

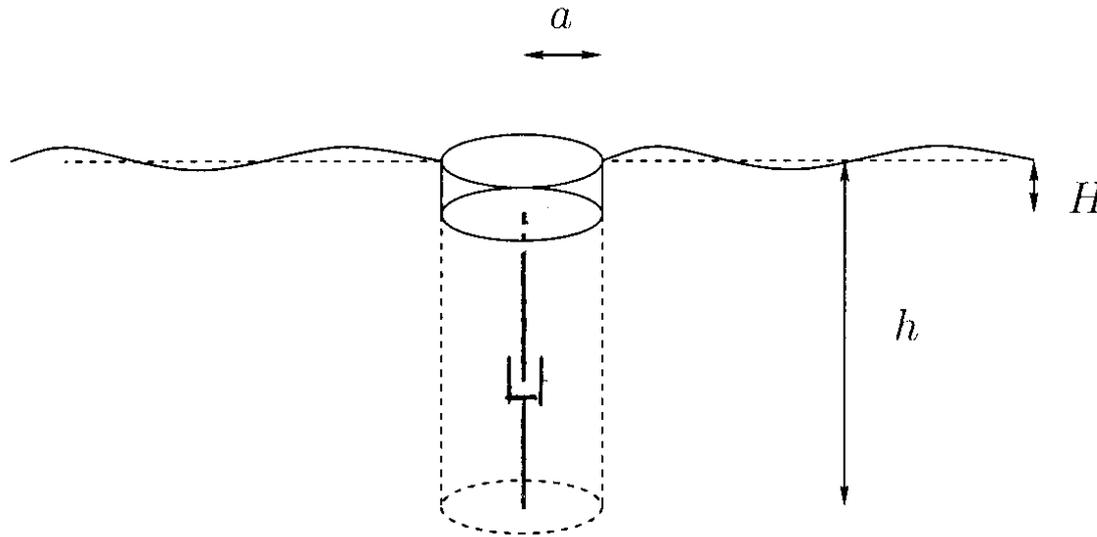
Buoy Arrays & Coastal OWC's for Wave Energy Extraction

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- Single Buoy
- Sparse Array of Buoys
- Compact Array of Buoys
- OWC on a coast

Background : single buoy



$$\text{Extractor} = \text{force on buoy} = -\lambda_g \frac{\partial \zeta}{\partial t}$$

$\lambda_g = \text{extraction coefficient}$

Power extraction

Force from PTO: $-i\omega\lambda_g\zeta$

Newton:

$$-\omega^2(M + \mu) = F^D - i\omega(\lambda + \lambda_g) + \pi a^2$$

Power extracted

$$P = \frac{(1/2)\lambda_g\omega^2|F^D|^2}{\omega^2(\lambda + \lambda_g)^2 + (\pi a^2 - \omega^2(M + \mu))^2}$$

Conditions for maximum extraction – impedance matching

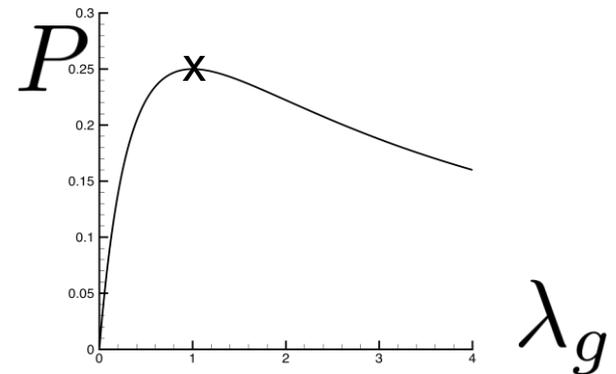
Resonance: $\pi a^2 - \omega^2(M + \mu) = 0.$

Special extraction rate : $\lambda_g = \lambda$

Max power extraction and capture width

$$P = \frac{1}{2k} \rho g |A|^2 C_g, \quad kL = 1$$

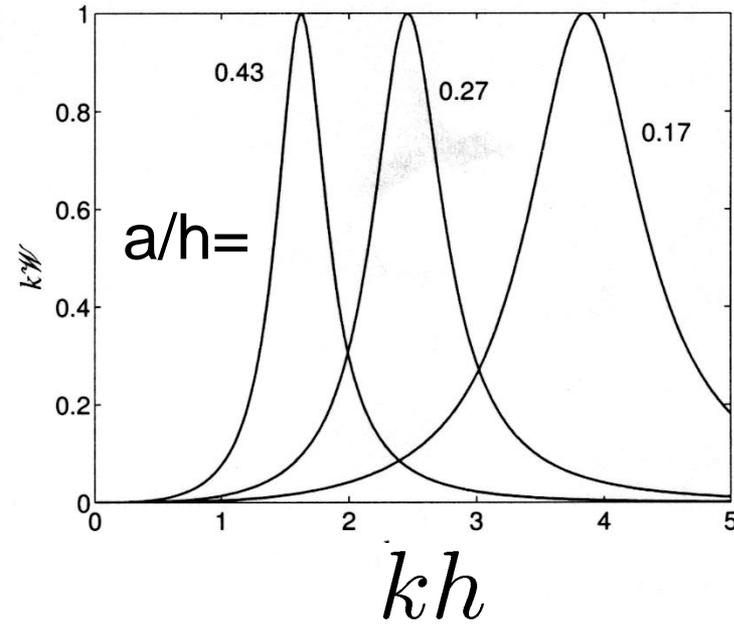
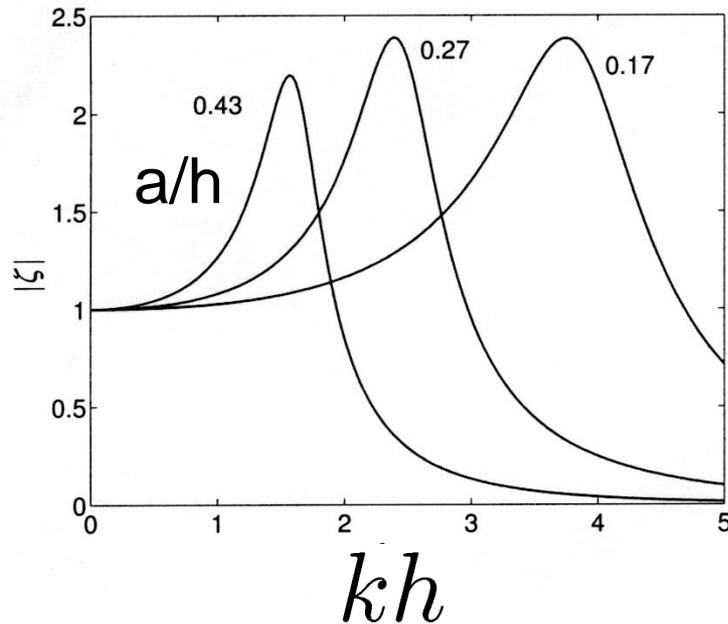
after using Haskind theorem



Size effect for a single buoy

ζ = buoy displacement

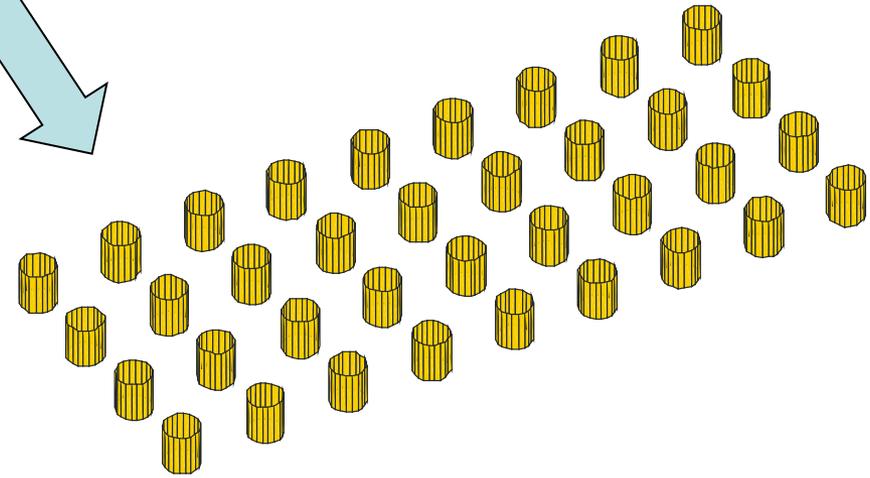
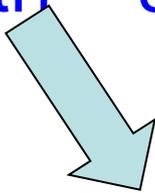
Capture width kL



For $h = 15 \text{ m}$	a/h	0.43	0.27	0.17
	$T(s)$	8	5	4

Sparse array

wavelength \sim spacing \gg buoy size



For 100 % extraction by

Single row: $W = 1/k$

Two rows: $W = 2/k$

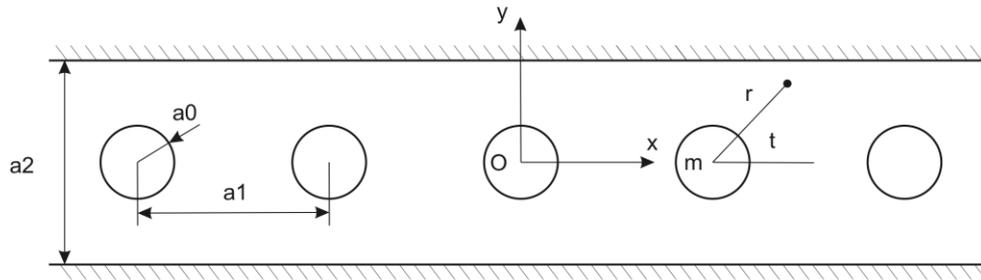
N rows: $N > 2 + 2kW/\pi$

Budal (1977)

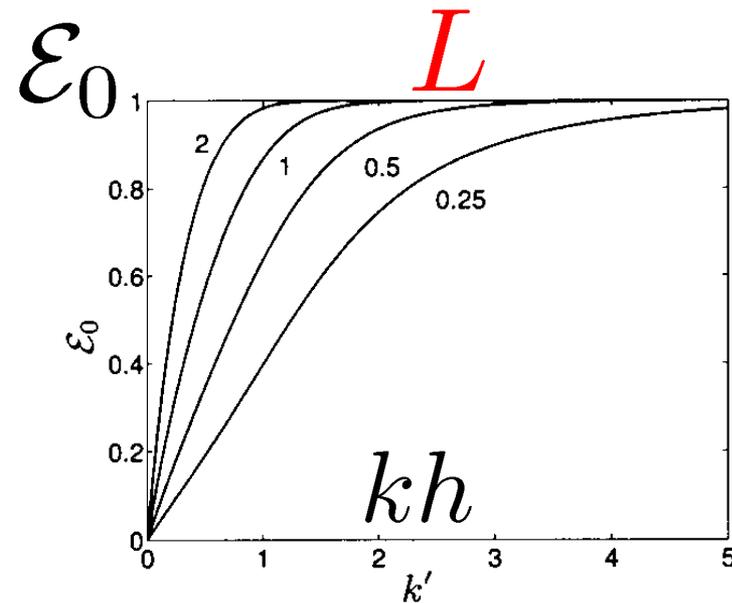
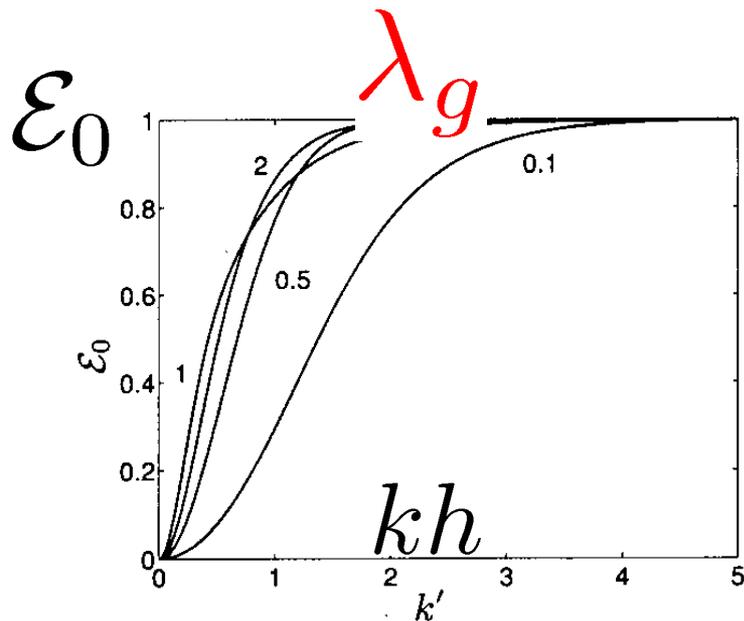
Falnes(1984)

Away from Bragg Resonance

Bragg resonance if $kd = n\pi$



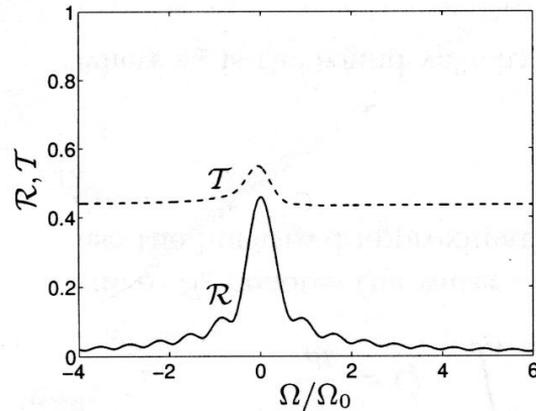
(Garnaud & Mei, 2009, submitted)



Effect of extraction rate and on Reflection and Transmission

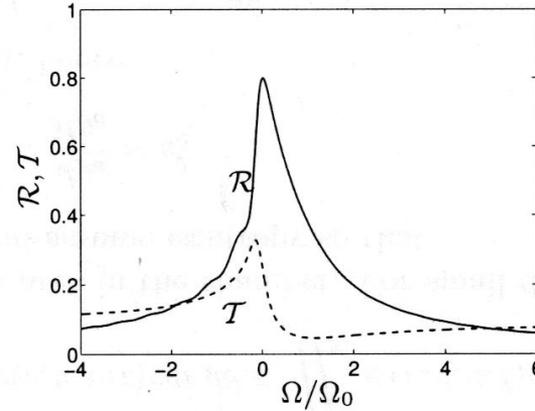
$$\lambda_g = 0.1, 0.5, 10, \infty$$

0.1



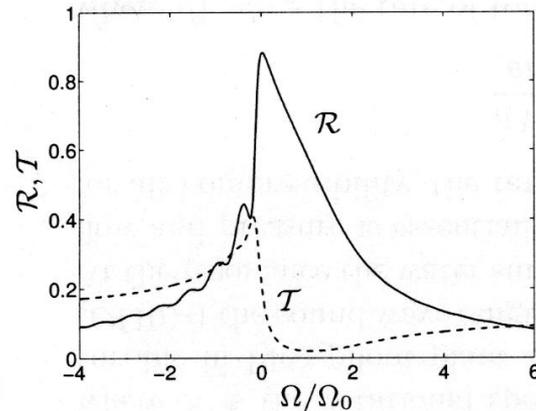
(a) $\lambda'_g = 1/10$

0.5



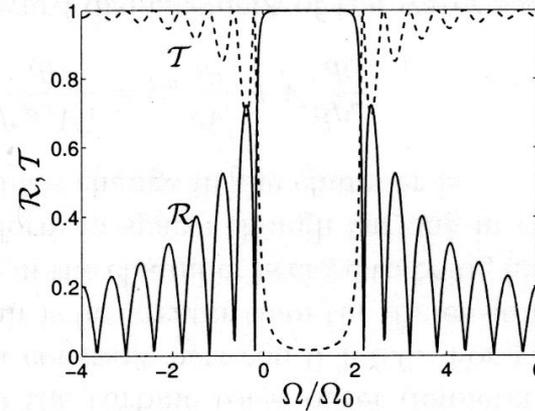
(b) $\lambda'_g = 1/2$

1.0



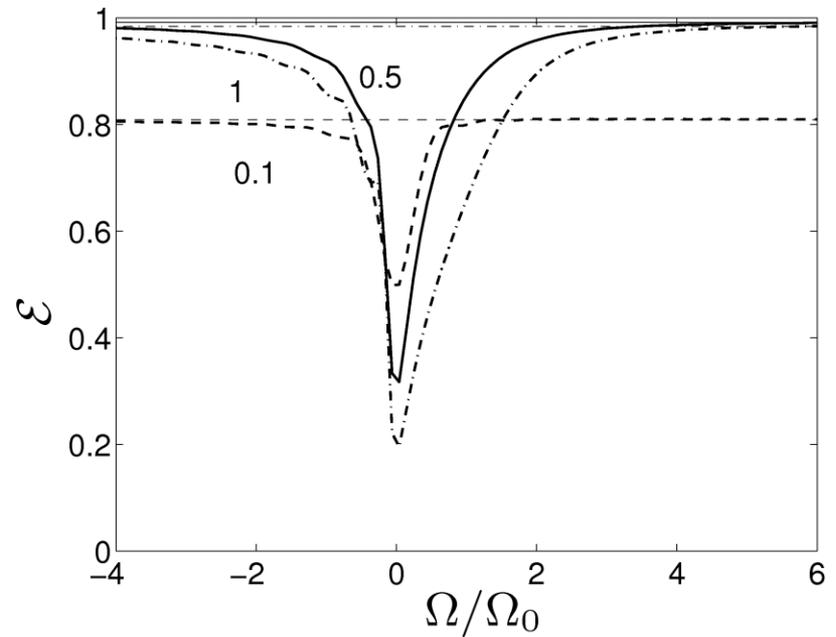
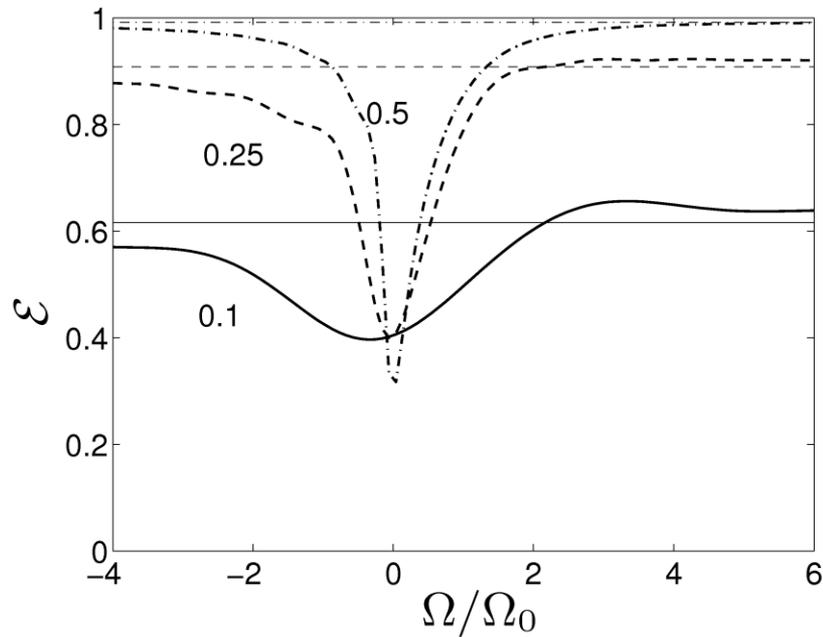
(c) $\lambda'_g = 1$

∞



(d) $\lambda'_g = \infty$ (fixed buoys)

Power absorption efficiency vs Detuning





Fred Olsen
(FO3)
ABB Power
Systems,
Norway



36 m x 36 m,
2.5 MW
2.8 million Euro

Buoy size, spacing
<< wavelength

Boundary Condition on water surface

Solid fraction : $f = \frac{\pi a^2}{d^2}$

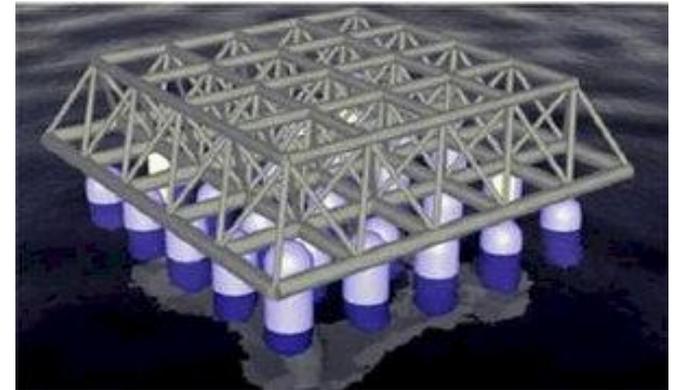
Not covered by buoys :

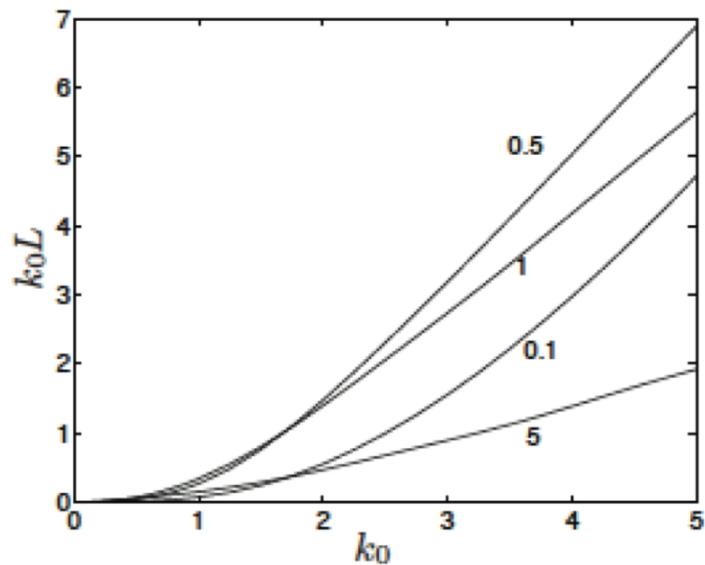
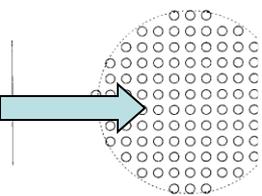
$$\frac{\partial \phi}{\partial z} - \frac{\omega^2}{g} \phi = 0, \quad z = 0.$$

Covered by buoys :

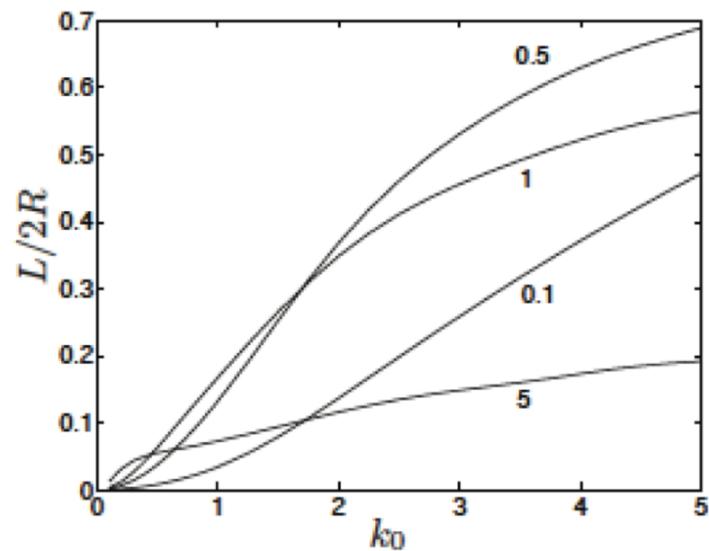
$$\frac{\partial \phi}{\partial z} - \frac{\omega^2}{g} \left[1 - f \left(\frac{i \lambda_g \omega}{1 + i \lambda_g \omega} \right) \right] \phi = 0, \quad z = 0.$$

Assume negligible buoy inertia: $\frac{\omega^2 H}{g} \ll 1$

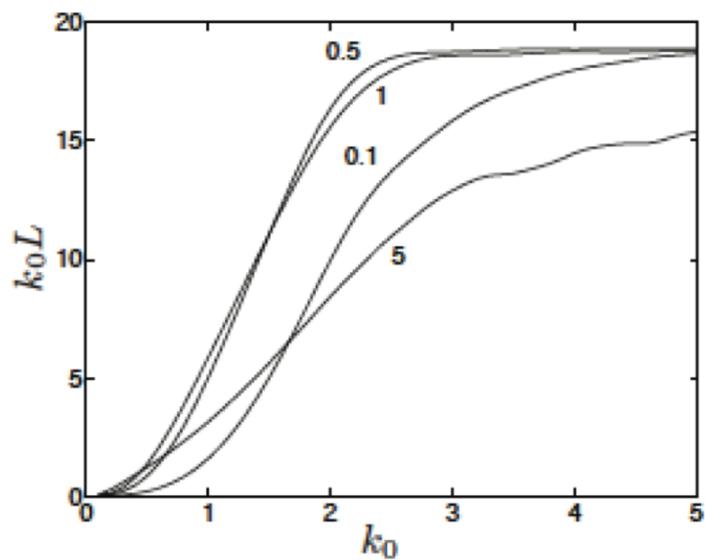




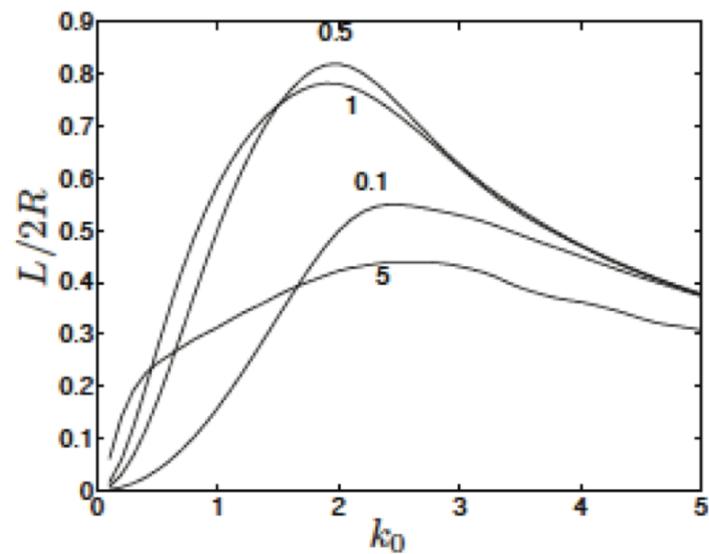
(a) $R = 1$



(b) $R = 1$

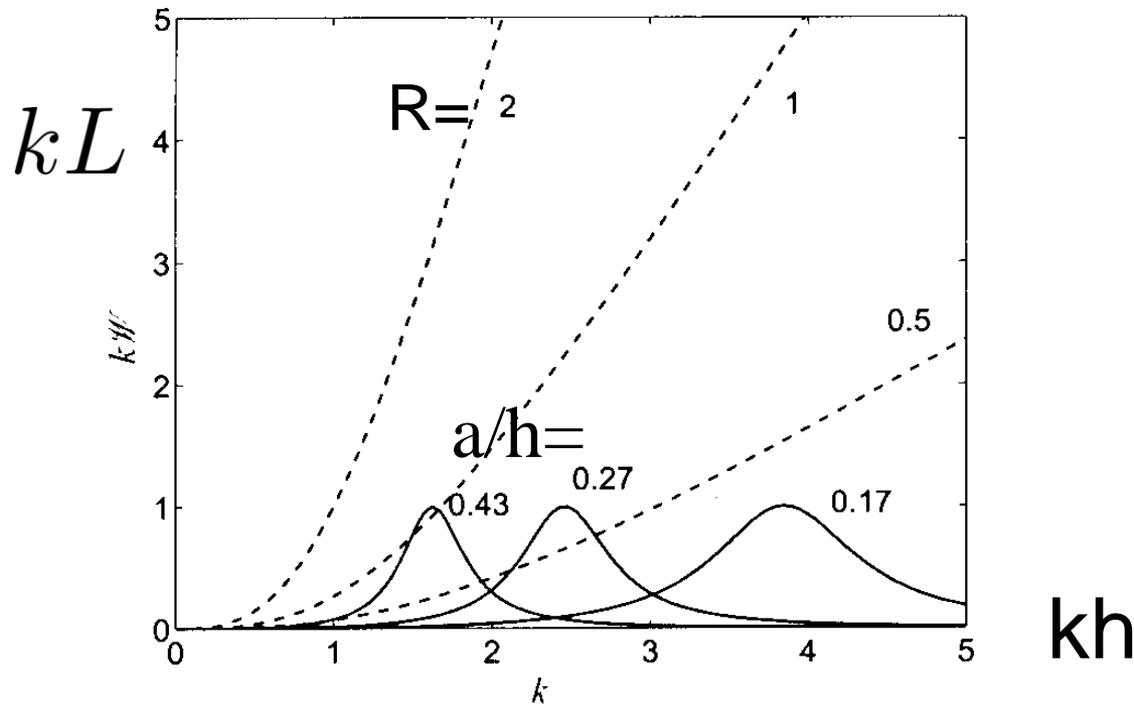


(c) $R = 5$



(d) $R = 5$

FO3 vs. single buoy of equal volume. $f=0.2$, $\lambda_g=0.5$



Array of compact arrays?

Dual purpose structure: OWC plant

integrated into a breakwater

**Mouth of Douro river,
Porto**

**New
breakwater**

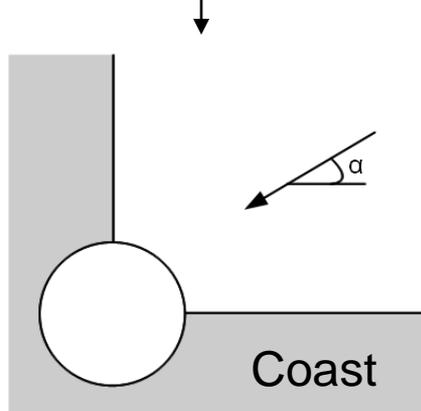


4 coastlines and OWC

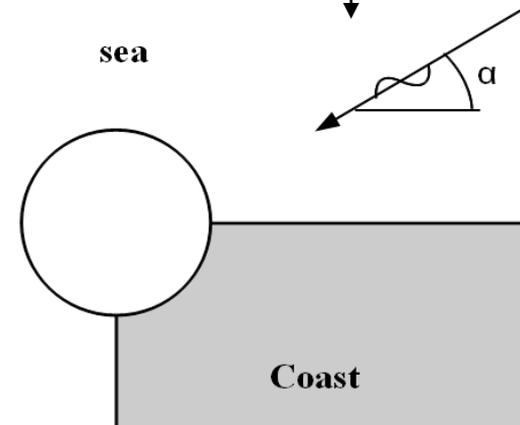
Martin-Rivas & Mei (2008)



Lovas & Mei (2009)



Concave corner



Convex corner

Strategy of solution

Total solution=

- Radiation due to uniform surface pressure
- + Diffraction (by solid cylinder and breakwater
+ correction for opening)
- + Coupling with chamber air and turbine

Assumptions:

- Radius not small compared to depth & wavelength
- Uniform air pressure in chamber.
- Air is compressible and isentropic.

Maximum efficiency for one frequency?

$$kL = \frac{gka}{\omega C_g} \frac{\chi |\Gamma|^2}{(\chi + \tilde{B})^2 + (\tilde{C} + \beta)^2}$$

Sarmiento & Falcao (1984)

(i) If $\chi = \frac{\rho_w \omega K D}{a N \rho_a^0} = \tilde{B}(kh),$

Turbine absorption = radiation damping;

(ii) $\tilde{C}(kh) = -\beta = \frac{\omega^2 V_0 \rho_w}{c^2 a \rho_a}$

Restoring force + Effective inertia = air elasticity

Theoretical optimum : $(kL)_{opt} = 1$

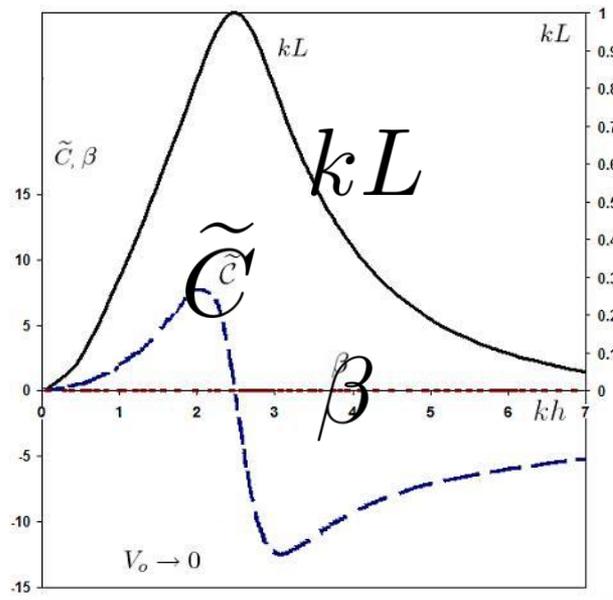
Optimization for all frequencies by proper design of turbine system alone

$$\frac{\partial(kL)}{\partial\chi} = 0$$

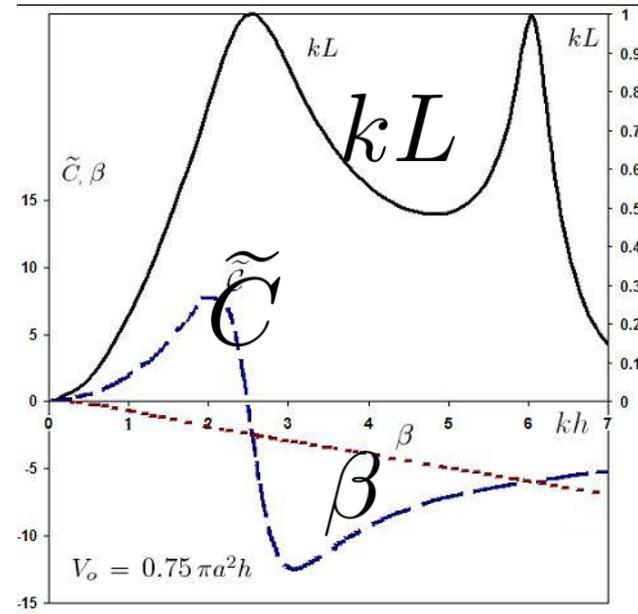
$$\chi_{opt}(\omega) = \sqrt{B^2 + (C + \beta)^2}$$

$$\beta = -\frac{\omega V_0}{c^2 \rho_0^2}, \quad V_0 = \text{fixed}$$

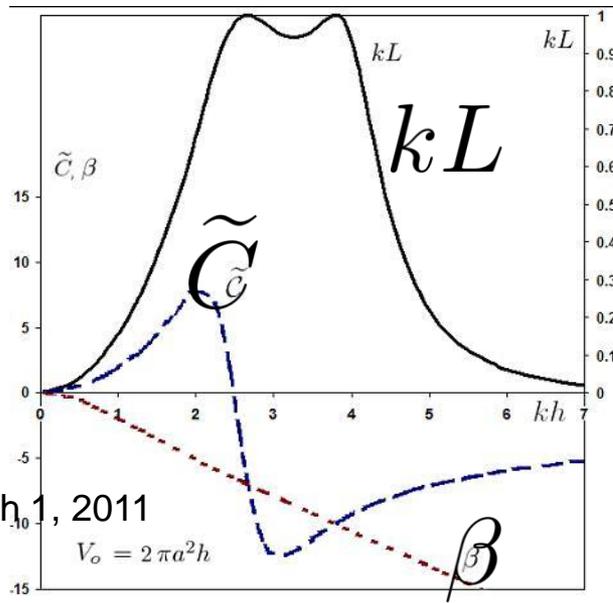
Fixed OWC radius, different chamber height (volume)



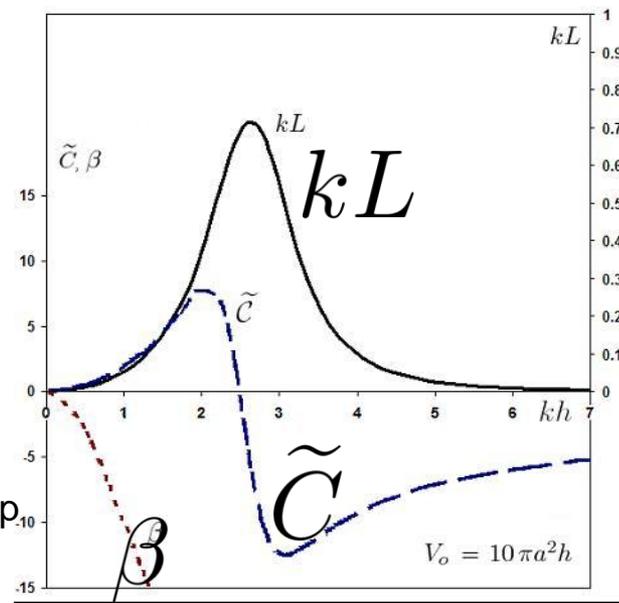
kh



kh



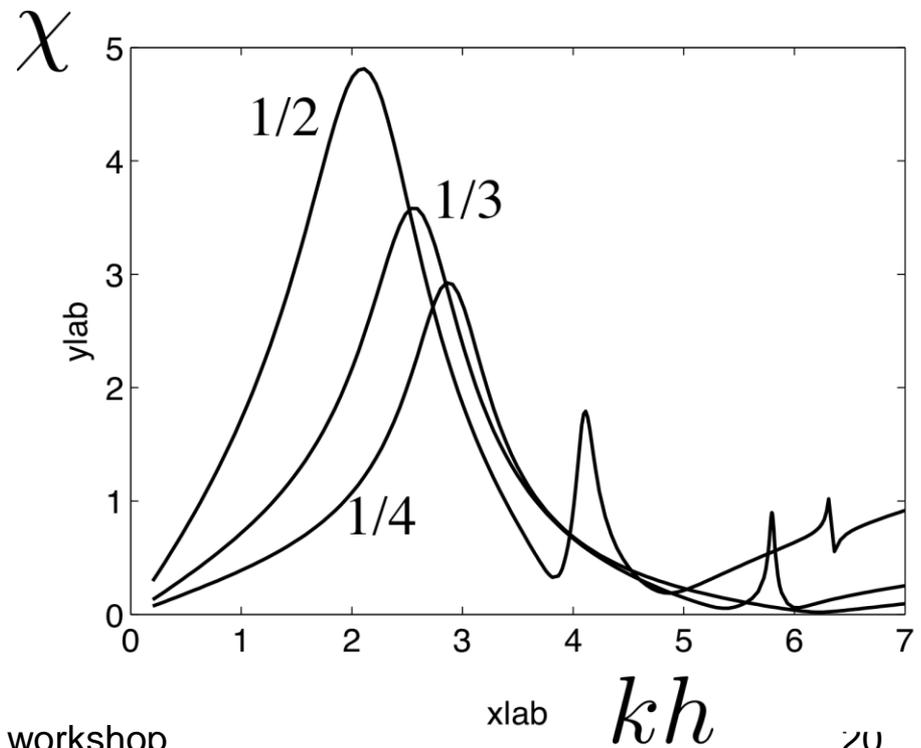
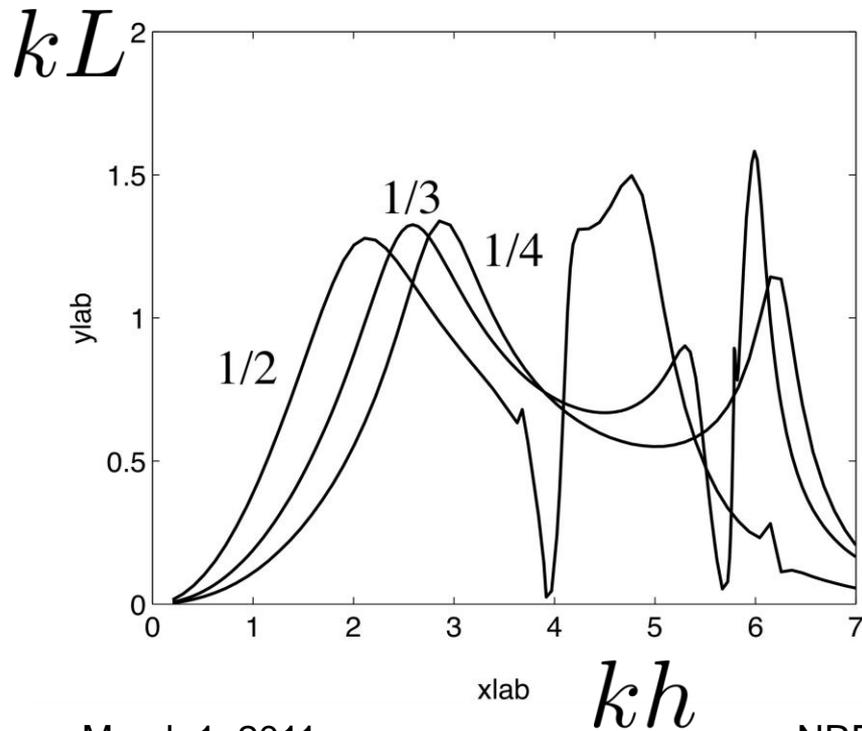
NREL workshop
 kh



19
 kh

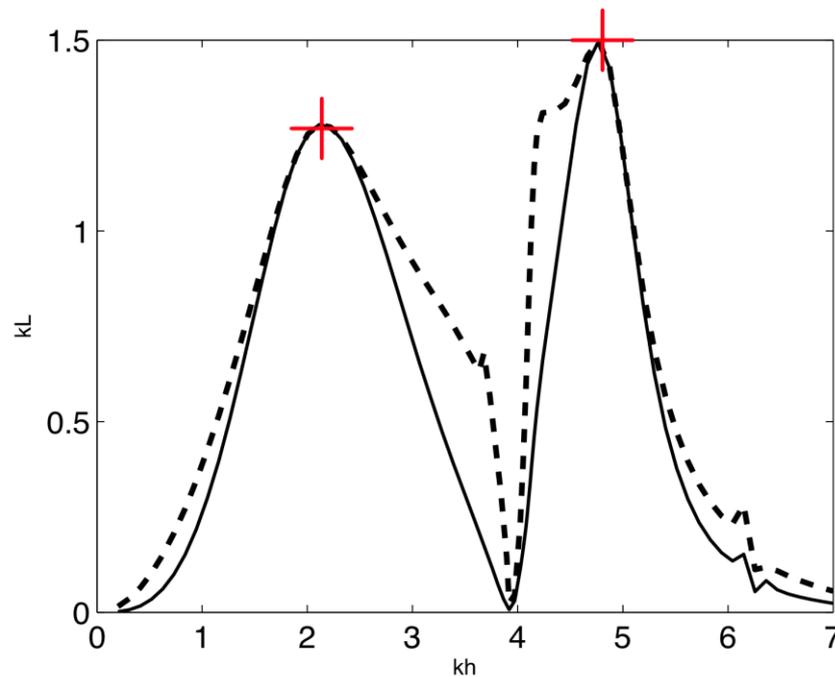
IDEAL OPTIMIZATION FOR ALL FREQUENCIES

Fixed chamber volume, $V_0 = \pi a^2 h$
 $a/h = 1/2, 1/3, 1/4$



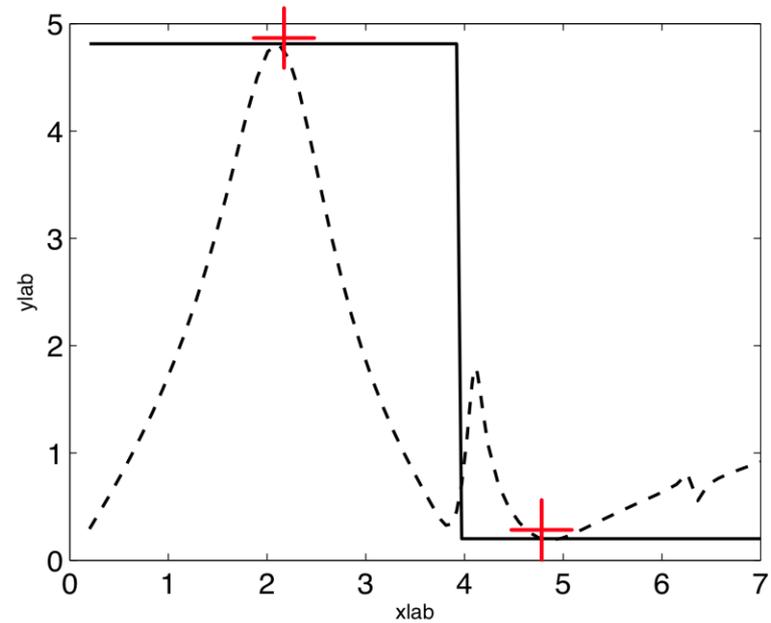
Practical optimization

kL



kh

χ



kh

Conclusions

- Large OWC allows more modes, efficiency bandwidth increases
- Chamber can be selected to broaden bandwidth
- Practical turbine control can broaden bandwidth.
- **Needed: Nonlinear modeling, Control of Power- takeoff**