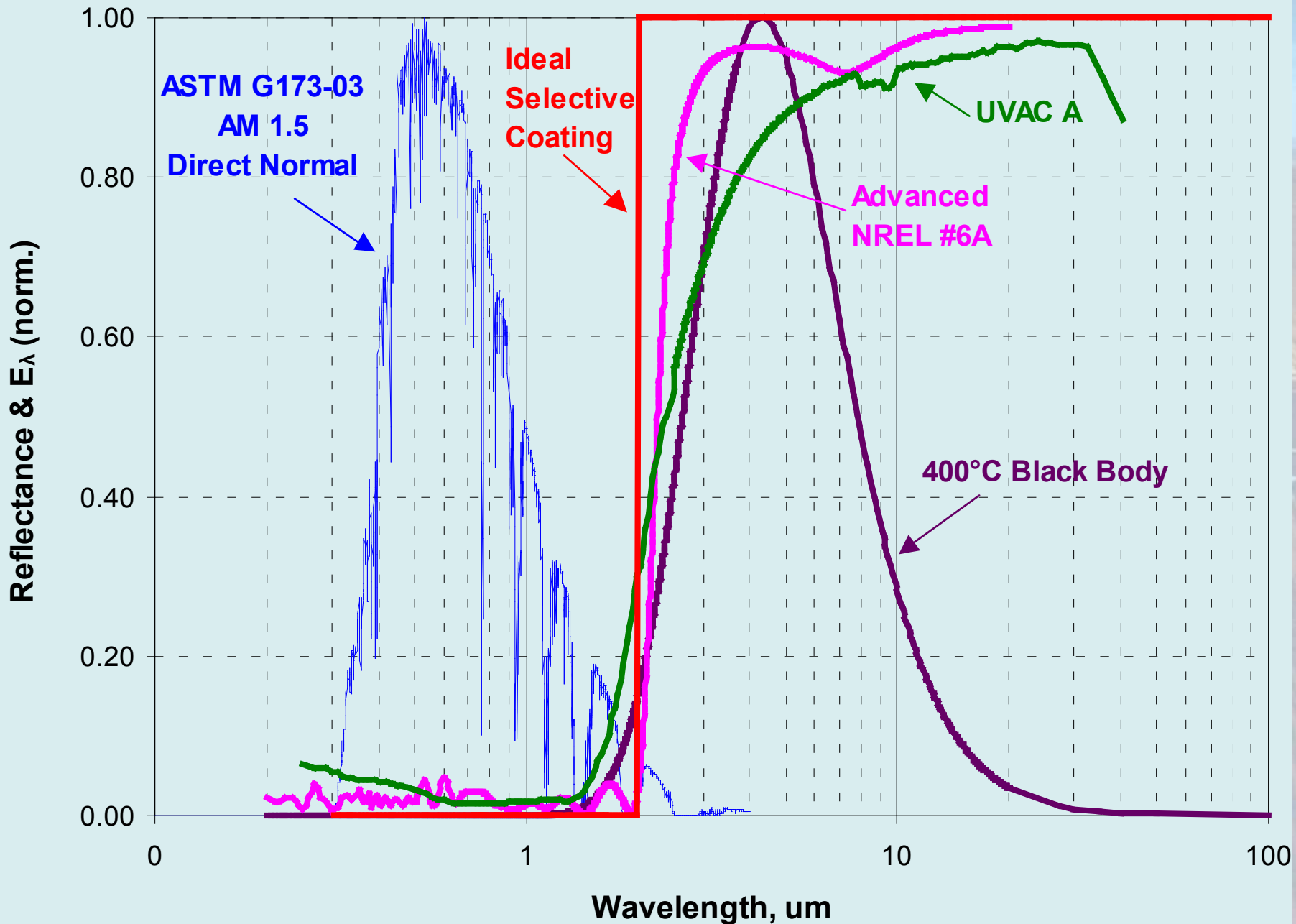
- High thermal & structural stabilities for combined & individual layers
  - Elevated melting points
  - Large negative free energies of formation
  - Materials that form a multicomponent oxide scale
  - Single-compound formation
  - Lack of phase transformations at elevated temperature
- Suitable texture to drive nucleation, subsequent growth of layers with suitable morphology
  - Stable nanocrystalline or amorphous materials
- Excellent adhesion between the substrate and the adjacent layers
- Enhanced resistance to thermal and mechanical stresses
  - Acceptable thermal and electrical conductivities
  - Higher-conductivity materials have improved thermal shock resistance
  - Some ductility at room temperature reduces thermal-stress failures
- Good continuity and conformability over the tube
- Compatibility with fabrication techniques

# NREL Modeled Selective Coating

Comparison of theoretical optical properties for NREL's modeled prototype solar selective coating with actual optical properties of existing materials.

	Commercial (as tested)			Modeled	
	Black Cr	Mo-Cermet	UVAC	# 6A	# 6B
<b>Solar Absorptance</b>	0.916	0.938	0.954	0.959	0.950
<b>Thermal Emittance@</b>					
<b>25°C</b>	0.047	0.061	0.052	0.013	0.027
<b>100°C</b>	0.079	0.077	0.067	0.017	0.033
<b>200°C</b>	0.117	0.095	0.085	0.028	0.040
<b>300°C</b>	0.156	0.118	0.107	0.047	0.048
<b>400°C</b>	<i>0.216</i>	0.146	0.134	0.074	0.061
<b>500°C</b>	<i>0.239</i>	<i>0.179</i>	<i>0.165</i>	0.110	0.073

# Modeled NREL Selective Coating



# Modeling Key Results

- Solar Selective Coating Development
  - Modeled solar-selective coatings with  $\alpha=0.959$  and  $\varepsilon=0.061$  that meet CSP goals
  - Emittance excellent & absorptance of modeled coatings is very good but further improvements are expected. However, trade-off exists between emittance and absorptance.

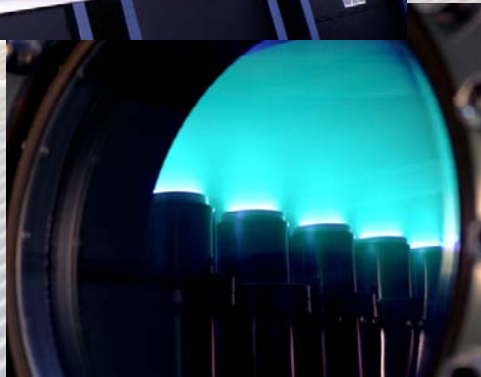
# Deposition Capabilities

- Three-Chamber In-line System

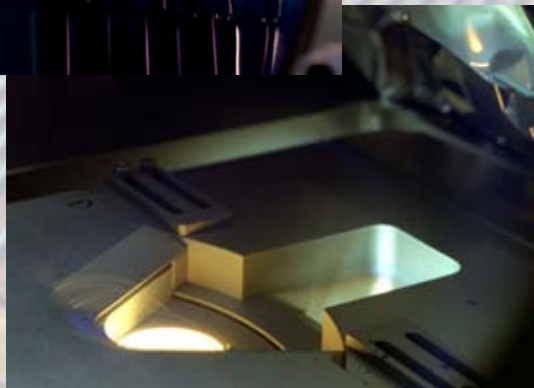
- Load-Lock Chamber
- Pulsed DC Sputtering Chamber
  - 3 - linear arrays of 5 - 1.5" Mini-mak guns
  - 2 - 12" planar cathodes
- Electron-Beam/IBAD Chamber
  - 6 multi-pocket e-beam source
  - Co-deposition bottom plate
  - IBAD w/ 12" Linear Ion Gun
- System
  - 12"x12" ambient or heated substrate
  - 4 Reactive Gases
  - Turbo molecular drag pumps
    - $2 \times 10^{-8}$  torr
  - Monitoring
    - RGA
    - Quartz Crystal Monitor
    - Pressure/Gas
    - Computer



Sputtering Chamber



E-Beam Chamber



# Prototyping Key Results

- Key issue is making deposited coating
- XPS showed evaporation from compounds produced layered stoichiometry
  - Despite depositing layers with over- and under-thickness and compound layered structure, the optical performance of the prototype NREL#6A was quite encouraging.
- Need to codeposit materials
  - Required significant upgrade to equipment
    - Installed codeposition guns & sweeps
    - Pneumatic shutters
    - Second quartz crystal sensor
    - Upgrade computer & RGA software
    - + associated air, water, & electrical
    - Automating control

# Prototyping Key Results

- Codeposit individual layers and modeled coating
  - Codeposition development
    - Deposited individual layers
    - Deposited modeled structure
    - Characterize properties
  - Optical performance lower than modeled
    - Typically optical coating need error <1%
  - Thickness error was >5% because of manual control
    - Install optical monitor
    - Provide positive feedback between quartz crystal and optical monitor
    - Automate control –remove human error and provide steering and cutting at sensitive turning points allowing mid-course corrections to be made
  - Compositional errors because stoichiometry not optimized
    - Composition with highest reflectance
    - Phase formation from Pretorius effective heat of formation model & TGA
  - Optimize morphology with ion assist



# Selective Coating Performance

- $\epsilon$  can be measured at higher temperatures but is typically reported based on calculations from reflectance measurements fitted to the black body curve
  - Actual performance of the absorber at high temperatures commonly does not correspond to the calculated  $\epsilon$ 
    - Small errors in  $\rho$  lead to large errors in  $\epsilon$
    - $\epsilon$  is a surface property & depends on surface condition of material and substrate
      - Surface roughness
      - Surface film
      - Oxide layers
    - Selective coatings can degrade at high T due to
      - Thermal load (oxidation)
      - High humidity or water condensation on the absorber surface (hydratization and hydrolysis)
      - Atmospheric corrosion (pollution)
      - Diffusion processes (inter-layer substitution)
      - Chemical reactions
      - Poor interlayer adhesion
  - Therefore it is important that  $\rho$  is measured accurately and to measure  $\epsilon$  of the selective coating at operating temperatures & conditions before using calculated  $\epsilon$
- Round Robin &**  
**Purchase Perkin Elmer 883 IR spectrophotometer**

# Thermal Stability

- Thermal stability is sometimes given based on the thermal properties of the individual materials or the processing temperature parameters
- Actual durability data is uncommon for high temperature absorber coatings
- Durability or thermal stability is typically tested by heating the selective coating, typically in a vacuum oven but sometimes in air, for a relatively short duration (100's of hours) compared with the desired lifetime (5-30 years)
  - IEA Task X performance criterion (PC) developed for flat plate collector absorber testing (i.e., non-concentrating, 1-2X sunlight intensity)
  - No analogous criterion known for testing high-temperature selective coatings for CSP applications
- Building capability for long term testing of thermal stability
  - Purchased & installed high-temperature (600°C) inert gas oven

# Conclusion

- DOE, the WGA, state RPS mandates, and feed-in tariffs have successfully jump-started growth in CSP technologies that would require 7 to 10 million square meters of reflector and more than 600,000 HCEs over the next 5 years.
- Commercial glass mirrors, Alanod, and ReflecTech may meet the 10-yr lifetime goals based on accelerated exposure testing. Predicting an outdoor lifetime based on accelerated exposure testing is risky because AET failure mechanisms must replicate those observed by OET.
- Experimental IBAD  $\text{Al}_2\text{O}_3$  front surface mirror has high potential to meet need; but needs development by roll-coating company
- None of the solar reflectors available have been in test long enough to demonstrate the 10-year or more aggressive 30-year lifetime goal, outdoors in real-time

# Conclusion

- Modeled solar-selective coatings with  $\alpha=0.959$  and  $\varepsilon=0.061$  that meet CSP goals
- Emittance excellent & absorptance of modeled coatings is very good but further improvements are expected. However, trade-off exists between emittance and absorptance.
- Key issue then becomes trying to make the coating
- Prototype development underway. Individual and modeled structure deposited by e-beam compound and elemental codeposition & characterized. Need to eliminate thickness errors by upgrading monitor and control and determine optimum stoichiometry.
- Purchased & installed PE 883 IR Spectrophotometer (2.5- 50 $\mu$ ) and high-temperature inert gas oven. Round-robin data being analyzed and commercial & prototyped coating samples being put into test
- Patent being pursued

# Acknowledgments

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